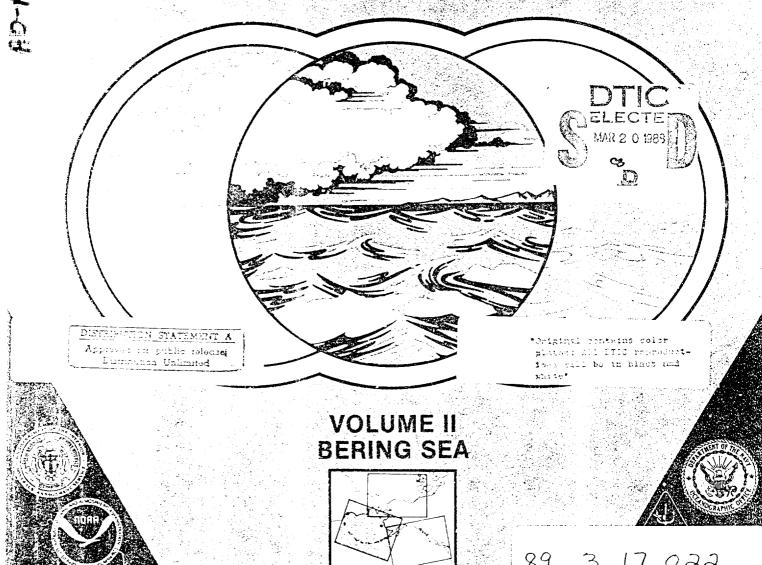
# CLIMATIC ATLAS



# OF THE OUTER CONTINENTAL SHELF WATERS AND COASTAL REGIONS OF ALASKA





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U.S. DEPARTMENT OF COMMERCE NOAA, NATIONAL OCEAN SERVICE OFFICE OF OCEANOGRAPHY AND MARINE ASSESSMENTS OCEAN ASSESSMENT DIVISION, ALASKA OFFICE

# **CLIMATIC ATLAS**

# OF THE OUTER CONTINENTAL SHELF WATERS AND COASTAL REGIONS OF ALASKA

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NCDC WILLIAM A. BROWER, JR. RONALD G. BALDWIN CLAUDE N. WILLIAMS, JR. AEIDC JAMES L. WISE LYNN D. LESLIE

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Climate Impact Perception and Adjustment Experiment (CLIMPAX), U.S. Department of Commerce Recreational Day Summaries, and numerous other special studies such as climate change in North America as related to increasing concentrations of CO<sub>2</sub>. Among his previous assignments were tours of duty as a National Weather Service specialist at Cordova. Cold Bay, and Annette. Alaska.

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The extremes data in the first section were updated through 1984 from a published Alaska Climate Summaries done by AEIDC in another project, published Canadian normals 1951-1980, and data supplied by Drs. Howard Critchfield and Kelly Redman, state climatologists for Washington and Oregon. Joseph C. LaBelle, glaciologist and geomorphologist at AEIDC assisted in the preparation of Cook Inlet ice and

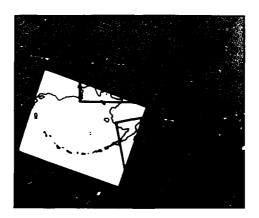
calving glacier ice in Volume I. Thanks also to Denise Cote for editing section I of all volumes and Laura J. Larson who was graphics project leader for the atlas and scheduled work on maps, charts, and text for all 3 volumes.

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## **Abstract**

This project updates the knowledge of climatological conditions presented in the 1977 publication of this three-volume atlas. Such environmental information for the three Alaskan marine and near-coastal areas is important for resource development of the outer continental shelf—The Gulf of Alaska (Volume I), the Bering Sea (Volume II), and The Chukchi and Beaufort Seas (Volume III) as shown on the map below.

The maps, graphs, and tables in the atlas present a detailed climatic profile of the marine and coastal regions of Alaska. Statistics give the means, extremes, and percent frequency of occurrence of threshold values for these elements: wind, visibility, present weather, sea level pressure, air and sea surface temperature, clouds, waves, and such supplemental information as storm surges, tides, sea ice, cyclone tracks, surface currents, bathymetry, detailed weather, and aviation weather. Data came from



4.5 million surface marine observations and 8.5 million observations for 66 coastal and island stations within the area 40°-84°N and 110°W-160°E, and provide the best possible climatological picture of the outer continental shelf waters and coastal regions of Alaska.

## Introduction

The nature of man's offshore activities depends to a large extent on weather conditions. Knowledge of these conditions can help insure efficient and safe operations. Extreme weather conditions that may be encountered in a given location largely determine the design, construction, and operation of permanent platforms and structures in the ocean as well as onshore support activities. This atlas is useful to those engaged in shipping, national defense, fishing, and applied research where a knowledge of coastal and offshore climate is essential. Weather information also aids in assessing the onshore impact of offshore activities.

This atlas is the result of a joint effort by the Arctic Environmental Information and Data Center (AEIDC), University of Alaska and the National Climatic Data Center/National Oceanic Atmospheric Administration (NCDC/NOAA) to present descriptive climatology and data analyses of surface marine and atmospheric parameters for those waters and coastal regions of the Alaskan outer continental shelf important to resource development. It is designed to serve as a climatological reference in the assessment of potential impact by oil and gas exploration and development and of leasing and operating regulations and monitoring programs that will permit resource development and insure environmental protection.

The evaluation is in the form of a climatic atlas for each of three marine and coastal areas: The Gulf of Alaska (Volume I), The Bering Sea (Volume II), and The Chukchi and Beaufort Seas (Volume III).

The first section in each volume contains information on such hazards as storm surges, superstructure icing, hypothermia, and wind chill; extremes data on winds, temperature, and precipitation; and planning information on surface currents, bathymetry, sea ice, and tides. The second section presents a detailed climatic profile in the form of isopleth analyses, graphs, and tables.

# Section I: Selected Topics in Marine and Coastal Climatology

by James L. Wise and Lynn D. Leslie

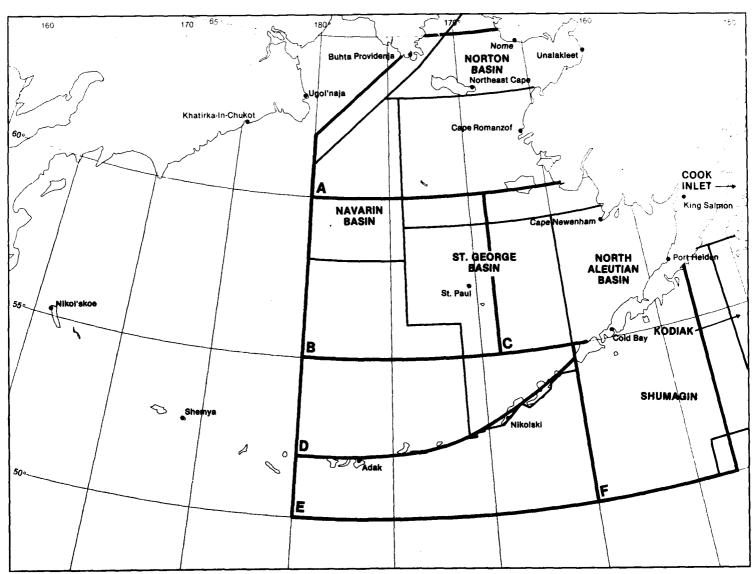


Figure 1. MMS Lease Sale Areas

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Figure 2. Place Names Map

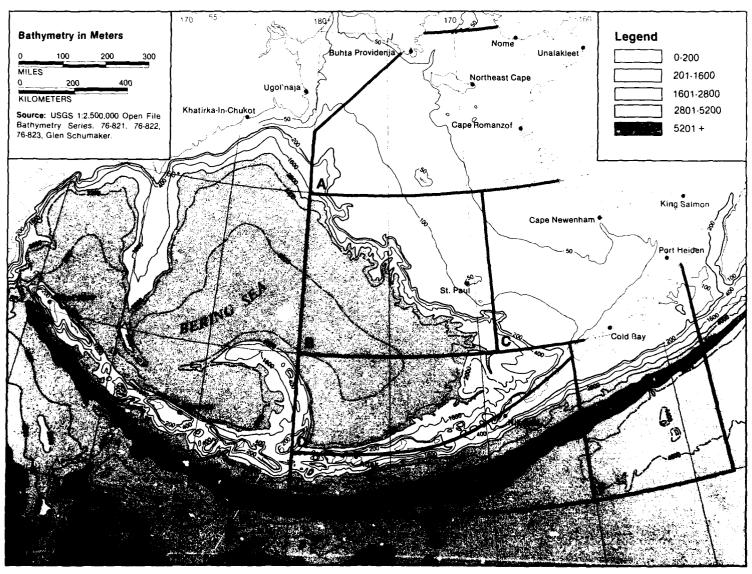


Figure 3. Bathymetry

# **Currents of the Bering Sea**

#### North Aleutian Shelf

The primary flow of water into the Bering Sea originates at Unimak Pass. The source water of this flow is the Alaskan Coastal Current, from south of the Aleutians. Within the pass and north of Unimak Island, much of the coastal current is entrained into the wind-driven flow along the north Aleutian coast. Typically, this current flows to the northeast into Bristol Bay in the direction of the prevailing wind, following bathymetry contours along the coast. At times, the north Aleutian coastal current will undergo a reversal in direction due to changes in the largescale and mesoscale wind direction. Because winds are highly variable, their contribution to net circulation is difficult to quantify, but the alongshore component of winds is highly correlated with both onshore and alongshore components of surface and subsurface currents.

Sea level changes on either side of Unimak Pass due to storm track and pressure cell movement are probably responsible for the fluctuation of magnitude and direction in the flow through the pass, which at times is southward. These reversals are more likely to occur when the flow from the seasonally variable Alaskan Coastal Current, from the Gulf of Alaska, is at its minimum. The shoaling bottom through Unimak Pass gives rise to vertical turbulence and mixes the water column.

On the north Aleutian shelf, the net northeasterly flow of approximately 1-5 cm/s is present within the coastal zone (Baker 1983; Cline et al. 1982; Thorsteinson 1984). This current is believed to be continuous with a weak current past Nunivak Island (Kinder and Schumacher 1981). Near Port Moller, currents have smaller magnitudes and do not intensify near the coast. Close inshore, within 50 km, currents ranges from 1 to 6 cm/s (Kinder and Schumacher 1982).

A weak mean flow shows a cyclonic tendency around the perimeter of Bristol Bay, with maximum speeds (roughly 3.5 cm/s) found near and inside the 50-m isobath and in the coastal domain. Mean speeds observed in the central shelf domain were less than 1.0 cm/s, with no sense of an organized circulation (Kinder and Schumacher 1981). There is apparently a net westward convection of water from the central basin of Bristol Bay into the Bering Sea. However, flow in this central region is highly variable, atmospherically forced, and difficult to

quantify. Coastal waters along the northern boundary of Bristol Bay, also called the coastal current, continue to follow the bathymetry. The coastal current flows northwesterly into the Bering Sea and then northerly along the Yukon/Kuskokwim Delta. Thus, the fundamental circulation in outer Bristol Bay consists of a typically unclosed, counterclockwise gyre open to the Bering Sea and driven by a combination of wind, tide, estuarian, and thermohaline effects.

Ninety to ninety-five percent of the velocity variance within the bay is tidal, with tidal currents an order of magnitude larger than the mean flow. For example, on the north Aleutian shelf, where net currents are only 1-5 cm/s and the typical wind-driven currents are approximately 10 cm/s at 5 m, the tidal currents are 40-80 cm/s or more (Thorsteinson 1984). Turbulence resulting from tidal currents causes mixing of the water column from the bottom to about 50-m above the bottom. Tidal currents in Bristol Bay are nearly reversing along the Alaska Peninsula and become more cyclonic and rotary offshore. National Ocean Survey current tables show a change in maximum ebb currents from 20-25 cm/s up to 30-40 cm/s in June near Amak Island. Near Port Moller, the tidal current speeds are as high as 100 cm/s (U.S. Department of Commerce 1980). At a depth of 2m the calculated tidal residual current is approximately 3-4cm/s, spatially highly variable, and directed to the northwest (Leendertse and Liu 1981).

Kinder and Schumacher (1981) identified three separate hydrographic flow regimes in the southeastern Bering Sea. The Coastal regime is present inside the 50-m isobath in the vicinity of Nunivak Island. It is characterized by generally warm, low saline, vertically well-mixed water which has typical currents on the order of 2-5 cm/s toward the northwest. The Middle regime is present in the central Bristol Bay region, where water depths are on the order of 50 to 100 m. It is divided from the coastal regime by a front with an enhanced salinity gradient and is characterized by a strongly stratified, twolayered structure extending approximately to the 100-m isobath. Mean flow is generally less than 1 cm/s, with no characteristic vector-mean direction. The Outer hydrographic region is divided from the middle region by a front along the 100-m isobath and is present out to the shelf break in the open waters beyond Bristol Bay. A fine vertical structure separates surface layers from the deeper, more well-mixed layers. The vector-mean current in this regime is directed to

the northwest, with magnitudes on the order of 1-10 cm/s and a statistically significant cross-shelf component of about 1-5 cm/s.

#### Yukon Delta

The dominant current near the Yukon Delta is the northward flowing Alaskan Coastal Water. The current is thought to bifurcate at the northwest corner of the delta, with one fork flowing inland, toward Norton Sound, and the remaining flow continuing northward (U.S. Navy 1958). Local and seasonal effects can produce variability in the prevailing flow directions. In winter. when winds are from the north, flow offshore of the delta can actually reverse for days or weeks at a time (Aagaard and Coachman 1981). This situation accounted for the flow of the Alaskan Coastal Water about 30% of the time between September 1976 and March 1977 (Zimmerman 1982). The surface currents offshore of the delta tend to flow in the same general direction as the synoptic and mesoscale winds, from the north or northeast in winter and from the southwest during open water season. The typical summer wind frequently produces downwelling and shoreward transport of water, which results in a raised water level and increased wave energy near the coast.

#### **Norton Sound**

The currents in Norton Sound are dominated by regional wind and surface pressure patterns. The highest observed flow was measured at about 50 cm/s; flow decreased with increasing depth (Muench 1981). These atmospheredriven flow events may differ from the mean flow and produce uncertain, intermittent variability in the circulation pattern. Oceanographic data from the mouth of Norton Sound indicate a net northward water transport, with strong seasonal differences in movement rates. Currents between the mouth of the sound and St. Lawrence Island to the west are characterized by somewhat pulsive north-south flow events having speeds of 50-100 cm/s (Muench, Pearson, and Tripp 1978). These speeds contrast with reported mean flow rates of 15 cm/s observed in relative synchrony with major meteorological events. The mean circulation pattern within the sound is cyclonic in character (Drake et al. 1980). A typical feature is westerly flow of water mass, varying in extent and intensity over time, along the northern coast (Cline, Muench, and Tripp 1981). The tidal component in the sound is on the order of 50 cm/s and reverses either diurnally or semidiurnally. The reversals are roughly northeast/southwest within Norton Sound.

The upper- and lower-layer circulation is decoupled in the eastern sound, but less so in the western sound, where there is a monotonic decrease in speed along with a slight rotation of flow as depth increases. Northwesterly surface flow rotates to westerly near the bottom. In summer, easterly flow enters the sound along its southern shore, curves cyclonically to the north, and is then deflected to the west at the north

coast, roughly following the bathymetry. This flow varies in intensity and extent from year to year. In the summer of 1979, a westerly mean flow paralleled the coastline and was superimposed upon a highly variable flow which included reversals (Muench 1981).

#### **Bering Strait**

The Bering Sea is characterized by an open shelf south of St. Lawrence Island. Mean currents are variable in direction and range from 1 to

4 cm/s, with the tidal current accounting for 55 (±31)% of the fluctuation (Coachman, Salo, and Schumacher 1983). Near St. Lawrence Island, the Bering Sea narrows into two straits, the Shpanberg and Anadyr. North of the island the two straits merge to form the Bering Strait. Circulation here is dominated by a northward mean flow ranging from 4 to 15 cm/s, with very small tidal influences 24 (±13)% variability (Coachman, Salo, Schumacher 1983). Flow in both the Anadyr and Shpanberg is to the north, approximately parallel to the local bathymetry. The flow appears to come from around both ends

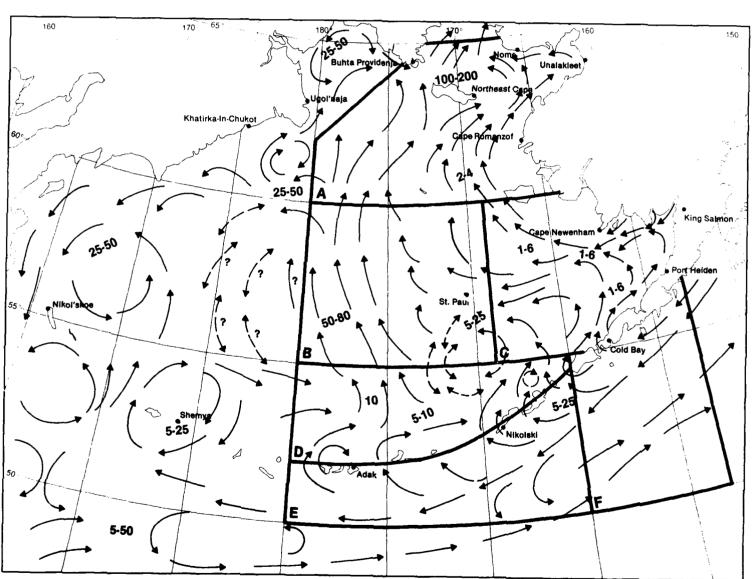


Figure 4. Bering Sea Currents - Summer

#### Legend

Bering Sea surface currents. Numbers indicate mean speed in cm/s. Arrows depict flow as follows:

◆ Prevailing current direction

←--- Variable current direction

Bering Sea surface currents synthesized from Arsen'er 1967; Goodman et al. 1942; Kinder and Schumacher 1981; LaBelle 1983; Marine Advisory Program, University of Alaska; Notorov 1963; Pelto 1981; Takenouti and Ohtahi 1974; and U.S. Navy 1977 of St. Lawrence Island. Frequent reversals are coincidental with meteorological events. These reversals can affect the flow over vast regions covering thousands of square kilometers. The presence of ice appears to dampen the impact of wind stress forcing. The major driving force for the northward flow through Bering Strait is the sea surface sloping down to the north (Aagaard and Coachman 1966). A slope of  $2 \times 10^{-6}$  is associated with average summer northerly transport of approximately 1.6 x10° m³/s. The normal condition is, thus, one in which sea level in the southern Chukchi Sea (in summer) is about

0.5 m lower than in the northern Bering Sea. A major cause of variations in the sea level difference must lie in fluctuations of the regional wind distribution. It is also possible that the atmospheric pressure field may itself directly modify the oceanic pressure field (Aagaard, Coachman, and Tripp 1975).

An examination of recent meteorologic data (Aagaard and Coachman 1981) showed the following results. In every case of southerly flow through the Bering Strait, the large-scale atmospheric pressure patterns were the same. One day

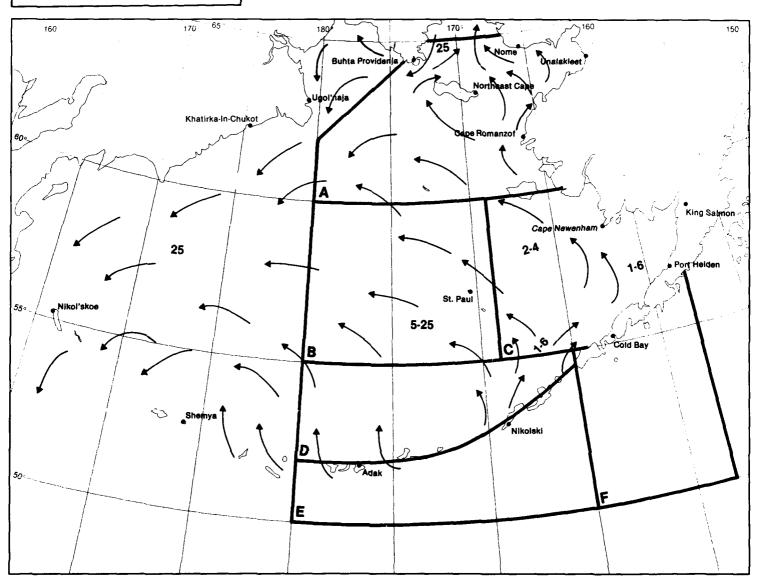


Figure 5. Bering Sea Currents — Winter

before a peak in southerly flow, a strong lowpressure system was centered some distance to the southeast of Bering Strait in the area of Bristol Bay, Kodiak, Anchorage, and the northern Gulf of Alaska. At the same time the Siberian high was centered some distance west or westnorthwest of the strait. The isobars signifying the strongest pressure gradient between pressure centers were located precisely over the Bering Strait region. Most significantly, they had a nearly north-south orientation which extended from over the Chukchi Sea south into the central Bering Sea-completely across the northern Bering Sea shelf. If the north-south orientation of the isobars did not extend totally across the northern shelf or if the isobars were oriented northeastsouthwest (the nearest typical configuration), strong southerly flow events did not occur.

The mechanism which drives major south flow events now seems clear. Strong north winds must develop over the entire northern Bering Sea, not just over the immediate region of Bering Strait. Large-scale, strong atmospheric pressure cells are required: a low far to the southeast and a high well to the west. The strong northerly winds generated thereby move water southward off the entire northern Bering Sea shelf. Removal of sufficient water off the northern shelf generates a sea-level slope down to the south-sea-level slope has been shown to be the major force driving transport through the strait (Coachman et al. 1975). This, together with the strong north winds caused by the east-west atmospheric pressure gradient, drives enhanced southerly transport. These conditions apparently require about one day to develop, so that maximum south transport occurs the following day. Because the system behaves to a marked degree as a coherent unit, water levels at both St. Lawrence Island and Cape Lisburne fall together and are nearly in phase with the transport.

Northward transport stands in contrast to the southerly transport events. Periods of northerly flow tend to be more persistent and not so great in magnitude, nor do they show the marked episodic character of the southerly flows. The greater persistence of northerly flow must reflect the basic driving force, a higher sea level in the Bering Sea than in the Arctic Ocean (Coachman et al. 1975), which still remains unexplained. There were, however, a number of relatively rapid northward accelerations of transport during the seven months of record which appear to have two basic causes:

- (1) After strong south transport events, rapid accelerations commonly occur which can be thought of as compensatory. When atmospheric conditions causing the southerly transport event dissipate, water is not being removed from the northern Bering shelf, but there is still voluminous southerly transport in the system. Water "piles up" in the region around St. Lawrence Island and Norton Sound, a condition reflected by a strong, positive difference in water level. Following this by about one day, a strong northward acceleration occurs.
- (2) Occasionally, major northward accelerations appear to be, at least in part, directly driven by atmospheric conditions. Specifically, these are a strong low pressure centered in the western Bering Sea southwest of Bering Strait, or a deep trough from the central Aleutians

toward the northwest, so that the isobars in the strong pressure gradient are directed northward from the central Bering Sea along the axis of the system. This configuration creates strong, southerly winds which can move water from the central Bering Sea onto the northern Bering Sea shelf, raising the water level in the vicinity of St. Lawrence Island and enhancing the sea-level slope down to the north.

#### **Central Bering**

West and northwest of the North Aleutian Basin and Yukon Delta lies St. George Basin, the Central Bering Sea, and still further west, the Navarin Basin, Circulation in these regions is not as well understood as in the coastal basins. Fewer studies have been conducted in the offshore Bering. Data are site-specific and sporadic over decades. No consistent flow patterns have emerged as representative of the regional circulation. In fact, there is little consensus among investigators that the principal flow is north-south, east-west, or cyclonic or anticyclonic in nature (See Natarov 1963; Arsen'ev 1967; Tak enovti and Ohtani 1974; Goodman 1942; Ratmanov 1937). The northward flowing, eastern boundary current is roughly balanced by a southward flow along the Soviet coast. Within the central region, flow is probably dominated by the location and strength of largescale atmospheric pressure cells. Response times, directions, and persistence are probably of a similar scale as those controlling flow through the Bering Strait (Aagaard and Coachman 1981). Thus, a dominant regional flow pattern is not readily observed nor easily quantified.

# Sea Ice

#### Introduction

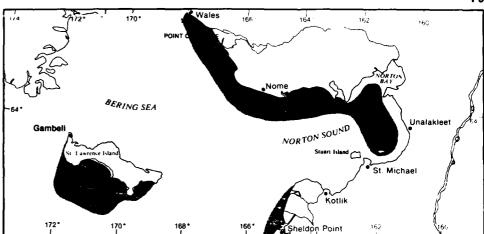
The annual cycle of formation and dissipation of sea ice in Alaska waters has widespread effects on a number of phenomena. When the ice forms, the coastal climate changes in character from maritime to continental with much colder temperatures and lower humidities than would be the case if open water were present. The ice also interferes and even stops water transportation with the possible exception of icebreakers and other specially designed ships. It makes the cleanup of oil spills difficult, if not impossible, by hampering the operation of cleanup equipment and by trapping oil under the ice. Sea ice also has important effects on the life cycles of living creatures in and near the sea.

In the Bering Sea, the sea ice generally begins as fast ice formation along the shores of the Seward and Chukotsk peninsulas in October. As the season progresses and waters in the more open portions of the Bering Sea cool off, the pack ice generally begins its seasonal southward formation in November. An estimated 97% of the ice in the Bering Sea is formed within the Bering Sea (Leanov 1960); very little is transported south through the Bering Strait. During periods of increasing ice and prevailing northerly winds, the ice apparently is generated along the south-facing coasts of the Bering Sea and moves southward with the wind at as much as 1 knot before melting at its southern limit (Pease 1971). During periods of southerly winds, ice coverage generally decreases in the Bering. Prevailing winds can persist in one direction for weeks at a time in winter in the Bering Sea, causing a wide variation in ice cover from month to month and from year to year (see Figure 6 and map set 17, Section II of this volume).

#### **Recurring Leads and Polynyas**

Wind and current stresses on the ice can cause tension or divergence and open relatively narrow, long stretches of open water in an otherwise dense ice cover. In the absence of strong currents, the wind induces leads which run perpendicular to the wind direction. Flaw leads generally occur just seaward of the stable fast ice zone when strong offshore winds develop.

In the Bering Sea a wind-induced polynya (Figure 6) immediately south of St. Lawrence Island is a frequent but undependable feature (McNutt 1981; Wohl pers. comm.). Northerly



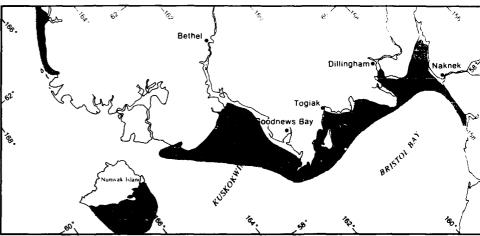


Figure 6. Recurring Polynyas

Synthesized from: McNutt 1981, Stringer, Barrett, and Schreurs 1980, Wohl 1982

winds cause the polynya to form in the lee of the island as sea ice is advected to the south. The polynya can extend more than 160 km and is frequently covered with thin ice. However, the feature is temporal, and a wind shift to southerly flow can close this area rapidly. At such times, a corresponding polynya to the north of St. Lawrence Island is sometimes observed, but it is generally much smaller and occurs less frequently.

A polynya can form on any side of Nunivak Island, depending upon the prevailing wind direction. Usually the feature is located to the north or south, under southerly or northerly winds, respectively. Like the polynya off

St. Lawrence Island, the appearance of this polynya is variable, but it is usually observed at least once each year, often more. Its extent is variable, and thin ice commonly covers the polynya quickly during cold, northerly wind storms.

The polynyas shown for Norton Sound, Bristol Bay, and Kuskokwim Bay were taken from Stringer, Barrett, and Schreurs (1980). These features were mapped from LANDSAT scenes collected between 1973 and 1976. Generally, the major polynyas in these areas open in response to northerly winds, which cause all but landfast ice to move toward the south. As the polynyas are opened by the wind,

new ice forms and is, in turn, advected southward. This mechanism for new ice production can be very efficient under the proper circumstances (Pease 1980). None of the polynyas can be considered even semipermanent since a reversal in the wind direction can completely close them. Furthermore, many of the areas shown are partially covered with very thin ice when the northerly winds bring below-freezing temperatures.

#### **Fast Ice and Shear Zones**

According to World Meteorological Organization seaice nomenclature, fast ice includes all ice that has become attached to the shore, even multiyear pack ice. A common feature at the seaward boundary of the fast ice is an area of shear ridges. Shear ridges in the Bering Sea tend to be more localized and of lesser extent and magnitude than farther north. Figure 7 shows the various kinds of ice near shore. Bering Sea ice does not have any multiyear ridges. The accompanying fast ice boundary maps, from the Alaska Marine Ice Atlas, were synthesized from Stringer, Barrett, and Schreurs (1980).

Any significance accorded to trends apparent on these maps must be tempered by consideration of the variability exhibited in the ice-edge data. At some locations, the edge of the fast ice varies considerably in position during each period. Although the average edges along the coast show a temporal trend, it has only minor significance. In other locations, the variability of the fast-ice edge of each period is small compared to the changes in the average position from period to period (Stringer 1981). The intraseason and interseason variability of the fast-ice edge are very dependent on the meteorology and associated wind patterns as well as the offshore bathymetry. Although the prevailing winds in winter are generally northeasterly, there are often periods of a week or more with southerly winds. During northeasterly winds, shore leads and polynyas open up, only to be closed again when winds shift to south or southwest. Also, the high tide ranges in Bristol Bay and along the coast south of Norton Sound tend to break up extensive areas of fast ice, except where it is grounded on mud flats or offshore shoals.

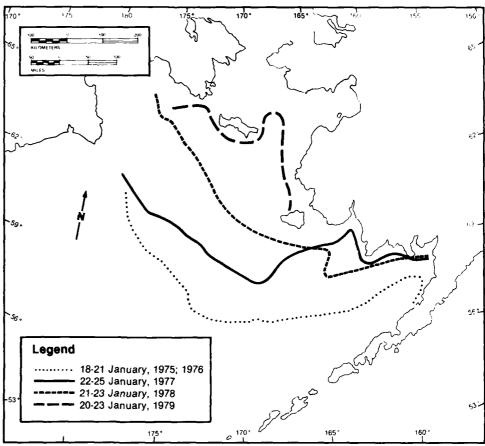


Figure 8. January Southern Ice Limit for 1975-1979.

Source: Niebaur 1981.

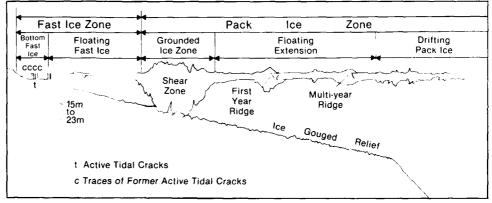
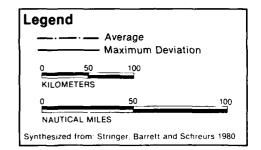


Figure 7. Sea ice Zones and Types



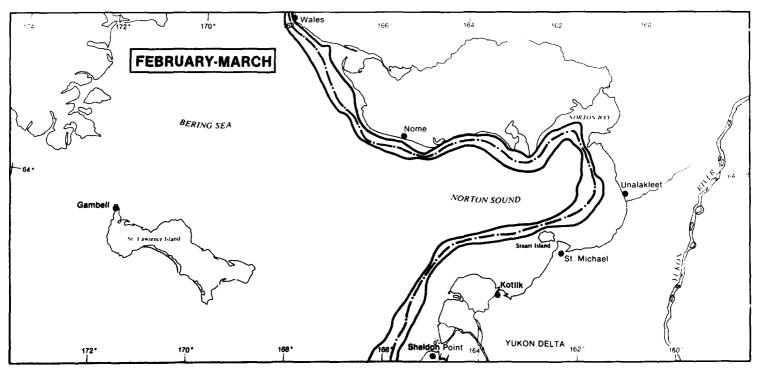


Figure 9. Seasonal Fast Ice Boundary—Norton Sound (February/March)

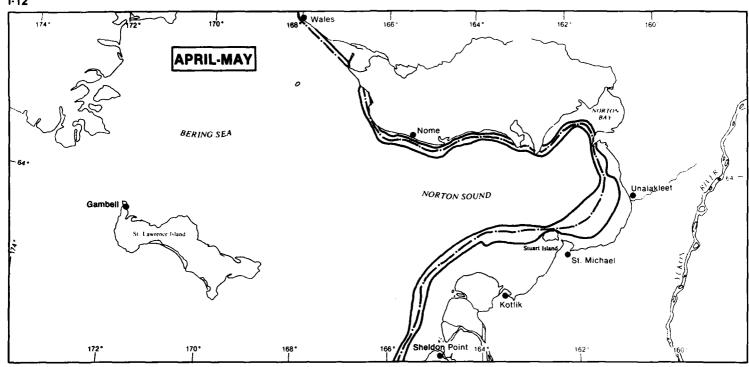


Figure 10. Seasonal Fast Ice Boundary - Norton Sound (April/May)

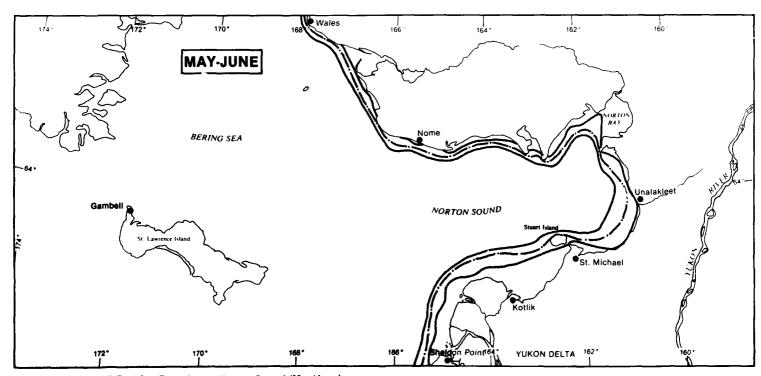
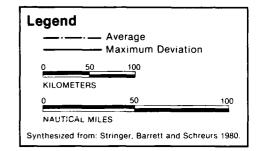


Figure 11. Seasonal Fast Ice Boundary - Norton Sound (May/June)



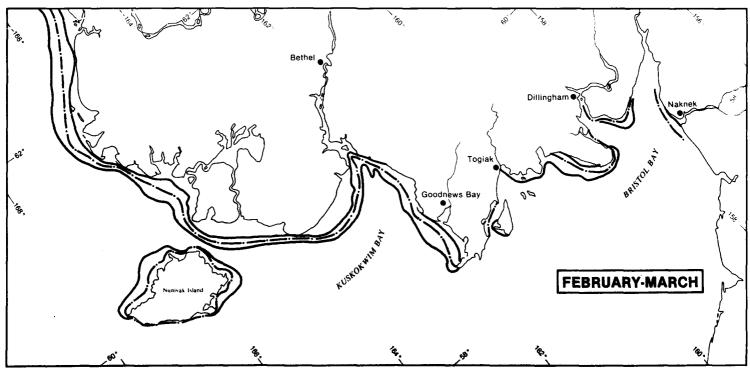


Figure 12. Seasonal Fast Ice Boundary—Southeast Bering (February/March)

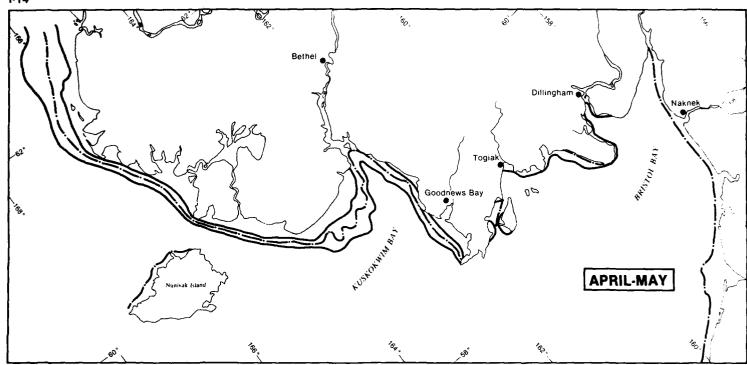


Figure 13. Seasonal Fast Ice Boundary—Southeast Bering (April/May)

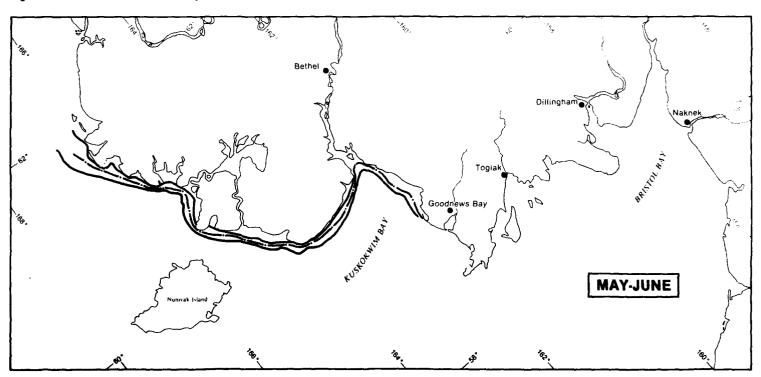


Figure 14. Seasonal Fast Ice Boundary—Southeast Bering (May/June)

# Tides

The practical study of tides, aimed at predicting surface elevations and times, involves the empirical treatment of observations made at the desired location over an extended period of time. The motion of the heavenly bodies, particularly the sun and the moon, relative to the earth is known with great precision, so the tide generating potential at any place and time can be computed. Mathematically the potential can be resolved into a finite number of strictly periodic components which, upon addition, produce the total potential of hundreds of tidegenerating components that are listed by various authors. Many of the components are of insignificant amplitude and can be excluded from consideration. In practice only seven components are widely used: four semidiurnal (Ma, S, N, K) and three diurnal components (K, O, P) (McLellan 1965). The names and relative weights of these components are shown in Figure 15.

Theoretical models of tides must be verified on the strength of observations at tidal stations where the tide wave has been distorted through passage over a continental shelf of complex topography. The nature of tides in a particular area is highly dependent on the bathymetry, shape, and direction of the coastline and latitude. In the Bering Sea in the last 10 years there have been a large number of presure gauge and current meter observations taken so that

tides can be modeled with a high degree of acuracy. The following discussion paraphrases material contained in Pearson, Mofjeld and Tripp, 1981 in which theoretical tide model results are compared to observations. The tides most concerned with are the principal tidal constituents  $N_2$  and  $M_2$  in the semi-diurnal band and O and K in the diurnal band. Ordinarily the S2 would be included in the discussion, however, S2 is anonymously small throughout the Bering Sea, possibly because it has small amplitudes in the adjacent North Pacific Ocean. The complicated distributions of semi-diurnal and diurnal tides in the Bering Sea produce a rich variety of tidal types, ranging from fully semi-diurnal in some regions to fully diurnal in others.

The tide wave enters the Bering Sea as a progressive wave from the North Pacific Ocean, mainly through the central and western passages of the Aleutian-Komandorski Islands. The Arctic Ocean is a minor secondary source of tides which propagete southward into the north Bering Sea where they complicate the tidal distributions.

Tides in the Bering Sea are considered to be the result of cooscilation with large oceans. Once inside the Bering Sea, each tidal constituent propagates as a free wave subject to Coriolis effect and bottom friction.

SYMBOL	NAME OF PARTIAL TIDE	COEFFICIENT RATIO
M,	Principal Lunar	100.0
s,	Principal Solar	46.6
N,	Larger Lunar Alliptic	19.2
κ,	Luni-Solar Semi-Diurnal	12.7
ĸ,	Luni-Solar Diurnal	58.4
O,	Principal Lunar Diurnal	41.5
P,	Principal Solar Diurnal	19.4
Contracted	d from table 15.1,	

Figure 15. Major Tide Components

Elements of Oceanography (McLellan 1965).

The tide wave propagates rapidly across the deep western basin. Part of it then propagates onto the southeast Bering shelf where large amplitudes are found along the Alaska Peninsula and in Kvichak and Kuskokwim Bays (Figure 17). Another part propagates northeastward past St. Lawrence Island and into Norton Sound. Over most of the Eastern Bering Shelf region the tide is mainly semi-diurnal, but in Norton Sound diurnal tides predominate. Over the remainder of the Bering tides tend to be mixed. In the Aleutians diurnal rather than semi-diurnal components are stronger.

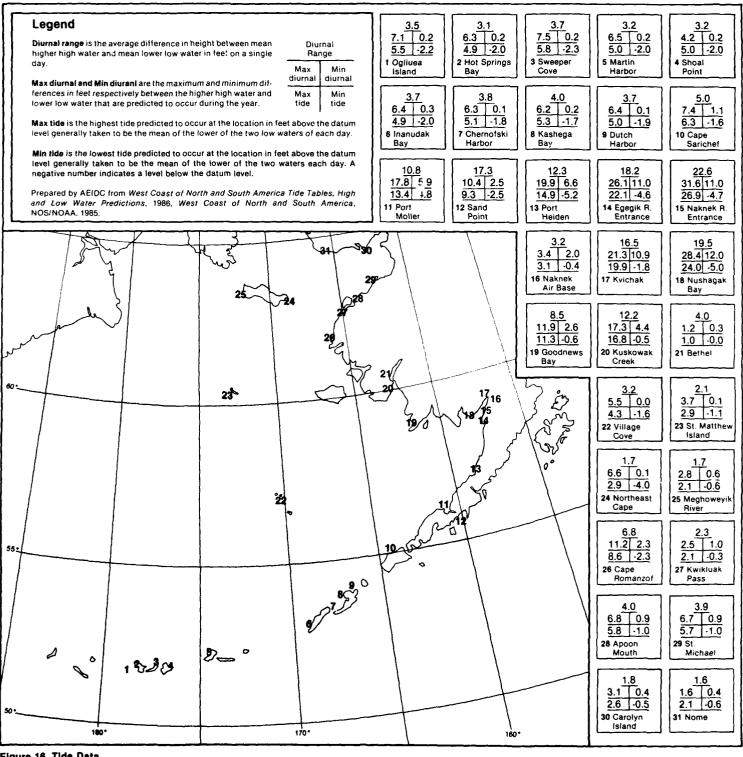


Figure 16. Tide Data

# Legend Type of Tide Semi-diurnal Diurnal Mixed Reministry Mixed Normal Mixed Normal Mixed Normal Mixed Normal Mixed Normal Mixed Normal Norm

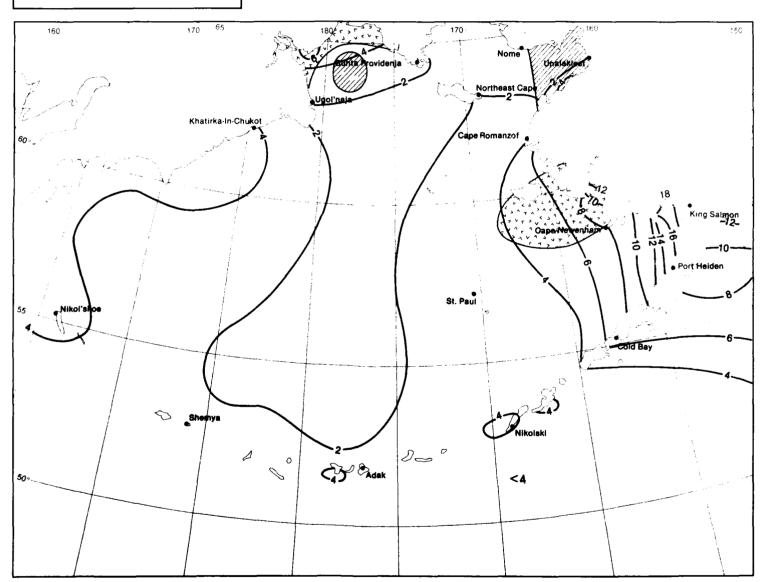


Figure 17. Tide Co-Range

# **Storm Surges**

Storm surges are waves oscillating in the period range of a few minutes to a few days, in a coastal or inland water body, resulting from forcing from atmospheric weather systems (Murty 1984). By this definition, wind-generated waves (often referred to as wind waves) and swell, which have periods of several seconds, are excluded. The spectrum of storm surge waves is centered around 10-1 cycles per second (CPS), which gives a period of about three hours. How-

ever, depending mainly on the topography of the water body and secondarily on other parameters, such as the direction of movement of the storm, strength of the storm, stratification of the water body, presence or absence of ice cover, and nature of tidal motion in the water body, the periods of the water level oscillations may vary considerably. Even in the same water body, storm surge records at different locations can exhibit different periods.

Although storm surges belong to the class known as long waves, as do astronomical tides and tsunamis, there are at least two important differences. First, whereas tides and tsunamis occur on an oceanic scale, storm surges are simply a coastal phenomenon. Second, significant tides and tsunamis cannot occur in an enclosed, small, coastal or inland water body, but storm surges can occur even in lakes, or in canals and rivers. The range or height of a storm

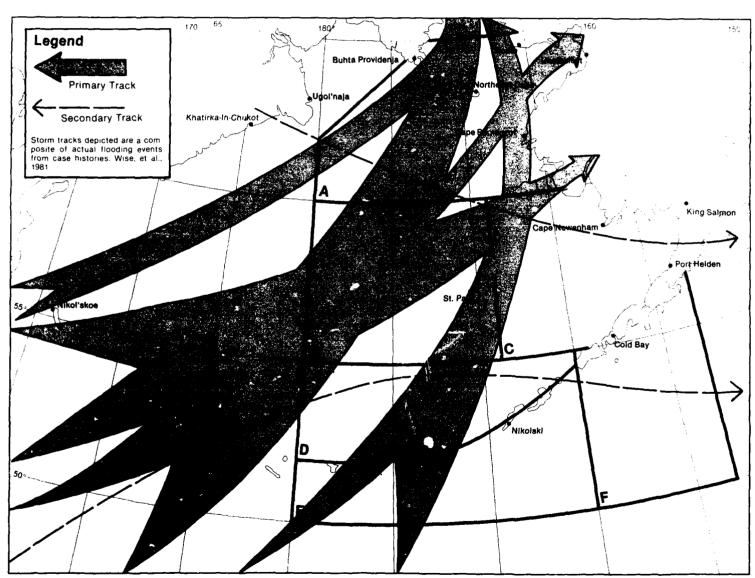


Figure 18. Storm Tracks with Storm Surge Floods

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surge depends not only on characteristics of the storm but also on the topography onshore and bathymetry offshore. Shallow water bodies generally experience surges with greater ranges. Also, the height of a storm surge is less if the sea floor is steep than if there is a shallow slope to the sea floor (Murty 1984). Storm characteristics that effect the height of a surge include atmospheric pressure; wind speed, direction, and length of fetch; the latitude; and the direction and speed of storm movement. Air and water temperature differences also affect the height of surges.

Following is a discussion of the storm surge potentials from a study done in 1981 (Wise, Comiskey, and Becker), supplemented by storm statistics since then (NOAA Storm Data, 1981-1986) and a modeling study for surges in Norton Sound (Wise, Comiskey, and Becker 1981; Kowalik and Johnson 1985).

Along the southwest and south coasts of the Seward Peninsula the terrain is generally of moderate relief, with the exception of Port Clarence and the east end of Norton Sound. The waters offshore are shallow with a gently sloping sea floor. The open waters of the Bering Sea provide a long fetch for the development of storm waves. Sea ice restricts the development of storm waves from about the first of December to the first of June on the average; however, there can be a high degree of annual variability. Of 13 known flooding events in Nome, all except two occurred in the fall. One destructive storm for which little factual information is available occurred in April 1906, and another occurred in July 1969. Surges above 4 m (12 ft) have occurred along this section of coast. The most recent was in November 1974; a 3 m (10-ft) surge brought water into the town over the sea wall. This particular storm caused widespread flooding all along the Bering Sea coast.

With the exception of the Shaktoolik River mouth, which is of low relief and marshy, the coast at the east end of Norton Sound is generally rugged due to the proximity of the Nulato Hills. The south coast of Norton Sound is generally of low relief. The sound itself is shallow, with a gently sloping sea floor that is very favorable for the development of storm surges. The range of wind directions for the development of storm surges is limited to west-

southwest to west. However, the east end of Norton Sound often experiences minor flooding, despite unfavorable winds, due to rising sea levels all over the sound.

A storm surge modeling study (Kowalik and Johnson 1985), determined that for the November 1974 storm the highest surge in Norton Sound was in Norton Bay, with a modeled surge of more than 3 m (10 ft). The same study also determined that negative surges of more than a meter can occur in the eastern end of Norton Sound in the presence of strong, persistent northeast winds in winter with an ice cover present. The winds tend to move the pack ice away from the shorefast ice and reduce ice cover from 0.7 or 0.9 coverage to less than 0.55 coverage over much of Norton Sound.

Eleven of the twelve storm surge cases at Unalakleet occurred in the fall; the other was in July. Sea ice and shorefast ice limit the fetch for the development of positive storm surges from about the first of December to the first of June.

The shores of Pastol Bay and the north coast of the Yukon River delta do not have long fetches favorable for the generation of waves and storm surges. However, this area experiences surges due to increases in the height of the water in Norton Sound. The remaining coast of the Yukon Delta is exposed to the open waters of the Bering Sea, where conditions are very favorable for the development of storm surges due to low relief onshore, shallow water offshore, and thousands of miles of open sea. Most surges causing property damage occur in the fall or in August. However, early summer surges can be very hard on nesting birds in the salt flats. In June 1963 80% to 90% of the black brandt production was lost due to flooding of the nesting area after eggs were laid.

The coastal area is generally of low relief from the Kuskokwim Delta to Goodnews Bay, with numerous lakes, sloughs, and marshes. From Goodnews Bay to the Nushagak Peninsula the coastline is more rugged due to the proximity of the Ahklun Mountains. The remainder of the coastline of Bristol Bay is similar to the stretch from the Kuskokwim River to Goodnews Bay. Offshore the shape of the sea floor is conductive to the formation and enhancement of storm surges. From Goodnews Bay northward an ade-

quate fetch can be generated with storm winds from south through west to northwest. East of Gocumens Bay, westsouthwest to west are the only directions from which an adequate fetch can develop.

Autumn and late summer are the seasons for destructive storm surge flooding in this area. There are ten known cases of storm surge flooding of populated areas; seven were in autumn and three were in August. Two storms, in November 1979 and in August 1980, account for most of the factual reports of storm surge flooding. The November 1979 storm caused storm surge flooding from Cape Newenham to Scammon Bay. Surges were estimated at 2.5 m (8 ft) in exposed locations in the Kuskokwim Delta. The storm was on a track from westsouthwest to eastnortheast, and a long fetch of more than 640 km (400 mi) developed with the storm. The August 1980 storm, one of the few summer flooding events, caused flooding on the shore of Bristol Bay. The storm was on a track from south-southwest toward north-northeast from near Atka Island, in the Aleutians, to Kuskokwim Bay. Exposed locations showed surge flooding up to 4 m (12 ft).

The coastal area from Hooper Bay to Kinak Bay is a favored nesting area of migratory birds in the spring and summer. Minor storm surges that cover nests in this area at the wrong time can be detrimental to the annual production of several species of birds. Five cases of minor summer flooding of the salt flats were documented in an annual report for the Clarence Rhode National Wildlife Refuge (USFWS 1964). One event (June 22, 1963) caused a loss of black brandt offspring estimated at 80% to 90% of the year's production.

Most of the north shore of the Alaska Peninsula east of Cold Bay is favorable for the occurrence of storm surge flooding, with low, marshy terrain onshore and a moderately sloping sea floor offshore. West of Cold Bay the Aleutian Islands and the south shore of the Alaska Peninsula conditions are not favorable due to rugged terrain onshore and steep ocean floor offshore. The only storm surges discovered in this area the Meshik, or Port Heiden, and St. Paul. Damage to structures in this area is more likely to be from strong winds and beach erosion caused by wave action than from flooding.

# Superstructure Icing

Structural icing on ships, offshore structures, and port facilities is a wintertime hazard in open waters and coastal sections of Alaska. The icing causes slippery decks, renders moving parts inoperable, and, in extreme cases, causes uneven loading and raises the center of gravity on small ships. Accumulation of ice on rigging and on deck equipment such as crab pots also increases wind effects because a larger surface area is presented to the wind. Ice forming on structural surfaces above or close to a body of water arises principally from sea spray (Nauman and Tyage 1985; Liliestrom 1985, with lesser amounts from atmospheric precipitation (freezing rain and wet snow) and fog (arctic sea smoke, white frost, black frost). Sea spray, the most dangerous source of icing, is produced by the breaking of waves against obstacles such as ships' hulls, other floating objects, shore structures, and, possibly, other sources (Minsk 1977).

Statistical analysis (Borisenkov and Panov 1972) of more than 3,000 cases of ship icing indicates that in 86% of the cases icing was caused by ocean spray alone. Spray combined with fog, rain, or drizzle (liquid sources) accounted for only 6.4% of the cases, and spray combined with (solid source) snow only 1.1%. The cases of icing attributable only to fog, rain, or drizzle account for 2.7% (Minsk 1977). In the remainder of icing cases data were not sufficient to determine the cause.

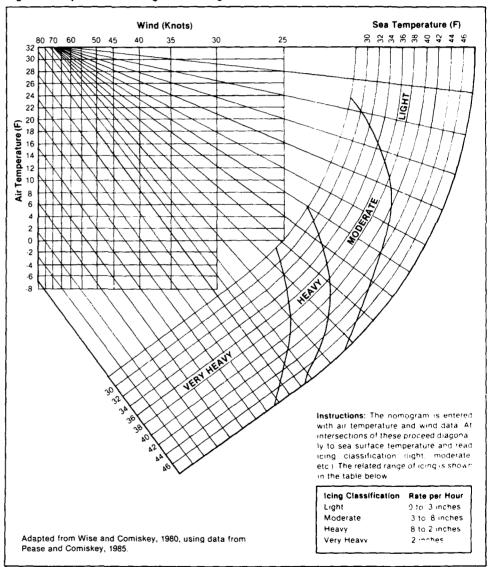
Since the overwhelming majority of superstructure icing on ships and offshore structures is from sea spray, the remainder of this section will concentrate on this type of icing. Since a ship can present different aspects to the wind and spray, it is to be expected that the amount of spray reaching the ship will vary: Russian observations (Kultashev, et al. 1972) showed that the greatest frequency of spray and, therefore, icing occurs when a ship is heading into the wind at an angle between 15° and 45°. Asymmetrical icing occurs under this condition, with the greater accumulation on the windward side. Less icing occurs with the ship headed directly into the wind, and then accumulation tends to be uniform. With ships heading downwind, spray icing is generally much less than at other angles. In developing the nomogram for forecasting spray icing potential, downwind cases (those for which the ship's heading was 120° or greater off the wind) were not used.

Meteorological/oceanographic conditions necessary for significant spray icing are water temperatures less than 8 °C, winds of 25 knots (13 meters per second) or more, and air temperatures less than  $-2\,^{\circ}\mathrm{C}$  (28 °F, the freezing temperature of seawater of average salinity). Generally, the stronger the wind, and the colder the air and water, the higher the rate of icing on comparable vessels or structures. In some

cases, however, where the wind fetch is not sufficient to fully develop waves, icing rates are lower.

The accompanying potential superstructure icing rate nomogram (Figure 19) is a modification of that shown in Wise and Comiskey (1980), using the open ocean cases appearing in Pease and Comiskey (1985), developed

Figure 19. Superstructure Icing Rate Nomogram



from icing case histories in the Gulf of Alaska and southern Bering Sea. Icing intensities in inches per hour are also from Pease and Comiskey (1985). If a vessel experiencing icing takes evasive action (i.e., changes heading, reduces speed, seeks shelter, etc.), icing rates experienced would probably be less.

Reported cases of ship icing (Figure 20) in the northern Gulf of Alaska and the Bering Sea are shown from two sources; Borisenkov and Panov (1972) and WBH29 (Dyson 1975-83). The lack of reported icing in the northern Bering may be a result of reduced ship traffic as well as conditions not favorable for icing. Kozo (1983) estimates a potential for superstructure icing for the northern Bering Sea in September, extending into Norton Sound in October, and even into the southern Bering during the most extreme conditions. Icing potential decreases in the north Bering as the sea ice cover advances; however, the potential for moderate or heavy icing downwind of the sea ice edge persists throughout the winter.

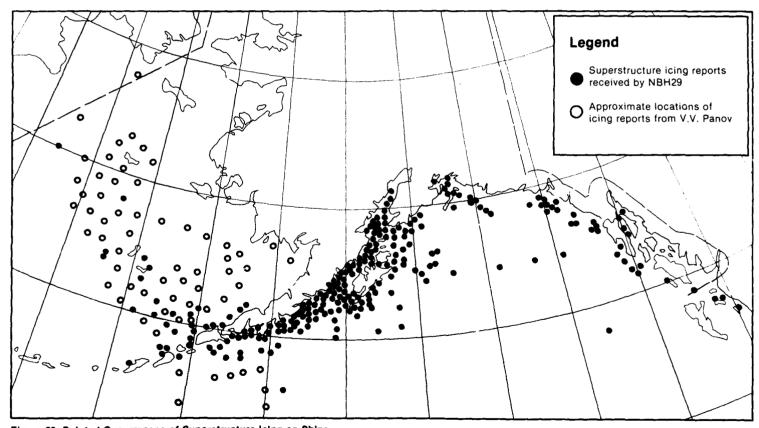
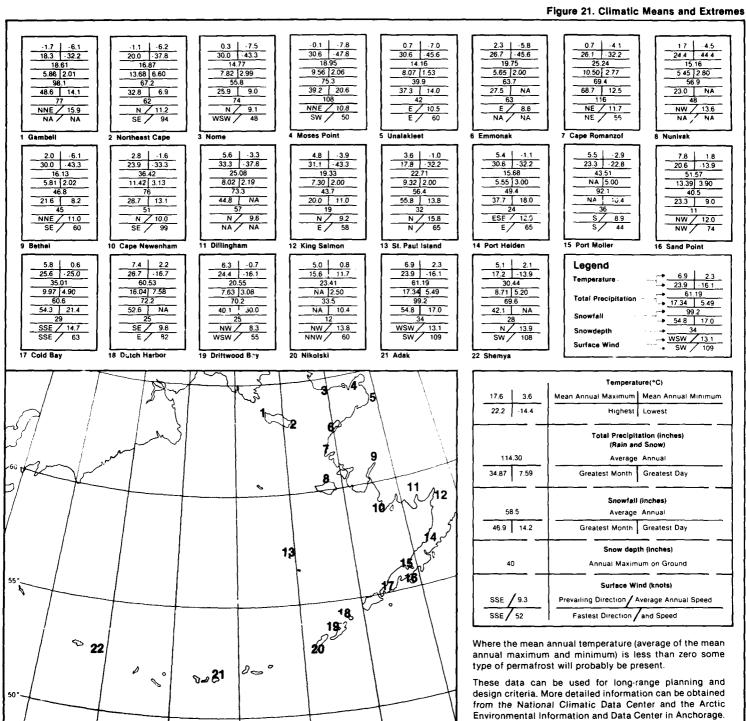


Figure 20. Related Occurrences of Superstructure icing on Ships

NA = Information is not available

Prepared from NOAA/NESDIS and Canadian AES data.



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# Hypothermia

Hypothermia is the cooling of the body's core temperature to 95°F or below. It can cause shivering, numbness, and disorientation. In the extreme it can cause death. The body loses heat gradually in cold, dry conditions, but quickly becomes hypothermic in wet conditions. Rain, immersion in cold water, and perspiration can all cause rapid heat loss. However, the evaluation and treatment of hypothermia, whether wet or dry, on land or water, is essentially the same, namely to warm the victim by whatever appropriate means are available.

The following discussion was taken in part from Peters (1982).

The body loses heat in five ways:

- A large amount of heat is lost from the body in respiration. Exhaled warm air is replaced by cooler inhaled air, producing a net heat loss. The amount of the net heat loss can be reduced by covering the mouth/nose with wool or fur, there by "prewarming" the inhaled air as it passes through the material which has been warmed by exhaled air and by heat radiating from the body.
- Evaporation of perspiration from the skin and moisture from the lungs contributes greatly to the amount of heat lost by the body. Although evaporation cannot be prevented, the amount of evaporation (and therefore cooling) can be controlled. Wearing clothing that can be opened or removed easily for ventilation will let water vapor escape and not condense to liquid water in the clothing. Keeping clothing dry preserves its insulating value and reduces heat loss.
- Sitting on snow, touching cold equipment, and being rained upon are all examples of how heat can be lost as a result of conduction. If an individual becomes wet a tremendous amount of body heat is lost rapidly. Deaths have occurred as a result of immersion in water below 40°F—body temperature could not be maintained. Although not as immediately serious, perspiration, rain, or wet snow should never be allowed to saturate articles of clothing, as this seriously reduces their insulating properties.

- Radiation causes the greatest amount of heat loss from the body from uncovered surfaces, particularly the head, neck, and hands. Coverage of these areas, therefore, is extremely important in keeping warm.
- The body continually warms (by conduction) a thin layer of air next to the skin. If the warm layer is removed by wind or air currents (advection), the body is cooled. The primary function of clothing is to retain this layer of warm air next to the skin by enclosing air in cell walls or between numerous fibers, while allowing water vapor to pass outward. Heat is lost rapidly with the lightest breeze unless the proper type of clothing is worn to prevent the warm air from being advected away.

Deaths have been attributed to a loss of body heat at temperatures of 40°F, with a 30 mph breeze. Under these conditions, the cooling effect on the skin is equal to that of much lower temperatures due to increased evaporation and convection. With lower temperatures and/or strong winds, cooling occurs even more rapidly. Wind protection and insulation (dead air space) can help ensure that body heat is retained at a safe level.

#### **Treatment**

Recognition and proper treatment of hypothermia must be prompt. Delays even after rescue can cost a person his life. Low body temperature is the best indication of hypothermia. Blood pressure and pulse are also good indicators. The pulse is generally slow and irregular, while blood pressure is low.

The hypothermia victim is pale in appearance, the pupils are constricted and react poorly to light, and respiration is slow and labored. He will usually be shivering violently, with frequent muscular rigidity. There may also be an appearance of intoxication.

Emergency treatment must begin as soon as possible to stop the drop in body temperature. Wet clothing should be removed. If the body temperature is 97°F or above, no treatment other

than dry clothing and moving the victim to a warm area is generally necessary. If these are not available, the wet clothing should not be removed.

Combatting "afterdrop" in the core body temperature is extremely important. When heat is applied to the arms and legs, it causes those blood vessels to relax. This allows cold blood to flow back into the body core, further cooling the vital organs. Warming of the trunk of the body should be the prime concern.

During experiments in conjunction with the U.S. Coast Guard, researchers determined that the best warming technique was from the inside out, by having the victim breathe moist, warmed oxygen (Wilson 1976).

The next best treatment is a hot bath, with the water temperature between 90 and 100°F. If a tub is not available, an inflated life raft could be used. If possible, the limbs should remain out of the water. When no tub-type facility is available, a hot (115°F) shower while wrapped in towels or blankets is preferable.

When hot water for a tub or shower is unavailable, wrap the victim in blankets in a warm room with a heating pad or well-wrapped hot water bottle on the chest, or apply body warmth by direct contact with a rescuer.

Warm liquids may be given, but care must be taken to insure the victim is conscious and does not breathe the liquid into his lungs. Alcohol should never be given because it causes "afterdrop." Observe the victim's respiration closely and monitor for vomiting.

It has been learned in studies done in Alaska that victims of wet hypothermia can survive for a prolonged time in cases of deep cooling. Apparently, in the rapid cooling which occurs with wet hypothermia, physiological changes undergone by the body are more likely to be reversible than in the slower cooling of dry hypothermia. There have been victims of immersion hypothermia who were apparently dead but revived with proper treatment.

# Wind Chill (Equivalent Temperatures)

The temperature of the air is not always a reliable indicator of how cold a person will feel outdoors. Other weather elements, such as wind speed, relative humidity, and sunshine (solar radiation), also exert an influence. In addition, the type of clothing worn, together with the state of health and the metabolism of an individual, influence how cold a person will feel. Cooling may be described as loss of heat from exposed flesh. Freezing occurs when there is such total heat loss that ice forms in the exposed tissues. The cooling power of the atmosphere (by wind) is primarily heat transfer by advection—in human cases, by exposure of uncovered flesh to the environment. Even small amounts of air movement have considerable chilling effect because this movement disrupts or removes the thin layer of warmed air that builds up near and about the body. This air movement leads to loss of total heat, since heat is transferred from the core of the body to rewarm the new colder air, replacing that blown away. Therefore, wind chill not only leads to frostbite locally, but may contribute to general hypothermia.

During the antarctic winter of 1941 Siple and Passel developed a formula to determine wind chill from experiments made at Little America (Siple and Passel 1945). The formula relates heat loss (H) from an object or person to wind speed and to the difference in temperature between the air and the object or person (DT). It is measured in heat units (calories) per unit area over time. The skin temperature of most people is approximately 33 °C (91.4 °F). Heat losses for the human body can then be computed for any combination of wind and temperature. Equivalent temperature is based on calm conditions and a person walking vigorously at 3 knots (4 mph). Each combination of wind and air temperature produces a heat loss H. The equivalent temperature is that temperature that would compute the same heat loss at a wind of 3 knots. The accompanying chart, figure 18, shows equivalent wind chill temperatures in °C for various combinations of winds in knots or km/hr and temperatures.

Concepts in the following discussion of wind chill are from an appendix to an article by

													erature							
Wind	Speed						Cooli	ng Powe	r OI Win	d Expres	sed As	Equivale	ent Chill	Tempera	lure					
			Temperature (°C)																	
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Equivalent Chill Temporature																				
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27	251	0	6	12	18	- 25	- 31	- 37	- 43	- 49	~ 56									6.36.34
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14	714	1	8	14	21	27	- 34	- 40	- 47	- 53						38 B				
Little Danger Increasing Danger													**			2				
		(Flash May Freeze Within 1 Minute)																		

Figure 22. Equivalent Wind Chill Temperature

Adapted from NWS/NOAA Technical Procedures Bulletin No. 165. Effective Temperature (Wind Chill Index) 1976.

William J. Mills, Jr., M.D., as published in Alaska Medicine (1973). Dr. Mills is still active in the treatment of cold injuries in Alaska.

Almost everyone knows that the increased speed of wind may cause increased danger of skin freezing. Many assume that the increase in wind speed causes the ambient air temperature to fall lower. This is not so. What does occur is air movement, so that warmed air is moved away from the individual exposed to the wind, causing first local, then general body cooling. Any resultant decrease of skin temperature is due to heat loss, insidious or sudden. Local vasoconstriction, vascular shunting, and cellular changes take place; eventually ice forms in the tissues, with true tissue freezing or frostbite.

This phenomenon can be readily proved. Place a laboratory recording thermometer with a thermistor attached (or any outdoor thermometer) out your car window on a calm day when the temperature is, say,  $-20\,^{\circ}\text{C}$  ( $-4\,^{\circ}\text{F}$ )—just a nice winter day in Anchorage, Alaska. Let it sit for a few minutes until the temperature

reading has stabilized. This temperature, as read, will remain at the ambient air temperature level. Now slowly accelerate your vehicle to 80 km/hr (50 mph); the temperature remains unchanged at -20°C (-4°F). Now attach the thermistor to your bare hand. Place your ungloved hand out the same car window in the same ambient temperature of -20°C (-4°F). After a few minutes at 0 km/hr, the skin temperature may be read at approximately 93°F (normal skin temperature in the nonsmoker). Your skin temperature will drop as heat is lost to the exterior, sometimes falling as low as 85° to 80°F very rapidly. As the car is accelerated and the warmed air layer is moved away, the thermistor records skin heat loss. If you continue driving, your skin temperature may drop to a level near 23°F (-5°C), the temperature at which freezing of skin may actually occur.

Wind chill may occur not only from natural wind, but also with air movement generated by automobile, snowmobile, aircraft, or helicopter rotoblade. These vehicles may predispose passengers to frostbite or general hypothermia.

# Section II: Marine and Coastal Climatic Atlas

by William A. Brower, Jr., Ronald G. Baldwin, and Claude N. Williams, Jr.

# Marine and Coastal Climatic Atlas — Section II

William A. Brower, Jr. Ronald G. Baldwin Claude N. Williams, Jr.

The marine observations used in computing the statistics for the maps, graphs, and tables in this section of the three-volume atlas were taken from the National Climatic Data Center's (NCDC) marine surface data files which include the Comprehensive Ocean Atmosphere Data Set (COADS). COADS is the result of a multiyear effort by NOAA and the National Center for Atmospheric Research (NCAR) to provide a quality-controlled marine data set which incorporates data from a variety of global sources for 1854-1979. Those files are: TD-1170 for COADS and TD-1129 for 1980-1985. Because relatively little data exist for near-coastal zones. observations from 66 U.S., Canadian, and Russian coastal stations were combined with the marine data in order to present the best possible climatological picture of the outer continental shelf waters and coastal regions of Alaska, and adjacent Canadian and Russian regions.

Data for the U.S. and Russian stations were taken from the edited digital files of NCDC and the U.S. Air Force's Environmental Technical Applications Center (ETAC) in Asheville, North Carolina. Digital data from the Canadian stations were purchased from the Canadian Climate Centre in Downsview, Ontario. All data were subjected to thorough computer and visual quality control in order to eliminate duplicate observations and exclude questionable elements detected during internal consistency and extreme value checks.

The percentages of the summarized 4.5 million marine and 8.5 million coastal station land observations that contain basic weather elements are:

	Marine	Coastal Stations
Wind	93.8	99.1
Visibility	79.5	97.5
Present weather	82.8	95.7
Total cloud amount	79.6	97.3
Low cloud amount	67.4	57.4
Sea level pressure	93.5	89.7
Air temperature	94.4	98.6
Wet bulb temperature	59.4	97.7
Sea surface temperature	85.6	
Waves	65.4	-

The marine and coastal study area for which data were compiled and analyzed was expanded from 50°-80°N and 130°-180°W (in the 1977 atlas) to 40°-84°N and 110°W-160°E in order to afford greater coverage for each of the three atlas areas, with a minimum of overlap between areas. Element statistics (with observation counts) were generated for each of over 2,550 marine squares and 66 coastal stations within the study area, and then plotted by computer on monthly charts which have an albers equal-area conic projection. The marine plots were 1° latitude by 1° longitude squares for the latitude belt 40°-75°N and 1° by 2° areas for 75°-84°N. An analysis was performed on the entire marine and coastal study area in order to permit continuity between the three atlas areas. Meteorologists, aided by computer-drawn isopleth contours south of 65°N, drew isopleths (lines connecting points of equal magnitude) on 420 monthly element maps, and made subjective adjustments to the analyses when data biases or insufficient observations were evident. They also performed consistency checks in the sets of monthly patterns for each element and among elements, as well as comparative checks with other marine atlases and publications (see Reference).

Although more than a four-fold number of marine data above 65°N was available for this presentation than for the same area in the 1977 atlas, the amount remained inadequate to permit a detailed isopleth analysis by meteorologists or by computer-contouring routines. This was especially true for the cooler months when seasonal sea ice prevented ships of opportunity from frequenting the area. Isopleth analyses for the Chukchi-Beaufort Sea area, by necessity, were based principally on the plotted coastal stations' statistics, extrapolations of weather patterns identified in isopleth analyses for the warmer months, the period of greater data availability, and other marine and continental atlases and publications.

To supplement the isopleth analyses, nearly 16,750 monthly statistical graphs, tables, and roses were produced for 50 of the 66 land stations, 16 representative marine areas, and 43 5° by 5° marine areas. The graphics represent the objective compilation of all available data; they were not adjusted for suspected biases, and differences may be found when comparing the graphics data with the isopleth analyses.

For each topic set, all months are grouped in calendar order with one or two pages preceding each set containing the legend and narrative for that set. The legends contain detailed instructions on how to read the graphics and provide remarks which aid in interpreting the data. The following paragraphs contain additional remarks which are likely to be of interest to those called upon to interpret the data and provide answers to specific operational questions. The table on page II-4 describes the data and marine areas for this volume.

A word of caution. The intent of this atlas presentation was to gather and present existing data on climatological conditions within the marine and near coastal areas of Alaska and adjacent Canada and Russia. The data are presented without discussion and interpretations. Given the information presented in the introductory text, legend descriptions with related text, and number of observations (with measures of variability for some) displayed with the graphics presentations, the user should be able to assess the degree of statistical confidence in the presented climatology for a given month and location.

#### Standard Deviation

Some of the graphs display approximation of the empirical probability of occurrence of selected criteria. This is a major factor in assessing the risk involved in operational planning. For certain elements, unbiased estimates of population standard deviations are given on the graphs to provide a measure of variability. The standard deviation was computed using the expression:

 $s = \begin{bmatrix} N\sum_{i}^{2} - \{\sum_{i}^{2}\}^{2} \\ \hline N(N-1) \end{bmatrix}^{1/2}$ 

where N is the number of observations in the sample and  $x_i$  is the *i*th realization of the random variable x.

#### Sea Ice

The ice isopleths presented in Sets 17-19 give the percent probability of finding ice of any kind, ice concentration of one-half coverage or more, and ice thickness of eight feet or more, within the Alaska study area. Actual concentration boundaries, under the influence of changing synoptic meteorological and oceanographic

situations, may vary widely from the averages. An isopleth label, therefore, does not explicitly define the conditions on either side of the line since presence of sea ice is discontinuous in nature and regions of 80% mean ice concentration may be bordering regions of 20% ice concentrations with no intermediate region of 50% ice concentration. However, the inherent continuity of persistence of sea ice features permit an isopleth presentation to provide meaningful information.

The sea ice data were derived from digitized weekly analyses of sea ice conditions based primarily on satellite imagery (90%) supplemented by ship and shore reports, and aerial reconnaissance. These weekly polar sea ice analyses have been operationally produced by the U.S. Navy/NOAA Joint Ice Center (JIC) since 1972. In 1981, JIC initiated a Sea Ice Digitization Program to digitize the weekly polar ice maps as they become available. NCDC was funded by the U.S. Navy to design software and digitize all weekly ice concentration charts available since 1972 and ice thickness charts available since 1980, and produce polar ice atlases based on data through 1982. The Antarctic Ice Atlas was published in 1985, and the Arctic West and the Arctic East Atlases in 1986 (U.S. Navy 1986). The U.S. Navy also funded NCDC to accelerate the digitization of the West Arctic weekly charts through 1985 and produce the ice statistics presented in this atlas.

#### **Low Pressure Center Movement**

The roses and tracks of the low pressure center movement maps presented in Set 22 are based on 20 years of Northern Hemisphere track charts (January 1966 - December 1985) prepared by the National Weather Service's National Meteorological Center. These charts show cyclone tracks based on 6-hourly positions of closed centers. The NCDC was funded by the U.S. Navy to develop the software and digitize some 240 monthly cyclone track charts to permit inclusion of the statistics in this atlas. Frequencies of cyclone centers passing through 5° squares were analyzed by meteorologists within the 35°-80°N, 115°W-160°E area of the North Pacific Ocean to obtain the mean tracks. Primary tracks were selected along axes of maximum cyclone center frequency and secondary tracks along axes of moderate frequency.

#### Persistence of Wind and Waves

Duration and interval tables are presented in Set 23 for wind speed and wave height. Seasonal and annual tables contain objective

compilations for 23 grid points in the Gulf of Alaska and Bering Sea. The statistics are based on numerically-derived wind and wave data generated by NCDC using the Hindcast Spectral Ocean Wave Model (SOWM), developed by Dr. Willard J. Pierson and others, in producing U.S. Navy's SOWM Climatic Atlases for the North Pacific and North Atlantic Oceans (U.S. Navy 1985). No SOWM data were available to produce persistence statistics for grid points within the Beaufort Sea (Vol. III) area.

Episodes of durations (continuous hours or days) of events and episodes of intervals (continuous hours or days) between events were tallied for various thresholds. These tables give an indication of how long an episode is likely to last once it has begun. For convenience, the time an episode persisted above a given threshold is arbitrarily referred to as a "duration" of the event. The times between episodes have been termed "intervals." Data were summarized on a seasonal and annual basis because 12.5 years of hindcast data were considered too small a sample to provide representative durations and intervals for long episodes of wind and wave conditions on a monthly basis. The winter season is January-March; spring, April-June; summer, July-September; and autumn, October-December (World Meteorological Organization, 1981).

# Return Periods for Maximum Winds and Waves

Tables of estimated maximum sustained wind speeds and wave heights for selected return periods are presented in Set 24 (Set 23 for Volume III). Estimates for winds are presented for 50 coastal stations within the 3-volume area and for 23 marine grid points within the Gulf of Alaska and Bering Sea areas (Vols. I and II). Hourly wind observations for the stations and numerically-derived wind and wave data generated by Pierson's Spectral Ocean Wave Model (SOWM) for the marine grid points were used in determining the wind and wave extreme estimates. No SOWM data were available for the Beaufort Sea (Vol. III) area. Following the method outlined by Lieblein (1954, 1974a, 1974b), these estimates were obtained by initially fitting an extreme value distribution to each station and marine grid point sample containing N maximum monthly or annual wind speed or wave height values, then inverting the distribution and computing extreme values for selected probabilities. Confidence bands were then computed following the techniques of Gumbel (1958), and Gumbel and Lieblein (1954).

The extreme value distribution has the form:

$$F(x) = F(x;\mu,\beta) = \exp \left[-\exp\left(-\frac{x-\mu}{\beta}\right)\right]$$

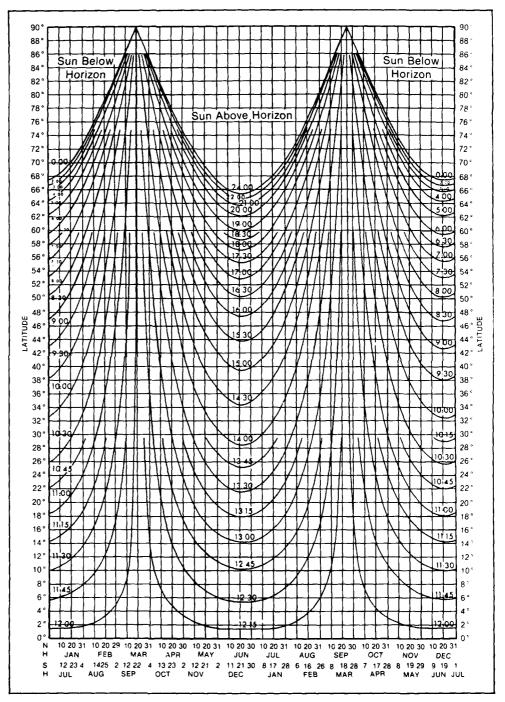
where F(x) is the probability that our observations are equal to or less than the specified value x,  $\mu$  is the mode, and  $\beta$  is the scale parameter. Since the wind data were transformed logarithmically,  $\mu$  and  $\beta$  refer to the transformed data, not to the wind maxima. The values given in the tables of Set 24 are the result of applying the natural logarithms of the N annual extreme wind to the extreme value model, determining the  $\mu$  and  $\beta$  for each data set, and them exponentiating the logarithms of the estimates to give the probability estimates in knots. The wave data were not transformed logarithmically and, therefore,  $\mu$  and  $\beta$  are in feet.

Graphic presentations similar to Figure 1 of Set 24 were drawn for each month and for the annual values, and are available on microfiche at the NCDC. The year/month extreme data for each station and marine grid point are also available on magnetic tape. These presentations provide a visual indication of the "goodness of fit" of the model to the data. The confidence limits shown by the envelope of lines about the line of "best fit" represent the level of uncertainty in the extreme value estimate corresponding to a given probability. For this study, 68% confidence limits were computed. This means that in 68% of repeated samples, the true extreme value will be contained within these limits.

#### **Duration of Daylight**

The duration-of-daylight chart for the Northern Hemisphere defines daylight as the period from sunrise to sunset. The upper scale at the bottom of the chart is for the Northern Hemisphere; the lower scale is for the Southern Hemisphere. For example, daylight on July 20 of any year at 48°N is about 15 hours and 30 minutes for any longitude. The data source was the U.S. Naval Observatory (1945) and is accurate for the entire twentieth century. Further details may be obtained from The Daylighter of the Navy Weather Research Facility (1960). Additional light (during twilight) may be usable for many purposes. Duration of daylight in high latitudes (poleward of about 60°) becomes increasingly dependent upon atmospheric conditions and refraction, and there may be some departure from the values depicted on the charts.

Figure 23. Duration of Daylight



Volume II

The following stations and representative marine areas have data plotted for analysis and graphics.

Land Stations	Lat.(°N)	Long.(°W)	Data Processed	No. of Obs.	No. of Obs./Day
Adak	51.9	176.7	Jan 1949-Apr 1985	264,528	8-24
Buhta Providenja	64.4	173.2	Jan 1959-Apr 1985 +	54,876	8
Cape Newenham	58.7	162.1	Jul 1953-Jan 1971; Jan 1973-Apr 1985	231,968	14-24
Cape Ozernoy*	57.7	163.3E	Jan 1959-Jul 1976 +	34,509	8
Cape Romanzof	61.8	166.0	Mar 1953-Dec 1968; Jan 1973-Apr 1985	226,254	17-24
Cape Shipunskiy*	53.1	160.0E	Jan 1959-Dec 1963; † Jan 1969-Jul 1976	25,082	8
Cold Bay	55.2	162.7	Jul 1955-Apr 1985	164,612	8-24
Khatirka-In-Chukot	62.1	175.3E	Jan 1959-Apr 1985 +	41,972	8
King Salmon	58.7	156.7	Jan 1949-Apr 1985	221,433	8-24
Nikolski	52.9	168.8	May 1959-Nov 1968	27,370	8
Nikol'skoe	55.2	166.0E	Jan 1959-Apr 1985	66,800	8
Nome	64.5	165.4	Jan 1945-Apr 1985	255,656	8-24
Northeast Cape	63.3	169.0	Jan 1953-Nov 1968	120,922	14-24
Port Heiden	57.0	158.6	May 1975-Apr 1985	73,676	14-24
St. Paul	57.2	170.2	Sep 1949-Apr 1985	135,031	4-24
Shemya	52.7	174.1E	Dec 1948-Apr 1985	227.236	4-24
Topata-Olyutorskaya*	60.6	171.1E	Jan 1969-Jul 1976 +	14,920	8
Ugol'naja	63.1	179.3E	Jan 1959-Apr 1985 +	60,852	8
Unalakleet	63.9	160.8	Jul 1948-Apr 1985	182,001	6-24

<sup>+</sup> Period excludes Jul 1971-Dec 1972.
\* Stations used for isopleth analyses only; no graphics produced.

Representative Marine Areas	Lat.(°N)	Long.(°W)	Data Processed	No. of Obs.
Α	60-65	Coast-180	1879-1984	42,930
В	55-60	169-180	1905-1984	58.806
С	55-60	Coast-169	1908-1984	87.604
D	Aleutian-55	165-180	1888-1984	110,471
Ε	50-Aleutian	165-180	1881-1984	116,510
F	50-Coast	158-165	1872-1984	123 020

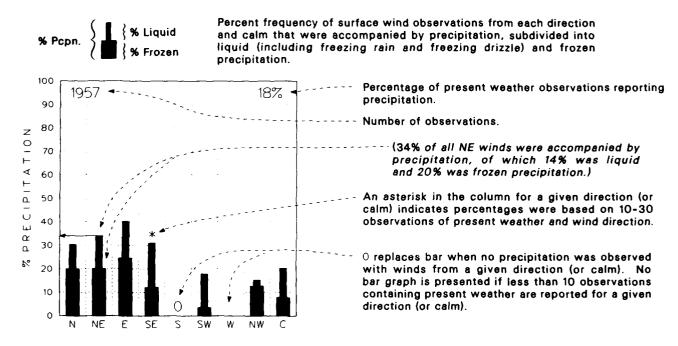
## Map 1. Precipitation

**BLACK LINE** – Percent frequency of observations reporting precipitation.

BLUE LINE - Percent frequency of precipitation observations reporting frozen precipitation.

Albers Equal—Area Conic Projection

## **Graphs:** Precipitation/wind direction



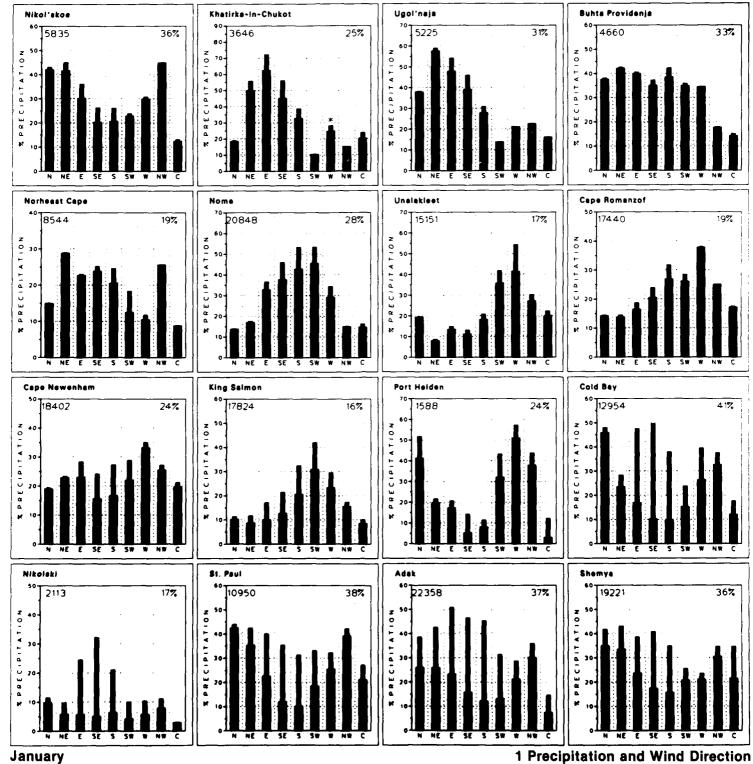
The percent frequency of observations reporting frozen precipitation for a given point on a monthly isopleth map can be determined by multiplying the percent frequency of observations reporting precipitation (BLACK LINE) with that of precipitation observations reporting frozen precipitation (BLUE LINE).

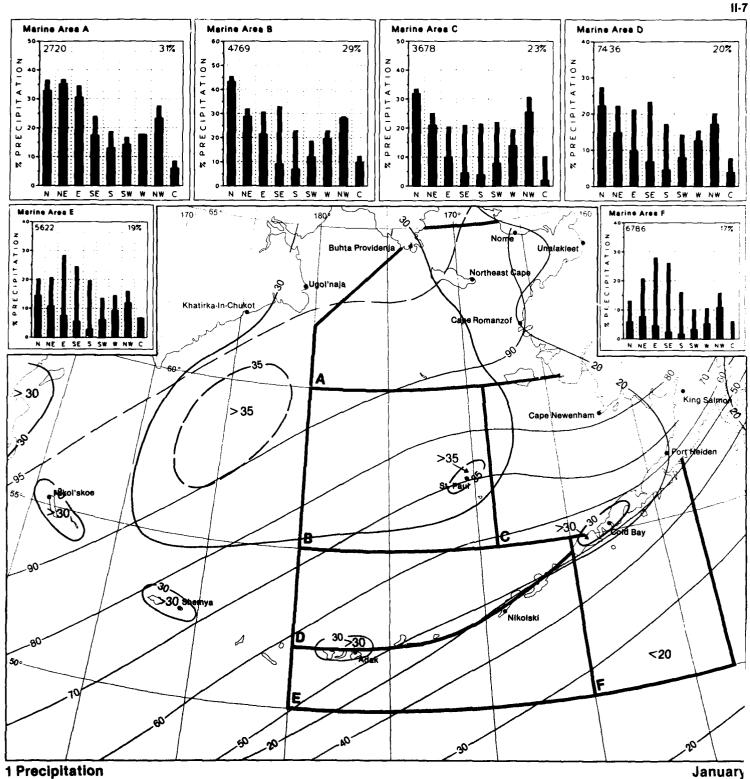
Of the elements recorded in the historical marine data base, precipitation is one that is most subject to error in both the way it is observed and the way it is interpreted. It is often implied in the literature that ships often try to avoid foul weather and thereby bias the oceanic climatology towards fair weather. A recent study by Elms (1986), in which he compared the Volunteer Observing Ship (VOS) data to Ocean Station Vessel (OSV) and buoy data, concluded there is little evidence that "fair weather bias" is a serious problem for most applications of marine climatic data.

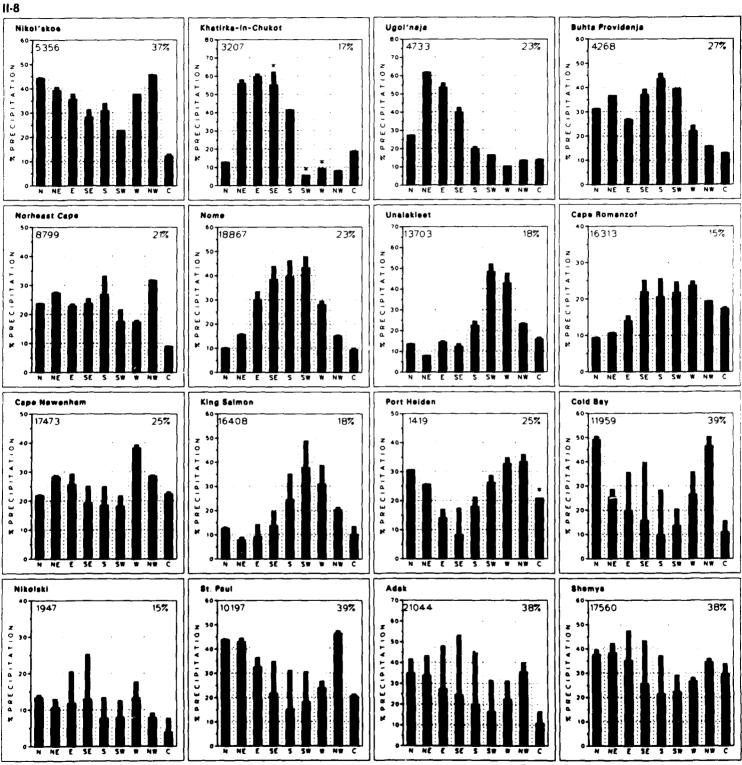
Assessing oceanic rainfall data is a major problem because transit ships are unable to take quantitative precipitation measurements. A number of studies have been conducted in efforts to predict precipitation amounts, or rates of fall, based on estimates derived from the use of present weather observations from ships of opportunity (Goroch, et al., 1984) and readings from satellites (Rao, et al., 1976). Refer to the text and table in Set 2 for additional information about precipitation.

1 Legend

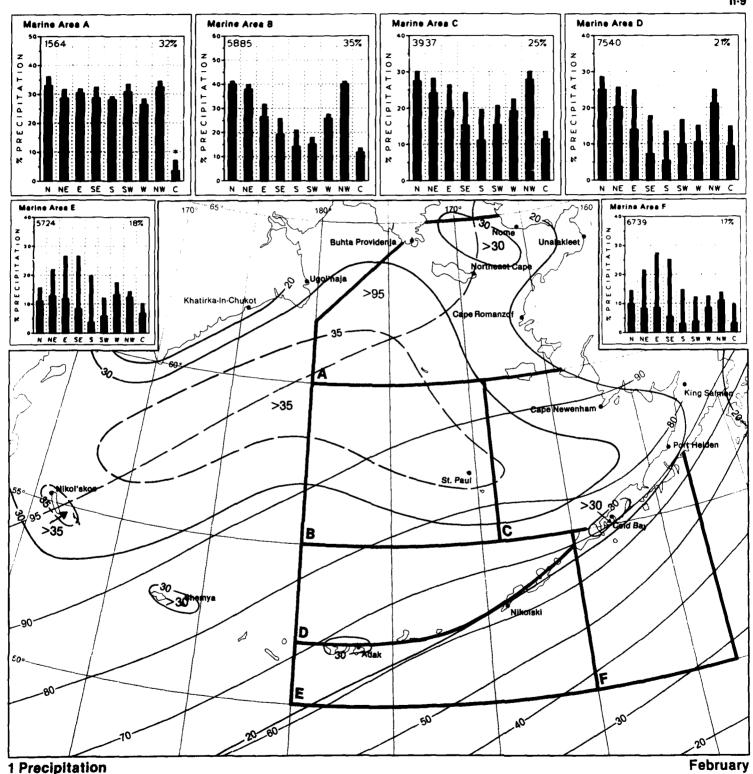
Legend 1



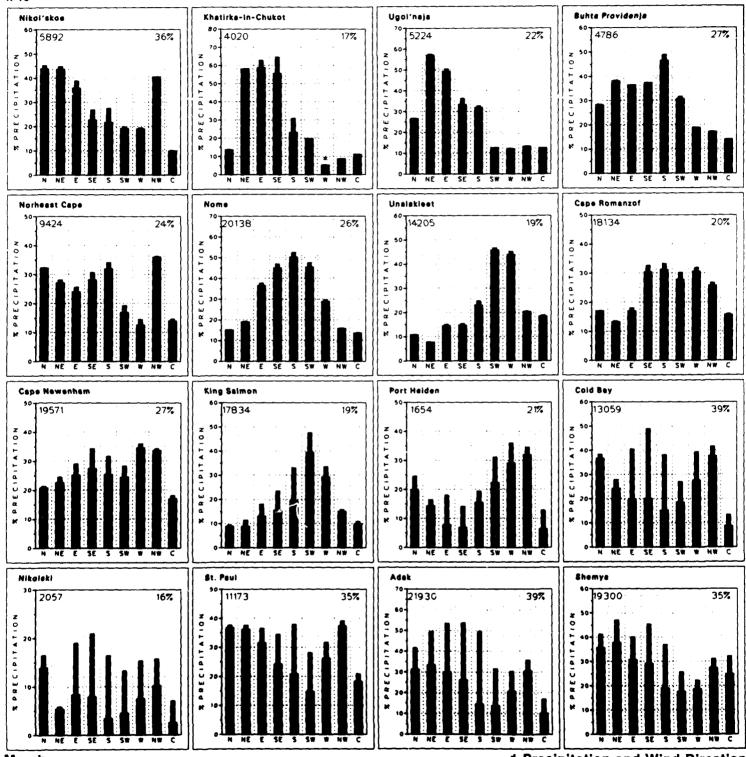




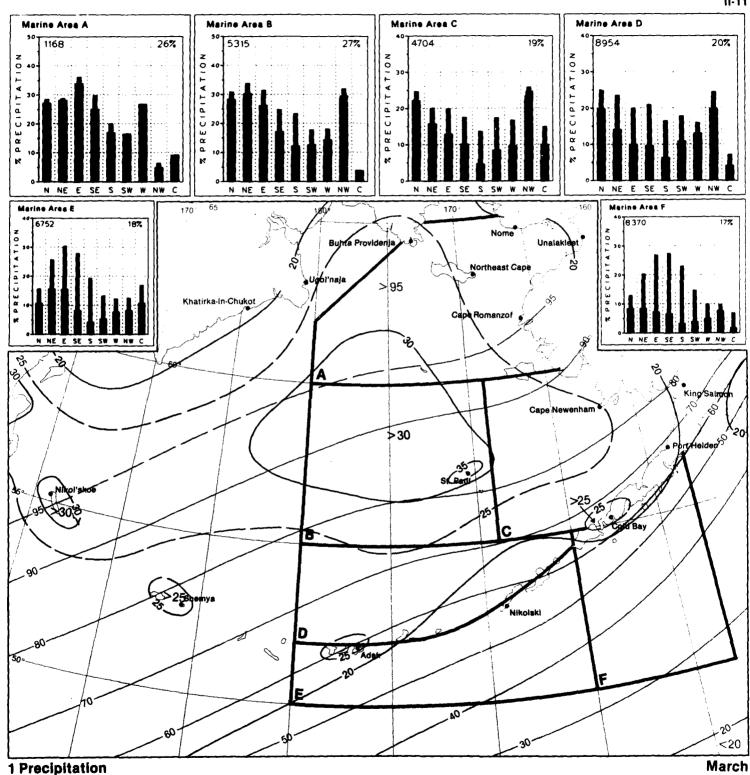
February 1 Precipitation and Wind Direction

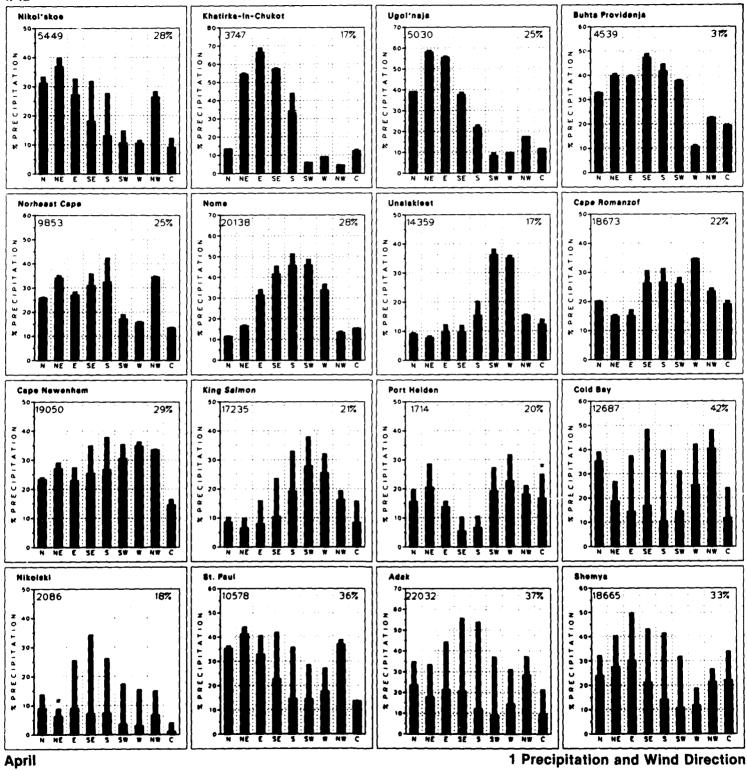


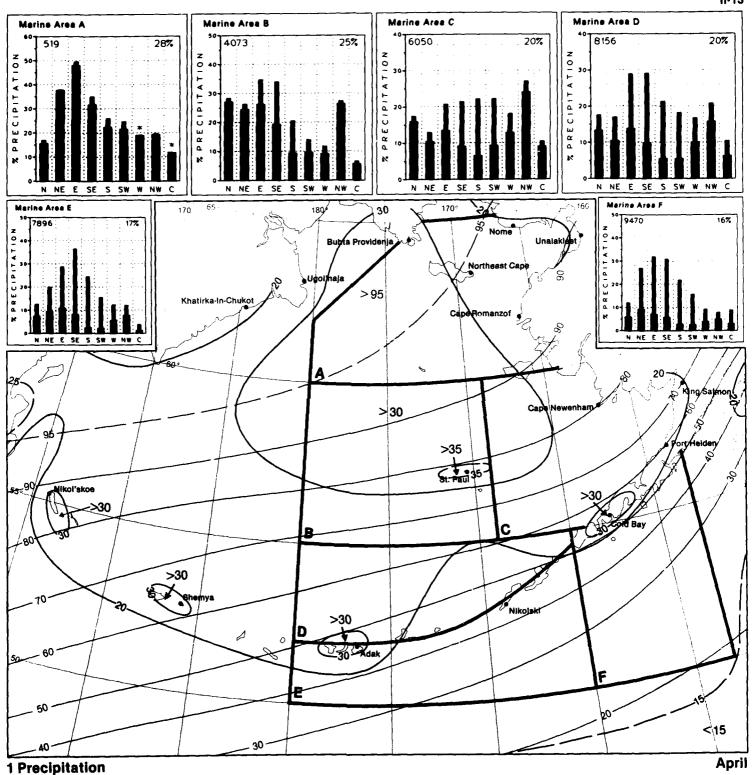
1 Precipitation

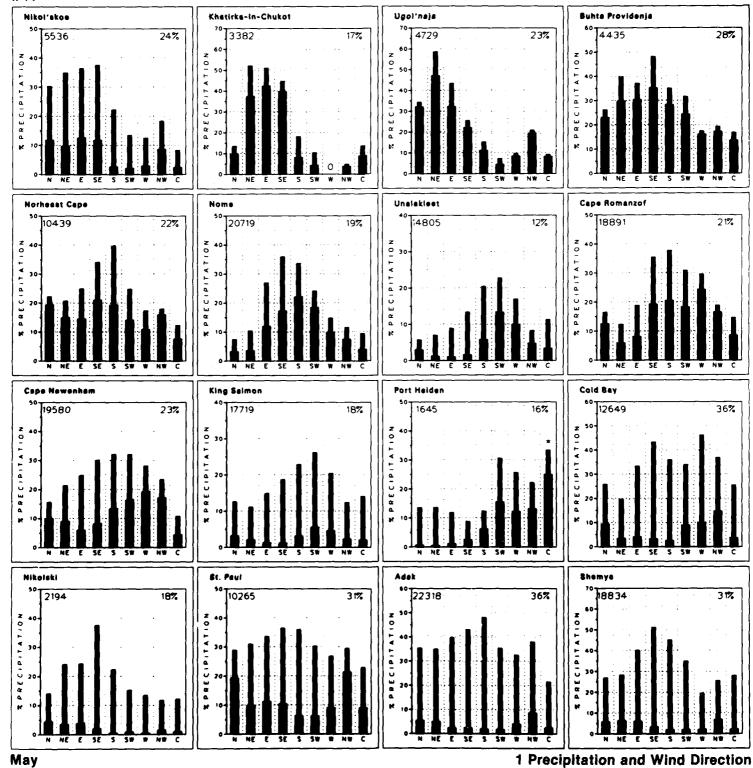


March 1 Precipitation and Wind Direction

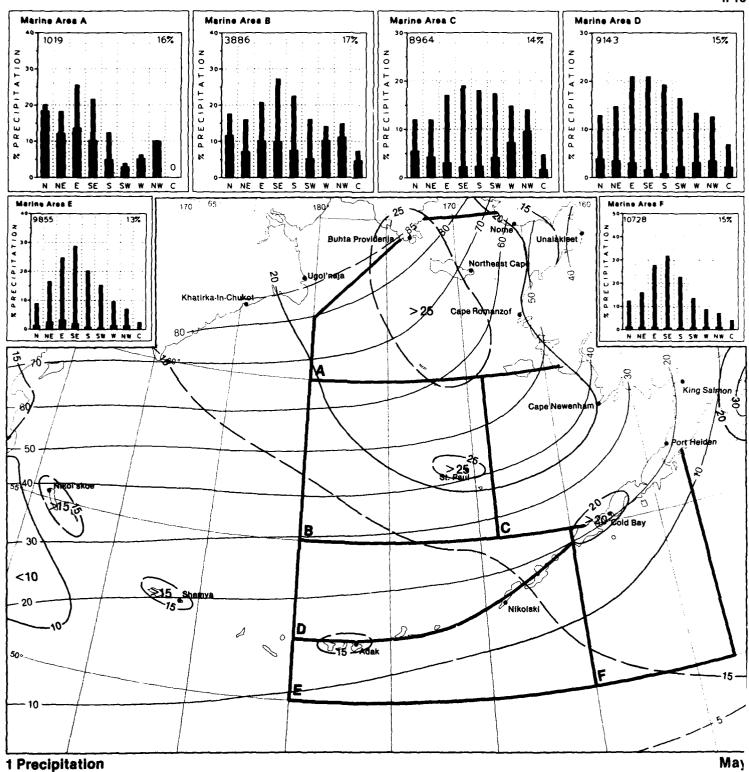


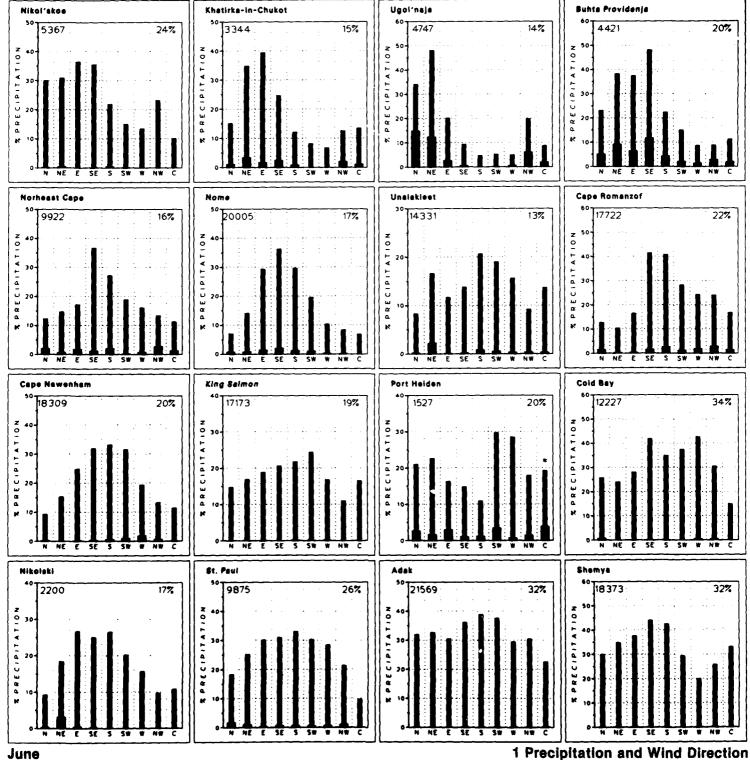


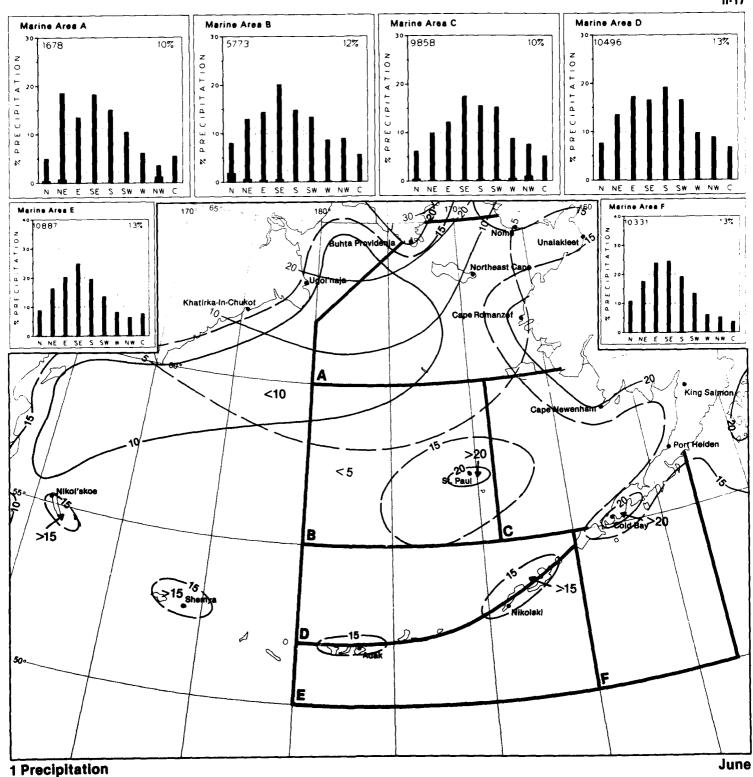


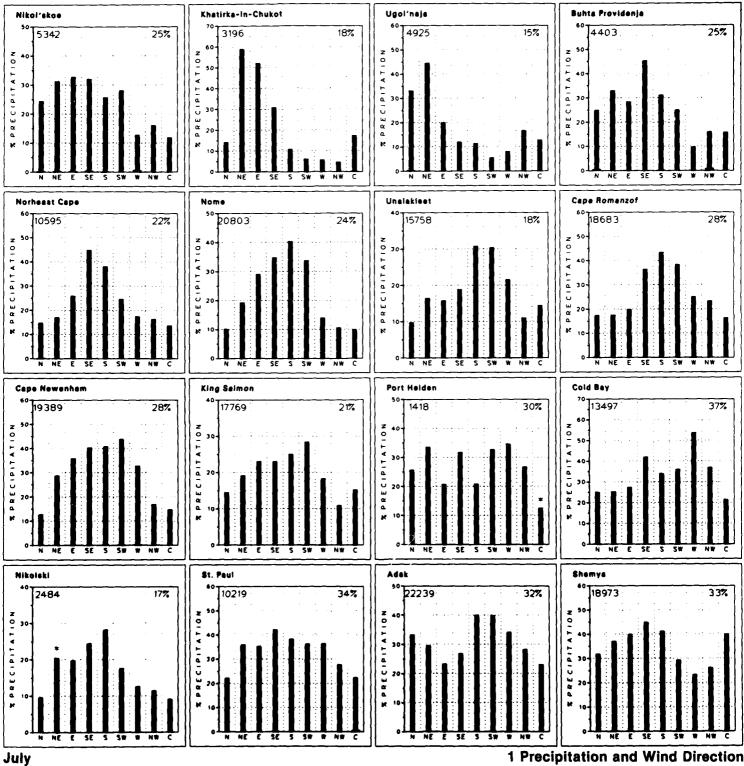


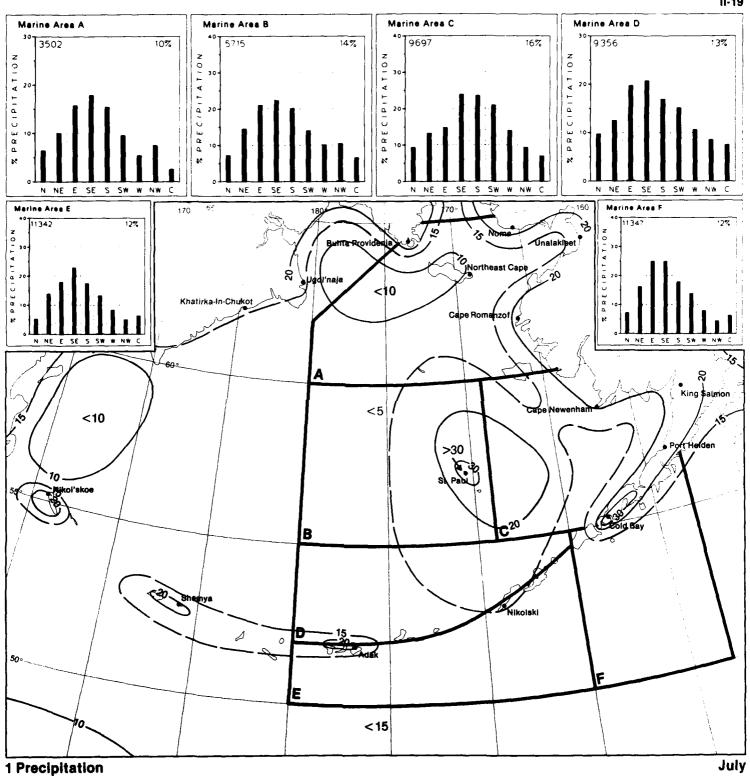
1 Precipitation and Wind Direction

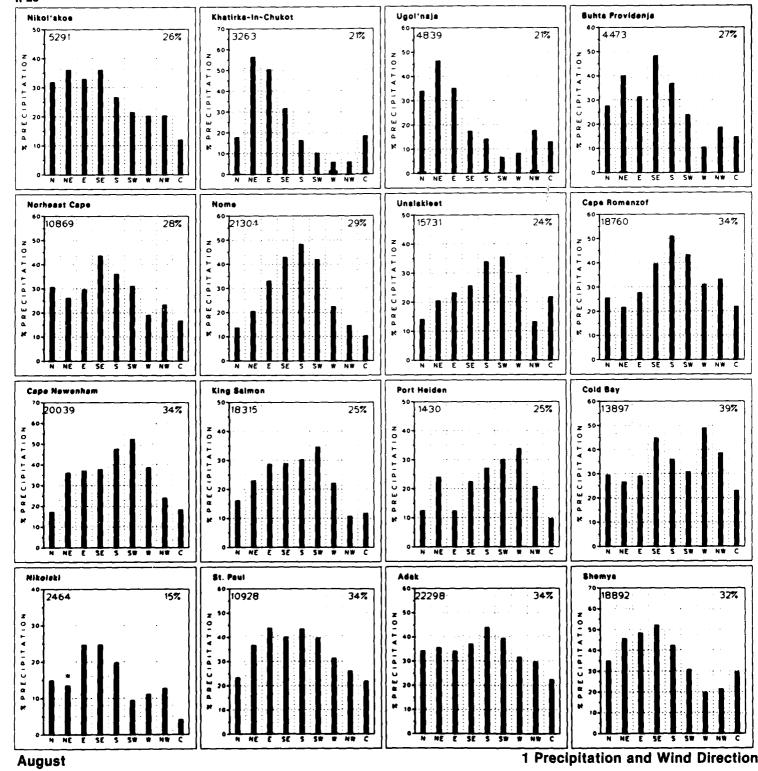


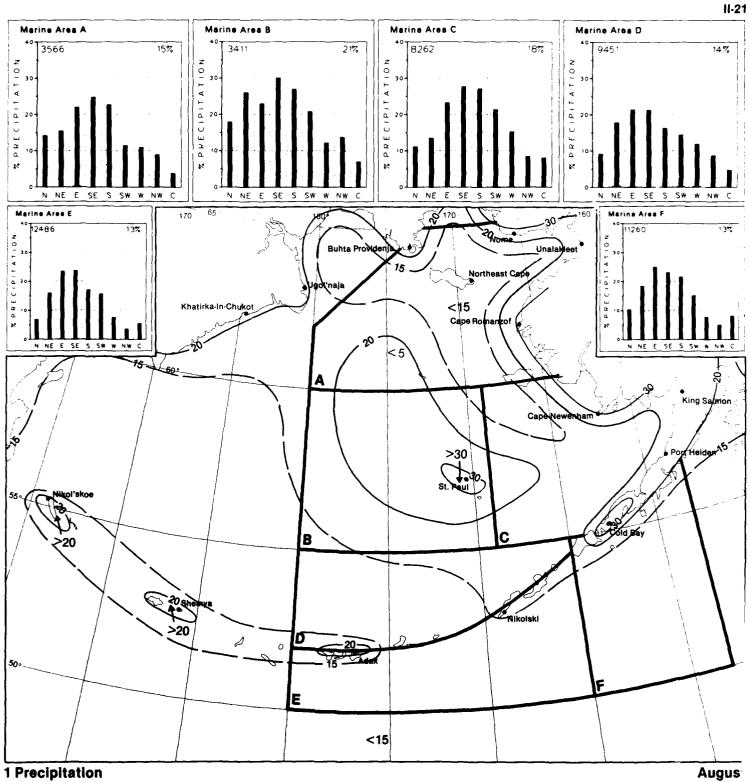


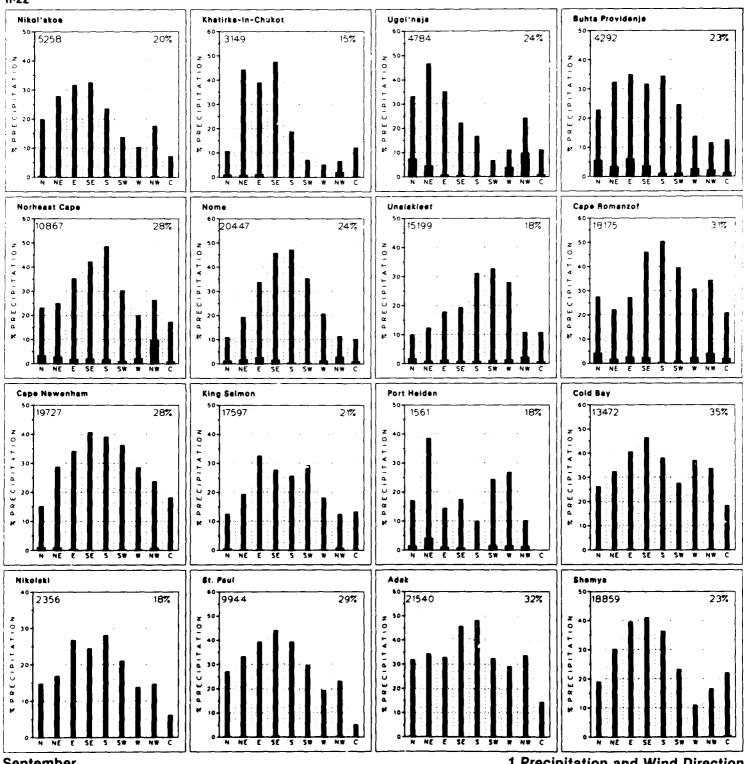




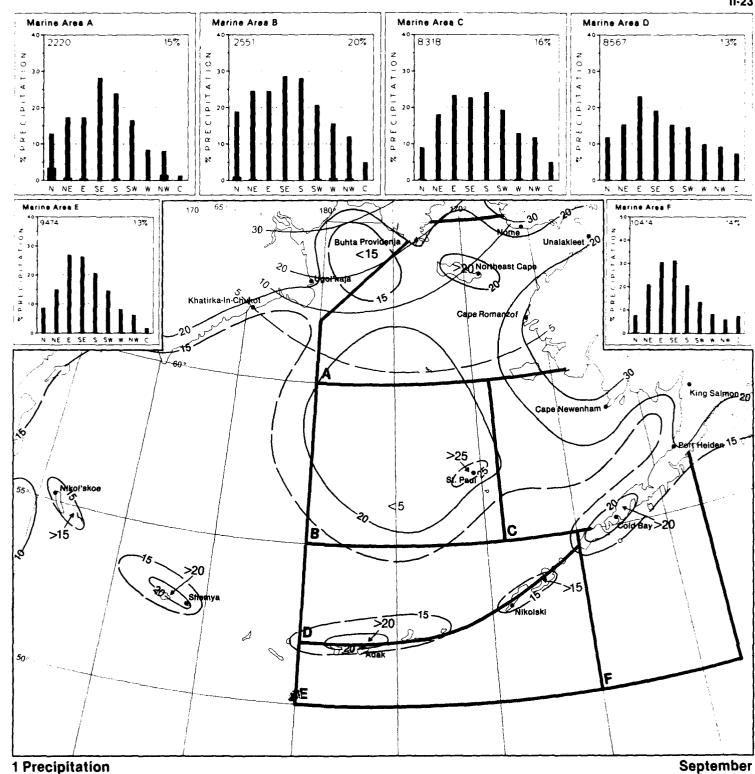


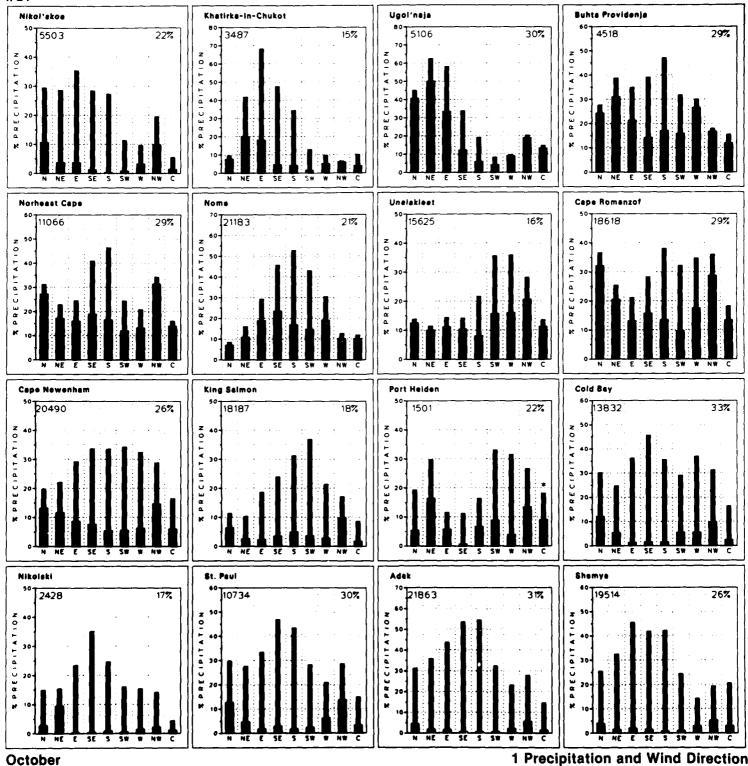




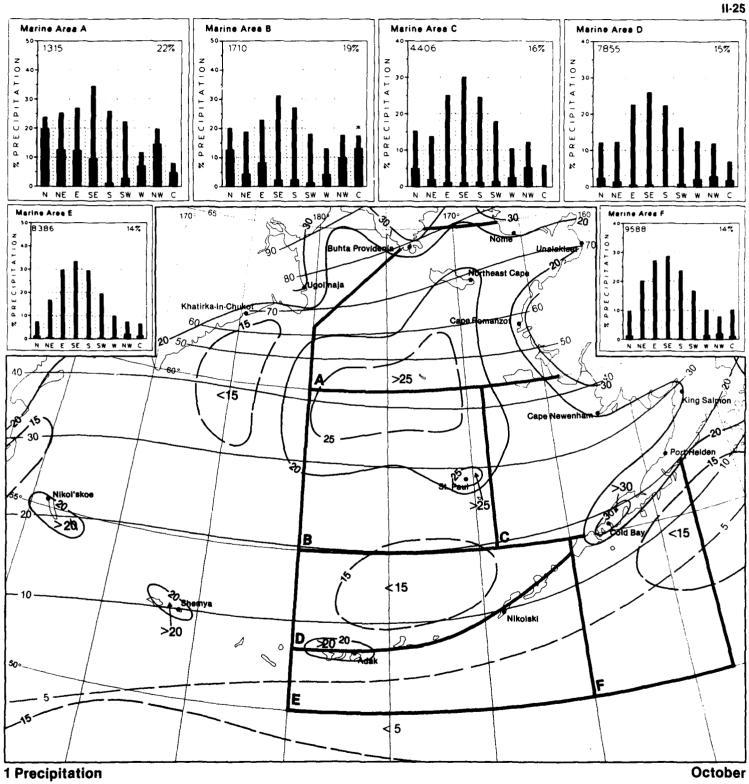


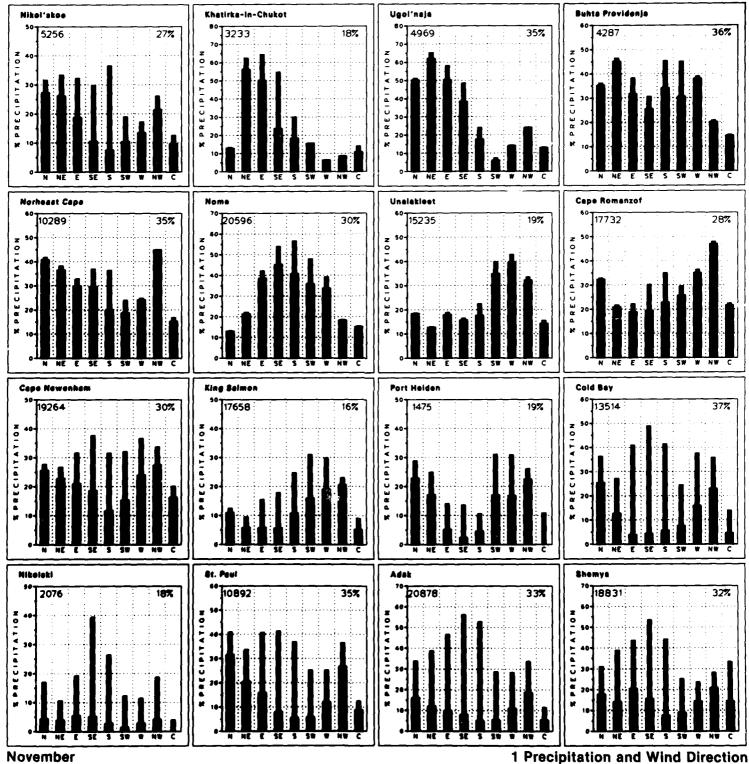
September 1 Precipitation and Wind Direction



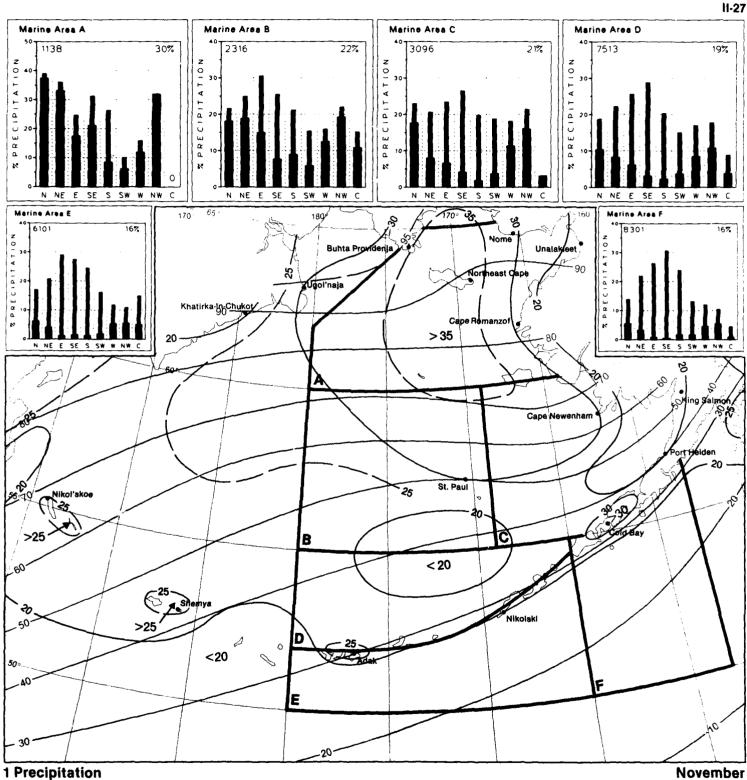


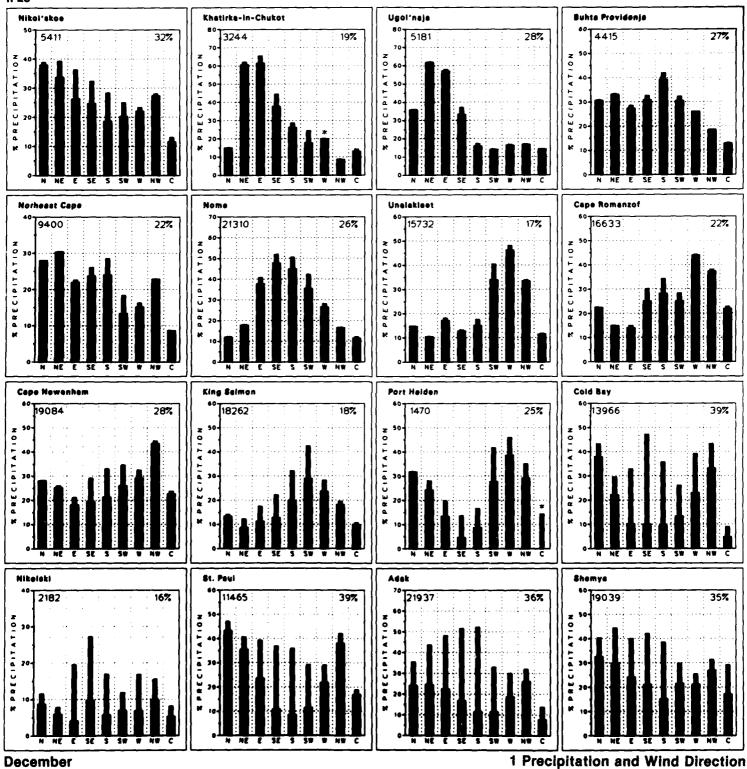
**October** 



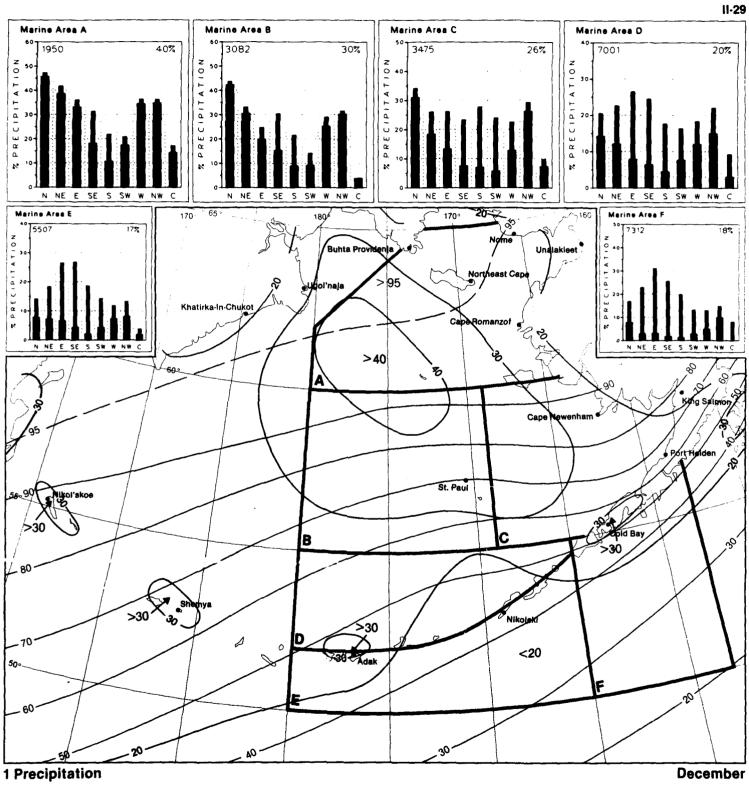


1 Precipitation and Wind Direction





December



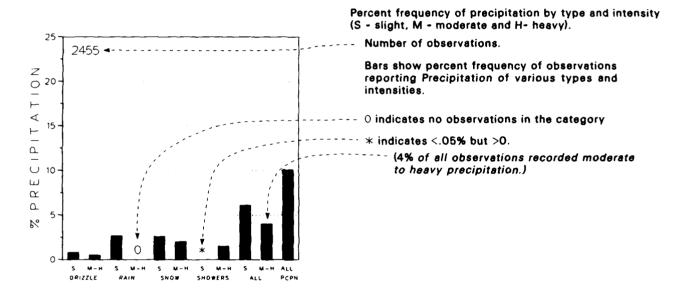
# Map 2. Wind/visibility/cloudiness

BLACK LINE - Percent frequency of optimum conditions: Low cloud ceiling (LCC) ≥5000 feet, (or no LCC), visibility ≥5 nautical miles and wind 11-21 knots.

BLUE LINE - Percent frequency of poor conditions. Any one of the following constitutes poor conditions: LCC <300 feet, visibility <1 nautical mile or wind <6 or ≥34 knots.

Albers Equal—Area Conic Projection

## **Graphs:** Precipitation types



Present weather elements that can be reported in an observation are thunderstorms, lightning, waterspouts, squalls, fog, haze, smoke, dust, and all forms of precipitation. Most present weather codes (ww = 00-99, see table) apply to phenomena occurring at the time of observation, but a few refer to phenomena occurring in the past hour. The highest applicable numerical ww code figure is recorded (except that code 17 has preference over 20 to 49, inclusive). Precipitation includes all forms of water particles, whether liquid or solid, that fall to the earth's surface—rain, drizzle, snow, snow pellets, snow grains, ice crystals, ice pellets, and hail. Each form is classified by its character (continuous, intermittent, showery, or combination), intensity (slight, moderate, or heavy), and type (liquid, freezing, or frozen). In this study, frozen precipitation is defined as any precipitation that reaches the ground in frozen form; it does not include liquid that freezes upon impact with the ground or exposed objects. Refer to the text in Set 1 for additional information on precipitation.

2 Legend

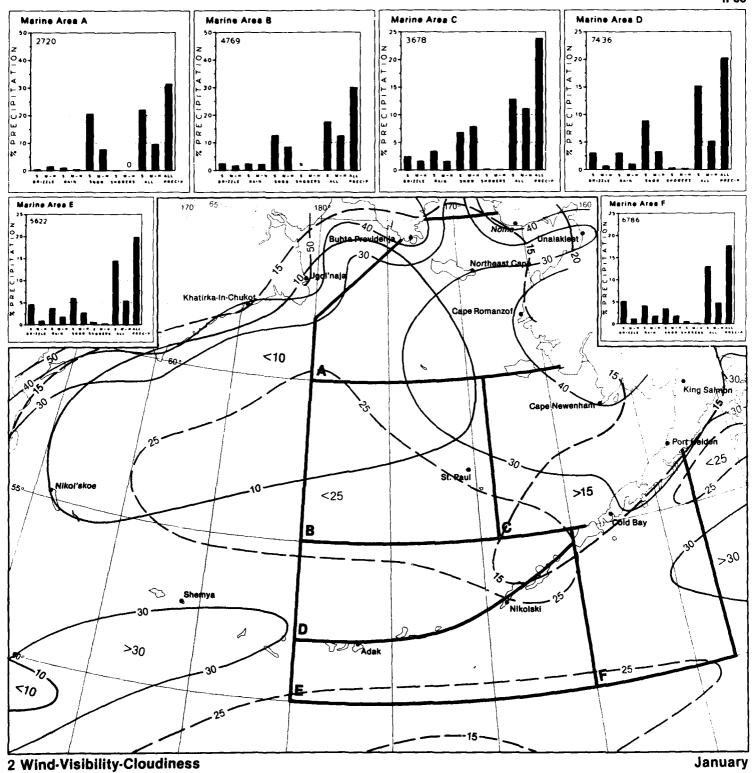
Legend 2

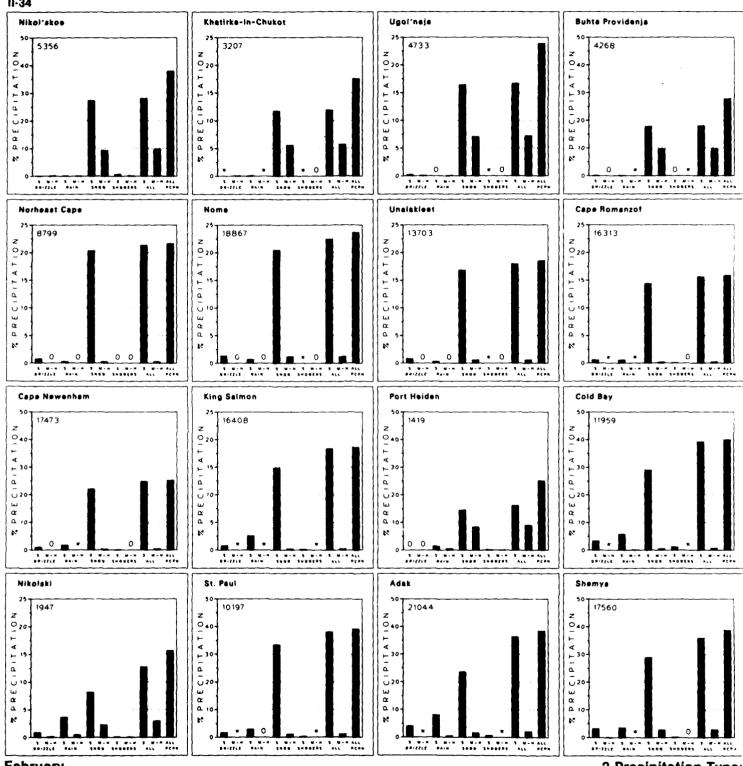
#### PRESENT WEATHER (WMO Code, 1982)

The present weather (ww) code is arranged in priority order. Reading down the list, select the first applicable (most severe) weather condition that you observe and enter the code number for ww.

	50-99 PRECIPITATION AT SHIP AT TIME OF OBSERVATION	Intermittent 74 Heavy snow in flakes 72 Moderate snow in flakes	Continuous 75 73	32 31 30	Duststorm or sandstorm, increasing Duststorm or sandstorm, unchanging Duststorm or sandstorm, decreasing	35 34 33
9	5-99 THUNDERSTORM AT TIME OF OBSERVATION	70 Slight snow in flakes	71		•	
3.	733 THOMBERSTORIN AT TIME OF OBSERVATION	•			20-29 PHENOMENA IN PAST HOUR BUT NO	~
99	Heavy thunderstorm with hail*	60-69 RAIN (NOT FALLING	AS SHOWEDS!		TIME OF OBSERVATION	JIAI
98	Thunderstorm with duststorm or sandstorm	Slight	Moderate or Heavy		THE OF OBSERVATION	
97	Heavy thunderstorm with rain and/or snow,	68 Rain or drizzle with snow	69	29	Thunderstorm, with or without precipitation	0.0
	but no hail*	66 Freezing rain	67	28	Fog (in past hour but not at time of obs.)	OII
96	Slight or moderate thunderstorm with hail*		•	27	Shower(s) of hail*, or of hail*, and rain m	IVAd
95	Slight or moderate thunderstorm with rain or	Intermittent	Continuous	26	Shower(s) of snow, or of rain and snow m	nkeu Nevil
	snow, but no haif*	64 Heavy rain	65	25	Shower(s) of rain	
		62 Moderate rain	63	24	Freezing drizzle or freezing rain	
Incl	udes hail, ice pellets, or snow pellets	60 Slight rain	61	23	Rain and chou mixed or ice sellets	
		• •		22	Snow	Not falling
91.9	4 THUNDERSTORM DURING THE PAST HOUR BUT	50-59 DRIZZI	E	21	Rain (not freezing)	as showers
	NOT AT THE TIME OF OBSERVATION			20	Drizzle (not freezing) or snow grains	
		Slight	Moderate or heavy		, and grama ,	
Note	Use code 29 if there is no precipitation at time of	58 Drizzle and rain mixed	59	*Inc	ludes hail, ice pellets or snow pellets	
	rvation.	56 Freezing drizzle	57		person person	
		,			18-19 SQUALLS, FUNNEL CLOUDS	
94	Moderate or heavy snow, or rain	Intermittent	Continuous		10-19 SQUALLS, FUNNEL CLOUDS	
	and snow mixed, or hail*	54 Heavy drizzle	55	19	Funnel cloud(s) seen in past hour or at tir	ma at aba
93	Slight snow, or rain and snow Thunderstorm	52 Moderate drizzle	53	18	Squalls (no precip.) in past hour or at time	
	mixed, or hail* in past	50 Slight drizzle	51		oqualis (no precip.) in past nour or at time	e 01 005
92 91	Moderate or heavy rain hour Slight rain			13	-16 PHENOMENA WITHIN SIGHT BUT NOT	AT SHIP
	,			16	Precip. within 3 naut. mi.—reaching surfa	ce
Inch	ides hail, ice pellets, or snow pellets	00-49 NO PRECIPITATION AT	CHID AT TIME OF	15	Precip. beyond 3 naut. mi reaching surf	
		OBSERVATION AT		14	Precipitation in sight, not reaching surface	
	85-90 SOLID PRECIPITATION IN SHOWERS	OBSERVATION	***	13	Lightning visible, no thunder heard	,,,
	20 00 COLID I IILON II ANION IN CHICALING				, , , , , , , , , , , , , , , , , , ,	
Sligh	Moderate or Heavy	17 Thunder at time of observat	on no precipitation		10-12 MIST AND SHALLOW FOG	Fog not
89	Shower or hail*, no thunder 90	at ship	on, no procipitation	12	Shallow fog-more or less continuous	deeper
87	Shower of snow pellets or ice pellets† 88	2. Jp		11	Shallow fog in patches	than 10 m
85	Shower of snow 86	40-49 FOG AT TIME OF C	BSERVATION	10	Mist (Visibility 1/2 nautical mile or more)	(33 feet)
†Wit1	or without rain, or rain and snow mixed	(Visibility in fog is less than	1/2 nautical mile)		04-09 HAZE, DUST, SAND, OR SMOKE	
'Incl	ude hail, ice pellets, or snow pellets	(,,			**************************************	
		Sky	Sky	09	Duststorm or sandstorm within sight	
	80-84 RAIN SHOWERS	visible	invisible	08	Dust whirls in past hour (NOT FOR MARIN	NE USE
		48 Fag. depositing rime	49	07	Blowing spray at ship	
84	Shower of rain and snow mixed, moderate or heavy	46 Fog, has begun or thickened	in past hour 47	06	Widespread dust suspended in the air	
83	Shower of rain and snow mixed, slight	44 Fog, no change in past hour	45	05	Dry haze	
82	Violent rain shower	42 Fog, has become thinner in p	ast hour 43	04	Visibility reduced by smoke	
81	Moderate or heavy rain shower	41 Fog in patches			, roddodd by omone	
80	Slight rain shower	40 Fog at a distance but not al	ship in past hour		00-03 CHANGE OF SKY DURING PAST HO	UR
ου	A	30-39 (Not likely to be used	in ship reports)	Code		
	SOLID PRECIPITATION NOT FALLING AS SHOWERS			figs.		
70-79		OII A				
70·79 79	ice pellets	Slight or		03	Clouds generally forming or developing	
70-79 79 78	ice pellets isolated star-like snow crystals(with or without fog)	moderate	Heavy	03 02	Clouds generally forming or developing State of the sky on the whole unchanged	
70·79 79	ice pellets		e level) 39	03	Clouds generally forming or developing	oped

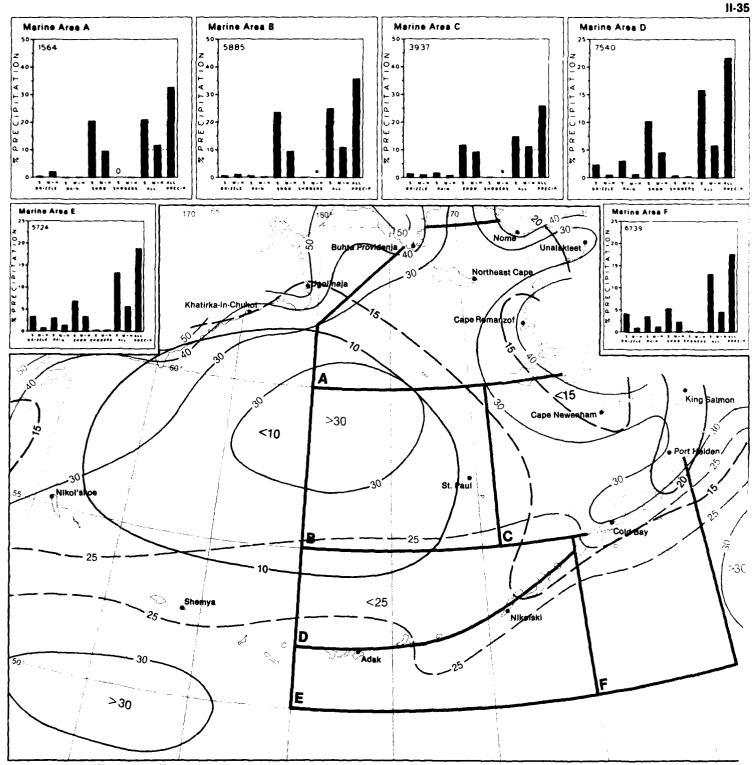
2 Legend





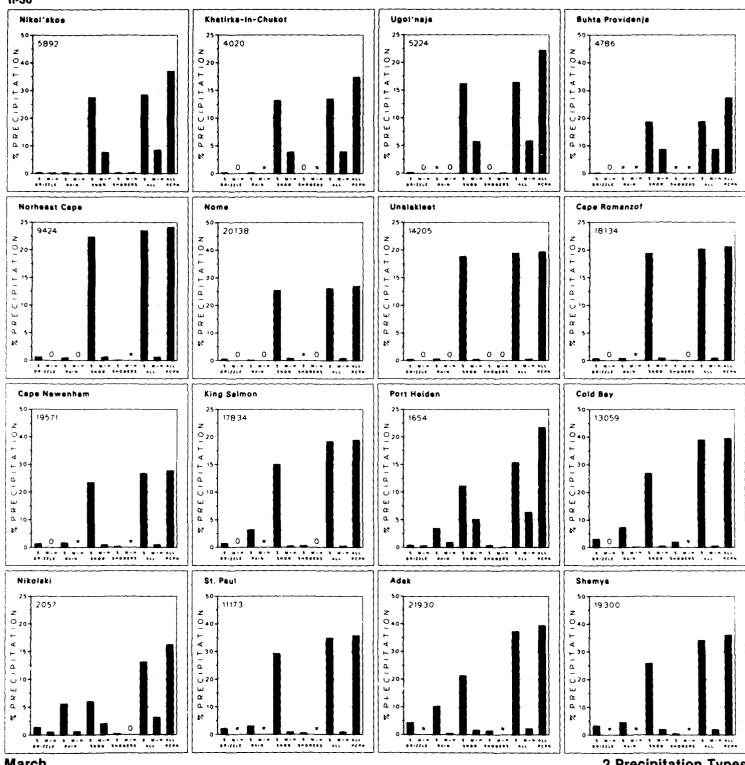
**February** 

2 Precipitation Type:



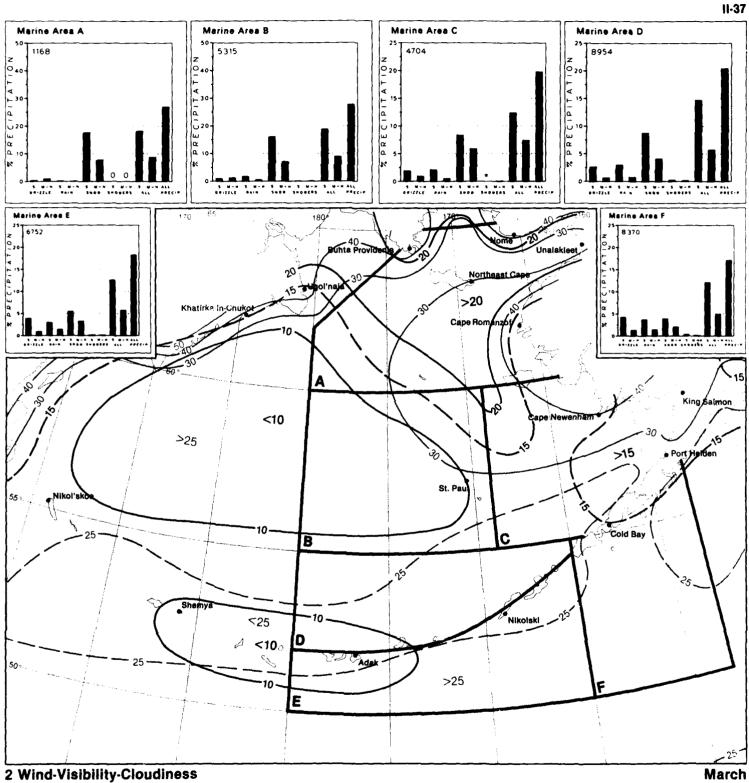
2 Wind-Visibility-Cloudiness

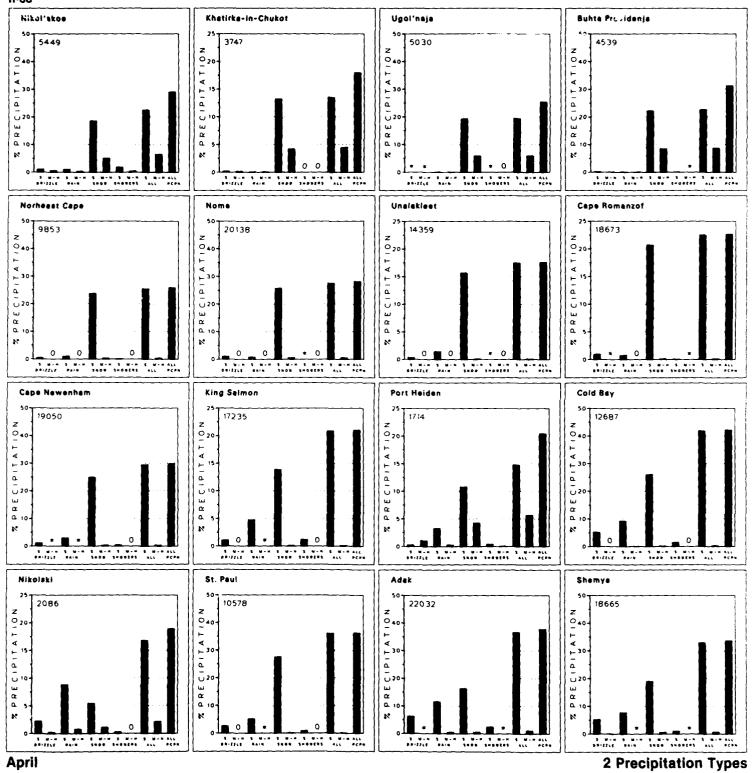
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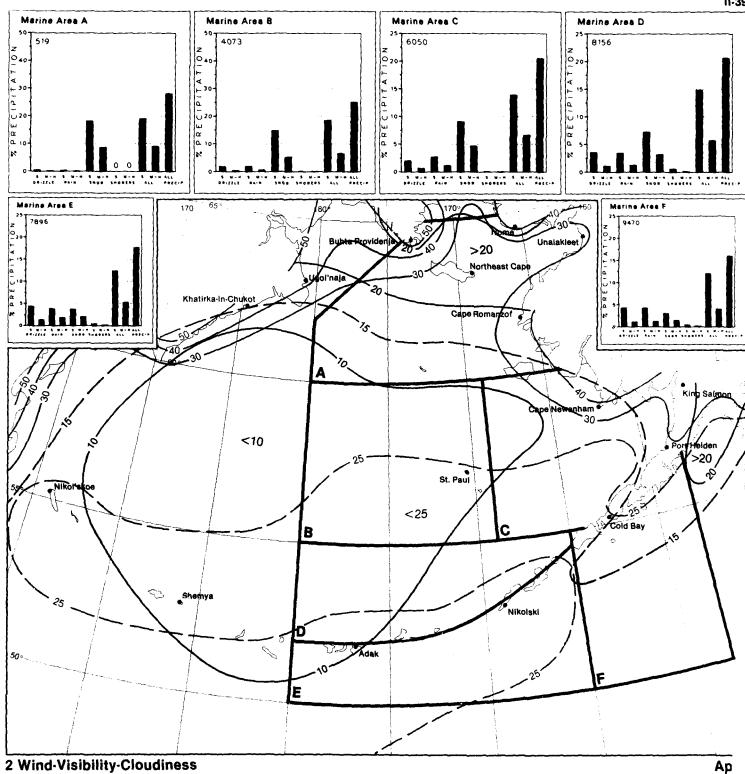


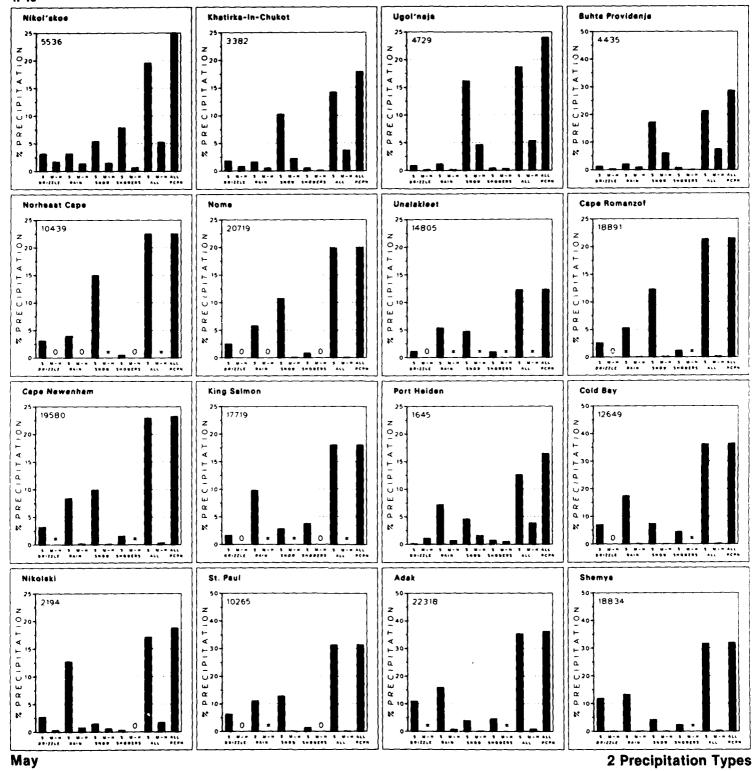
March

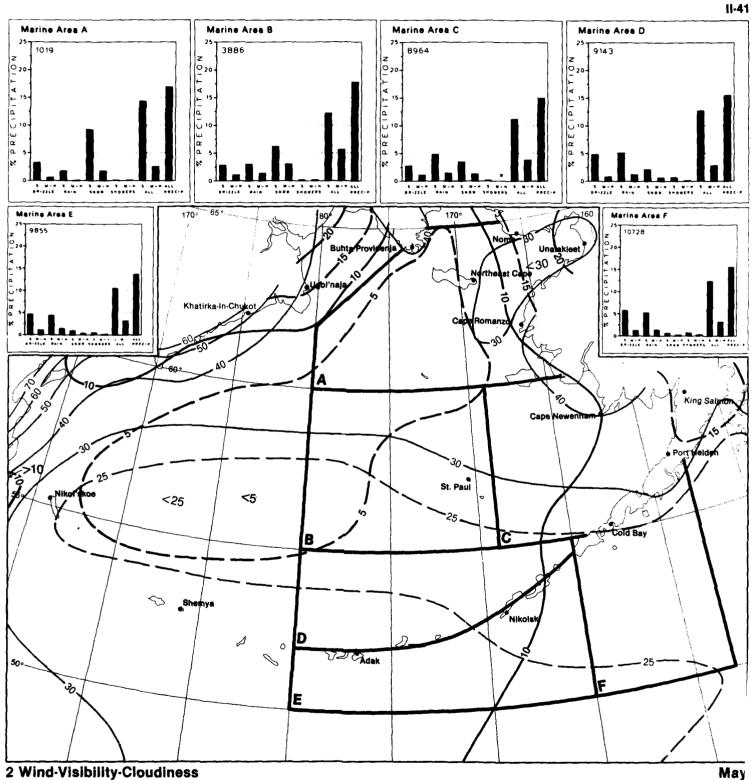
2 Precipitation Types

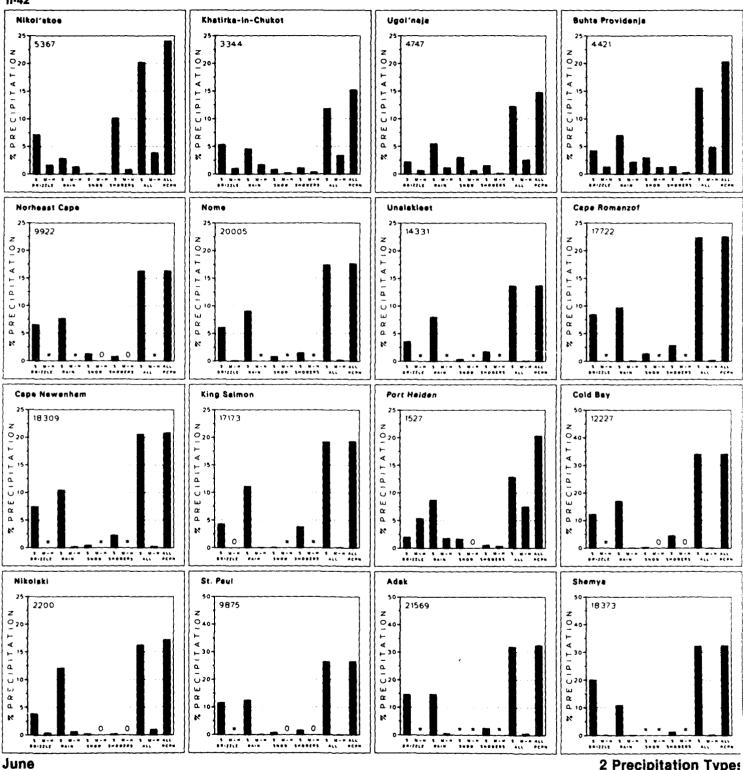




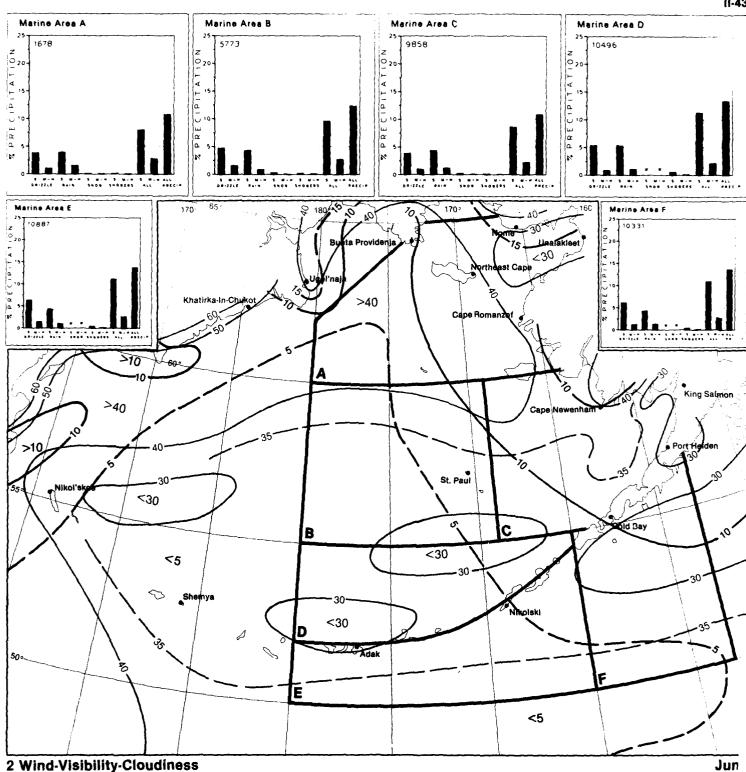


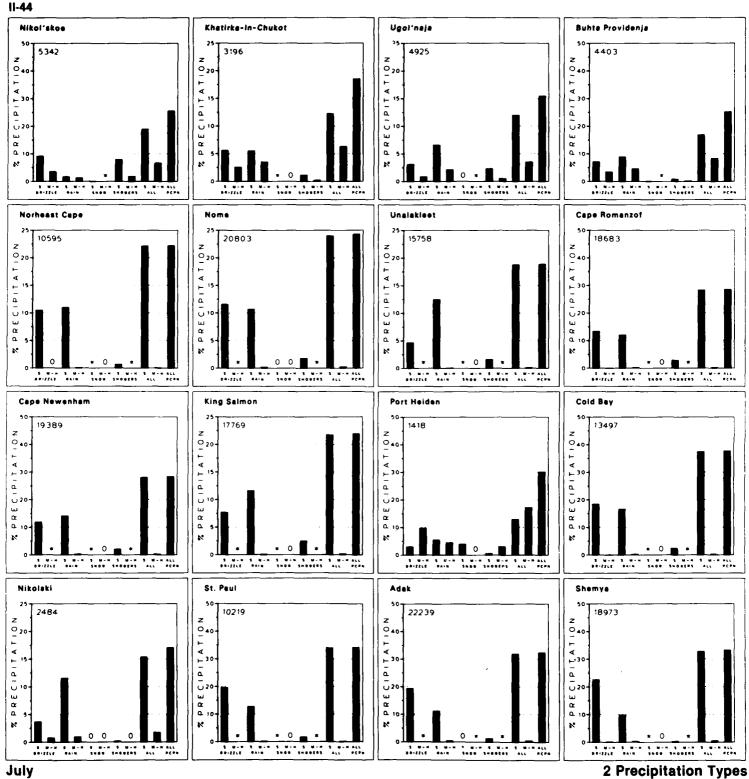


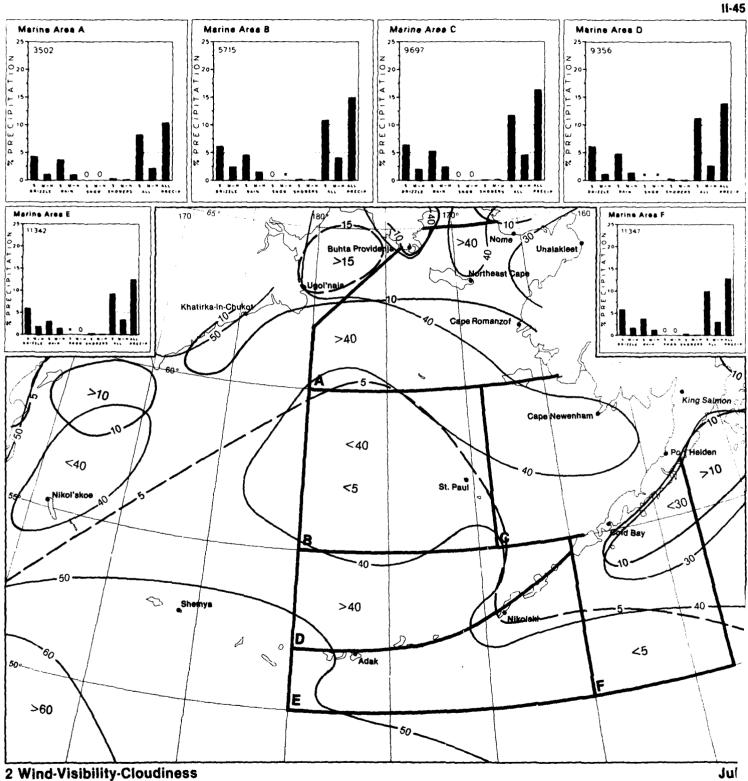


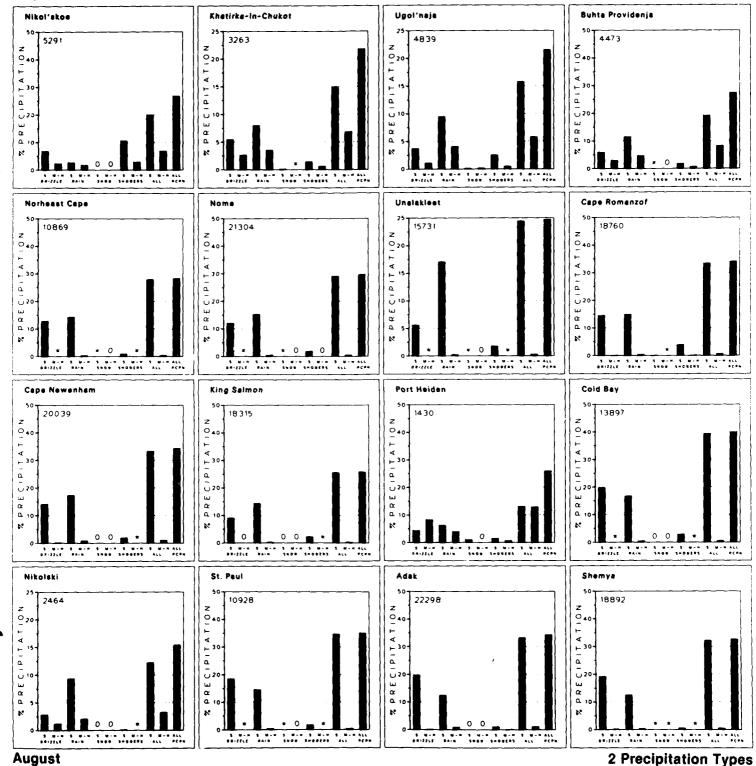


2 Precipitation Types

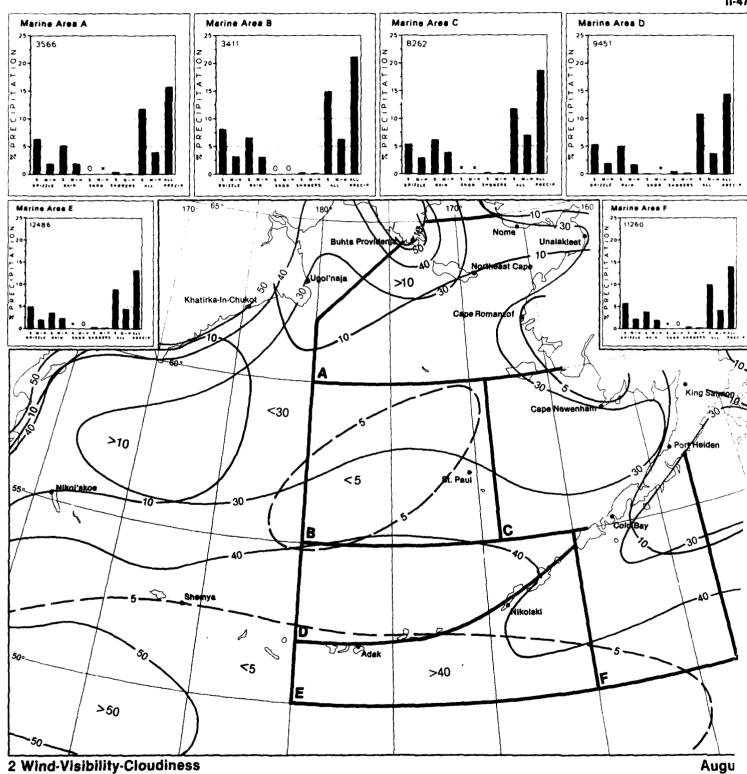


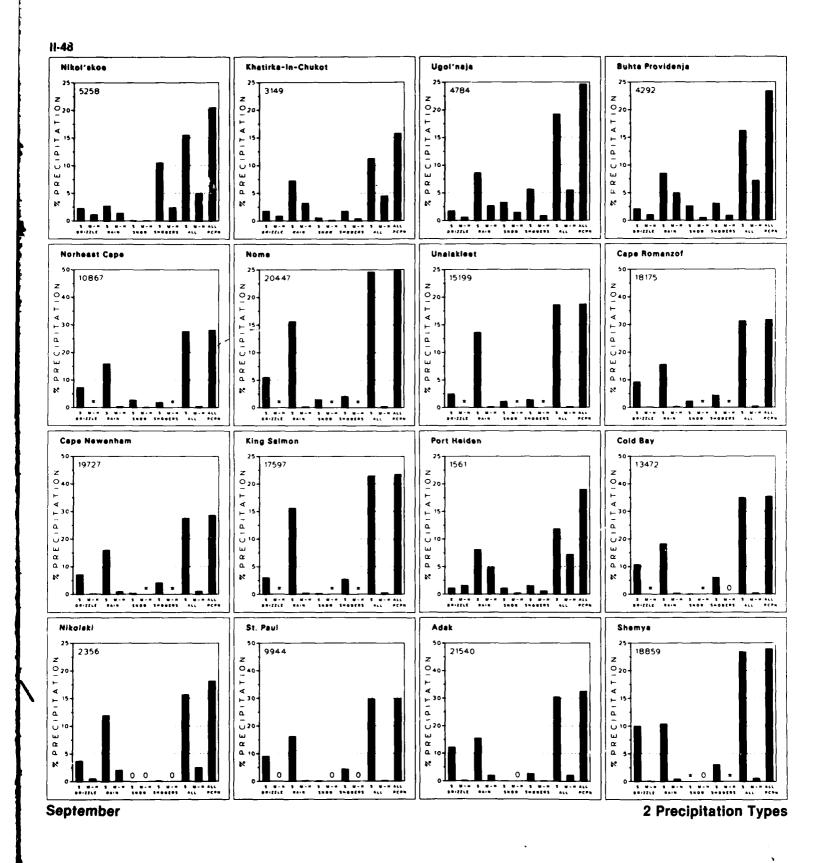


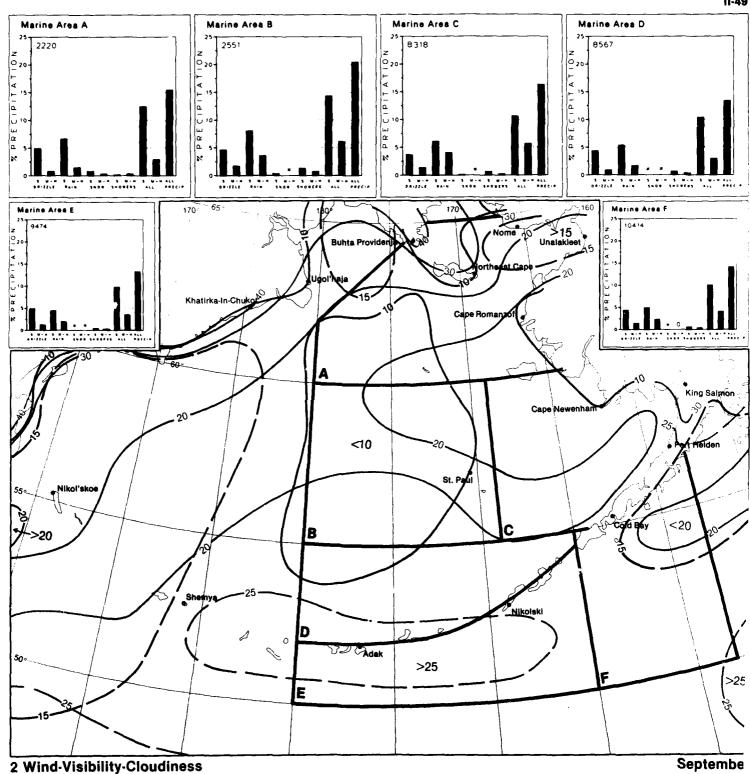


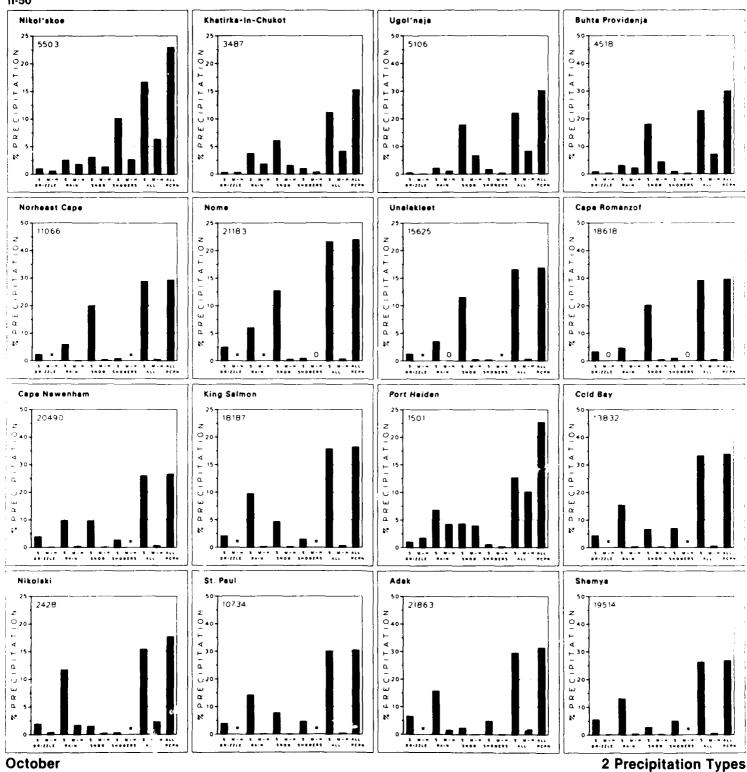


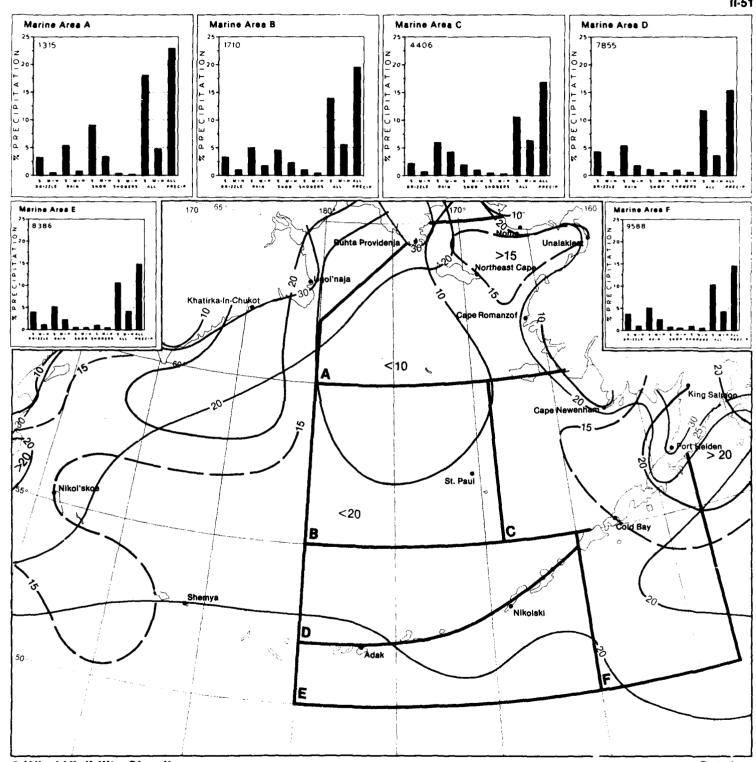
2 Precipitation Types





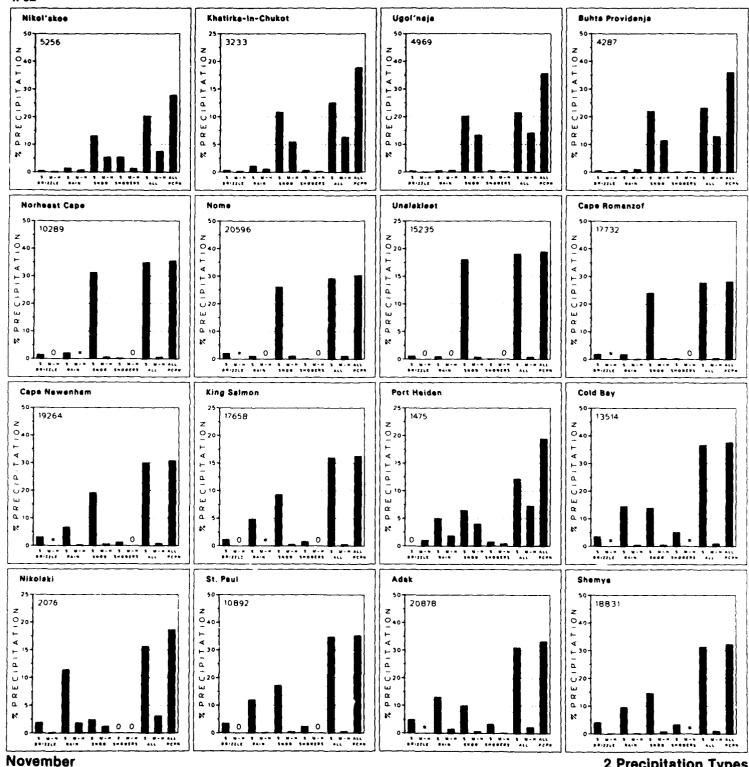




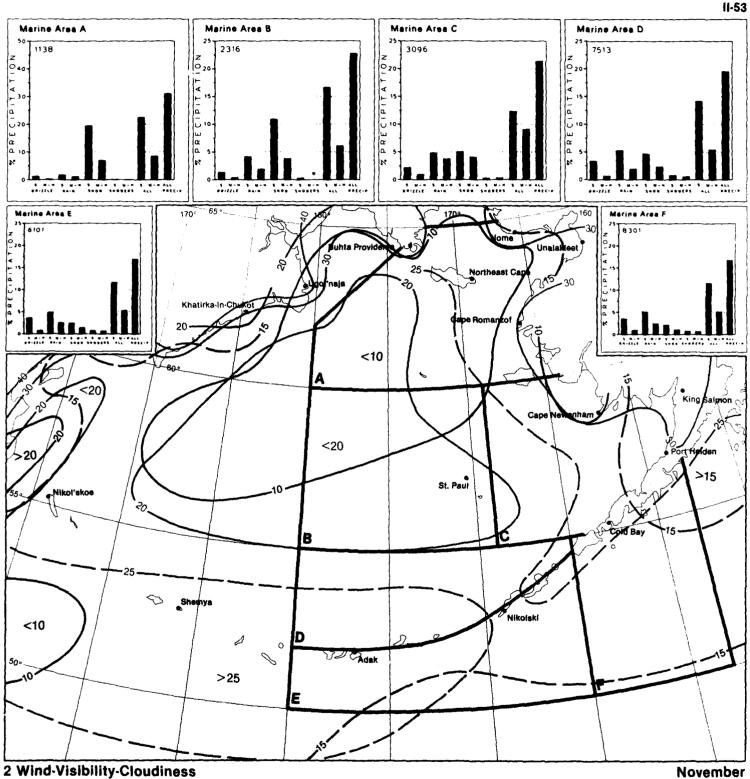


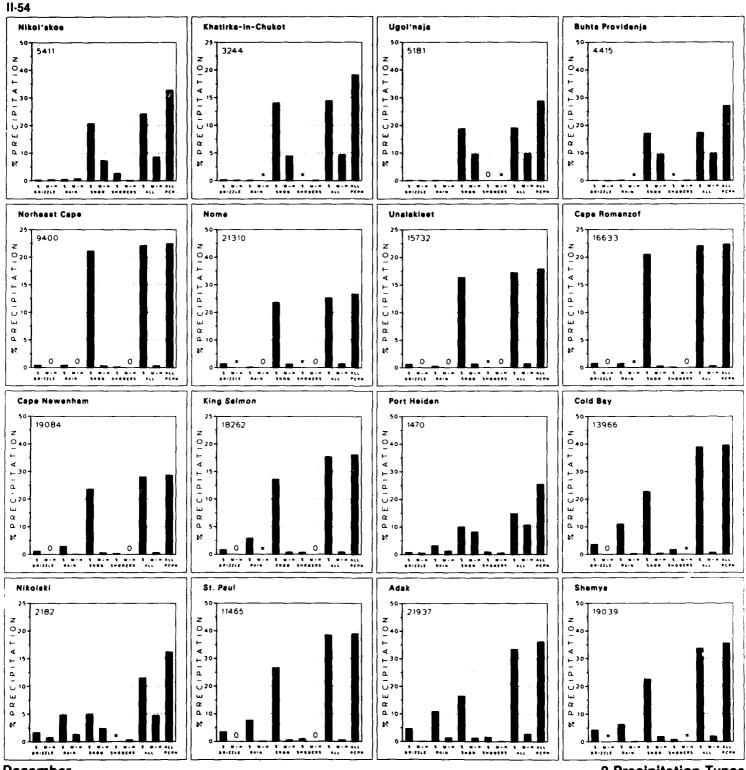
2 Wind-Visibility-Cloudiness

October



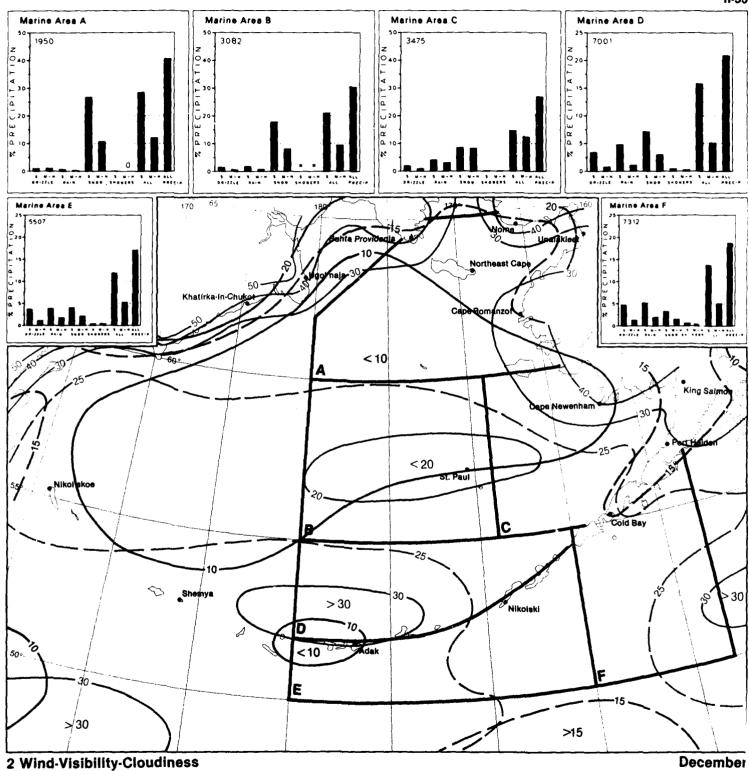
2 Precipitation Types





December

2 Precipitation Types



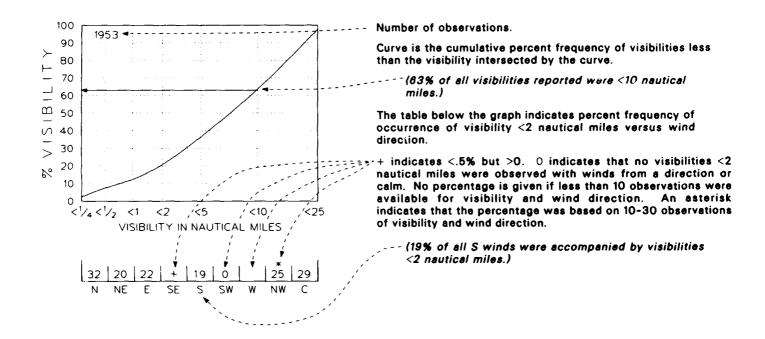
## Map 3. Ceiling/visibility (low range)

BLACK L!NE - Percent frequency of low cloud ceiling (LCC) <300 feet and/or visibility <1 nautical mile.

BLUE LINE - Percent frequency of LCC <600 feet and/or visibility <2 nautical miles.

Albers Equal-Area Conic Projection

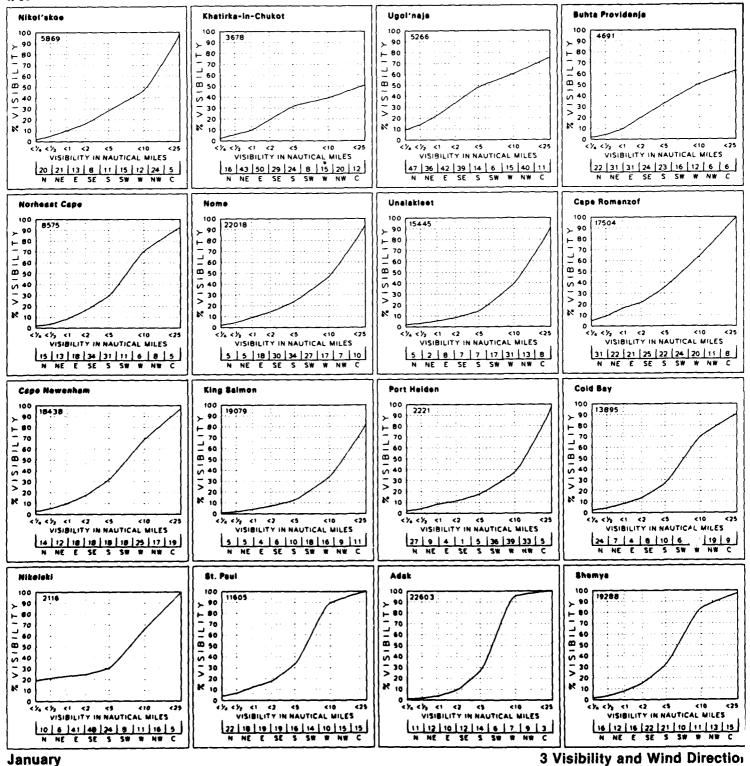
## Graphs: Visibility/wind direction

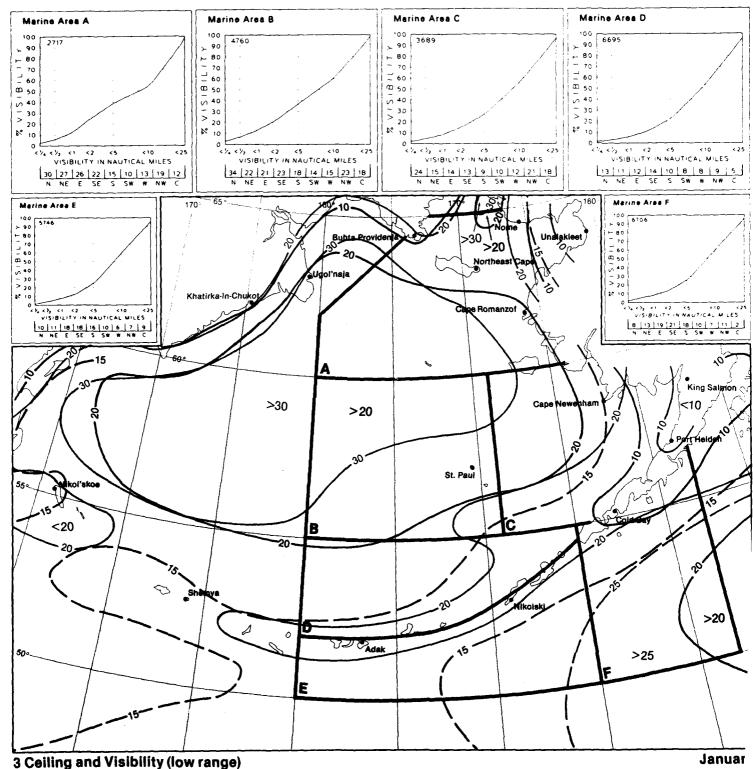


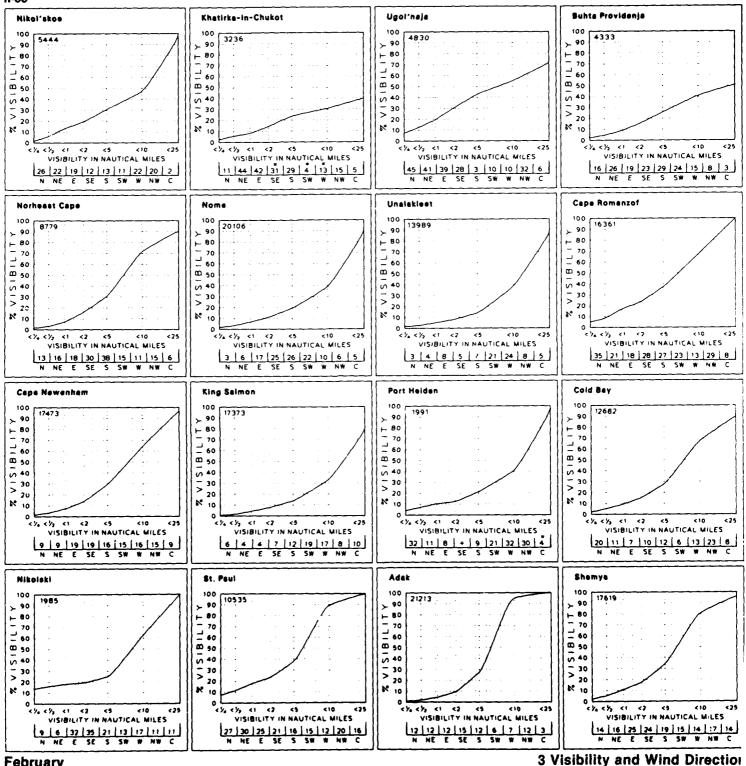
The percent frequency of visibilities equal to or greater than a given value can be obtained from the graph by subtracting the cumulative percent frequency of that value from 100%. Refer to the text in Set 5 for descriptive information on visibility.

Aircraft-type ceilings are not available from marine observations. The ceilings are estimated from the height of the lowest cloud when low clouds (heights of less than 8,000 feet) cover more than half the sky. When the sky is totally obscured by snow, rain, fog, or other phenomena, the total obscuration is considered a ceiling with a height of zero. Refer to the texts in Sets 4 and 6 for additional information on clouds.

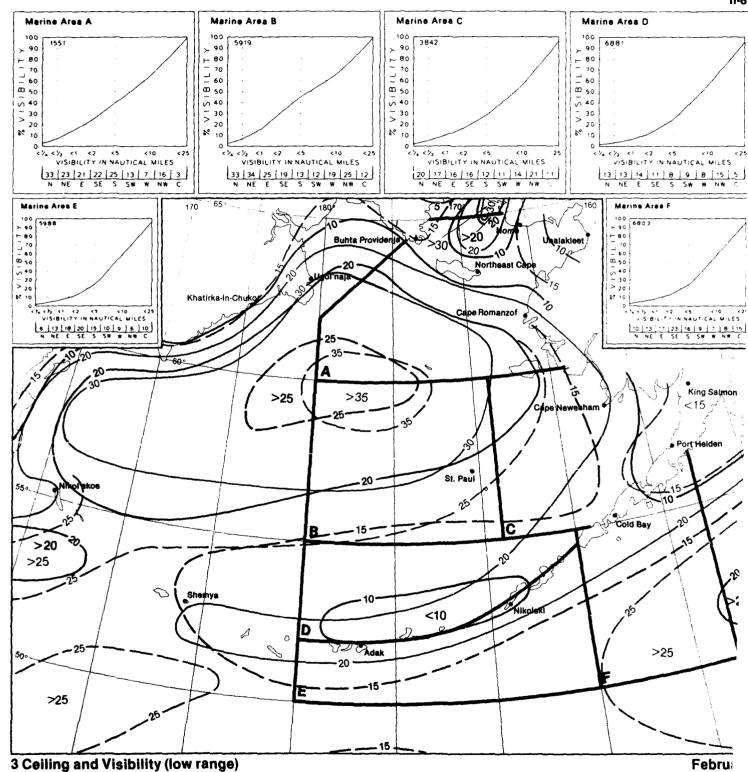
3 Legend Legend 3

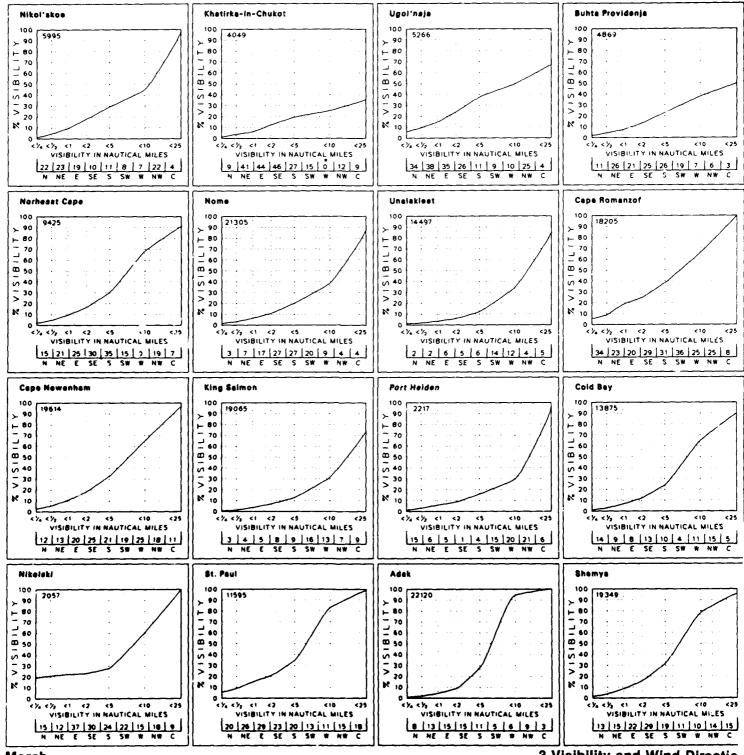






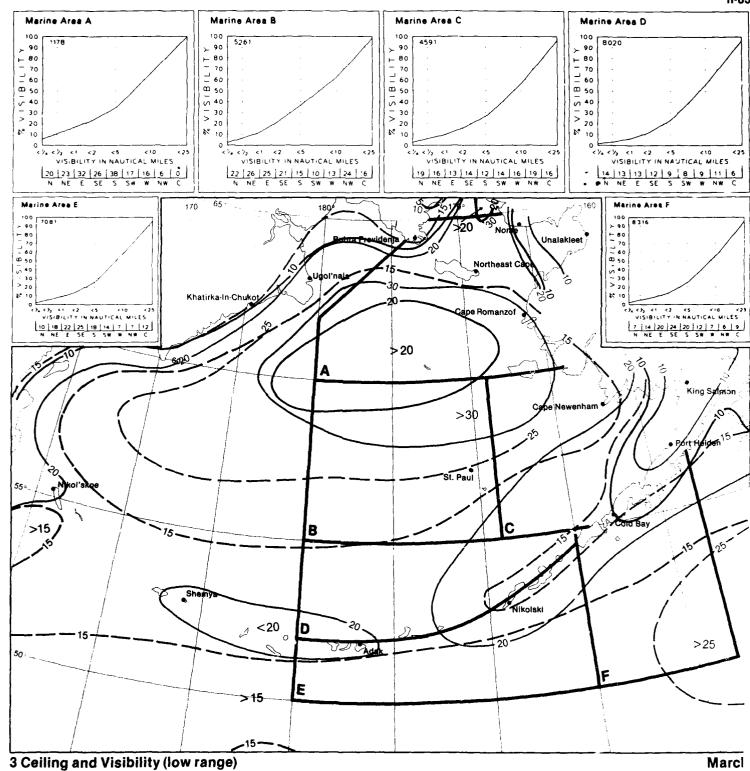
**February** 

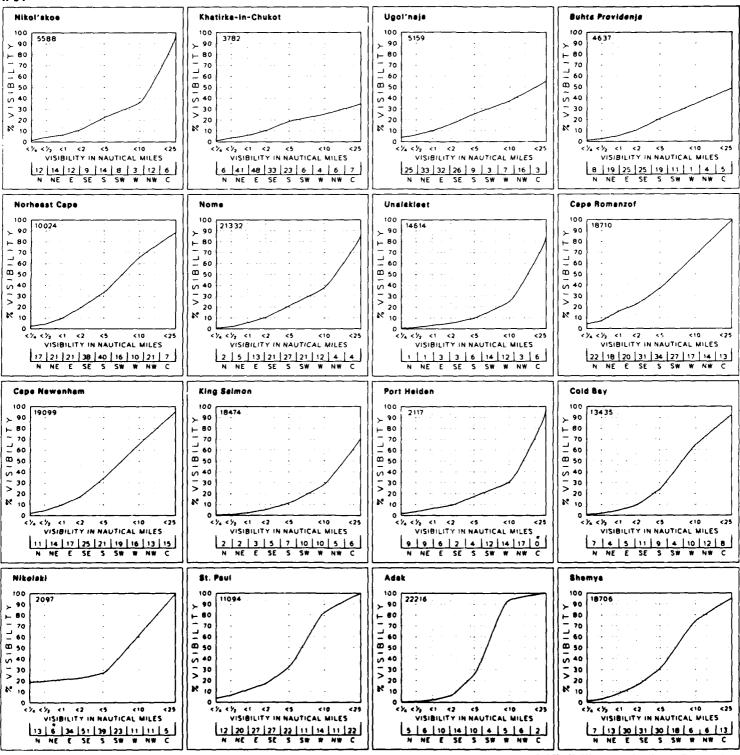




March

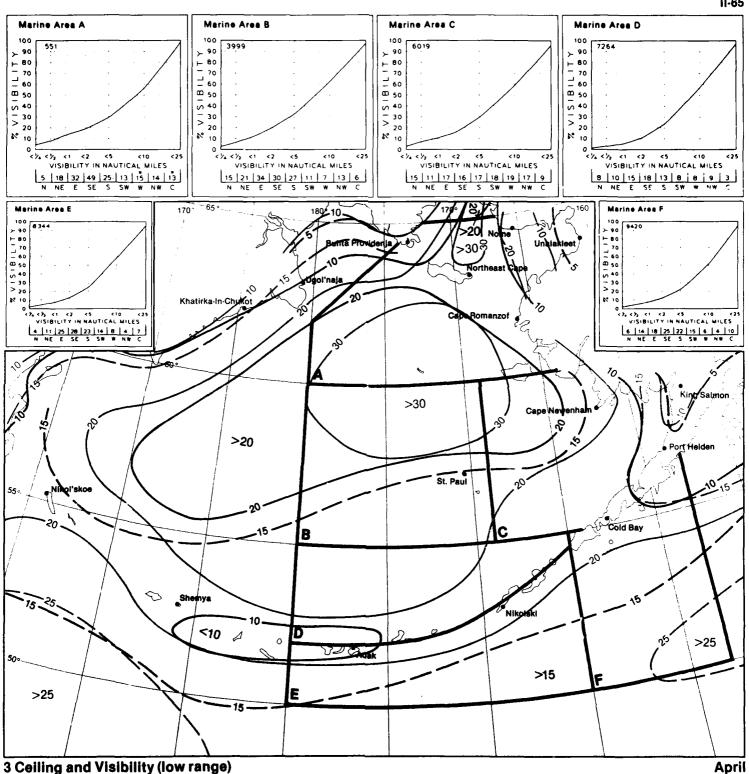
3 Visibility and Wind Directio

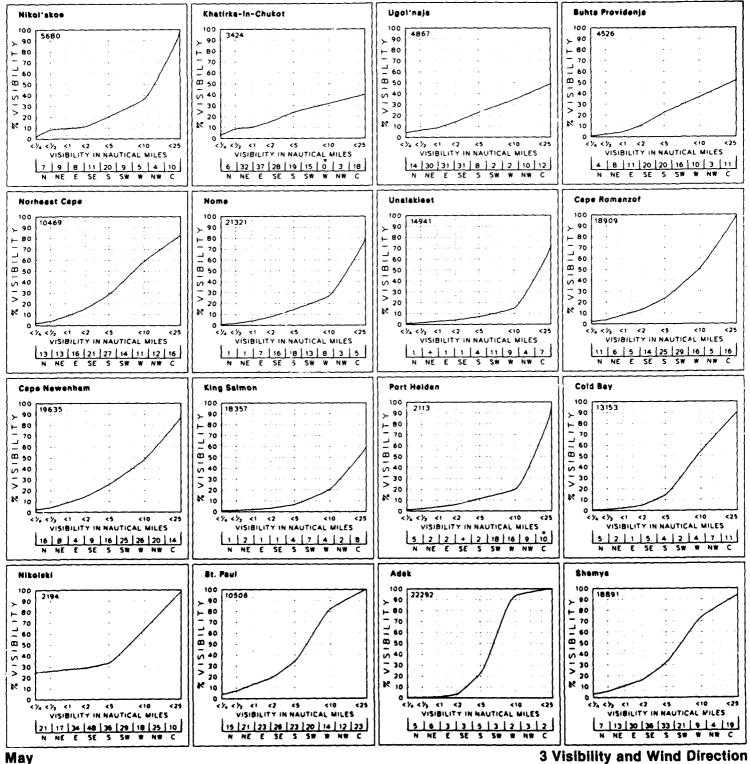




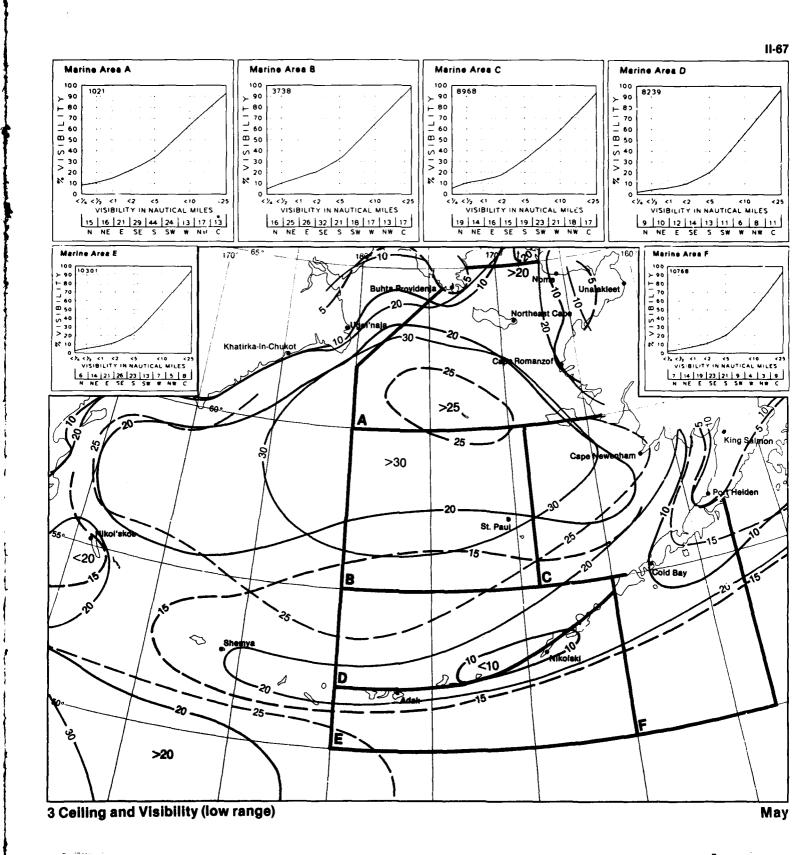
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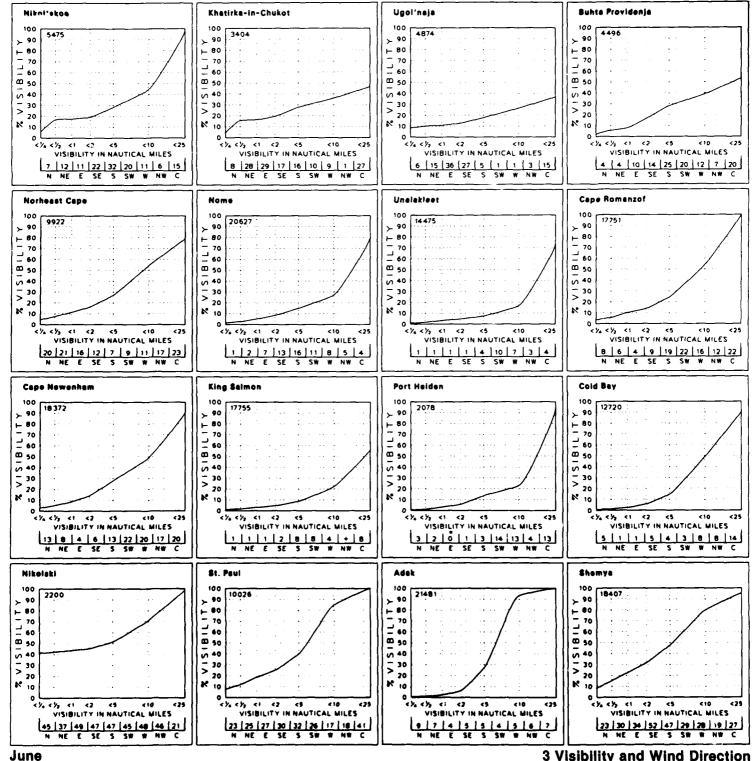
3 Visibility and Wind Direction



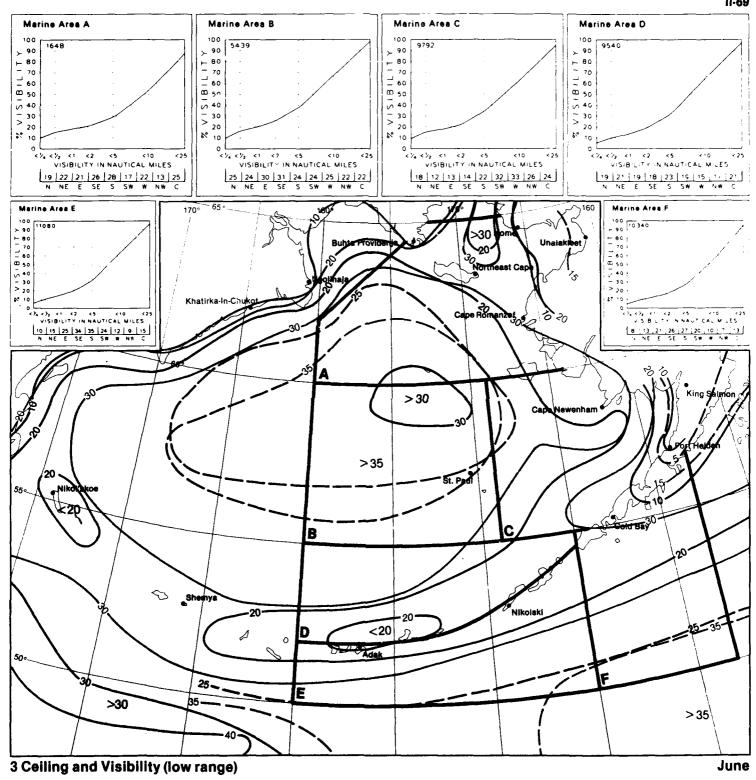


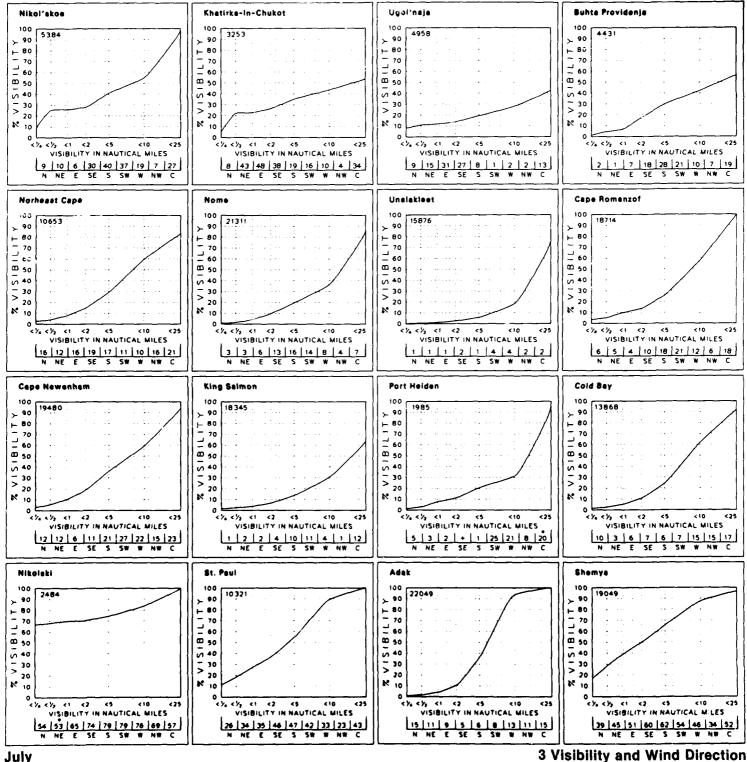
May



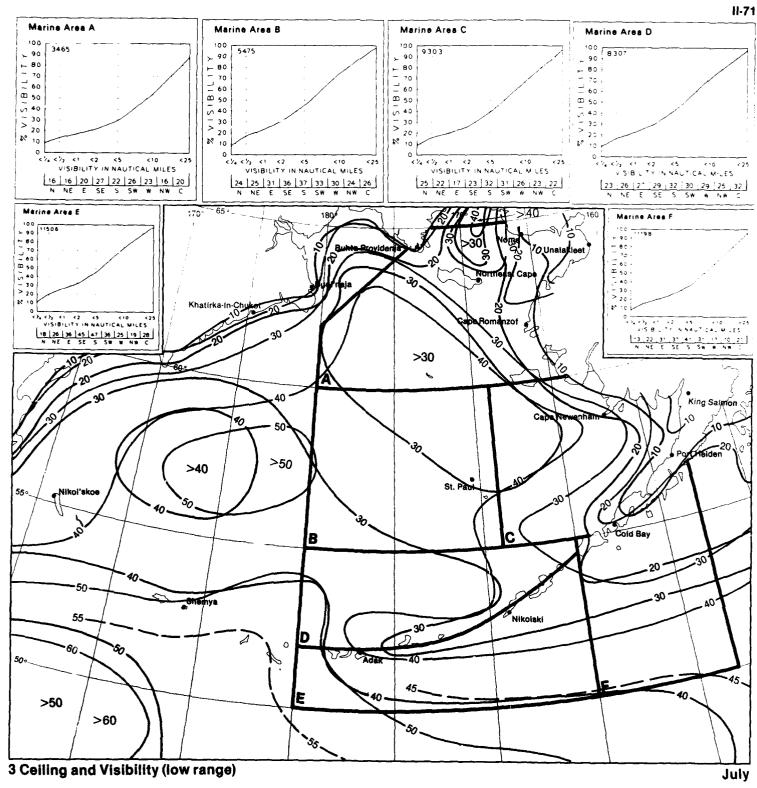


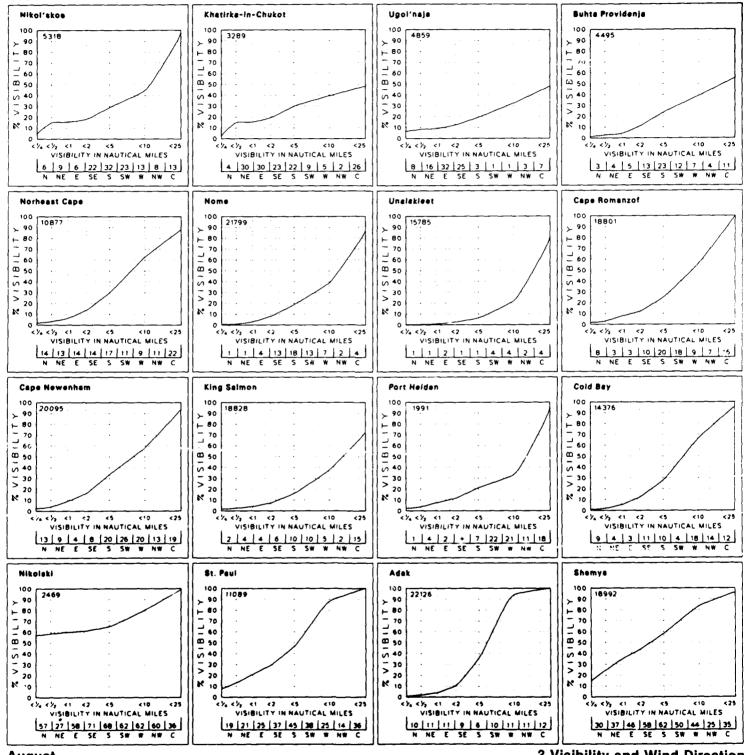
3 Visibility and Wind Direction





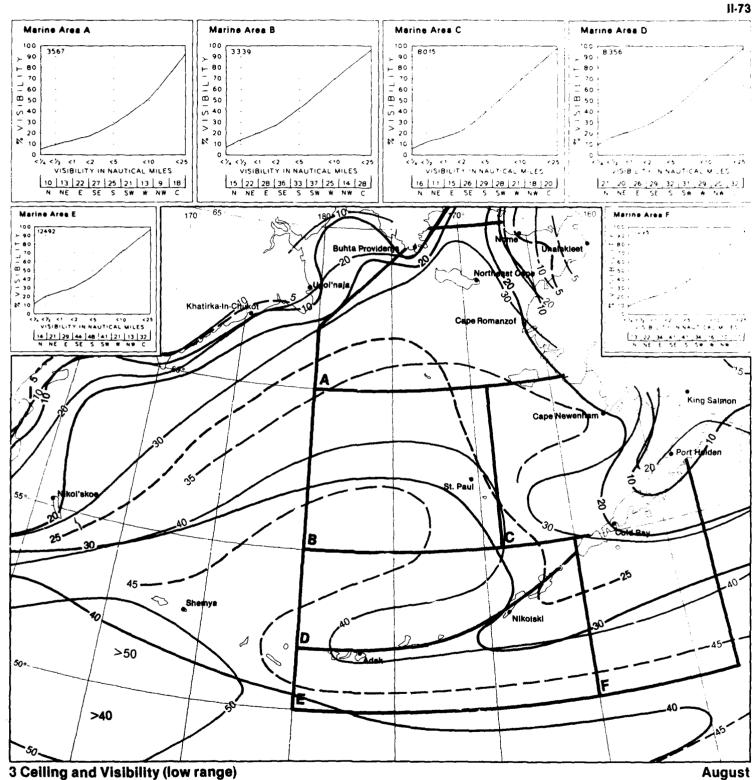
July

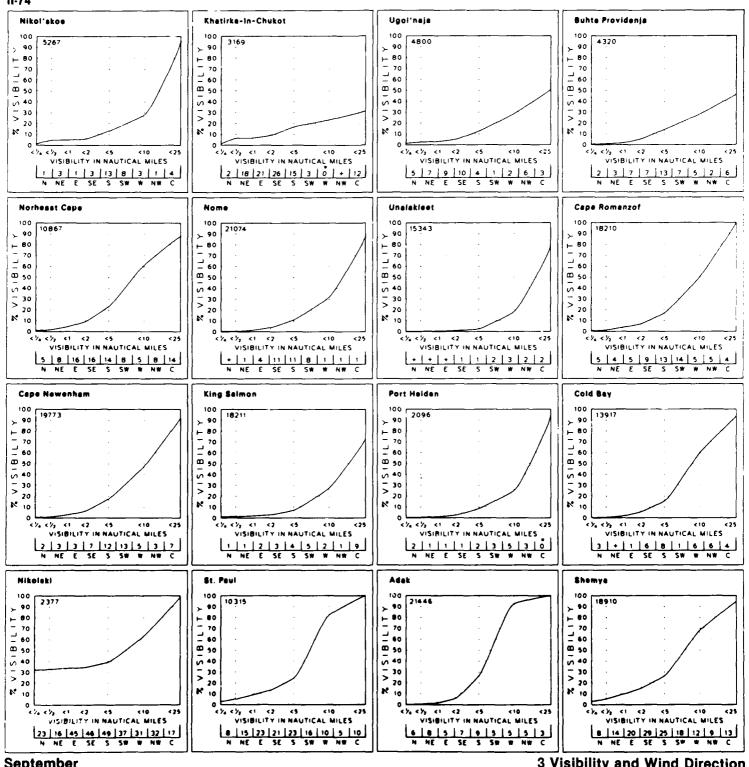




August

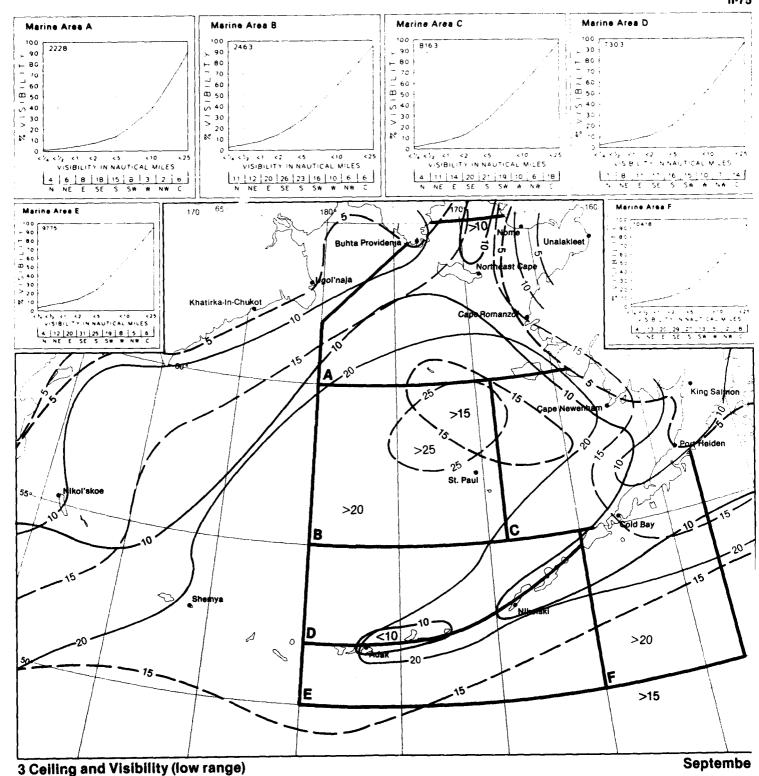
3 Visibility and Wind Direction

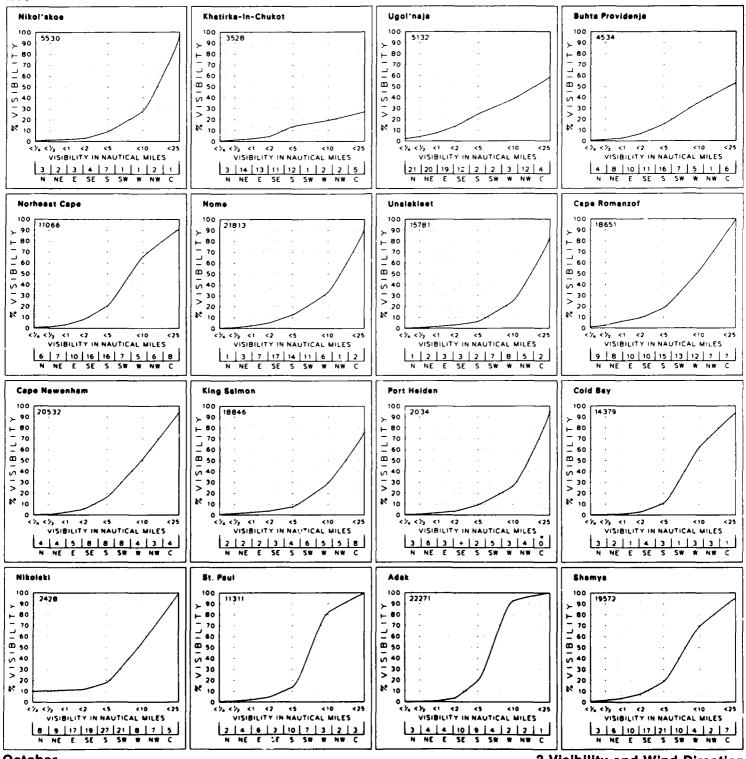




September

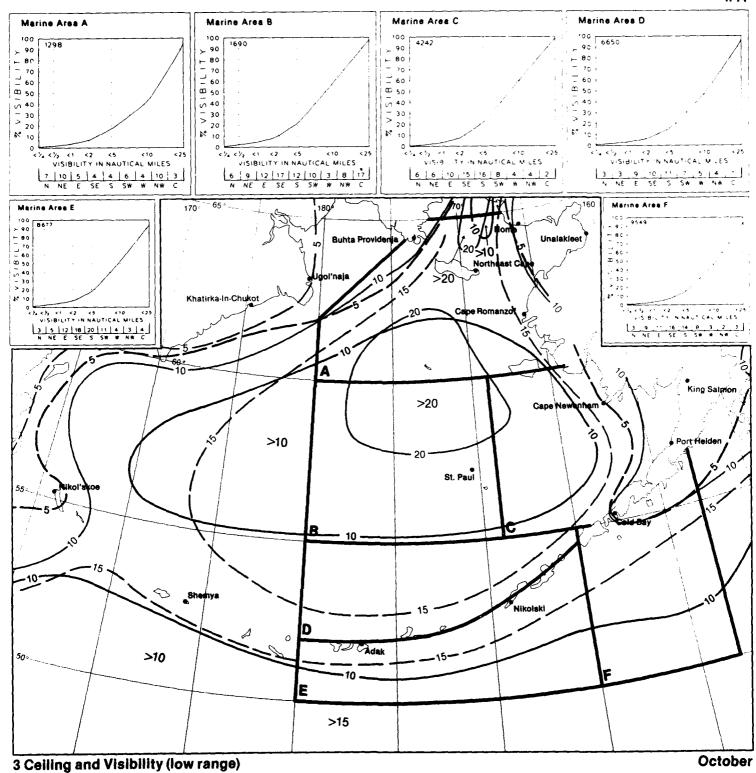
3 Visibility and Wind Direction

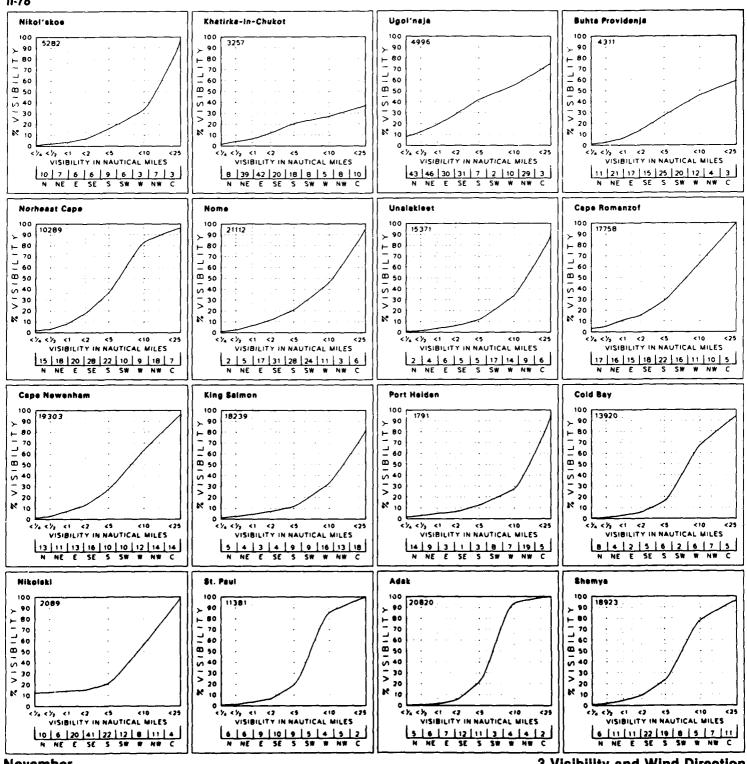




**October** 

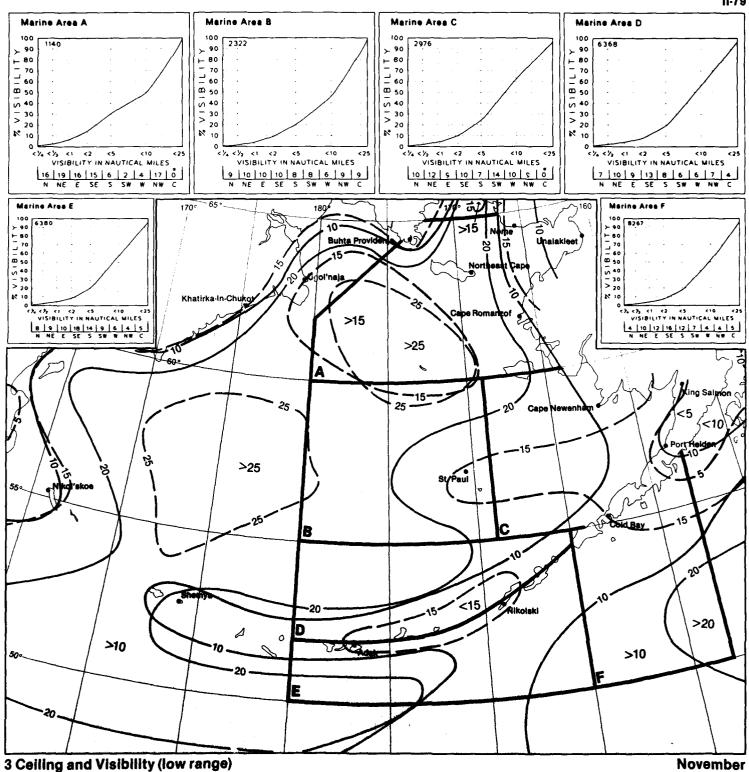
3 Visibility and Wind Direction

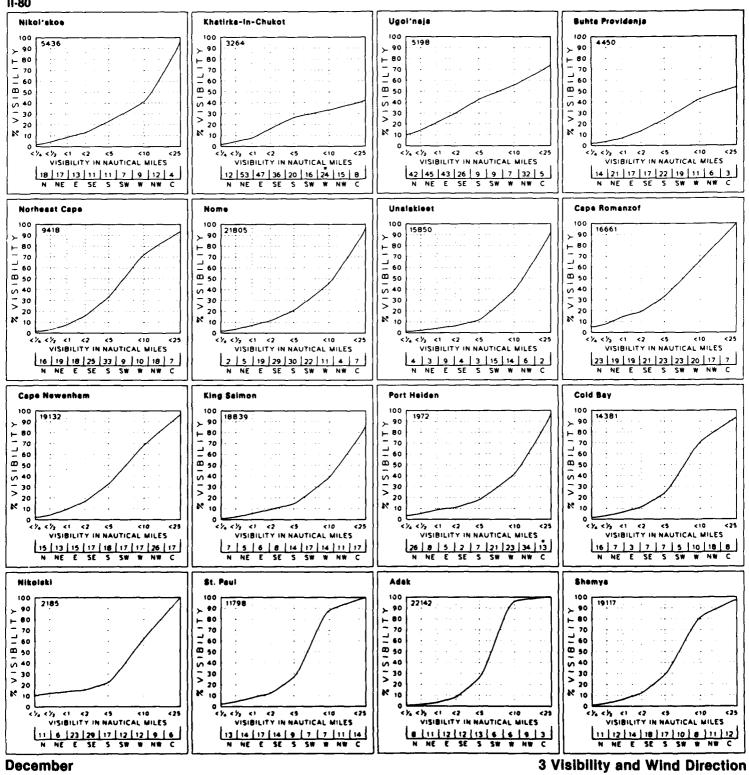




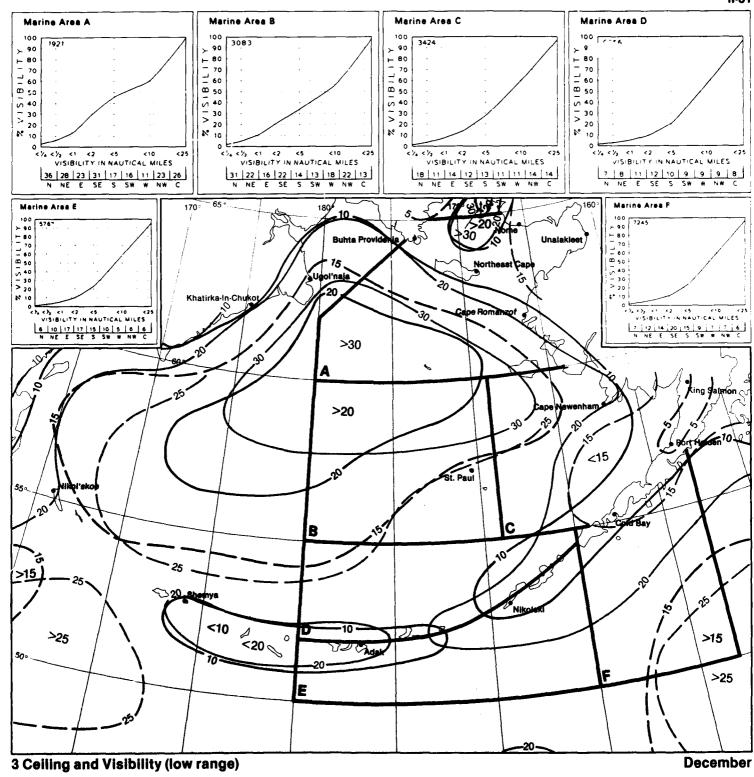
November

3 Visibility and Wind Direction





December



# Map 4. Ceiling/visibility (mid range)

BLACK LINE - Percent frequency of low cloud ceiling (LCC) <1000 feet and/or visibility <5 nautical miles.

BLUE LINE - Percent frequency of LCC <8000 feet and/or visibility <10 nautical miles.

Albers Equal—Area Conic Projection

# Graphs: Low cloud ceiling/visibility

LOW		Į VI	SIBIL	JTY	(MM)	)	1659	₹.
CLOU			1/2-	l 1 –	2-	5-	}	1
(10 <sup>2</sup> F)		<1/2	<1	<2	<5	<10	≥10	1
N	C	+	_0	+	2	7	11	
50<8	0	0	0	+	+	1	1	
35<5	0	+	+	+	1	2	3	
20<3	5	1	1	2	3	8	11	
10<2	0	1	3	3	4	8	. 8	
6<1	0	+	+	1	2	1	1	
3<	6	+	+	+	1	+	+	
1.5<	3	0	0	+	0	0	+	
0<1.	5	5	2	2	1	2	+.	

Percent frequency of simultaneous occurrence of specified low cloud ceiling (hundreds of feet) and visibility (nautical miles).

Number of observations.

Low cloud ceiling heights are estimated from the height of low clouds (h) when low cloud amount  $(N_h)$  is  $\geq 5/8$ .

Obscurations are included under ceiling "0<1.5".

"NC" (no ceiling) includes bases of clouds  $\ge$ 8000 feet or N<sub>h</sub> <5/8.

(8% of all observations reported ceiling  $\geq$ 1000 feet but <2000 feet simultaneously with visibility  $\geq$ 5 but <10 nautical miles).

+ indicates <.5% but >0.

Cloud classification is based upon the cloud appearance and, when possible, the formation process. In estimating the height of the lowest cloud base (h), the observer first determines the type of cloud; and, based on the normal height range for that cloud type, determines the height. Heights are generally higher in the tropics and lower at high latitudes. Similarly, clouds will generally be higher in summer and lower in winter. The appearance of the cloud, such as motion visible in the cloud base and the size of the cloud elements, gives some indication as to how much it is higher or lower than the average. After the observer estimates the height of the base of the lowest cloud in sight, he selects and records the appropriate code (see height table and LCC column in graph). Refer to the texts in Sets 3 and 6 for additional information on clouds.

#### HEIGHT (h) ABOVE THE SEA OF THE BASE OF THE LOWEST CLOUD SEEN (WMO Code, 1982)

If sky is clear or has only Cirrus-type clouds, code h as 9.

Code		
figs.	Height in meters	Height in feet
Õ	0 to 49	100 or less
1	50 to 99	200 or 300
2	100 to 199	400 to 600
3	200 to 299	700 to 900
4	300 to 599	1000 to 1900
5	600 to 999	2000 to 3200
6	1000 to 1499	3300 to 4900
7	1500 to 1999	5000 to 6500
8	2000 to 2499	6600 to 8200
9	2500 or more, or no clouds	8300 or more, or no clouds
I	Sky obscured by fog or snow	

#### Nikoi'skos

CLOUD CLOUD | 1/2 - 1 - 2 - 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 - 1 | 2/2 | 5 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/2 | 2/

#### Khetirke-li,-Chukot

LO® VISIBILITY (NM) 3669

CEILING (10° FT) < 1/2 - 1 - 2 - 5 - (10° E10)

NC 1 1 2 3 4 50

50<80 0 0 + + + + + + 

35<50 + + + + + + + 3

20<35 1 1 3 4 2 5

10<20 2 1 3 3 2 2

6<10 1 + 1 1 + + 

3<6 + + + + + + + + 

1.5<3 0 0 + + 0 + 

0<1.5 1 0 0 0 0 0

#### Ugol'naja

COW CLOUD CEILING (10° FT) (10

#### Buhta Providenja

#### Norheast Cape

	ا					
LOW CLOUD CEILING (10° FT)	1	1BIL 1/2 - <1	Y  -   <2	ı İ	5 -	498 ≥10
NC	1	+	1	3	20	35
50<80	0	0	0	0	+	1
35<50	0	0	0	+	+	+
20<35	+	+	+		5	1
10<20	+	1	2	5	6	1
6<10	0	1	1	2	7	+
3<6	+	+	+	+	+	+
1,5<3	+	Ō	+	0	0	0
0<1.5	5	3	1	+	0	0

#### Nome

LOW	VIS	IBIL	ITY	(NV	1) 16	5011
CEILING	.,.	1/2-	1-	2-	5 -	
(10° FT)	< 1/2	<1	<2	\ <u>\$</u>	10	≥10 45
N.C.					10	43
50<80	+	+	+	+	_1	_ 2
35<50	+	+	+	+	2	
20<35	+	+	1	2	4	2
10<20	+	1	1	3	4	2
6<10	+	1	-	1	2	+
3<6	+	+	1	1	1	+
1.5<3	+	+	+	+	+	+
0<1.5	3	3	1	+	+	0

#### Unalakleet

LOW	VIS	BIL	TT.	(NN	1) 2	659
CLOUD		1/2 -	1 -	2-	5-	
(10° FT)	< 1/2	[ 1	<2	<5	<10	≥10
NC	+	+	+	1	23	32
50<80	+	+	+	+	3	3
35<50	0	0	0	+	4	3
20<35	+	+	+	1	6	6
10<20	0	+	+	2	5	3
6<10	+	+	+	1	1	+
3<6	+	+	+	+	+	+
1.5<3	0	0	O	0	0	0
0<1.5	2	1	1	1	0	0

### Cape Romanzof

LOW	VIS	BIL	IT Y	(NN	1) 4	1150
CLOUD CEILING (10 <sup>7</sup> FT)	< 1/2	1/2 - <1	1 - < 2	2 - <5	5 - < 10	≥10
NC	3	2	1	6	31	14
50<80	0	O	+	+	1	1
35<50	0	0	+	+	1	+
20<35	+	1	1	1	5	i
10<20	1	1	1	3	4	+
6<10	+	2	1	3	2	+
3<6	+	+	1	+	+	0
1.5<3	+	0	0	0	0	0
0<1.5	6	3	+	+	0	0

#### Cape Newenham

LOW	1 1/10	iBiL	ıτ∨	/NIK	4) 7	3956
CLOUD	V13	l. i	i.	1 .		1
(10° FT)	<1/2	/ <sub>2</sub> - <1	1-	2 – < 5	5-	≥10
NC NC	1	1	1	1	18	24
50<80	+	0	+	+	1	-1
35<50	0	+	Ó	+	1	+
20<35	+	+	+	1.	3	1
10<20	+	1	1	4	8	3
6<10	1	1	2	4	7	2
3<6	+	+	1		2	+
1.5<3	0	0	+	0	0	0
0<1.5	5	2	1	1	+	O

### King Salmon

LO#	lvis	IRII	ΙΤΥ	(NM	1) 16	185
CLOUD CEILING (102 FT)	< 1/2	ے درا ا >	1-	2- <5	5~	≥10
NC	+	+	+	1	10	50
50<80	0	+	+	+	_1	4
35<50	+	0	+	+	2	3
20<35	+	+	+	1	4	4
10<20	+	+	+	1	3	2
6<10	+	+	+	1	2	1
3<6	+	+	+	1	1	+
1.5<3	+	+	+	+	+	+
0<1.5	1	1	1	1	+	+

### Port Heiden

LOW	VIS	IBIL	IΤΥ	(NN	1)	123
CLOUD		/ <sub>2</sub> - <1	1-	2~ <5	5-   <10	≥10
(10° FT)	< 1/2	_				
NC.	0	0		0	9	35
50<80	0	0	0	0	0	6
35<50	0	0	0	0	0	3
20<35	0	0	0	1	0	10
10<20	0	1	O	1	10	10
6<10	0	0	0	1	6	0
3<6	0	0	1	0	0	0
1.5<3	0	0	0	0	0	0
0<1.5	5	2	ō	1	0	0

### Cold Bay

10#	VIS	SIBIL	IT Y	(NN	/) 1 <sup>1</sup>	1814
CLOUD CEILING		1/2-	1 -	2 –	5 -	Ì
(10° FT)	< 1/2	< 1	<2	< 5	< 10	₹10
NC	+	+	+	1	11	20
50<80	+	+	+	+	+	1
35<50	+	+	+	+	2	1
20<35	1	1	1	2	10	5
10<20	1	1	1	4	11	4
6<10	+	1	1	4	5	1
3<6	+	+	1	2	2	+
1.5<3	+	+	+	+	+	0
0<1.5	3	2	1	+	+	0

### Nikoleki

No Data Available

#### St. Paul

LOW	VIS	IBIL	YTI.	(NN	1) 9	069
CEILING	ĺ	1/2-	) -	2 -	5 –	1
(10° FT)	< 1/2	<1	<2	<5	<10	≥10
NC	+	+	1	1	18	7
50 <b0< td=""><td>0</td><td>+</td><td>0</td><td>+</td><td>+</td><td>+</td></b0<>	0	+	0	+	+	+
35<50	0	+	+	+	1	+
20<35	+	+	T	2	10	3
10<20	1	1	1	5	19	2
6<10	1	1	1	3	4	+
3<6	1	1	1	2	_1	+
1.5<3	+	+	+	+	+	0
0<1.5	4	2	1	+	+	0

# Adak

LOW	VIS	iBIL	ITY	(NN	1) 13	3760
CLOUD CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1- <2	2 - <5.	5 - <10	≥10
NC	+	+	+	+	16	3
50<80	+	0	0	+	1	+
35<50	0	Ô	+	+	6	1
20<35	+	+	T +	3	25	1
10<20	+	+	1	8	17	+
6<10	+	+	1	4	2	+
3<6	+	+	- 1	1	1	0
1.5<3	+	+	+	+	+	Ō
0<1.5	_ 2	2	2	1	+	0

## Shemya

LOW	VIS	BIL	ITY	(NN	1) 10	000
CLOUD CEILING (10° FT)	< 1/2	½- <1	1-	⊋- <5	5 - <10	≥10
NC	+	+	+	+	13	10
50<80	0	0	0	+	+	+
35<50	0	+	+	+	3	1
20<35	+	+	+	2	16	6
10<20	+	1	2	5	12	2
6<10	+	1	2	4	4	+
3<6	+	1	2	2	1	+
1.5<3	+	+	+	+	0	0
0<1.5	3	2	1	+	+	0

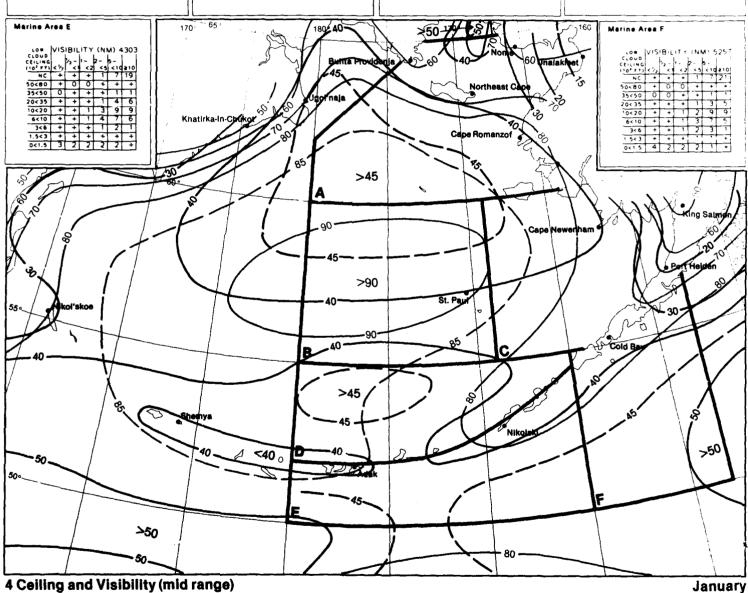
January

Marine Area A								
CLOUD	VIS	181L	,17 Y 1.	(NA	4) 2  _	?35 		
CEILING (10 <sup>3</sup> FT)	< 1/2	13-	<2	<5	<10	≥10		
NC	+	+	1	1	3	14		
50<80	+	0	+	+	1	1		
35<50	+	+	+	+	1	1		
20<35	7	1	2	4	3	28		
10<20	1	3	7	6	4	3		
6<10	+	+	1	1	T	+		
3<6	+	+	+	+	+	+		
1.5<3	+	+	+	+	Ō,	0		
0<1.5	4	2	2	2	1	+		

Marine Area B								
LOW	) VIS	BIL	YTI.	(NN	1) 4	304		
CLOUD		i		L.		i 1		
CEILING	l . '	/ <sub>2</sub> -	1 - 1		5 -			
(10° FT)	< 1/2	<1	<2	< 5	<10	≥10		
NC	+	+	+	1	4	13		
50<80	+	0	+	+	1	1		
35<50	+	+	+	+	_1	2		
20<35	1	1	2	4	7	20		
10<20	1	2	3	4	5	4		
6<10	+	+	1	2	2	1		
3<6	+	+	+	+	1	+		
1.5<3	+	+	+	+	+	+		
0<1.5	4	2	2	2	1	+		

Marine Area C								
<b>L</b> O₩	lvis	iBiL	ΙΤΥ	(NN	1) 3	3073		
CEILING (10 <sup>2</sup> FT)	< 1/2	1/2 ~ 51	1-	2 - < 5	5-	≥10		
NC	+	+	+	1	6	21		
50<80	0	0	+	+	1	2		
35<50	+	+	+	1	2	3		
20<35	+	+	Ĩ	2	5	11		
10<20	1	1	2	4	9	7		
6<10	+	+	1	5	4	1		
3<6	+	+	+	1	+	+		
1.5<3	+	+	0	+	Ö	+		
0<1.5	3	5	3	3	Ī	+		

arine Ai	ea l	0				
LOW	VIS	<b>IBIL</b>	IT Y	(NN	() 6	470
CFOOD		, ,			_	1 1
(10° FT)	< 1/2	-2- <1	< 2	<5	5- <10	≥10
NC	+	+	+	1	6	19
50<80	+	+	0	+	1	+
35<50	+	0	+	+		1
20<35	+	+	+	1	4	7
10<20	+	+	1	2	7	10
6<10	+	1	1	3	7	7
3<6	+	+	1	1	2	2
1.5<3	+	+	+	+	1	+
0<1.5	2	1	2	2	2	+



## Nikol'akoe

LOW CLOUD CEILING (10° FT) (NM) 54 19 (10° FT) 
#### Khatirka-In-Chukot

| VISIBILITY (NM) | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 3233 | 323

#### Ugol'naja

#### Buhte Providenja

#### Norheast Cape

	Luc	iBiL	itu	(NI)		3698
CFOOD FO#			,,,,,, 		") _  5-	1
(10° FT)	< 1/2	γ <sub>2</sub> - <1	<2	<5		≥10
NC	+	+	1	2	18	38
50<80	0	0	+	+	+	1
35<50	0	0	+	+	1	+
20<35	+	+	+	1	3	1
10<20	+	1	2	5	7	2
6<10	+	1	1	2	2	+
3<6	0	+	+	+	+	0
1.5<3	0	0	0	0	+	Ō
0<1.5	4	2	1	+	Ö.	0

#### Nome

LOW	VIS	BIL	JT Y	(NN	1) 14	734
CLOUD CEILING (10° FT)	< 1/2	- ولا 1>	1- <2	2 - < 5	5 - <10	≩10
NC	+	+	+	1	9	52
50<80	+	+	+	+	1	2
35<50	+	+	+	+	1	2
20<35	+	+	1	2	3	2
10<20	+	1	1	3	4	2
6<10	+	+	1	2	1	+
3<6	+	+	1	1	+	+
1.5<3	+	+	+	+	+	0
0<1.5	2	2	1	+	+	0

## Unalakieet

			.+			
CLOUD CEILING (10° FT)	< ½	B L   /2 -  <1	.11 Y 1-   <2	(NN 2- <5	5 –	192 ≥10
NC	+	+	+	1	20	43
50<80	0	0	+	+	2	3
35<50	+	+	+	+	2	3
20<35	+	+	+	1	4	5
10<20	+	+	+	1	3	3
6<10	0	+	+	1	1	+
3<6	0	+	+	+	+	+
1.5<3	0	0	0	+	0	+
0<1.5	2	2	1	+	0	_ 0

## Cape Romanzof

LOW	VIS	i <b>B</b> iL	IT Y	(NA	4) 3	8883
CLOUD CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1 - < 2	-	5 - <10	<b>≩</b> 10
NC	2	2	2	4	31	15
50<80	+	1	+	+	1	1
35<50	0	+	0	+	,	+
20<35	1	1	+	1	7	1
10<20	1	1	1	4	5	
6<10	+	2	1	$\lceil 7 \rceil$	2	+
3<6	+	+	+	+	+	
1.5<3	0	Ó	+	Ó	0	0
0<1.5	5	3	+	+	О	0

#### Cape Newenham

LOW	VIS	iBiL	ΙΤΥ	(NN	1) 3	84 .
CLOUD CEILING (10 <sup>2</sup> FT)	< 1/2	½- <1	1-	2- <5	5-   <10	≥10
NC	+	+	1	1	16	24
50<80	0	0	+	+	+	П
35<50	0	0	0	+	1	1
20<35	+	+	+	1	4	2
10<20	+	1	1	3	7	5
6<10	+	1	3	6	6	3
3<6	7	1	1	2	1	+
1.5<3	0	+	+	+	0	0
0<1.5	3	2	1	1	+	+

#### King Salmon

	1		ıтv	/A14		071
LOW	) V 12	PIRIT	II Y	(NN	1) 14	871
CLOOD		,	l_	_	_	
CEILING		/2 -	1-	- 1	5-	
(10° FT)	< 1/2	<1	<2	<5	<10	[≥10]
NC.	1	+	+	1	8	50
50<80	+	+	+	+	2	5
35<50	0	+	+	+	2	3
20<35	+	+	+	2	4	5
10<20	+	+	1	1	3	2
6<10	+	+	+	1	1	1
3<6	+	+	+	1	1	+
1.5<3	+	+	+	+	+	0
0<1.5	1	1	1	1	+	0

### Port Heiden

LOW	VIS	IBIL	ΙΤΥ	(NN	1)	109
CLOUD CEILING (10° FT)	< 1/2	/ <sub>フ</sub> - <1	1- <2	2 - <5	5 - <10	≥10
NC	T	1	0	1	11	38
50<80	Ō	0	0	0	0	2
35<50	0	0	٥	0	0	3
20<35	0	0	Ô	2	3	14
10<20	0	1	0	2	6	6
6<10	0	0	Γ	2	2	0
3<6	0	0	Ó	0	0	0
1.5<3	0	0	0	0	0	0
0<1.5	5	1	1	1	0	0

# Cold Bay

LO#	VIS	iBiL	iΤΥ	(NN	1) 1(	760
CEILING		Y2-	1-	2 -	5 -	
(10° FT)	< 1/2	<1 +	<5	< 5	3	≥10 20
50<80	1	0	-			20
35<50	1	-	+	+	1	
20<35	+	1	i i	3	8	5
10<20	1	1	1	4	11	5
6<10	+	+	1	2	5	1
3<6	+	1	1	2	2	+
1,5<3	+	+	+	+	+	+
0<1.5	3	_2	1	+	+	0

### Nikolski

No Data Available

### St. Paul

LOW	VIS	BIL	IT Y	(NN	1) 8	3596
CEILING	ĺ	1/2 -	1-	2 –	5-	1 1
(10 <sup>2</sup> FT)	<1/2	<1	<2	<5	<10	≥10
NC	1	+	1	1	18	7
50 <b0< td=""><td>+</td><td>0</td><td>+</td><td>+</td><td>+</td><td>+</td></b0<>	+	0	+	+	+	+
35<50	Ö	Ó	+	+	1	+
20<35	1	+	+	2	7	2
10<20	3	2	2	7	18	2
6<10	T	1	1	2	5	+
3<6	1	1	1	1	1	+
1,5<3	+	+	+	+	+	0
0<1.5	5	T	+	+	Ó	0

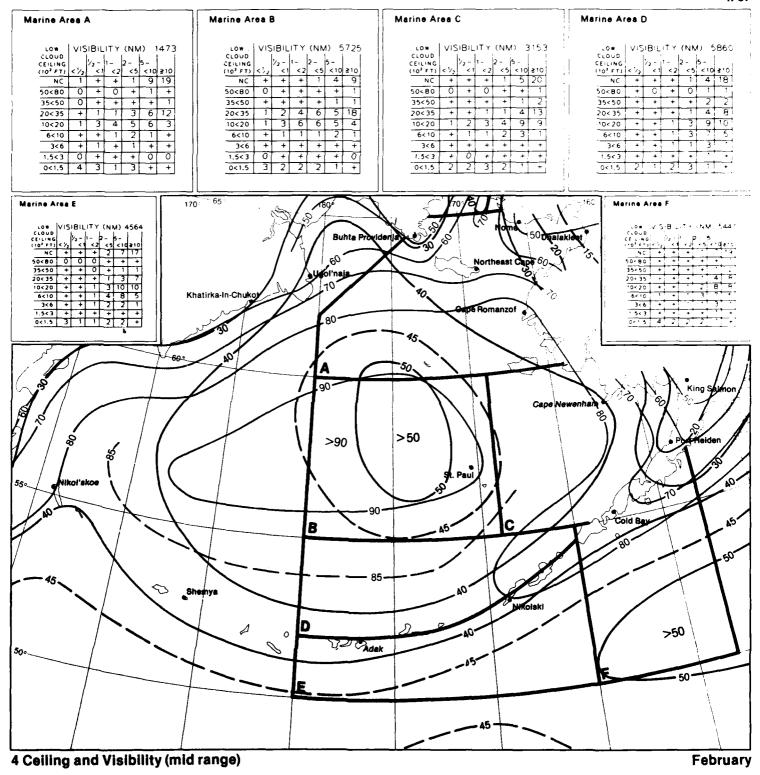
#### . . . .

LOW	VIS	BIL	ΙΤΥ	(NN	1) 12	622
CEILING (10° FT)	< 1/2	ے د <sup>را</sup> 1 >	1-	2- <5	5-	≩10
NC NC	+	+	+	+	16	3
50<80	0	0	ō	+	1	+
35<50	0	+	+	+	5	1
20<35	+	+	7	3	27	2
10<20	+	+	1	9	16	+
6<10	+	+	1	3	2	+
3<6	+	+	+	+	+	0
1.5<3	0	+	+	+	0	0
0<1.5	2	2	2	1	+	+

### Shemya

LOW	VIS	VISIBILITY (NM) 9339						
CEILING		/ <sub>2</sub> -	1-	2 -	5-			
(102 FT)	< 1/2	< 1	<2	< 5	<10	≥10		
NC	+	+	+	+	10			
50<80	0	+	0	+	+	+		
35<50	+	0	+	+	2	[ 2]		
20<35	+	+		3	18	8		
10<20	1	2	2	6	12	2		
6<10	+	1	2	3	2	+		
3<6	+	1	1	1	+	+		
1.5<3	+	+	+	0	0	0		
0<1.5	4	2	1	+	+	+		

**February** 



#### Nikol'skos

COUNT CEILING (10° FT) (NM) 5966
CEILING (10° FT) (10° FT

#### Khatirka-In-Chukot

COUNT CLOUD (NO. ) 4054
CLOUD (CELLING (10° FT) 
### Ugol'neja

#### Buhta Providenja

#### Norheast Cape

LO:	VIS	iBiL	iT Y	(NN	4) 3	886?
CLOUD CEILING (10 FT)	<'/ <sub>2</sub>	½- <1	1-<2	2 - < 5	5 - < 10	<u>≩</u> 10
NC	1	1	1	3	17	33
50<8C	+	+	0	+	,	1
35<50	0	+	+	+	+	+
20<35	+	+	+	1	2	1
10<20	+	+	2	5	8	2
6<10	1	1	2	Ž	2	+
3<6	+	+	+	+	+	0
1.5<3	0	0	0	0	0	Ô
0<1.5	6	3	1	+	ા	0

#### Nome

LO#	VIS	i Bi L	iT r	(NA	1) 16	143
CLOUD CEILING (10° FT)	< > 2	'2 - <1	1 - 2	2 -	5 - < 10	≥10
NC	+	+	+	1	7	53
50<80	+	+	+	1	1	2
35<50	+	+	+	+	1	7
20<35	+	+	+	2	3	2
10<20	+	1	1	3	4	1
6<10	+	+	1	2	T	+
3<6	+	+	1	1	1	+
1.5<3	+	+	+	+	+	0
0<1.5	2	1	1	+	+	0

#### Haalaklaas

LO#	VIS	BIL	ITY.	(NN	1) 2	353
CLOUD		k	\	l <sub>2 -</sub>	5 -	1 1
CEILING	< 1/2	<1	<2	<5	-	≥10
NC	+	+	+	1	18	45
50 <b0< td=""><td>O</td><td>+</td><td>+</td><td>+</td><td>1</td><td>3</td></b0<>	O	+	+	+	1	3
35<50	0	0	0	+	7	3
20<35	+	+	+	1	3	6
10<20	+	+	+	2	3	3
6<10	0	+	+	1	2	1
3<6	+	+	+	+	+	+
1.5<3	0	0	0	+	+	+
0<1.5	1	1	1.	+	+	0

### Cape Romanzof

10#	VIS	BIL	IT Y	(NN	4) 4	356
CEILING		ν <sub>2</sub> -	1 -	2 -	5-	i
(10° FT)	< 1/2	-<1	< 2	< 5	<10	≥10
NC	1	3	2	4	26	16
50<80	+	+	+		2	+
35<50	0	+	+	+	1	+
20<35	1	1	+		5	7
10<20	1	1	1	3	3	+
6<10	1	3	2	3	2	+
3<6	+	1	1	1		0
1.5<3	Ō	Q	0	0	0	0
0<1.5	7	4	+	+	0	0

### Cape Newenham

CLQUD	V15	BIL	,11 Y	(NN	1) 4	327
CEILING	l	- ولا	1 _	2 -	5 -	. !
(10 FT)	< 1/2	< 1	<2	< 5	< 10	₹10
NC	+	+	+	7	15	24
50<80	0	+	0	+		1
35<50	0	0	0	0	+	1
20<35	+	+	+	+	2	2
10<20	+	+	1	3	8	4
6<10	+	2	2	4	7	2
3<6	+	1	1	2	2	+
1.5<3	+	0	+	+	+	Ō
0<1.5	8	2	2	1	+	0

# King Salmon

L <b>0</b> ₩	VIS	iBiL	IT Y	(NA	1) 16	7.74
CLOUD		½ - ∫	1 -	2	5 -	
(10° FT)	< 1/2	< 1	<2	< 5	<10	<u>≯</u> 10
NC	+	+	+	+	6	52]
50<80	0	+	+	+	1	4
35<50	+	0	+	+	2	3
20<35	+	+	+	1	4	5
10<20	+	+	1	2	4	3
6<10	+	+	î	1	2	1
3<6	+	+	+	1	1	+
1.5<3	+	+	+	+	+	+
0<1.5	1	1	1	+	+	+

#### Post Heider

ιO#	VIS	iBiL	iT 1	ONN	4)	134
CLOUD CEHLING (10° FT)	< '/2	½ ~ <1		2 - <5	5 - 510	≥10
NC	0	0	0	4	4	42
50<80	Õ	0	0	0	0	4
35<50	0	0	0	0	0	5
20<35	0	1	0	0	3	8
10<20	0	0	0	1	6	13
6<10	0	0	7	1	1	1
3<6	0	0	0	0	Ō	0
1.5<3	Ō	0	0	0	Ò	0
0<1.5	1	2	1	0	0	0

# Cold Bay

10#	VIS	JBIL	JT Y	(NN	40 °2	2337
CEILING (102 FT)	ر د ان	√2 - <1	  -   <2	2 - < 5	  5 -   < 10	≥10
NC	+	+	+	1	10	22
50 <b0< td=""><td>0</td><td>+</td><td>+</td><td>+</td><td>+</td><td></td></b0<>	0	+	+	+	+	
35<50	+	+	+	+	•	
20<35	+	+	,	2	8	6
10<20	+	1	2	4	• •	-5
6<10	+	1		3	5	7
3<6	+	+	,	2	2	+
1.5< 3	+	+	+	+	+	+
0<1.5	2	7		+	+	

### Nikoleki

No Data Available

#### St. Pau

€0#	VIS	1BIL	IT Y	(NA	1) 9	589	,
CLOUD :		1/2-	1-	2 -	5-		
(10° FT)	< 1/2	< 1	< 2	< 5	<10	≥10	
NC	+	+	+	1	18	11	
50<80	+	0	0	+	+	+	
35<50	+	+	0	+	1	1	
20<35	+	+	+	1	6	3	ı
10<20	2	2	2	5	15	3	ĺ
6<10	1	2	1	3	5	+	
3<6	1	1	1	2	2	+	ĺ
1.5<3	+	+	+	+	+	0	i
0<1.5	5	1	+	+	0	0	l

# Adak

10#	VIS	BIL	JΤΥ	(NN	1) 14	073
CLOUD CEILING (102 FT)	< 1/2	/ <sub>2</sub> -	1-	2 - <5	5-	≥10
					15	- 4
NC	0	+	+	1	13	4
50<80	0	0	0	+	+	+
35<50	0	Ó	+	+	5	1
20<35	+	+	+	3	28	1
10<20	+	+	1	9	17	+
6<10	+	+	1	4	3	+
3<6	+	+	<u> </u> + .	ιŌ	+	Ö
1.5<3	0	+	+	+	0	0
0<1.5	2	2	2	1	+	0

#### Shemya

LO#	VIS	BIL	ITY	(NN	0.10	525
CLOUD	.,.	٠, -	1 -	2 -	5 -	
(10° FT)	< /2	< 1	< 2	< 5	4 10	≥10
NC	+	+	+	+	10	10]
50<80	Ö	+	0	+	+	+
35<50	+	0	+	+	- 2	1
20<35	+	+	+	2	18	10
10<50	+	1	2	6	11	2
6<10	+	1	3	3	2	+
3<6	+	1	1	1	+	+
1.5<3	+	+	+	+	+	Ô
0<1.5	3	2	1	+	0	0

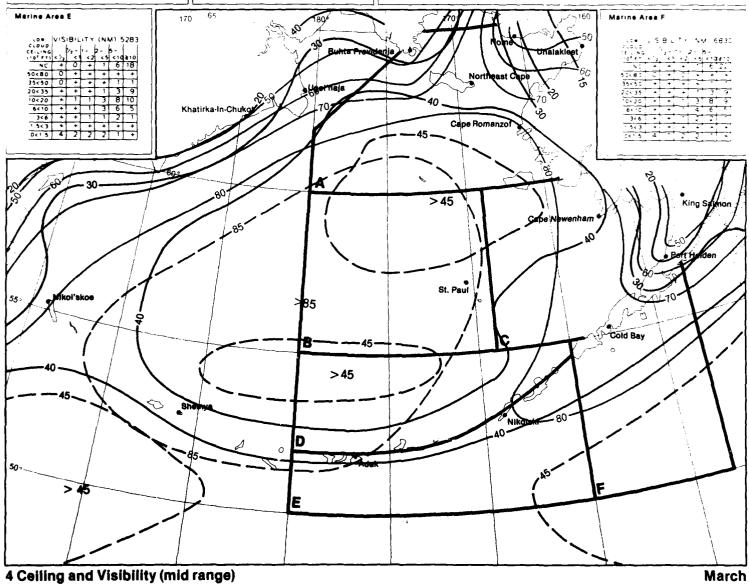
March

Marine Area A										
C.CO.D	\ v15	SIBIL	JTY I.	(NN	1) ·	1198				
CEILING (10 <sup>2</sup> FT)	< 1/2	/2 - <1	< 2	- <5	>- <10	≩10				
NC	+	+	1	2	20	24				
50<80	0	+	+	+	1	1				
35<50	0	+	0	+	+	1				
20<35	1	+	+	1	2	4				
10<20	1.	1	1	3	4	4				
6<10	2	1	2	3	3	1				
3<6	2	ī	1	1	1	+				
1.5<3	1	+	0	+	Ó	+				
0<1.5	6	2	1	1	+	0				

Marine Area B									
LOW	VIS	BIL	ITY	(NN	4) 5	044			
CLOUD		l	ì	1	i i	l = l			
CEILING		1/2-	1 -	2 -	5 -				
(10° FT)	<1/2	<1	< 2	< 5	<10	≥10			
NC	+	+	+	1	4	12			
50<80	+	+	+	+	1	1			
35<50	+	+	+	+	1				
20<35		1	2	4	6	16			
10<20	1	1	4	6	9	7			
6<10	+	1	1	2	3				
3<6	+	+	+	1	+	+			
1.5<3	+	+	+	+	+	+			
0<1.5	4	1	1	2	+	+			

arine Ai	rea (	Ü				
LOW	VIS	:BIL	1ΤΥ	(NA	1) 4	1230
CLOUD CEILING (10° FT)	< ½	/2 ~ '  /2 ~ '	1_ <2	2	5-   <10	: 
NC.	+	+	-,-	7	7	2
50<80	0	Õ	Õ	+	+	
35<50	+	+	+	+	·	2
20<35	+	+	+		4	12
10<20	+	1	2	-4	10	9
6<10	+	i	2	- 2	5	2
3<6	+	+	+	+		+
1.5<3	0	0	+	+	+	0
0<1.5	5	1	1	2	+	+

Marine Area D										
LO#	, V:S	BIL	ΙΤΥ	(NN	!) 7	1122				
CEIL NG	1	)  -	, -	2 -	5 ~	,				
(10 <sup>2</sup> FT)	< 1/2	< 1	< 2	< 5	< 10	210				
NC	+	+	+	1	-5	17				
50 <b0< td=""><td>0</td><td>Ò</td><td>0</td><td>+</td><td>1</td><td>1</td><td></td></b0<>	0	Ò	0	+	1	1				
35<50	+	0	+	+		2				
20<35	+	+	+	1	4	9				
.0<50	+	+	•	3	9	0				
6<.0	+	+		3	9	5				
3<6	+	+		2	- 2					
1.5<3	+	+	+	+	+	+				
0<1.5	2		2			+				



#### Nikol'skoe

#### Khatirka-In-Chukot

| LOW | VISIBILITY (NM) | 3772 | CLOUD | CELLING (10° FT) | (10° F

#### Ugol'neja

### Buhta Providenja

CLOUD CELLING (10° FT) (2°) 2 - 1 - 2 - 5 - 10° 210 (10° FT) (2°) 2 - 1 - 2 - 5 - 10° 210 (10° FT) (2°) 2 - 1 - 2 - 5 - 10° 210 (10° FT) (2°) 2 - 10° 210 (10° FT) (2°) 2 - 10° 210 (10° FT) (10

#### Norheast Cape

LO#	VIS	iBiL	ΙTΥ	(NN	4) 4	198
CLOUD CEILING (10 <sup>3</sup> FT)	د <sup>ر</sup> / >	- درا د ۲	1~	2 - <5	5 - < 10	<b>≥</b> 10
NC	+	1	1	3	11	30
50<80	0	+	+	0	0	+
35<50	0	+	0	+	+	+
20<35	+	+	+	1	2	
10<20	+	1	3	5	8	5
6<10	1	1	3	3	5	2
3<6	+	1	1	1	1	+
1.5<3	+	+	+	0	+	0
0<1.5	4	2	1	+	+	+

#### Nome

LOW	VIS	iB:L	ΙΤΥ	(NN	1) 15	680
CEILING (10° FT)	< ½	½ - <1	1 - < 2	2 - <5	5 - < 10	≥10
NC	+	+	+	1	5	53
50<80	+	+	+	+	+	2
35<50	+	+	+	+	1	2
20<35	+	+	+	1	3	3
10<20	+	+	1	3	4	2
6<10	+	1	1	3	2	+
3<6	+	- 1	1	2	1	+
1.5<3	+	+	+	+	+	+
0<1.5	1	2	1	+	+	+

### Unalakleet

LO#	VI\$	SIBIL	ΙΤΥ	(NN	1) 2	2428
CEILING (10 <sup>3</sup> FT)	< ½	/ <sub>2</sub> - < 1	1 < 2	2 - <5	5 - <10	≥10
NC	+	+	+	1	7	49
50 <b0< td=""><td>0</td><td>0</td><td>0</td><td>+</td><td>+</td><td>4</td></b0<>	0	0	0	+	+	4
35<50	0	0	+	+	1	4
20<35	+	+	+	1	2	8
10<20	+	+	+	2	3	6
6<10	0	+	+	1	1	2
3<6	+	0	+	+	+	+
1.5<3	0	0	0	0	+	Ö
0<1.5	1	2	1	1	0	Ó

### Cape Romanzof

LO#	VIS	BIL	ITΥ	(NN	4) 4	886
CEILING		1/2-	r =	2-	5 -	
(10° FT)	< 1/2	< 1	< 2	< 5	< 10	≥10
NC	1	2	1	4	23	17
50<80	+	+	+	+	1	1]
35<50	+	+	0	+	1	+
20<35	+	+	+	2	5	2
10<20	+		1	4	6	1
6<10	+		2	3	5	1
3<6	+	1	1	1		[ 0]
1.5<3	+	0	+	0	+	0
0<1.5	6	2	1	+	0	0

#### Cape Newenham

LO#	VIS	iBiL	ΙΤΥ	(NN	1) 4	301
CEILING (10° FT)	< 1/2	½ - <1	t - <2	2- <5	5 - <10	<b>≩</b> 10
NC	1	+	+	1	15	20
50<80	+	+	+	0	+	+
35<50	+	+	0	0	+	+
20<35	0	+	+	1	2	2
10<20	0	+	+	3	7	5
6<10	+	1	2	6	9	3
3<6	+	+	1	3	3	1
1.5<3	0	0	+	+	+	+
0<1.5	6	3	2	1	0	0

#### King Salmon

LOW	VIS	BIL	ITΥ	(NN	1) 16	296
CEILING		/ <sub>2</sub> -		17	5-	
(10° FT)	< 1/2	<1	< 2	<5	<10	≥10
NC	+	+	+	+	4	49
50<80	+	0	0	+	1	4
35<50	+	+	+	+	1	4
20<35	+	+	+	1	4	9
10<20	+	+	1	2	5	5
6<10	+	+	1	1	2	1
3<6	+	+	+	1	1	+
1.5<3	+	+	+	+	+	+
0<1.5		1	1	+	+	+

### Port Heiden

LO#	VIS	IBIL	ΊΤΥ	(NN	1)	157
CLOUD CEILING	< <i>′</i> / <sub>2</sub>	1/2 - <1	1-	2 - <5	<10	≥10
NC.	0	1	1	1	1	39
50<80	0	0	0	0	0	4
35<50	0	0	0	Ó	0	4
20<35	0	0	0	0	1	17
10<20	0	1	Ō	0	5	9
6<10	0	0	0	4	3	1
3<6	C	Ō	1	1	1	0
1.5<3	0	0	0	0	Ō	0
0<1.5	4	2	1	1	0	0

### Cold Bay

. <b>○₩</b>	VIS	IBIL	ΙΤΥ	(NM	1) 11	940
CLOUD CEILING (10° FT)	< 1/2	/ <sub>フ</sub> - <1	1-	2- <5	5- <10	≥. ∘
NC	+	+	+	1	6	
50<80	0	0	0	+	+	
35<50	Ō	+	+	+	1	•
20<35	+	+	+	1	7	8
10<20	+	+	1	5	13	9
6<10	+	+	1	-5	8	2
3<6	+	+	1	3	2	+
1.5<3	+	+	+	+	+	0
0<1.5	1	1	1	+	+	0

#### Nikolski

No Data Available

#### St. Paul

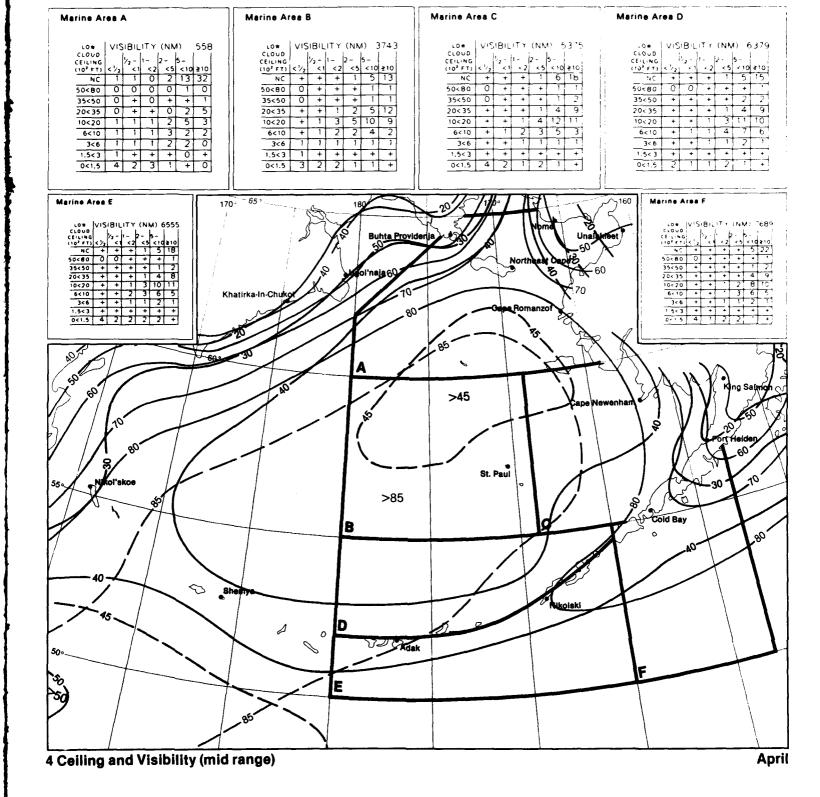
LOW	VIS	BIL	Y TI,	(NIV	1) 9	9455	)
CFOAD	ĺ	W		2 -	5-	1	1
(10° FT)	< 1/2	½ − <1	< 2	<b>^ &lt;5</b>		≥10	
NC	+	+	+	1	14	9	
50<80	0	0	+	+	+	+	
35<50	0	0	+	+	1	1	
20<35	+	+	+	1	7	4	
10<20	$\Box$ 1	1	2	5	18	5	
6<10	1	1	1	3	5	1	
3<6	+	1	2	3	3	+	
1.5<3	+	+	+	+	+	+	
0<1.5	4	1	+	+	+	+	

### Adak

LOW	VIS	BIL	ΙŤΥ	(NN	1) 13	3735
CEILING		/ <sub>2</sub> -	1-	2 -	5 -	
(10° FT)	< 1/2	< 1	<2	< 5	<10	≥10
NC	+	+	+	1	10	3
50<80	0	0	0	+	+	+
35<50	0	+	0	+	5	1
20<35	0	+	+	2	31	2
10<20	+	+	1	9	20	1
6<10	+	+	1	4	2	+
3<6	+	+	+	1	+	+
1.5<3	0	+	+	+	+	0
0<1.5	,	1	1	1	+	0

# Shemya

LOW	VIS	BIL	iΤΥ	(NN	1) 10	142
CEILING	١.	/2 -		2 -	5 -	
(10° FT)	< 1/2	< 1	< 2	< 5	< 10	<b>≩</b> 10 ,
NC	+	+	+	1	8	10
50<80	0	0	0	+	+	+ }
35<50	0	+	0	+	2	2
20<35	+	+	+	1	13	12
10<20	+	1	1	5	15	4
6<10	+	1	2	4	3	+
3<6	+	2	2	2	1	+
1.5<3	+	+	+	+	+	0
0<1.5	3	2	1	+	0	+



MI	 	koe

L0:	l vis	iBiL	IT Y	(NN	4) 5	645
CLOUD	[	1/2-	ا ا ـ ا	la _	اا	1 [
CEILING (10° FT)	<1/2	,3- (1)	<2	<5	<10	≩10
NC .	+	+	+	+	1	21
50<80	0	+	0	+	+	+
35<50	0	0	+	+	+	2
20<35	+	+	+	1	_3	15
10<20	+	+	7	5	9	22
6<10	+	+	+	2	2	3
3<6	+	+	+	1	1	
1.5< 3	Ò	+	0	+	+	+
0<1.5	8	+	+	+	+	+

### Khatirka-In-Chukot

LOW	Lvis	iBiL	iτν	/ NI N	1) 7	3465
CLOUD CEILING (10° FT)	< ½	ן פונ - גל ני	1- <2	2 - <5	5 -	±0 ≥10
NC	1	+	+	1	1	47
50<80	0	0	0	0	0	+
35<50	0	+	0	+	1	7
20<35	+	+	1	2	2	9
10<20	+	+	2	3	3	4
6<10	+	+	7	2	1	+
3<6	+	+	7	+	+	+
1.5< 3	+	+	+	+	+	+
0<1.5	7	+	0	0	0	+

### Ugol'naja

LOW	1 ///5	iBiL	iTV	(NIA	() 5	031
CLOUD CEILING (10° FT)	د ا ۷ د/ >	/ <sub>2</sub> - (1	1-<2	ı	5 -	₹10
NC		+	1	1	2	43
50<80	0	0	O	+	+	+
35<50	+	0	0	+	+	2
20<35	+	+	+	1	2	9
10<20	1	1	3	4	4	9
6<10	+	+	1	2	2	2
3<6	0	+	+	1	1	1
1.5<3	0	+	+	+	+	+
0<1.5	4	+	+	+	+	+

### Buhta Providenja

10#	VIS	iBiL	ITY	(NA	1) 4	680
CLOUD CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1- <2	2- <5	5- <10	<b>≩</b> 10
NC	+	+	+	1	3	42
50<80	0	0	+	+	+	+
35<50	+	0	+	+	+	2
20<35	+	+	+	2	3	10
10<20	+	1	3	6	6	9
6<10	+	+	1	2	Ť	1
3<6	+	+	7	7	1	+
1.5<3	Ö	+	+	+	0	+
0<1.5	2	+	+	0	Ó	+

### Norheest Cape

	م ا			/ h : h		
CLOUD CEILING (10° FT)	V15	BIL 72-		(NN 2- <5	1) 4 5 - <10	1679    ≥10
NC.	+	+	+	7	4	25
50 <b0< td=""><td>0</td><td>0</td><td>0</td><td>+</td><td>+</td><td>1</td></b0<>	0	0	0	+	+	1
35<50	0	0	+	+	+	+
20<35	+	+	+	+	1	4
10<20	+	+	+	2	8	12
6<10	+	1	3	3	8	6
3<6	+	1	3	3	4	1
1.5<3	0	0	+	+	+	0
0<1.5	3	2	1	+	0	0

# Nome

10 W	VIS	BIL	IT Y	(NN	1) 15	788
CLOUD	İ	l. 1	١.	la .	ا ا ۔	
(10° FT)	< 1/2	り <sub>2</sub> - く1	< 2	< 5	< 10	≥10
	_	- ` '		-		
NC.	+	+		+		53
50<80	_+	+	0	+	+	5
35<50	0	+	0	+	+	4
20<35	+	+	+	+	2	6
10<20	+	+	+	1	4	4
6<10	+	+	1	2	3	2
3<6	+	1	1	2	2	1
1.5<3	+	+	+	+	+	+
0<1.5	1	1	1	+	+	0

### Unalakleet

LOW	VIS	iBiL	IT Y	(NN	1) 2	700
CLOUD CEILING (10° FT)	< 1/2	り2 - <1	1 - < 2	2 - <5	5 - <10	≥10
NC	+	+	+	+	1	52
50<80	0	Ò	0	+	+	4
35<50	0	0	0	0	1	8
20<35	0	Ò	+	+	1	11
10<20	0	Ō	+	1	7	6
6<10	0	0	+	-	1	3
3<6	+	+	+	1	2	2
1.5<3	0	+	+	+	+	+
0<1.5	1	1	+	+	+	+

## Cape Romanzof

LOW	VIS	IBIL	ITY	(NN	1) 5	104
CEILING (10° FT)	< 1/2	/ <sub>フ</sub> - <1	1- <2	2 - < 5	5 ~ <10	≥10
NC	+	+	+	1	18	20
50<80	0	+	+	+	2	1
35<50	Ö	0	0	+	1	1
20<35	+	+	+	1	8	5
10<20	+	+	1	3	8	3
6<10	+	+	2	3	4	_1
3<6	+	1	2	2	2	+
1.5<3	+	+	+	+	+	+
0<1.5	3	2	+	+	0	0

### Cape Newenham

LOW	VIS	iBiL	iΤΥ	(NN	1) 4	1495
CEILING (10° FT)	< ½	り <sub>2</sub> - く1	1 – < 2	2 - <5	5 -	≥10
NC	+	+	+	1	13	19
50 <b0< td=""><td>T+</td><td>+</td><td>+</td><td>+</td><td>1</td><td>1</td></b0<>	T+	+	+	+	1	1
35<50	0	0	0	0	+	1
20<35	+	0	0	+	2	4
10<20	0	+	1	2	6	7
6<10	+	1	2	4	7	5
3<6	0	+	2	3	3	1
1.5<3	+	+	+	+	+	+
0<1.5	5	3	2	1	+	0

### King Selmon

LO#	VIS	IBIL	ΙΤΥ	(NN	1) 16	705
CLOUD CEILING (10° FT)	< 1/2	ر ا > درا	1- <2	2- <5	5 - <10	≥10
NC	+	+	+	+	2	45
50<80	+	0	0	+	+	6
35<50	+	+	0	+	1	8
20<35	+	+	+	+	3	13
10<20	+	+	+	1	4	6
6<10	+	+	+	1	3	1
3<6	+	+	+	1	1	+
1.5<3	+	+	+	+	+	+
0<1.5	1	+	+	+	+	+

### Port Heiden

LOW	VIS	IBIL	ITY	(NN	1)	128
CEILING		1/2-	1	2-	5-	1
(10 <sup>2</sup> FT)	< 1/2	<1	< 2	<5	<10	≩10
NC	0	0	3	2	4	63
50<80	0	0	0	0	0	2
35<50	0	0	0	0	Ô	4
20<35	Ö	0	0	0	0	7
10<20	Ò	0	0	0	_1	5
6<10	0	1	0	1	3	1
3<6	0	0	0	1	0	0
1.5<3	0	0	0	0	0	0
0<1.5	2	1	0	0	Ō	1

# Cold Bay

LO#	VIS	IBIL	ΙΤΥ	(NN	<b>()</b> 1 1	627
CEILING		1/2-	1-	2 -	5 –	
(10° FT)	< 1/2	<1	<2	< 5	<10	≥10
NC	+	+	+	+	4	17
50<80	0	0	0	0	+	+
35<50	0	+	+	+	1	2
20<35	+	+	+	+	5	10
10<20	+	+	+	2	13	12
6<10	+	+	1	4	11	4
3<6	+	+	1	4	4	1
1.5<3	+	+	+	+	+	+
0<1.5	1	+	+	+	+	0

### Nikolski

No Data Available

# St. Paul

LOW	VIS	iBil	,ΙŤΥ	(NM) 9221			
CLOUD		1/2-	1-	2 -	5 -		
(10 <sup>2</sup> FT)	<1/3	<1	_ < 2	< 5	<10	≥10	
NC	+	+	+	1	9	8	
50<80	+	Ô	+	+	+	+	
35<50	+	O	0	+	1	1	
20<35	+	+	+	+	6	4	
10<20	+	+	+	2	16	6	
6<10	+	+	1	3	7	1	
3<6	+	2	3	6	7	1	
1.5<3	+	_1	1	1	+	+	
0<1.5	6	_3	1	+	+	0	

### Adek

LOW	VIS	BIL	ΙΤΥ	(NN	1) 14	156
CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1- <2	2 – <5	5~ <10	<u>≥</u> 10
NC	+	0	+	+	7	3
50<80	0	0	0	0	+	+
35<50	0	0	0	+	3	1
20<35	0	+	<b>+</b>	1	21	2
10<20	+	+	1	10	32	1
6<10	0	+	1	6	6	+
3<6	0	+	1	_2	1	+
1.5<3	+	+	+	+	+	0
0<1.5	+	+	1	1	+	0

### Shemya

LOW	VIS	IBIL	ΙΤΥ	(NN	1) 10	380
CEILING	. !	1/2 -	1-	2-	5 -	
(10° FT)	< 1/2	< 1	<2	<5	<10	10 €
NC	+	+	+	+	5	6
50<80	+	0	0	+	+	+
35<50	0	0	0	+		1
20<35	+	+	+	+	6	9
10<20	+	+	+	4	17	10
6<10	+	+	2	5	9	1
3<6	+	2	3	4	2	+
1.5<3	+	1	+	+	+	0
0<1,5	6	3	1	+	+	Ô

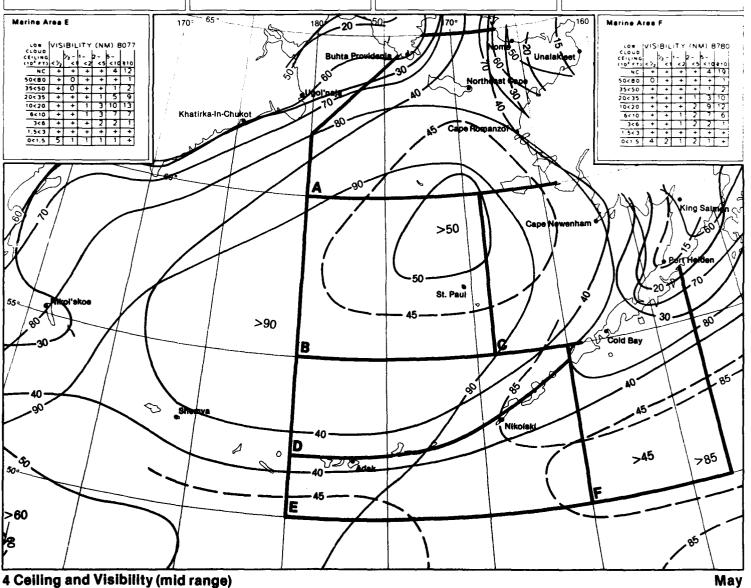
Marine Area A								
LOW CLOUD CEILING (10 <sup>2</sup> FT)	1	31BIL	.ITY 1- <2	(NN 2- <5	5 -	99! ≧10		
NC	Ť	+	0	1	5	14		
50<80	0	0	+	0	+	+		
35<50	0	0	+	+	1	1		
20<35	O	0	+	1	4	6		
10<20	+	0	1	3	10	12		
6<10	1	1	2	6	7	3		
3<6	1	1	1	1	1	1		
1.5<3	2	0	+	+	1	0		
0<1.5	8	3	3	1	+	+		

Marine Area B										
LOW CLOUD CEILING (10° FT)	VIS	اBIL اري -	ITY 1- <2	(NN 2- <5	5 -	3541     <sub>≩10</sub>				
NC NC	+	+	+	+	4	9				
50<80	0	0	0	+	1	1				
35<50	+	0	+	+	1	2				
20<35	+	+	+	1	5	15				
10<20	+	1	1	4	13	8				
6<10	+	1	1	3	6	2				
3<6	+	+	+	1	2	1				
1.5<3	+	+	+	+	+	+				
0<1.5	9	2	2	2	+	+				

LOW	VIS	BIL	IT Y	(NN	4) 7	199
CEILING		1/2 -	1-	2 -	5-	
(10° FT)	< 1/2	\ ^<1	< 2	< 5	<10	<u>≩</u> 10
NC	+	+	+	1	5	18
50<80	+	+	0	+	+	1
35<50	+	+	+	1	1	2
20<35	+	+	+	2	4	8
10<20	+	+	1	5	11	10
6<10	+	+	1	3	4	-3
3<6	+	+	1	1	1	1
1.5<3	+	+	+	+	+	+
0<1.5	7	1	2	1	1	+

Marine Area C

LO#	1 1/15	SIBIL	iTV	CNIK	4) 7	700
CFOOD	٧,-	1		(1911)	'' '	
CEILING		1/2-	1 -	2 -	5-	
(10 <sup>2</sup> FT)	< 1/2	< 1	< 2	<5	<10	≩10
NC	+	+	+	7	4	11
50<80	+	+	+	+	1	- 1
35<50	+	0	+	+	2	3
20<35	+	+	+	1	5	9
10<20	+	+	+	2	11	13
6<10	+	+	1	3	8	7
3<6	+	+	1	1	3	2
1.5<3	+	+	+	+	-1	+
0<1.5	3	1	1	2	1	+



#### Nikol'skoe

CLOUD CEILING | 1/2 - 1 - 2 - 5 - | 1/2 - 1 | 1/2 | 1/2 - 1 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2

#### Khatirka-In-Chukot

#### Ugol'naja

#### Buhta Providenja

COW CELLING (10° FT) (NM) 4476 (10° FT) (10° FT

### Norheast Cape

LO#	VIS	IBIL	IT Y	(NN	1) 4	<b>148</b> 0
CLOUD		١. ا	١.	L	L	
CEILING	ì. ·	1/2-		2	P -	1 1
(10° FT)	< 1/2	< 1	<2	<5		≩10
NC	[ 1	1	+	1	5	[26]
50<80	0	+	+	+	+	2
35<50	0	+	0	+	+	2
20<35	+	+	+	+	1	4
10<20	+	+	+	2	7	11
6<10	+	+	1	3	8	4
3<6	+	1	2	3	4	1
1.5<3	+	+	+	+	+	+
0<1.5	6	1	1	+	0	0

# Nome

LO#	VIS	IBIL	ITY	(NN	1) 15	898
CLOUD CEILING (10° FT)	< ½	ر ا> ا>	1- <2	2- <5	5 - <10	≥10
NC	+	+	+	+	1	53
50 <b0< td=""><td>+</td><td>+</td><td>0</td><td>+</td><td>+</td><td>4</td></b0<>	+	+	0	+	+	4
35<50	+	0	+	+	+	3
20<35	+	+	+	+	1	5
10<20	+	+	+	1	3	5
6<10	+	+	1	2	4	2
3<6	+	1	2	3	3	1
1.5<3	+	+	+	+	+	+
0<1.5	2	1	+	+	+	+

### Unalakleet

LOW	VIS	BIL	(TY	(NN	1) 2	2573
CLOUD		١,	۱. ا	1	5-	1
(10° FT)	< 1/2	/2~ <1	<2	<5	<10	≥10
NC	+	+	+	+	+	41
50<80	0	0	0	0	+	5
35<50	0	+	0	0	+	8
20<35	+	0	0	0	1	13
10<20	Ò	+	+	+	1	11
6<10	0	+	+	+	2	5
3<6	+	+	+	1	2	2
1.5<3	0	+	+	+	+	+
0<1.5	2	1	+	1	+	+

#### Cape Romanzof

LO#	VIS	IBIL	IΤΥ	(NN	1) 4	996
CLOUD CEILING (10 <sup>7</sup> FT)	< 1/2	り <sub>2</sub> - <1	1- <2	2 - <5	5- <10	<u>≩</u> 10
NC	+	1	+	2	14	16
50<80	0	0	0	+	1	1
35<50	Ò	0	0	0	1	1
20<35	Ô	+	+	1	4	5
10<20	0	+	+	2	9	4
6<10	0	+	1	4	9	3
3<6	Ô	1	1	3	5	_1
1.5<3	0	+	+	+	+	0
0<1.5	5	3	1	+	+	0

#### Cape Newenham

LOW	VIS	IBIL	ΙΤΥ	(NN	1) 4	431
CLOUD		1/2-	1 –	2-	5-	
(10° FT)	< 1/2	<1	<2	<5	<10	≥10
NC	+	1	T 1	2	8	20
50<90	+	+	+	+	+	1
35<50	0	+	0	0	+	1
20<35	+	0	+	+	2	3
10<20	+	+	1	2	4	5
6<10	0	+	1	3	6	7
3<6	+	+	2	5	7	3
1.5<3	0	+	+	+	+	+
0<1.5	8	2	2	1	+	0

### King Salmon

LO W	V15	iBiL	ΙΤΥ	(NN	1) 16	181
CLOUD	j	1/2 -	1 -	2-	5-	
(10° FT)	<1/2	¯<1	<2	<5	<10	≥10
NC	+	+	+	+	2	40
50<80	+	+	+	+	+	5
35<50	+	0	+	+	1	8
20<35	+	+	0	+	2	13
10<20	+	+	+	+	3	8
6<10	+	+	+	1	3	3
3<6	+	+	+	2	2	1
1.5<3	+	+	+	+	+	+
0<1.5	1	1	+	+	+	0

# Port Heiden

LO#	VIS	BIL	ITY	(NN	1)	136
CEOUD CEILING (10° FT)	<1/2	/ <sub>2</sub> - <1	1- <2	2 - <5	5 - <10	≥10
NC	0	1	0	4	3	57
50 <b0< td=""><td>0</td><td>0</td><td>0</td><td>0</td><td>0</td><td>4</td></b0<>	0	0	0	0	0	4
35<50	0	0	0	0	0	4
20<35	0	0	0	Ö	0	13
10<20	0	0	0	0	1	5
6<10	0	0	0	1	1	1
3<6	0	0	1	0	1	0
1.5<3	0	0	0	0	0	0
0<1.5	_1	1	0	0	0	0

# Cold Bay

LO#	VIS	BIL	iTY	(NN	4) 1 1	236
CLOUD CEILING (10° FT)	< 1/2	γ <sub>2</sub> - <1	1- <2	2 - <5	5- <10	≩10
NC	+	+	+	+	3	16
50<80	0	0	0	+	+	1
35<50	Ö	0	0	0	+	2
20<35	+	+	+	+	2	9
10<20	0	+	+	1	9	16
6<10	+	+	+	3	13	6
3<6	+	+	2	5	7	1
1.5<3	+	+	+	+	+	+
0<1.5	1	1	+	+	+	0

#### Nikolski

No Data Available

# St. Paul

LOW	VIS	IBIL	IΤΥ	(NN	1) 8	841
CLOUD CEILING (10° FT)	< ½	//2 - <1	1 - <2	2- <5	5- <10	≩10
NÇ	1	+	+	1	8	7
50 <b0< td=""><td>0</td><td>+</td><td>0</td><td>0</td><td>1</td><td>+</td></b0<>	0	+	0	0	1	+
35<50	+	0	0	+	1	+
20<35	+	+	Ô	4	3	3
10<20	+	+	+	7	14	4
6<10	+	+	1	3	8	1
3<6	1	2	3	8	9	1
1.5<3	+	1	1	1	1	+
0<1.5	10	4	1	+	+	0

#### Adak

LOW	VIS	iBiL	IT Y	(NN	1) 14	017
CLOUD		1/2-	1 -		5 -	
(10° FT)	< 1/2	<1	<2	<5	<10	210
NC	+	+	+	+	6	3
50<80	+	+	0	+	+	+
35<50	0	0	0	+	1	[ +]
20<35	O	Ō	+	+	12	2
10<20	+	+	+	8	32	2
6<10	+	+	1	9	11	+
3<6	+	+	1	3	3	+
1.5<3	+	+	+	+	+	Ó
0<1.5	_1	1	1	+	+	0

#### Shemya

LOW	VIS	IBIL	łΤΥ	(NN	1) 9	991
CLOUD CEILING (10° FT)	< 1/2	ر ا ک	1-	2- <5	5 - <10	≥10
NC	+	+	+	+	2	6
50<80	0	+	0	+	+	+
35<50	0	0	0	0	+	+
20<35	+	0	+	+	2	4
10<20	+	+	+	1	1.1	10
6<10	+	+	1	4	10	3
3<6	1	3	5	7	7	1
1.5<3	+	1	1	1	+	+
0<1.5	12	4	2	1	+	+

June

June

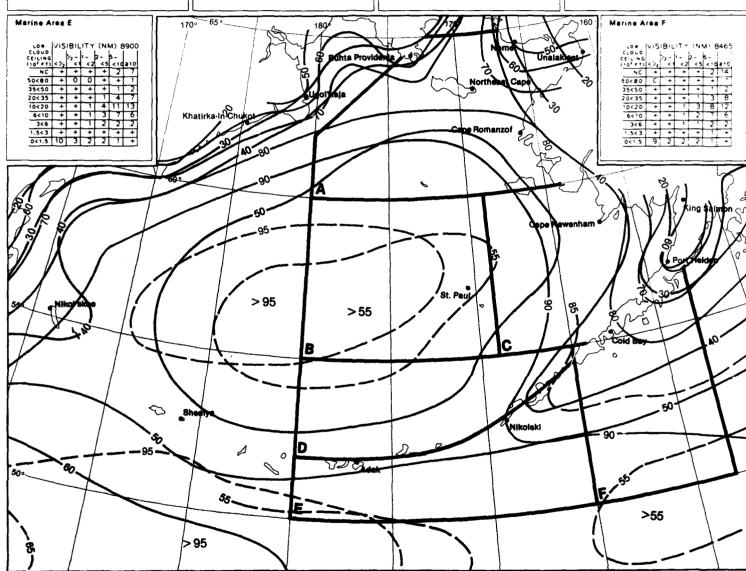
Marine Area A									
C0.000	VIS	iBiL	ITY  ,	(NN  -	1) 1  -	548			
CEILING (10° FT)	<1/2	½ - <1	<2	∠- <5	<10	≩10			
NC	1	+	+	+	4	21			
50<80	0	0	0	+	+	1			
35<50	+	+	+	0	1	3			
20<35	0	0	+	+	3	6			
10<20	+	+	+	1	7	9			
6<10	+	+	7	П	5	5			
3<6	1	+	+	1	2	1			
1.5<3	+	+	1	1	1	1			
0<1.5	14	2		2	1	+			

4 Ceiling and Visibility (mid range)

Marine Area B										
LOW CLOUD CEILING (10 <sup>2</sup> FT)	VIS    -  -  -	B L  ½ -  < 1	ITY 1- <2	(NN 2- <5	5-	164 ≥10				
NC NC	+	+	+	+	2	7				
50<80	+	0	0	+	+	1				
35<50	+	0	+	+	1	3				
20<35	+	+	+	2	6	11				
10<20	+	+	1	4	12	10				
6<10	+	+	1	4	5	3				
3<6	+	+	1	1	2					
1.5<3	+	+	+	+	+	+				
0<1.5	15	2	1	1	+	+				

Marine Area C									
LO*	VIS	BIL	iΤΥ	(NN	1) 8	1597			
CLOUD CEILING (10 <sup>2</sup> FT)	< 1/2	1/2 - <1	1-	2- <5	5- <10	≥10			
NC	+	+	+		5	17			
50<80	+	0	Ö	+	1	1			
35<50	+	+	+	+	2	2			
20<35	+	+	+	2	5	8			
10<20	1	+	1	4	10	7			
6<10	+	+	1	2	4	2			
3<6	+	+	+	1	1	+			
1.5<3	+	+	+	+	+	+			
0<1.5	14	1	1	1	1	+			

Marine Area D								
LOW	VIS	BIL	ΙTΥ	(NN	() 8	3006		
Crond		l	i. !	_ !	_	1 1		
CEILING	i .	1/2-	1 -	2	٠- د			
(10° FT)	< 1/2	< 1	< 2	< 5	<10	≥10		
NC	+	+	+	+	3	7		
50<80	+	0	0	+	+	1		
35<50	+	+	+	+	1	2		
20<35	+	+	+	1	6	10		
10<20	+	+	,	3	10	11		
6<10	+	+	1	3	7	5		
3<6	+	+		2	2	1		
1.5<3	+	+	+	+	+	+		
0<1.5	8	2	2	2	1	+		



# Nikol'skoe

٠0.	1 1/15		ιTν	(NA	4) 5	348
CLOUD	V 1.3	ا دردا ا - دردا		2 -	5 -	
(10° FT)	< 1/2	< 1	<2	< 5	<10	≩10
NC	+	+	+	1	1	16
50<80	+	0	Ô	0	+	+
35<50	0	0	0	+	+	
20<35	+	0	+	+	1	7
10<20	+	+	+	3	5	15
6<10	+	+	1	5	4	5
3<6	+	+	1	3	2	2
1.5<3	+	+	+	+	+	+
0<1.5	25	+	+	+	+	+

### Khatirka-In-Chukot

LOW	VIS	BIL	!TY	(NV	<b>()</b>	325 1
CLOUD		/ <sub>2</sub> -	l	h _	5 -	
(10° FT)	< 1/2	/3 =   <1	< 2	` <5	<10	≥10
NC.	1	0	1		-	33
		_		_		27
50<80	0	0	0	+	Lo	+
35<50	0	0	0	+	+	8
20<35	+	0	+	1	1	8
10<20	+	+	1	3	2	5
6<10	+	+	1	3	2	2
3<6	+	+	1	1	1	+
1.5<3	+	+	+	+	1	+
0<1.5	21	+	+	0	+	+

### Ugol'neje

10#	VIS	IBIL	ITY	(NA	1) 4	940
CLOUD CEILING (10° FT)	< 1/2	/ <sub>2</sub> -	1-	2- <5	5 - < 10	<b>≥</b> 10
NC	1	+	+	1	2	47
50<80	0	0	0	Ō	+	+
35<50	0	0	0	+	+	4
20<35	+	+	+	+	1	10
10<20	+	+	+	1	2	8
6<10	+	+	1	2	2	2
3<6	0	+	+	)	2	1
1.5<3	+	+	+	+	+	+
0<1.5	10	1	+	+	+	+

### Buhte Providenje

LO#	VIS	BIL	JT Y	(NN	4) 4	40
CLOUD	}	1/2 -	ļ,_	2-	5-	ļ
(10° FT)	<1/2	<1	<2	<5	<10	≩10
NC	+	+		1	2	37
50<80	0	0	0	+	+	+
35<50	0	+	+	+	+	2
20<35	0	0	+	1	1	7
10<20	+	+	2	6	6	9
6<10	+	+	3	3	2	2
3<6	+	1	3	2	1	+
1.5<3	+	+	1	+	0	+
0<1.5	4	+	+	0	0	+

### Norheest Cape

	ما		. <del>.</del>			
LOW CLOUD CEILING (10° FT)	< 1/2	181L	Y  -   <2	)	5 -	466   ≥10
NC	1	+	+	1	6	24
50<80	+	+	+	+	+	- 1
35<50	0	0	0	0	+	+
20<35	+	+	+	+	+	3
10<20	+	+	1	3	8	11
6<10	+	1	2	4	10	4
3<6	+	1	2	3	3	1
1.5<3	0	0	+	+	+	+
0<1.5	3	2	1	+	0	0

### Nome

LOW	VIS	ıBıL	jΤΥ	(NN	1) 16	600
CEILING (10° FT)	< ½	½- ≤1	1 - < 2	2 - <5	5 - < 10	≥10
NC	+	+	+	+	2	42
50<80	+	+	0	+	+	3
35<50	Ö	0	0	0	+	3
20<35	0	+	+	+	1	5
10<20	Ò	+	+	1	4	8
6<10	+	+	1	4	7	3
3<6	+	1	3	4	3	1
1.5<3	+	+	+	+	+	+
0<1.5	1	+	+	+	+	0

### Unalakieet

LOW	VIS	BIL	11 Y	(NN	1) _	898
CLOUD		1/2-	, [	2~	5 -	
CEILING	- 17			2 ~ < 5	1-	≥10
(10° FT)	< 1/2	< 1	< 2		< 10	_
NC	+	+	+	+	1	35
50<80	0	0	0	0	0	3
35<50	+	0	0	+	+	7
20<35	0	0	0	+	1	16
10<20	0	+	+	1	_3	17
6<10	0	+	+	1	3	6
3<6	0	+	+	1	1	1
1.5<3	0	0	+	0	0	+
0<1.5	+	+	+	+	+	+

# Cape Romanzof

LOW	VIS	iBiL	iΤΥ	(NA	1) 4	84
CLOUD CEILING (10° FT)	< 1/2	½ - <1	1- <2	2 - <5	5- <10	≥10
NC	+	+	+	2	15	13
50<80	0	+	0	+	1	+
35<50	0	0	0	0	+	+
20<35	0	0	Ó	+	2	4
10<20	0	+	+	1	5	4
6<10	0	+	1	3	13	5
3<6	+	1	2	6	-8	1
1.5<3	+	+	+	1	+	+
0<1.5	5	4	-	+	0	0

### Cape Newenham

LOW	VIS	IBIL	ΙΤΥ	(NN	1) 4	057
CLOUD CEILING		½-	1-	2-	5-	
(10° FT)	<1/2	<1	<2	<5	<10	≥10
NC.		+	1	2	6	18
50<80	+	+	+	+	+	
35<50	O	+	+	+	+	1
20<35	+	+	+	+	2	2
10<20	+	+	1	2	5	5
6<10	+	+	1	4	7	9
3<6	+	7	2	6	5	3
1.5<3	+	+	+	+	+	+
0<1.5	6	4	1	1	+	Ö

# King Salmon

LO#	VIS	iBiL	IT Y	(NA	1) 16	739
CLOUD		1/2 -	1 -	2	5-	
(10° FT)	< 1/2	< 1	< 2	< 5	<10	₹10
NC	1	+	+	1	2	35
50<80	+	+	+	+	+	4
35<50	+	+	0	+	1	6
20<35	+	0	+	+	2	12
10<20	+	+	+	1	5	8
6<10	+	+	1	2	4	2
3<6	+	+	1	3	2	1
1.5<3	+	+	+	+	+	+
0<1.5	2		1	+	+	+

# Port Heiden

LOW	Lvie	iBiL	ıт∨	/ K13	45	93
CLOUD			'''	(1417)	לוי ו ו	נפ ו
CEILING		1/2 -	1-	2-	5-	
(10° FT)	< 1/2	< 1	<2	< 5	<10	≥10
NC	0	1	2	4	1	38
50<80	0	0	0	0	Ö	1
35<50	0	0	0	0	0	1
20<35	0	0	0	0	1	11
10<20	0	0	2	0	1	6
6<10	0	1	0	3	4	2
3<6	0	0	0	4	3	3
1.5<3	0	0	0	0	0	0
0<1.5	5	1	1	1	Ô	0

# Cold Bay

LOW	) VIS	iBit	Y Ti.	(NN	A) 12	2361
CLOUD	,	ا - درا	1_	2 -	5_	i
(10° FT)	< 1/2	/ · < 1	<2	<sup>2</sup> <5	<10	≩10
NC	+	+	+	1	4	13
50<80	+	0	+	+	+	+
35<50	0	+	Ó	+	1	1
20<35	0	+	+	+	2	5
10<20	+	+	+	1	7	12
6<10	+	+	1	4	13	6
3<6	+	1	3	6	9	Ž
1.5<3	+	+	1	1	+	+
0<1.5	2	1	1	+	+	Ò

# Nikolski

No Data Available

# St. Paul

LOW	VIS	BIL	IT Y	(NN	1) 9	9078
CEILING (10° FT)	<ツ <sub>2</sub>	/2 - <1	1-	2- <5	5 - < 10	<u>≩</u> 10
NC	1	+	+	+	5	4
50<80	+	+	0	0	+	+
35<50	+	+	+	+	+	+
20<35	+	+	+	+	2	1
10<20	+	+	+	1	9	4
6<10	+	+	1	2	9	1
3<6	1	3	5	10	9	1
1.5<3	1	1	2	1	1	+
0<1.5	16	4	2	+	+	+

# Adak

LOW	VIS	IBIL	ITY	(NN	1) 14	420
CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1-	2- <5	5 ~ <10	≥10
NC	+	+	+	1	8	4
50<80	0	+	+	+	+	+
35<50	0	0	+	0	+	+
20<35	0	+	+	+	5	ì
10<20	+	+	1	5	23	1
6<10	+	+	2	11	16	Ĩ
3<6	+	1	3	7	5	+
1.5<3	+	+	+	+	+	0
0<1.5	2	2	1	1	+	0

# Shemya

LOW	VIS	IBIL	IT Y	(NN	1) 10	27
CLOUD CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1- <2	2 – <5	5 - <10	≥10
NC	+	+	+	+	2	4
50 <b0< td=""><td>+</td><td>+</td><td>+</td><td>0</td><td>+</td><td>+</td></b0<>	+	+	+	0	+	+
35<50	0	0	0	+	+	+
20<35	+	+	+	+	1	1
10<20	+	+	+	1	3	3
6<10	+	+	1	2	7	3
3<6	1	3	5	8	8	1
1.5<3	1	2	2	1	+	+
0<1.5	27	7	2	1	+	+

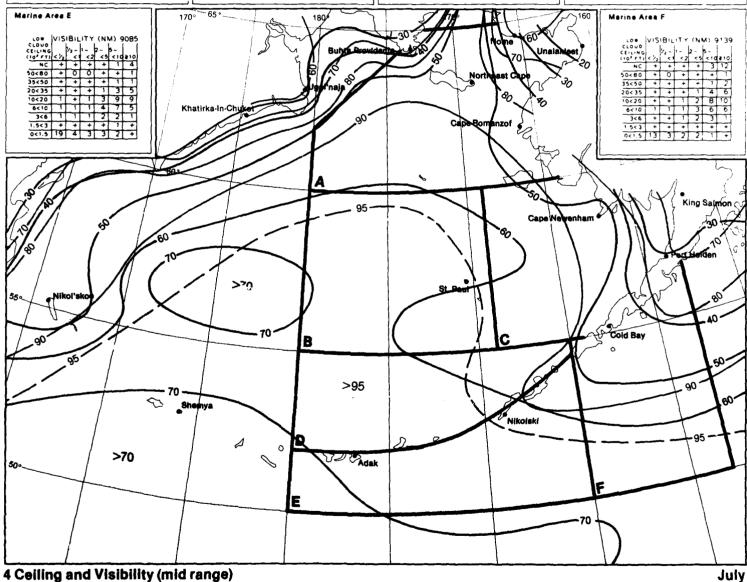
July

Aarina A		A				
LOW	VIS	i BIL	ITY.	(NN	() 3	3277
CLOUD	1	١.	1		l_	1
CEILING	١.	1/2-	1 – '	2-	5-	
(10° FT)	< 1/2	<1	<2	<5	<10	≩10
NC	1	+	+	1	3	19
50<80	+	0	+	+	1	2
35<50	+	0	0	7	1	2
20<35	+	+	+	1	3	8
10<20	+	+	1	2	7.	8
6<10	+	+	1	2	5	5
3<6	+	+	+	1	2	1
1.5<3	+	0	+	+	+	+
0<1.5	12	2	2	1	1	+
0(1.5	1.2		ــــــــــــــــــــــــــــــــــــــ		<u> </u>	

LOW	VIS	BIL	JTY.	(NN	1) 5	25
CLOUD	ł	lu i	],	ا ام	5-	1
(10° FT)	< 1/2	/2 = 1	<2	 <5		≥10
				<b>-</b>	1	
NC	+	+	+	+		6
50<80	0	+	+	+	+	+
35<50	0	+	+	+	1	1
20<35	+	+	+	1	6	9
10<20	+	+	2	5	11	8
6<10	1	1	2	4	7	2
3<6	1	1	1	2	2	+
1.5<3	+	+	1	+	+	0
0<1.5	15	3	2	1	+	+

Marine Ar	·ee (	2					
LO# CLOUD	VIS	i iBiL	JT Y	(N.N.	1) E	3462	2
CEILING (10° FT)	< ½	ン <sub>2</sub> - <1	1-	2 ~ <5	5 - <10	≥10	
NC	+	+	+	7	4	11	İ
50<80	0	+	0	+	+	1	ĺ
35<50	+	+	+	1	1	2	)
20<35	+	+	+	1	5	8	
10<20	1	1	1	5	1 1	7	
6<10	1	1		4	5	3	
3<6	+	+	+	1	1	1	
1.5<3	+	+	+	+	+	+	ļ
0<1.5	14	2	2		1	+	]

rin <b>e</b> Ar	98 1					
LOW CLOUD	VIS	BIL	ITY I	(NN	4) <del>(</del>	72
CEILING		1/2-	1 -	2 -	5-	
(10° FT)	< 1/2	<1	< 2	< 5	<10	≥10
NC	+	+	+	+	2	5
50-80	0	+	+	+	+	1
35<50	+	+	+	+	1	2
20<35	+	+	+	1	4	7
10<20	+	+	1	3	8	8
6<10	1	+	1	3	7	4
3<6	+	+	1	2	3	1
1.5<3	+	+	+	+	1	+
0<1.5	15	4	3	3	2	+



### Nikol'skoe

CELLING COLORD VISIBILITY (NM) 5277 CLOUD CEILING COLORD VISIBILITY (NM) 5277 CLOUD VISIBILITY (NM) 52

#### Khatirka-In-Chukot

COW VISIBILITY (NM) 3266
CLOUD (FILMS (1) 2- 1- 2- 5- 10 (10) FT (1) (10) FT (1) (10) FT (1) (10) FT (1) (10) FT (1) (10) FT (1) (10) FT (1) (10) FT (1) (10) FT (10)

#### Ugol'naja

### Buhta Providenja

CLOUD CLOUD | 1- 2- 5- | 10 210 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10 2 15 | 10

#### Norheast Cape

LOW	VIS	BIL	ITY	(NN	1) 4	533
CLOUD	ļ	/ <sub>2</sub> - 1	١.	١,	ا عا	
(10° FT)	< 1/2	/2 =     </td <td>&lt;2</td> <td>- &lt;5</td> <td>210</td> <td>≩10</td>	<2	- <5	210	≩10
	1 1/2	<b>├</b>	_			1.5
NC	+		+		_ 3	כי
50<80	+	0	0	+	+	1
35<50	0	0	0	+	+	1
20<35	+	+	+	+	2	5
10<20	0	+	1	4	9	13
6<10	+	1	3	6	10	4
3<6	+	1	3	4	4	1
1.5<3	+	0	+	+	+	+
0<1.5	3	2	1	+	0	0

#### Nome

LOW	VIS	IBIL	IT Y	(NN	1) 16	615
CLOUD CEILING (10° FT)	< 1/2	ン <sub>2</sub> - <1	1 ~ < 2	2 - <5	5 - < 10	<b>≩</b> 10
NC	+	+	+	+	2	35
50<80	+	+	+	+	+	3
35<50	+	0	+	+	+	3
20<35	0	+	+	+	2	7
10<20	+	+	+	1	7	9
6<10	+	+	1	4	7	3
3<6	+	1	3	4	2	1
1.5<3	+	+	+	+	+	+
0<1.5	1	+	+	+	+	+

### Unalekiest

LOW	VIS	JBIL	ΙΤΥ	(NN	1) 2	789
CLOUD CEILING (10° FT)	< 1/2	り <sub>2</sub> - くり	1-	2 - < 5	5 ~ < 10	≥10
NC	+	0	+	+	2	36
50<80	0	0	0	0	+	4
35<50	0	0	0	+	1	5
20<35	+	0	0	+	3	17
10<20	0	0	+	+	4	15
6<10	+	+	+	1	2	4
3<6	0	+	+	1	1	1
1,5<3	+	0	0	0	0	+
0<1.5	+	+	+	+	+	Ó

### Cape Romanzof

LOW	VIS	iBIL	IT Y	(NN	4) 4	858
CEILING (10° FT)	< 1/2	ソ <sub>2</sub> - <1	1	2 - <5	5- <10	<u>≥</u> 10
NC	+	+	+	ī	7	9
50 <b0< td=""><td>0</td><td>0</td><td>0</td><td>Ö</td><td>1</td><td>1</td></b0<>	0	0	0	Ö	1	1
35<50	0	0	0	0	1	+
20<35	0	0	+	+	3	4
10<20	0	+	+	2	12	8
6<10	0	+	1	5	13	4
3<6	+	2	2	8	5	-1
1.5<3	+	+	+	+	+	+
0<1.5	3	5	1	1	0	+

#### Cape Newenham

LOW	VIS	iBiL	IT Y	(NN	1) 4	1668
CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1- <2	2 - <5	5 - <10	≥10
NC	+	+	+	1	4	11
50<80	0	0	0	+	+	7
35<50	0	Ó	+	0	+	1
20<35	+	+	+	+	2	4
10<20	+	+	+	2	7	11
6<10	+	+	2	7	8	8
3<6	÷	$\Box$	3	6	4	2
1.5<3	+	+	+	+	+	+
0<1.5	7	3	1	+	+	+

### King Salmon

LOW	VIS	iBiL	IT Y	(NN	1) 16	720
CEILING		γ <sub>2</sub> -	1-	2-	5 -	
(10° FT)	< 1/2	<1	<2	< 5	<10	[≥10]
NC	1	+	+	1	4	31
50<80	+	+	+	+	1	4
35<50	+	+	+	+	1	6
20<35	+	+	+	+	3	11
10<20	+	0	+	1	5	8
6<10	+	+	1	3	4	_2
3<6	+	+	1	3	3	1
1.5<3	+	+	+	+	+	+
0<1.5	1	1	1	+	+	+

### Port Heiden

LOW	VIS	IBIL	ΙΤΥ	(NN	1)	123
CEILING		<b>シ</b> ョー	1-	i -	5-	
(10° FT)	< 1/2	< 1	< 2	< 5	<10	≥10
NC	5	2	2	1	9	41
50<80	0	0	0	0	0	2
35<50	0	0	Ô	0	0	1
20<35	0	0	0	0	0	2
10<20	0	0	0	0	2	5
6<10	0	0	0	2	4	4
3<6	0	1	1	5	3	0
1.5<3	0	0	0	0	0	0
0<1.5	5	3	2	0	0	0

### Cold Bay

LOW	VIS	IBIL	ITY	(NN	1) 12	385
CLOUD CEILING (10° FT)	< 1/2	/ <sub>2</sub> - く1	1-	2 - <5	5 - < 10	≥10
NC	+	+	+	1	4	10
50 <b0< td=""><td>0</td><td>0</td><td>+</td><td>0</td><td>+</td><td>1</td></b0<>	0	0	+	0	+	1
35<50	0	+	+	+	1	1
20<35	+	+	+	+	4	6
10<20	+	+	+	1	9	10
6<10	+	+	1	5	12	5
3<6	+	1	4	8	8	1
1.5<3	+	+	1	1	+	+
0<1.5	2	2	1	+	+	+

### Nikolski

No Data Available

### St. Paul

LOW	VIS	IBIL	ITY	(NN	1) 9	425
CEILING		½-	1-	2-	5-	
(10° FT)	< 1/2	<b>1</b>	<2	<5	<10	≥10
NC	+	+	+	+	6	4
50<80	+	Ô	0	+	+	+
35<50	0	+	0	+	1	+
20<35	+	+	0	+	3	3
10<20	+	+	+	1	11	5
6<10	+	+	1	3	11	1
3<6	1	3	5	10	8	1
1.5<3	+	2	1	1	+	+
0<1.5	11	3	. 1	+	+	+

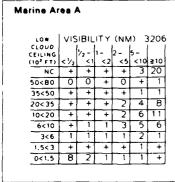
## Adak

LOW	VISIBILITY (NM) 14440							
CLOUD CEILING (10° FT)	< ½	ソ <sub>2</sub> - <1	1- <2	2 <5	5- <10	≥10		
NC	+	+	+	1	9	4		
50<80	+	+	0	+	+	+		
35<50	0	Ô	0	+	1	+		
20<35	Ò	+	+	+	7	1		
10<20	+	+	+	5	24	1		
6<10	+	+	1	10	14	+		
3<6	+	1	2	6	6	+		
1.5<3	+	+	+	+	+	0		
0<1.5	2	1	_1	1	+	0		

### Shemya

10#	VIS	BIL	ΙΤΥ	(NN	1) 10	211
CLOUD CEILING (10° FT)	< 1/2	ν <sub>2</sub> - <1	1 - < 2	2 - < 5	5 - <10	≥10
NC	+	+	+	+	3	7
50<80	+	+	+	+	+	+
35<50	+	+	O	+	+	
20<35	+	+	+	+	2	3
10<20	+	+	+	1	6	6
6<10	+	+	1	3	7	3
3<6	1	3	4	7	8	1
1.5<3	1	1	1	1	+	+
0<1.5	20	5	1	1	+	0

**August** 

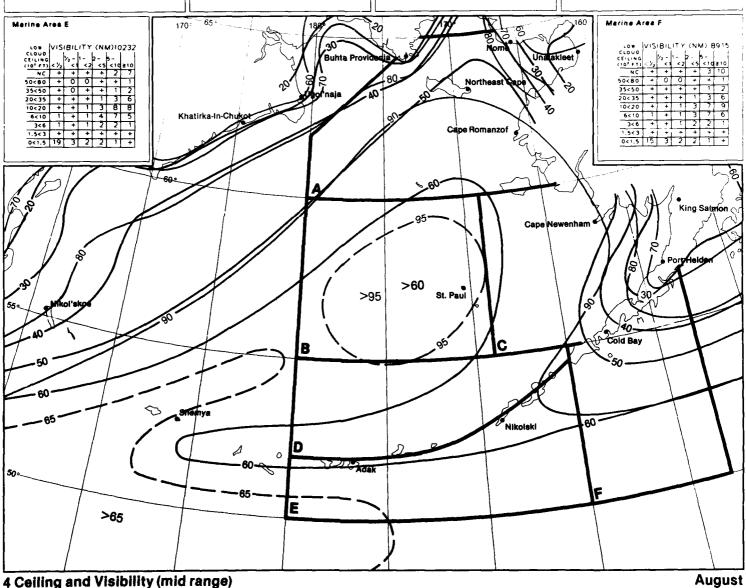


Marine Area B									
LOW CLOUD CEILING (10 <sup>2</sup> FT)	VIS	IBIL 1/2 - <1	IT Y 1- <2	(NN 2- <5	5 –	3277 			
NC	+	+	+	+	3	8			
50 <b0< td=""><td>+</td><td>0</td><td>0</td><td>+</td><td>+</td><td>1</td></b0<>	+	0	0	+	+	1			
35<50	0	+	0	+	1	1			
20<35	+	+	_+	1	3	8			
10<20	+	+	1	4	10	10			
6<10	+	1	2	6	6	3			
3<6	1	1	1	2	2	1			
1.5<3	+	+	+	+	+	+			
0<1.5	12	4	2	2	1	0			

LOW	VIS	BIL	ITY.	(NN	4) 7	729
CLOUD		l <sub>2</sub>	,_	J	5_	ļ
(10° FT)	< 1/2	/3 -     <1	<2	< 5	<10	≥10
NC	+	+	+	1	4	10
50<80	+	0	0	+	+	1
35<50	+	0	+	1	1	2
20<35	+	+	+	1	5	8
10<20	1	1	1	5	11	8
6<10	+	1	1	4	6	3
3<6	+	+	1	2	1	1
1.5<3	+	+	+	+	+	+
0<1.5	10	2	2	2	1	+

Marine Area C

Marine Ar	ea (	)				
LOW CLOUD CEILING (10° FT)	VIS	اBIL - ردا	1 -	(NN 2- <5	1) 6 5-  <10	420
NC.	+	+	+	+	3	7
50<80	+	0	+	+	+	1
35<50	+	+	0	+	1	2
20<35	+	+	+	1	4	8
10<20	1	+	1	3	8	8
6<10	1	+	1	4	6	4
3<6	+	1	1	2	2	
1.5<3	+	+	+	+	+	+
0<1.5	15	3	3	3	1	+



4 Ceiling and Visibility (mid range)

# 11-100

Nikol'skos	1					
10+	VIS	BIL	IT y	(NA	1) 5	248
CLOUD CEIL-NG	1	٠,٠	1	2 -	5.	
(10° FT)	< 1/2	(1	<2	< 5	<10	≩10
NC	+	+	+	1	2	37
50480	0	0	0	0	0	+
35<50	0	0	0	+	+	2
20<35	+	0	+	+	2	12
10<20	+	+	+	4	8	20
6<10	+	+	+	2	2	2
3<6	+	+	+	1	+	1
1563	+	0	ò	Ô	C	0

Khatirka-le	n-Ch	uko	1				_
LO# CLOUD	VIS	iBiL	iΤγ	(NN	t) ]	3162	
CEILING (10° FT)	< '-2	- را ا >	1- <2	2 - < 5	5 - < 10	<u>₹</u> 10	
NC	+	0	0	+	+	43	
50<80	0	ō	0	+	0	+	i
35<50	0	0	0	0	+	13	
20<35	Ò	0	+	1	2	17	
10<20	0	+	1	3	3	4	
6<10	+	+	1	3	1	1	
3<6	0	+	+	1	+	+	
1.5< 3	+	+	+	+	0	+	
0<1.5	6	+	Õ	0	+	+	

Nome

King Salmon

St. Paul

LO#	VIS	BIL	Y <b>T</b> 1.	(NN	4) 4	179
CFOOD		h.	١. ا	1	l_	i
CEILING	١.	/, -	'-	¥	- د	
CIO' FTI	< 1/2	< 1	< 2	< 5	<10	4.
NC.	+	+	+	+	2	32
50<80	0	0	0	+	+	+
35<50	+	0	0	+	+	2
20<35	0	+	+	1	2	21
10<20	+	+	1	3	7	14
6<10	+	+	+	2	3	- 2
3<6	+	+	+	1	1	1
1.5< 3	0	0	+	+	+	+
0<1.5	1	+	+	+	0	4

Ugol<sup>\*</sup>neja

Unalakleet

Port Heiden

luhta Prov	ider	nja				
LO#	Lvis	i <b>R</b> ii	IT Y	(NA	1) 4	1284
CLOUD	* ' '	1.	 I	ı ```	i i	1
CEILING		/2 -	1-	2 -	5-	
(10° FT)	<1/2	<1	<2	<5	<10	<b>≩</b> 10
NC	+	+	+	+	4	40
50<80	0	0	0	+	+	1
35<50	0	+	0	+	1	6
20<35	+	+	+	7	3	17
10<20	0	+	2	5	6	8
6<10	+	+	+	ī	1	1
3<6	+	+	+	+	+	+
1.5<3	0	+	+	+	0	0
0<1.5	1	0	0	0	0	+

Norheast	Cape	,				
Crono Fo#	_	181L  2-	17 Y	(NN	1) 4	505 
CEILING (10° FT)	< 1/2	/3 - 1	<2	<5	<10	≥10
NC	+	+	+	1	4	17
50<80	0	+	0	+	+	1
35<50	+	+	+	+	+	1
20<35	0	+	+	+.	4	9
10<20	0	+	1	3	11	15
6<10	+	+	1	7	9	2
3<6	+	+	2	2	2	+
1.5<3	0	0	+	+	+	+
0<1.5		2	1	+	+	0

LOW.	VIS	iBiL	TΤ	(NN	1) 16	00
CEILING		y2 -	1 -	2 '	5 -	
(10° FT)	< 1/2	<b>1</b>	< 2	< 5	< 10	≥10
NC	+	+	+	+	3	43
50<80	0	0	0	+	1	4
35<50	0	0	0	+	1	4
20<35	0	+	+	+	3	9
10<20	+	+	+	2	8	8
6<10	+	+	1	3	4	1
3<6	+	+	1	2	1	+
1.5<3	+	+	+	+	+	0
0<1.5	+	+	+	+	+	0

LOW	VIS	181	ITY	(NN	1) 2	661
CLOUD		ショー	1 - 1	2 -	5 -	
(10° FT)	< 1/2	<b>1</b>	<2	< 5		≥10
NC	0	0	0	1	7	39
50<80	0	0	0	0	1	4
35<50	0	0	0	+	2	7
20<35	0	0.	+	+	4	15
10<20	+	+	0	+	4	10
6<10	0	0	+	+	1	3
3<6	0	0	+	+	+	+
1.5<3	0	0	0	0	+	+
0<1.5	+	0	0	0	0	0

LOW	VIS	BIL	Y TI.	(NN	1) 4	156
CLOUD		/ <sub>2</sub> -	1 -	7 -	5 -	
(10° FT)	< 1/2	<sup>7</sup> <1	<2	໌ < 5	<10	≥10
NC	+	+	+	1	10	12
50<80	0	+	0	0	1	1
35<50	0	+	0	0	1	+
20<35	0	+	+	1	9	6
10<20	0	+	+	3	17	8
6<10	+	1	2	5	10	2
3<6	+	1	2	3	2	+
1.5<3	0	+	0	+	0	0
0<1.5	1	1	+	+	0	0

Cape Romanzof

Cold Bay

Shemya

157	1) 4	(NN	ITY	BIL	VIS	LOW
J				l. 1		CLOUD
l l	p-	2 -	1-	/2 -	l . :	CEILING
≥10	<10	< 5	< 2	< 1	< 1/2	(10° FT)
[16	9	+	+	+	+	NC
1	+	0	0	0	Ō	50<80
2		+	0	0	0	35<50
7	5	+	+	+	0	20<35
11	9	2	+	+	+	10<20
7	8	4	Ž	+	+	6<10
1	3	3	1	+	+	3<6
+	+	+	+	+	0	1.5<3
0	0	+	$\neg$	2	2	0<1.5

Cape Newenham

LOW	VIS	BIL	IT Y	(NN	1) 16	120
CEILING		1/2-	1 -	2 -	5-	
(10° FT)	< 1/2	<1	<2	<5	<10	≥10
NC	1	+	+	1	5	40
50 <b0< td=""><td>+</td><td>+</td><td>+</td><td>+</td><td>1</td><td>6</td></b0<>	+	+	+	+	1	6
35<50	+	0	+	+	2	7
20<35	+	+	+	1	5	12
10<20	+	+	+	1	4	5
6<10	+	+	+	1	2	1
3<6	+	+	+	1	1	1
1.5<3	0	+	+	+	+	+
0<1.5	+	+	+	+	+	0

LOW	VIS	BIL	ITY	(NA	1)	136
CLOUD CEILING (10° FT)	< ½	/ <sub>2</sub> - <1	!_ <2	2- <5	5 - <10	<u>≥</u> 10
NC	0	Ó	Т	3	4	58
50<80	0	Ō	0	0	0	3
35<50	0	0	0	0	0	5
20<35	0	0	0	0	Ü	10
10<20	0	0	0	0	2	7
6<10	0	1	0	0	3	1
3<6	0	0	0	1	0	Ö
1.5<3	0	0	0	Ö	Ō	Ō
0<1.5	T	Ō	0	0	0	0

LOW	VIS	BIL	JTY.	(NN	4) 1 °	196
CEILING		V	,_	l> -	5-	1
(10° FT)	< 1/2	<b>1</b>	<2	< 5	<10	≥10
NC	+	+	+	+	7	15
50<80	+	+	+	0	+	1
35<50	0	0	0	+	2	3
20<35	0	+	+	+	8	11
10<20	0	0	+	1	117	- 8
6<10	0	+	1	4	10	3
3<6	+	1	2	4	4	1
1.5<3	+	+	+	+	+	+
0<1.5	+	+	1	+	+	+

No Data	Available

LO#	Vi\$	IBIL	ΙTΥ	(NM	1) 8	3749
CLOUD		/ <sub>2</sub> -	1 –	2 -	5 -	
(10° FT)	< 1/2	L <1	< 2	<5	<10	≥10
NC	+	+	+	_	12	8
50480	+	+	0	+	+	+
35<50	+	+	0	0	2	1
20<35	+	0	+	+	8	4
10<20	+	+	+	1	19	6
6<10	0	+	1	3	9	1
3<6	+	1	3	5	4	+
1.5<3	+	1	1	1	+	+
0<1.5	4	1	1	+	+	0

LOW	VIS	IBIL	ITY.	(NN	1) 13	357
CLOUD CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1-	2 - <5	5- <10	≥10
NC	+	+	+	1	12	4
50<80	0	0	0	+	+	+
35<50	0	0	Ò	+	2	+
20<35	0	0	+	1	17	2
10<20	0	+	1	7	22	1
6<10	+	+	1	7	8	+
3<6	+	1	1	5	3	+
1.5<3	+	+	+	+	+	Ô
0<1.5	+	+	1	+	+	0

LOW	VIS	iBIL	ΙΤΥ	(NN	1) 10	395
CLOUD		1/2-	\ _	ا ۔ ا	5-	
(10° FT)	<1/2	/2 = <1		<5		≥10
NC	+	+	+	+	10	18
50<80	0	+	Ó	+	+	1
35<50	0	0	0	+	2	-1
20<35	0	+	+	+	7	7
10<20	+	+	+	2	11	7
6<10	+	+	1	3	6	ī
3<6	+	2	3	4	3	+
1.5<3	+	+	1	+	+	0
0<1.5	5	2	1	+	+	0

September

Nikolski

September

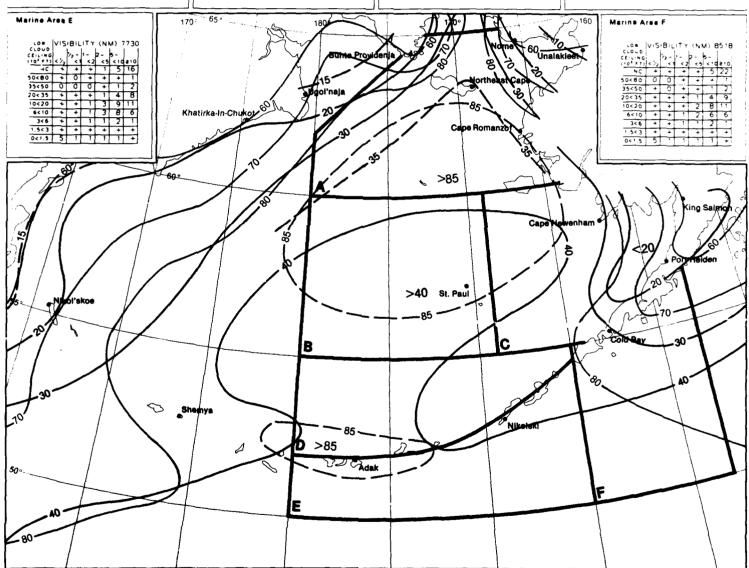
Marine A	.06	A				
LO#	VIS	iBiL	.ITY	(NA	1) 2	2063
CLOUD		1/2-	1 -	2 -	5 -	
(10° FT)	< 1/2	< 1	<2	< 5	<10	≩10
NC	+	+	+	+	4	23
50<80	+	0	+	+	+	2
35<50	+	0	+	+	1	3
20<35	+	+	+	1	3	12
10<20	+	+	+	1	8	15
6<10	+	+	1	- 1	5	5
3<6	+	+	+	1	2	1
1.5< 3	0	+	+	1	+	+
0<1.5	2	1	1	1	1	+

4 Ceiling and Visibility (mid range)

FO#	VIS		JTY I.	(NN	4) Z	?39
(10° FT)	< 1/2	½ − <1	1 - 2	2 −   <5	5- <10	<u>≥</u> 10
NC	+	+	+	1	5	16
50 <b0< td=""><td>0</td><td>0</td><td>+</td><td>0</td><td>+</td><td>+</td></b0<>	0	0	+	0	+	+
35<50	0	+	0	+	1	1
20<35	+	+	+	1	3	7
10<20	+	+	1	3	13	14
6<10	+	1	3	5	6	2
3<6	1	1	1	1	2	+
1.5<3	1	+	+	+	+	+
0<1.5	3	1	1	1	1	+

LO W	VIS	BIL	IT Y	(NN	1)	767
CLOUD		1/2-	1~	2 -	5 -	!
(10 <sup>2</sup> FT)	<1/2	<1	< 2	<5	<10	: בייב
NC	+	+	+	,	7	18
50 <b0< td=""><td>0</td><td>0</td><td>+</td><td>+</td><td>+</td><td>1</td></b0<>	0	0	+	+	+	1
35<50	+	0	+	+	-	1
20<35	+	+	+	1	5	9
10<20	+	+	1	5	12	9
6<10	+	+	1	3	4	3
3<6	+	+	1	2	1	1
1.5<3	+	+	+	+	+	+
0<1.5	4	2	2	2	1	+

rin <b>e</b> Aı						
-0*	V19	BiL	iΤΥ	(NN	1) 6	24
CEILING		ا. آگ <b>و</b> -	jı -	2 -	5 -	
(10° FT)	< 1/2	< +	<2	< 5	<10	≩10
NC	+	+	+	+	4	16
50<80	0	0	+	+	+	1
35<50	+	0	Ö	+	1	2
20<35	+	+	+	1	5	10
10<20	+	7	1	2	9	12
6<10	+	+	1	3	7	6
3<6	+	+	1	2	3	1
1.5<3	+	+	+	+	-	+
0<1.5	4	1	2	2	٠,	+



-102			
Nikol'skoe	Khatirka-In-Chukot	Ugol'neja	Buhte Providenje
CONTROL VISIBILITY (NM) 5510  CEILING  CEILING  10 FFT C 1 2	LOW VISIBILITY (NM) 3525  CLOUD CELLING 12-1-2-5- (10777) C1 C1 C2 C5 C10 210  NC + 0 + 1 1 1 61  50<80 + 0 0 + + + + +  35<50 0 0 0 + + 7  20<35 + + 1 2 1 9  10<20 + 1 1 4 3 3  6<10 + + 1 1 1 +  3<6 0 + + + + + +  1,5<3 0 0 + + + + + +  1,5<3 0 0 0 + + + + 0  0<1.5 1 0 0 0 0 0	CON VISIBILITY (NM) 5104 CLOUD CEILING	COW VISIBILITY (NM) 4518 CLOUD CEILING (10) FT)  NC + + + 1 7 37  50<80 0 0 0 0 + + + 1 35<50 + + + 1 2 6 17  10<20 + 1 2 5 5 4 6<10 + + + + + + 0 1,5<3 + + + 0 + 0 0<1,5<1 0 + 0 + 0
Norheast Cape	Nome	Unalakioot	Cape Romanzof
CEILING  CEILING  NC + + + + 5 12  50×80 + 0 0 0 + + 1  35<50 0 0 0 0 1 2  20<35 0 + 1 1 1 1 1 1 0 0	CLOUD CEILING (10° FT) (10° C) (10° FT) (10° C	COW VISIBILITY (NM) 2720  CEILING (10° FT) < 1/2 - 1 - 2 - 5 - 10 210  NC 0 0 + 11 31  50<80 0 + 0 + 1 2 5  20<35 + 0 + 1 8 12  10<20 + + 1 1 2 2  3<6 0 + + + 1 2 2  3<6 0 + + + + 1  1.5<3 0 + 0 + + + + + + + + + + + + + + + +	LOW VISIBILITY (NM) 4423 CLOUD CELLING (10) FT (1/2) <1 2 5 - 1 16 14  50:80 0 + + 1 16 14  50:80 0 + 0 + 2 1  20:35 + + + 1 16 6  10:20 + 1 1 3 15 4  6:10 + 1 1 2 4 1  3:6 + + + 1 1 + 1  1:5:3 0 0 0 0 + 0 5  0:1.5 1 2 + + 5 0
Cepe Newenhem	King Salmon	Port Heiden	Cold Bay
COM VISIBILITY (NM) 4523  CLOUD CEILING (10) FF) <1/2   2 -   5 -    NC	COW VISIBILITY (NM) 16550  CEILING (10° FT) < 1/2 - 1 - 2 - 5 - 1	LOW VISIBILITY (NM) 92  CLOUD CELLING NC 0 1 0 0 3 47  50<80 0 0 0 0 0 1 7  20<35 0 0 0 0 1 15  10<20 0 0 0 0 1 15  10<20 0 0 0 0 1 4 1  3<6 0 0 0 0 1 1 0  1,5<3 0 0 0 0 0 0  0<1.5 0 0 0 0 0  0<1.5 0 0 0 0 0 0  0<1.5 0 0 0 0 0 0  0<1.5 0 0 0 0 0 0  0<1.5 0 0 0 0 0 0 0  0<1.5 0 0 0 0 0 0 0	COW VISIB LITY (NM) 12355 CELLING CELLING NC 4 4 + 100 17 50:80 0 0 0 0 + 1 1 1 35:50 0 0 + 1 3 3 20:35 + + 1 14 10 10:20 + + 3 15 6 6:10 0 + 2 6 1 3:6 + + 1 2 2 + 1.5:3 + + + 1 + + 0
Nikoleki	St. Peul	Adak	Shemys
No Data Avaîlable	CEILING (10° FT) (10° C) (10° FT) (10° C) (10° FT) (10° C) (10° FT) (10° C) (10° FT) (10° C) (10° FT) (10° C) (10° FT) (10° C)	LOW VISIBILITY (NM) 14044  CLOUD CEILING NC 0 + + 1 16 4  50<80 0 + 0 + 1 + 1  35<50 0 0 0 + 5 1  20<35 + + + 2 26 3  10<20 + + 1 8 20 1  6<10 0 + 1 3 3 + 3<6 + + 1 1 1 1 + 4	COW VISIBILITY (NM) 10745 CELLING CELLING (10° FT) < 1/2

Merine Area A    COO   VISIBILITY (NM)   1179	Marine Area B   LOW CLOUD CEILING (10 $^{3}$ FT) $< \frac{1}{2}$ $> 1 - \frac{1}{2}$ $> 5 - \frac{1}{2}$ (10 $< \frac{1}{2}$ $> 1 - \frac{1}{2}$	Marine Area C  LOW CLOUD CEILING (10 FT) < 1/2 - 1 - 2 - 5 - 2   10 E10    NC + 0 + 1 1 10 16    50<80 0 0 0 0 + 1 1    35<50 0 0 0 0 + 2 2    20<35 + 0 + 2 5 11    10<20 + 1 1 4 13 9    6<10 + 1 3 4 3	Marine Area D  VISIBILITY (NM) 5794  CLOUD CELLING (10 ft) (2) 21 - 2 5 10 210  NC + + + 1 6 20  50480 0 0 0 + + 1  35450 0 + 0 + 1 2  20435 + + + 1 4 10  10420 + + 1 2 9 12
CLOUD CELLING ( $\frac{1}{2}$ ) $\frac{1}{2}$	CLOUD CEILING (10° FT) (2°) $\begin{pmatrix} 2 & 1 & 2 & 5 & -1 & 10 \\ 10° FT) & (2°) & (1) & (2°) & (5°) & (10° §10°) \\ \hline NC & + & + & + & 2 & 6 & 12 \\ \hline 50 < 80 & 0 & 0 & 0 & 0 & + & + \\ 35 < 50 & 0 & 0 & 0 & + & 1 & + \\ 20 < 35 & 0 & + & 0 & + & 5 & 14 \\ \hline 10 < 20 & + & + & 2 & 5 & 14 & 11 \\ \hline 6 < 10 & + & 1 & 1 & 4 & 6 & 3 \\ \hline 3 < 6 & + & + & + & 1 & 2 & 1 \\ \hline 1.5 < 3 & + & + & + & + & + & + \\ \hline \end{pmatrix}$	CEUING (10° FT) C 1/2 C 1 C 2 C 5 C 10° E 10 C 10° FT) C 1/2 C 1 C 2 C 5 C 10° E 10 C 10° FT) C 1/2 C 10° E 10° C 10° E 10° C 10° E 10° C 10° E 10° C 10° E 10° C 10° E	CELLING (10 <sup>2</sup> FT) < 12
0<1.5 1 1 1 2 1 1	0(1.5   1   1   1   1   1	3<6 + + + 1 2 1 1.5<3 + + + + + + + 0<1.5 1 1 2 2 1 +	6<10 + + 1 2 7 7 3<6 + + + 2 2 2 1.5<3 + + + + 1 + 0<1.5 1 1 1 1 +
Merine Area E 170	65 180		Marine Area F
VISIBILITY (NM) 7025   COUD   CELLING   Part   Pa		North ast Cab	Kleet 60
Nikol'skoe	>35	St. Paul	Cold Bay 30
She	100 35D	Nikglaki	75 35
50	80 Ada	-35 >35	F
4 Ceiling and Visibility (mid ra	inge)		Octobe

# II-104

Nikol'skoe	1					
.0*	į vis	BIL	(TY	(NA	4) 5	266
CEILING	١,	ر - د ا	1 -	2 -	5 -	
(10° FT)	< : 2		< 2	<u> </u>		₹10
NC	+	+	+	1	4	30
50<80	0	+	+	0	+	+
35<50	0	+	+	+	+	,
20< 35	+	+	1	1	4	12
10<20	1	1	2	6	9	23
6<10	+	+	+	1	1	7
3<6	+	+	+	+	+	+
1.5< 3	0	+	0	+	0	0
0<1.5	1	0	+	+	+	+

Khatirka-li	n-Ch	uko	t			
.0₩	vis	iBiL	IΤΥ	(NA	4) 3	3249
CLOUD CEILING	]	72 -	1 -	2 -	5 ~	
(10° FT)	15'5	< 1	<2	< 5	<10	≥10
NC	+	+	7	2	2	60
50<80	+	0	+	0	0	+
35<50	+	+	+	+	+	4
20<35	2	1	2	3	1	6
10<20	1	+	2	3	2	2
6<10	+	+	1	1	+	+
3<6	+	+	+	+	+	+
1,5< 3	0	+	+	+	+	0
0<1.5	1	0	0	0	O	0

Ugol'neja						
LO#	VIS	IBIL	JTY.	(NN	1) 4	1978
CLOUD	i	L.	1	1	1 1	
CEILING		1/2-	1 -	2	5 - '	i i
(10° FT)	< 1/2	< !	< 2	< 5	<10	≥10
NC	2	1	2	3	5	32
50<80	+	0	+	+	+	+
35<50	+	0	+	+	+	1
20<35	1	1	ī	3	3	6
10<20	6	4	5	6	4	5
6<10	1	+	ī	1	1	+
3<6	1	+	+	1	+	+
1.5<3	+	+	+	+	0	+
0<1.5	1	+	+	+	0	+

LO#	VIS	IBIL	IT Y	(NN	1) 4	29
CLOUD		1/2 -	ا ـ ا	ا <sub>م</sub> ا	K - 1	
(10° FT)	< 1/2	´´<1	<2	<5	<10	<b>≩10</b>
NC	+	+	1	2	9	39
50<80	0	0	+	+	+	+
35<50	0	0	+	+	1	2
20<35	+	1	Т	4	5	10
10<20	2	3	5	ó	4	4
6<10	+	+	+	+	+	+
3<6	0	+	+	+	+	+
1.5< 3	0	+	0	0	0	+
0<1.5	1	0	0	0	0	+

Norheast	Сере	•				
LOW CLOUD CEILING (10° FT)	V19	181L /2 - <1	1 -		5 -	<b>≩</b> 10
NC	+		+		7	10
50<80	0	+	0	+	+	+
35<50	0	+	0	+	+	+
20<35	+	+	1	2	12	7
10<20	+	1	3	10	16	4
6<10	+	+	2	3	4	1
3<6	+	+	1		1	+
1.5< 3	0	0	0	0	+	0
0<1.5	5	3	3	+	+	0

10 W	VIS	BIL	IT Y	(NN	1) 16	198
CLOUD		b	ļ, _	2 -	5 -	
(10° FT)	< 1/2	Í<1	<2	< 5	< 10	≥10
NC	+	+	+	+	6	42
50<80	+	+	+	+	1	3
35<50	+	+	+	+	1	3
20<35	+	+	+	2	6	5
10<20	+	1	1	3	6	4
6<10	+	+	1	2	2.	+
3<6	+	+	1	1	+	+
1.5<3	+	+	+	+	+	+
0<1.5	2	2	1	+	+	0

LO#	VIS	BIL	ITY	(NA	() 2	62
CLOUD		1/2 -	1 -	2 -	S	
(102 FT)	<1/2	2-1	< 2	< 5	< 10	≥10
NC	+	+	0	+	17	31
50<80	0	0	+	+	[ 2	Ž
35<50	0	+	+	+	3	3
20<35	+	+	+	1	8	7
10<20	0	+	+	2	7	5
6<10	+	+	+	1	1	ī
3<6	0	+	+	+	+	+
1,5<3	0	0	0	0	0	Ö
0<1.5	2	2	1	T	+	0

Unalakleet

Adak

LO#	VIS	BIL	IT Y	(NN	1) 4	L7 1
Crond		١,,	1.	ا ا	e	1
CEILING	< 1/2	/ 2 = < 1	<2	∠ -   <5	2.10	  ≥10
(10° FT)	< /2	· · ·		-53	210	£ 10
NC	+	1 1	+	_ 2	20	112
50<80	+	+	+	+	2	
35<50	+	+	+	+	2	1
20<35	+	1	+	2	17	-3
10<20	+	1	1	4	10	-2
6<10	+	1	1	4	3	,
3<6	+	+	+	1	1	+
1.5< 3	+	0	0	0	Ô.	0
0<1.5	4	2	1	+	+	0

	VIS	BIL	ITY	(NN	1) 4	214
CEILING	1	1/2 -	t	2 -	5 -	
(10° FT)	<1/2	_ < 1	<2	< 5	<10	≥10
NC	+	+	+	1	9	18
50<80	0	0	0	+	+	1
35<50	0	0	0	+	1	1
20<35	+	+	+	1	6	4
10<20	+	+	1	4	15	6
6<10	+	1	2	4	7	3
3<6	+	1	,	3	2	1
1.5<3	0	+	+	+	0	Õ
0<1.5	3	2	1	+	0	0

Cape Newenham

LO W	VIS	i BiL	IT Y	(NN	1) 15	95
CLOUD CEILING (10 <sup>2</sup> FT)	< 1/2	/ <sub>2</sub> - <1	1 - < 2	2- <5	5 - <10	≥10
NC.	1	+	+	1	8	47
50<80	+	+	+	+	1	4
35<50	+	+	+	+	2	4
20<35	+	+	+	1	4	6
10<20	+	+	+	1	4	3
6<10	+	+	+	Ĭ	Ž	1
3<6	+	+	+	1	1	1
1.5<3	+	+	+	+	+	+
0<1.5	1	1	1	1	+	+

King Salmon

St. Paul

10₩	VIS	BIL	ITY	(NN	1)	148
CLOUD		1/2 - 1	1~	2~	5-	
(10° FT)	< 1/2	<b>1</b> <1	<2	< 5	<10	≥10
NC	0	0	1	1	1	34
50<80	0	0	0	0	0	3
35<50	0	0	0	0	0	3
20<35	0	0.	0	0.	1	14
10<20	0	0	1	3	9	14
6<10	0	0	1	2	8	0
3<6	0	0	0	0	1	Ö
1,5<3	0	0	0	0	0	0
0<1.5	7	1	0.	0	0	0

LOW	VIS	BIL	IT Y	(NA	4) 11	938
CLOUD	ļ	1/2 -	ļ, _	2 -	5 -	į
(10° FT)	< 7,	<b>1</b> < 1	<2	< 5	<10	≥10
NC	+	+	+	1	12	' 8
50 <b0< td=""><td>0</td><td>+</td><td>0</td><td>0</td><td>+</td><td>•</td></b0<>	0	+	0	0	+	•
35<50	+	+	+	+	3	2
20<35	+	+	+	2	14	8
10<20	+	+	1	4	13	4
6<10	+	+	1	2	5	•
3<6	+	+	1	2	2	+
1.5<3	0	+	+	+	+	0
0<1.5	1	1	1	+	+	0

No Data Available

LO#	VIS	iBiL	YTI.	(NN	1) 8	394
CEILING		1/2 -	1-	2 -	5 -	
(10° FT)	< 1/2	<1	< 2	< 5	<10	≥10
NC	+	_+	_+	1_	20	7
50<80	0	0	0	+	+	+
35<50	+	0	+	+	1	1
20<35	+	+	+	1	12	5
10<20	+	+	1	5	24	3
6<10	+	+	1	4	6	+
3<6	+	7	1	1	1	+
1.5<3	+	+	+	+	+	Ö
0<1.5	1	1	ī	+	+	ō

CLOUD LOW	VIS	BIL	IΤΥ	(NN	1) 13	3576
CEILING	ļ	1/2 -	1 –	2-	5-	
(10° FT)	<1/2	<b>^</b> < 1	< 2	<5	<10	≥10
NC	0	+	+	1	19	4
50<80	0	0	0	0	1	+
35<50	Ó	+	+	+	5	1
20<35	+	+	+	3	29	2
10<20	+	+	T	8	16	+
6<10	+	+	1	3	2	+
3<6	+	+	+	1	+	0
1.5<3	0	0	+	+	+	0
0<1.5	1	1	1	+	+	0

LOW	i VIS	iBIL	IT Y	(N/N	10 10	138
CLOUD	i	l.		1	l. !	!
CEILING		1/2 -	1	2 -	5-	ĺ
(10° FT)	< 1/2	<1	< 2	<5	<10	₹.0
NC	+	+	+	+	14	71
50<80	0	+	0	+	+	+
35<50	0	+	0	+	2	2
20<35	+	+	+	1	17	10
10<20	+	+	1	4	16	3
6<10	+	+	1	3	4	+
3<6	+	1	1	1	1	+
1.5<3	+	+	+	+	+	0
0<1.5	7	1	1	+	+	0

Nikolski

Shemye

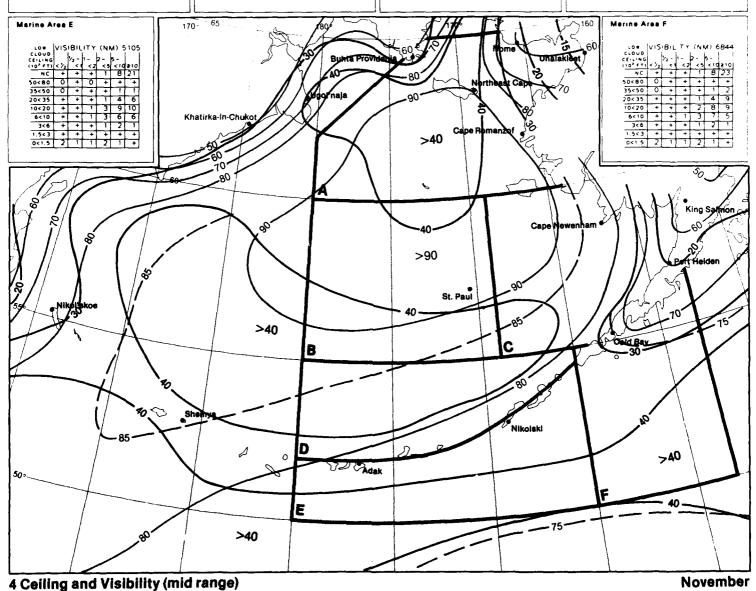
٤0*	VIS	BIL	ITY	(NN	1)	1060
CLOUD		/ <sub>2</sub> -	١,_	l	k	l
(10° FT)	< 1/2	\ \ < 1	<2	<5	<10	≩10
NC	0	0	+	+	2	12
50<80	0	0	+	+	1	+
35<50	0	0	+	0	+	1
20<35	0	+	+	2	4	26
10<20	1	1	4	8	7	8
6<10	+	1	2	2	3	3
3<6	+	+	+	1	1	+
1.5<3	0	0	0	+	+	0
0<1.5	1	2	2	2	1	+

Marine Ar	ea l	3				
10 M	VIS	IBIL	IJΥ	(NV	1) 2	259
CLOUD		١.	l.	_	5	. 1
CEILING	Ι.	1/2-	1 -	-		
(10° FT)	< 1/2	<1	<2	<5	_	≥10
NC	-+	+	[ 1]	1	4	14
50<80	0	0	0	+	+	
35<50	0	+	0	+	1	2
20<35	+	+	+	2	4	28
10<20	+	1	2	4	8	7
6<10	+	1	1	2	4	1
3<6	+	+	+	1	2	+
1.5<3	+	+	+	+	+	+
0<1.5	+	1	1	2	1	+

CLOUD CEILING	VIS	iBiL ½-	1T Y 1-	(NN 2-	1) 2 5-	559
(10° FT)	< 1/2	Î<1	< 2	<5	<10	≩10
NC	+	+	+	1	10	15
50<80	0	+	+	+	+	+
35<50	0	+	+	1	1	1
20<35	0	+	+	1	5	12
10<20	+	1	1	5	15	7
6<10	+	+	1	2	4	2
3<6	+	+	+	1	1	1
1.5<3	+	+	+	+	+	0
0<1.5	1	1	2	2	1	+

Marine Area C

LOW	VIS	BIL	ITY	(NN	1) 5	31
CLOUD		١.	l	_	L	
CEILING		1/2 -	1	2 -	5 -	
(10 <sup>3</sup> FT)	< 1/2	< 1	< 2	< 5	<10	<b>≩10</b>
NC	+	_+	+	1	9	20
50<80	+	0	+	+	+	1
35<50	+	+	+	+	2	1
20<35	+	+	+	1	5	7
10<20	+	+	1	2	8	8
6<10	+	+	1	3	8	6
3<6	+	+	+	2	3	2
1.5<3	+	+	+	+	1	+
0<1.5	1	1	1	2	1	+



# 11-106

.0∗	VIS	i Bi L	1T 7	(NA	A) 5	o <b>4</b> 21
CLOUD		l:	J1	2-	5-	ļ
(10° FT)	672	<b>(</b> <1	< 2	< 5	< 10	₹10
NC	+	+	+	1	4	26
50<80	+	0	0	+	0	,
35<50	0	+	0	+	+	2
20<35	+	+	1	2	3	11
10<20	-2	3	3	7	9	21
6<10	+	+	+	1	+	+
3<6	+	+	+	+	0	+
1.5< 3	+	0	0	ō	0	0
0<1.5	1	+	+	+	+	+

Khatirka-li	1-Ch	uko	1			
.0*	VIS	iBit.	IT Y	(NN	1) ]	3257
CEILING (10° FT)	ψ,	2~	1 ~ 2	2 - <5	5- <10	≥10
NC		1	3	3	2	56
50<80	+	0	0	+	0	+
35<50	+	+	1	+	1	4
20< 35	1	1	2	4	2	6
10<20	1	1	2	2	1	1
6<10	1	+	1	1	+	+
3< 6	+	+	+	+	+	+
1.5< 3	+	0	+	+	+	0
0<1.5	1	Ö	+	0	0	+
		<u> </u>	<u>.                                    </u>		L	

LO#	VIS	iBiL	ΙŤΥ	(NN	1) 5	190
Crono	i	<b>.</b>	ì. I	L		}
CEILING	1.,.	/2 -	٠	<5	3	
(10' FT)	< 1/2	<1	<2	< 3	< 10	₹10
NC	3	2	3	5	7	35
50<80	+	0	+	+	+	+
35<50	+	+	0	+	+	1
20<35	2	1	1	2	3	6
10<20	5	3	3	4	3	3
6<10	1	1	1	1	1	+
3<6	+	+	+	+	+	+
1.5<3	0	0	+	+	0	0
0<1.5	3	+	+	0	Ö	+

Ugol'naja

Unalakleet

Port Heiden

Adak

Buhta Prov	uhte Providenje								
LO#	VIS	BIL	ΙΤΥ	(NN	1) 4	45			
CEILING		ار دولا	h	2-	<b>b</b> -				
(10° FT)	< 1/2	< 1	<2	<u>`</u>	<10				
NC.	+	+	ᆫᆜ	و	13	49			
50<80	0	0	+	+	+	+			
35<50	+	+	+	+	+	-			
20<35	1	1	1	3	_3	5			
10<20	2	2	3	4	2	2			
6<10	+	+	+	+	+	+			
3<6	0	+	+	+	+	+			
1.5<3	0	0	0	0	0	0			
0<1.5	1	0	0	+	0	0			

Norheast	Cape	)				
LO#	VIS	i BiL	jΤΥ	(NN	4) ]	1916
CLOUD		١,.	١. '	١,	ا ا	1
CEILING		77.	ا - ا	Z	7	
(10° FT)	< 1/2	_ < 1	< 2	<5	<10	≩10
NC	+	+	+	4	15	31
50<80	+	0	0	0	+	+
35<50	0	+	+	0	+	+
20< 35	+	+	1	2	5	1
10<20	+	1	3	7	11	3
6<10	+	+	1	3	3	+
3<6	+	+	+	+	+	+
1.5<3	0	0	0	+	+	0
0<1.5	3	2	1	+	0	0

10#	VIS	BIL	IT Y	(NN	1) 16	38
CEILING		- ولا	1 -	2 -	5 -	
(10° FT)	< 1/2	T<1	<2	<sup>*</sup> < 5	<10	₹10
NC	+	+	+	1	9	50
50<80	+	+	+	+	1	2
35<50	+	+	+	+	2	1
20<35	+	+	+	, 2	5	3
10<20	+	+	1	3	4	2
6<10	+	+	1	1	1	+
3<6	+	+	1	1	1	+
1.5<3	+	+	+	+	+	0
0<1.5	2	2	1	T +	+	0

LOW CLOUD CEILING (10° FT)	VIS	IBIL '⁄₂-	ITY 1 2	1	1) 2 5 -   <10	
NC	+	+	+	1	20	29
50<80	Ò	+	0	+	2	2
35<50	+	+	+	+	3	3
20<35	+	+	+	2	9	5
10<20	+	+	1	2	6	2
6<10	0	+	+		1	1
3<6	0	+	+	+	+	+
1.5<3	0	0	+	0	+	0
0<1.5	2	2	T	1	+	0

Cape Rom	enzo	f			_	
LOW	l vis	BIL	ITY	(NN	1) 4	024
CLOUD		1.	1	1	1	1 1
CEILING		1/2 -	1 -	2 - 1	5 -	
(10° FT)	< 1/2	< 1	<2	< 5	<10	≥10
NC	1	2	2	5	30	11
50<80	+	+	+	+	2	7
35<50	+	+	+	+	1	1
20<35	+	1	+	2	8	1
10<20		1	1	4	11	+
6<10	+	1	1	2	2	+
3<6	+	+	1	1	1	0
1.5<3	0	+	0	0	+	0
0<1.5	3	2	1	+	0	0

LOW	VIS	IBIL	ITY	(NN	1) 4	120
CLOUD	Ì	١. ا	l. 1		_	
EILING		1/2 -	1-	2-	ا - د	1
10° FT)	< 1/2	< 1	<2	< 5	<10	₹10
NC	+	+	1	1	12	20
0<80	+	0	0	+	+	1
35<50	Ò	0	+	+	1	ī
20<35	+	+	+	1	5	3
10<20	+	1	1	5	11	4
6<10	1	1	2	5	6	2
3<6	+	+	1	1	1	+
1.5<3	0	0	+	+	+	0
0<1.5	4	3	1	+	0	0

LOW	VIS	IBIL	ITY	(NA	1) 16	33
CEILING	ļ	1/2 -	ļ,_	2-	5-	
(10° FT)	<1/2	(<1	<2	ົ<5	<10	≥10
NC	1	1	1	1	11	46
50 <b0< td=""><td>+</td><td>+</td><td>+</td><td>+</td><td>2</td><td>3</td></b0<>	+	+	+	+	2	3
35<50	+	+	+	+	2	3
20<35	+	+	+	1	4	4
10<20	+	+	+	1	3	2
6<10	+	+	+	1	2	1
3<6	+	+	+	1	1	1
1.5<3	+	+	+	+	+	+
0<1.5	1	2	2	1	+	+

King Salmon

St. Paul

LOW	VIS	IBIL	ITY	(N <sub>N</sub>	1)	109
CLOUD		1/2-	1-	2 -	5-	
(10° FT)	< 1/2	<b>~</b> <1	<2	<5		≩10
NC	1	0	0	Ò	1	38
50<60	0	0	0	0	0	1
35<50	Ĵ	0	Ō	0	0	2
20<35	0	0	0	0	4	9
10<20	0	0	0	0	11	12
6<10	0	0	1	2	9	0
3<6	0	0	0	3	1	0
1.5<3	0	0	0	0	0	0
0<1.5	2	3	0	2	0	0

LOW	VIS	BIL	ITY.	(NN	1) 12	315
CEILING	ĺ	Y2-	1-	2-	5-	
(10° FT)	< 1/2	<b>1</b> <1	<2	<5	<10	≥10
NC	+	+	+	1	11	18
50<80	0	+	+	+	1	1
35<50	+	+	+	+	3	2
20<35	1	1	1	3	12	6
10<20	+	+	1	4	12	4
6<10	+	+	1	3	4	1
3<6	+	1	1	2	2	+
1.5<3	0	+	+	+	+	+
0<1.5	2	2	1	+	+	+

Cold Bay

Shemya

Ni	kol	8	į.

Cape Newenham

No Data Available

<b>LO₩</b>	l vis	iBiL	ΙΤΥ	(NA	4) 9	926 i
CLOUD CEILING (10° FT)	<1/2	½- <1	1- <2	2 ~ <5	5- <10	≥10
NC	+	+	+	1	18	6
50<80	0	0	+	0	+	+
35<50	+	+	+	+	2	1
20<35	1	+	-	2	15	4
10<20	1	1	1	5	20	2
6<10	+	+	1	3	4	+
3<6	+	7	1	2	1	+
1.5<3	+	+	+	+	+	0
0<1.5	2	1	+	+	0	0

LO#	VIS	SIBIL.	JTY.	(NN	1) 14	1074
CLOUD CEILING (10° FT)	< 1/2	/ <sub>2</sub> - <1	1-	2 - <5	5 - < 10	≥10
NC	+	+	+	1	17	2
50<80	0	0	0	+	1	+
35<50	0	0	+	+	6	1
20<35	0	+	+	3	28	1
10<20	+	+	2	8	16	+
6<10	+	+	1	4	2	Õ
3<6	+	+	+	1	+	0
1,5<3	+	0	+	+	+	0
0<1.5	1	1	1	1	+	0

268	1) 10	(NN	ITY	BIL	VIS	LOW
	5-	2-	1-	γ <sub>2</sub> -		CEILING
≥10	<10	<5	<2	<b>1</b> <1	< 1/2	(10° FT)
11	15	+	+	+	+	NC
+	+	0	0	0	0	50<80
1	2	+	+	0	+	35<50
9	18	2	+	+	+	20<35
2	13	4	1	1	+	10<20
+	3	3	1	1	+	6<10
+	1	2	2	1	+	3<6
0	+	+	+	+	+	1.5<3
0	+	+	1	2	2	0<1.5

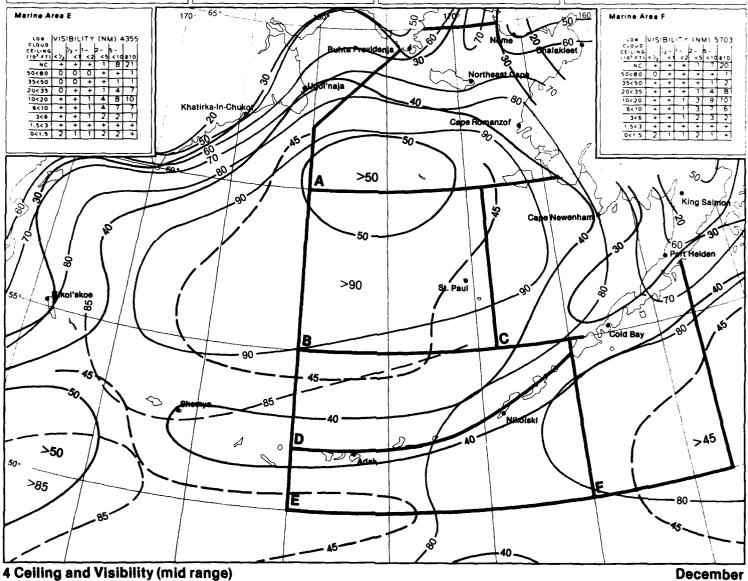
December

Marine Area A									
LOW	l vis	181L	JT Y	(NN	<b>(</b> )	1817			
CLOUD CEILING (10 <sup>3</sup> FT)	< 1/2	/ <sub>2</sub> - <1	1-	2 - <5	5- <10	≥10			
NC	+	+	ī	1	2	6			
50<80	0	+	+	+	+	+			
35<50	0	0	+	+	+	1			
20<35	7	+	1	3	3	28			
10<20	7	2	9	8	5	6			
6<10	+	1	1	1	1	2			
3<6	+	+	+	+	+	1			
1.5<3	+	0	+	+	+	+			
0<1.5	4	3	4	3	1	+			

LO#	VIS	BIL	ITY	(NN	4) 2	86
CLOUD		1,	Į.,	l-	ا	
CEILING		/2-		2~	٦- ا	l <b>.</b>
(10° FT)	< 1/2	<1	<2	<5		≥10
NC	+	+	1,	1	4	11
50<80	0	0	+	+	1	1
35<50	+	0	+	+	1	3
20<35	+	+	2	3	5	26
10<20	1	2	4	4	7	7
6<10	+	1	1	.2	2	3
3<6	+	+	+	1	+	2
1.5<3	0	0	+	+	0	+
0<1.5	3	2	3	3	1	+

			. +			
LOW CLOUD	\ V 13	BIL	11 7	(NN	1) _	2891
CEILING	Į.	1/2-	1-	2-	5~	
(10° FT)	< 1/2	<b>1</b> <1	<2	<5	<10	≩10
NC	+	+	+	1	6	13
50<80	0	0	+	+	1	1
35<50	+	+	+	+	2	4
20<35	1	1	+	2	5	15
10<20	+	1	2	4	11	9
6<10	+	+	1	2	3	2
3<6	+	+	+	1	+	1
1.5<3	0	+	+	0	+	+
0<1.5	2	2	3	3	2	+

Marine Area D									
CLOUD CLOUD		1B1L	IT Y  ,_	(NN)	1) 4  s_	984			
(10° FT)	< 1/2	<1	< 2	<5	<10	≥10			
NC	+	+	+	7	7	20			
50<80	0	0	+	+	1	1			
35<50	+	+	+	+	2	2			
20<35	+	+	+	1	3	7			
10<20	+	+	1	2	9	11			
6<10	+	+	1	3	8	7			
3<6	+	+	1	2	3	2			
1.5<3	+	+	+	+	1	+			
0<1.5	2	1	1	2	1	+			



# Map 5. Visibility thresholds

TABLE - Percent frequency of visibility (nautical miles).

Albers Equal—Area Conic Projection

# Graphs: Visibility thresholds

VISIBILITY (NM)	<u>%</u>	Percent frequency of visibility of various designated marine areas and coastal state.						for
<.5	1.2							
.5 <1	2.9	(2.9% o ≥1/2 na						
1<2	1.2	similarly						
2 < 5	3.2		l _	J .	_ ا	! _	1	ı
5 < 10	30.7	Nautical miles Kilometers	.5	1 2	4	10	10	1
≥10	60.8	Miorifierers	<u> </u>				20	}
N=	342•	N = Observat	tion co	unt.				

5 Legend

Legend 5

Visibility is a term that denotes the greatest distance from an observer that an object of known characteristics can be seen and identified with the unaided eye. When the visibility is not the same in all directions, the greatest distance common to one-half or more of the horizon circle is determined. Visibilities are difficult to measure at sea because of the lack of reference points. Climatically, many low visibility observations probably are missed because the observer is too busy with other duties (this is a form of fair weather bias). Also, some observers seem to report reduced visibilities at night because of darkness, though this tendency has abated in recent years. However, the coarseness of the visibility intervals (see code table) tends to minimize the problem, thereby permitting the summarized data to be relatively consistent. Visibilities greater than 25 nautical miles should be interpreted cautiously because the earth's curvature makes it impossible to see that distance horizontally from the bridge of most ships.

~~~	Visibility (vv)	MO Code, 1982) Visibility (vv)	Code
Code	in m/km	in yd./naut. mi.	
figs.	m m/Km	m yamaat. mi.	figs.
90	less than 50 m	less than 55 yd.	. 90
91	50 but less than 200 m	55 but less than 220 yd.	. 91
92	200 but less than 500 m	220 but less than 550 yd.	. 92
93	500 but less than 1000 m	550 but less than 1/2 n. mi	
94	1 but less than 2 km	1/2 but less than 1 n. mi.	
95	2 but less than 4 km	1 but less than 2 n. mi.	
96	4 but less than 10 km	2 but less than 5 n. mi	
97	10 but less than 20 km		
98	20 but less than 50 km		
99	50 km or more	27 n, mí, or more	99
The	visibility ranges correspo	nding to various weather ty	pes
are <b>90</b>	as follows:	nding to various weather ty	, 90
are		-	
are 90 91 92	as follows:	zzle Fog. thick haze	90 91 92 93
are 90 91 92 93 94	as follows:  Heavy snow, heavy dri	zzle Fog. thick haze rate drizzle	90 91 92 93 94
are 90 91 92 93 94 95	as follows:  Heavy snow, heavy dri  Moderate snow, moder Heavy rain	zzle Fog. thick haze	90 91 92 93 94 95
are 90 91 92 93 94 95 96	as follows:  Heavy snow, heavy dri  Moderate snow, moder  Heavy rain  Moderate rain	zzle Fog. thick haze rate drizzle Mist. haze	90 91 92 93 94 95 96
are 90 91	as follows:  Heavy snow, heavy dri  Moderate snow, moder  Heavy rain  Moderate rain	zzle Fog. thick haze rate drizzle	90 91 92 93 94 95

5 Legend

Legend 5

Nikol'skoe		Khatirka-In-Chukot		Ugol'neje		Buhta Providenja	
VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	3	VISIBILITY (NM)	<u>7</u>	VISIBILITY (NM)	<u>z</u>
<.5	5.1	<.5	5.9	<.5	14.2	<.5	4.3
.5 <1	5.1	.5 <1	3.0	.5 <1	8.1	.5 <1	5.0
1<2	6.1	1<2	9.8	1<2	11.5	1<2	10.5
2 <5	12.1	2 < 5	12.0	2 <5	14.6	2 < 5	12.8
5 < 10	18.2	5 < 10	7.8	5 < 10	11.9	5 < 10	17.7
≥10	53.4	≥10	60.7	≥10	39.6	10 ≥10	49.6
N=	5899	N=	3702	N=	5289	N=	4710
Norheest Cape		Nome		Unalakieet		Cape Romanzof	
VISIBILITY (NM)	3	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3
<.5	4.0	<.5	4.6	<.5	3.3	<.5	9.2
.5 <1	4.8	.5 <1	4.6	.5 <1	2.1	.5 <1	7.1
1<2	7.8	1<2	5.2	1<2	3.0	1<2	5.3
2 < 5	13.6	2 <5	9.4	2 <5	6.2	2 < 5	13.8
5 < 10	40.6	5 < 10	22.9	5 < 10	24.8	5 < 10	28.8
≥10	29.2	≥10	53.3	≥10	60.5	≥10	35.8
N=	8664	N=	22020	N=	15445	N=	17545
Cape Newenhem		King Salmon		Port Heiden		Cold Bay	
VISIBILITY (NM)	3	VISIBILITY (NM)	ž	VISIBILITY (NM)	3	VISIBILITY (NM)	3
<.5	5.1	<.5	1.9	<.5	4.3	<.5	4.4
.5 <1	4.6	.5 <1	2.2	.5 <1	4.1	.5 <1	3.8
1<2	7.5	1<2	3.1	1<2	2.8	1<2	5.5
2 < 5	14.9	2 < 5	5.3	2 < 5	6.5	2 < 5	13.3
5 < 10	36.6	5 <10	21.4	5 < 10	19.9	5 < 10	42.5
≥10	31.2	≥10	66.1	≥10	62.4	≥10	30.5
N=	19026	N=	19082	N=	2250	N=	13895
Nikoleki		St. Paul		Adek		Shemye	
VISIBILITY (NM)	<b>%</b>	VISIBILITY (NM)	<u> 3</u>	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3
<.5	20.3	<.5	6.7	<.5	1.8	<.5	3.6
.5 <1	1.8	.5 <1	5.5	.5 <1	2.1	.5 <1	4.3
1<2	1.4	1<2	5.5	1<2	5.3	1<2	7.3
2 < 5	5.9	2 < 5	15.6	2 <5	18.0	2 < 5	17.0
5 <10	35.7	5 < 10	56.0	5 < 10	68.0	5 < 10	51.2
≥10	34.9	≥10	10.8	≥10	4.9	≥10	16.6
N=	2223	N=	11605	N=	22604	N=	19321
anuarv		<u> </u>	· · · · · · · · · · · · · · · · · · ·			5 Visibility	Three

January

5 Visibility Thresholds

Marine Area D

VISIBILITY (NM)	2	VISIBILITY (NM)	3	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	7.
<.5	5.8	<.5	6.9	<.5	4.5	<.5	3.1
.5 <1	6.2	.5 < 1	5.9	.5 < i	3.8 ¦	.5 ::	2.7
1<2	12.4	1<2	9.2	1<2	6.6	1<2	5.1
2 < 5	14.2	2 <5	15.3	2 < 5	12.1	2 < 5	11.5
5 <10	15.7	5 < 10	23.1	5 < 10	28.8	5 < 10	31.3
≥10	45.7	≥10	39.6	≥10	44.2	≥10	46.2
N=	2787	N=	5098	N=	3785	N=	6925
Merine Area E	173	65	180	170°	7	160 Marine Area F	
VISIBILITY (NM)	3	922	<del></del>	4		VISIBILITY CNM	, ,
<.5	3.7			VV (NM) % VV (N	m ž	<.5	5.2
.5 <1	3.4	ું -	VV (NM) Z	<u> </u>		1> 5.	2.9
1<2	4.9		<.5 4.	8 (	1 4.5	1<2	5.1
2 < 5	12.8		≥ 1.5 <1 6.		2 8.31	2 < 5	12.1
5 <10	34.4		) 1<2 12.	0 2	(5 18.21	5 < 10	33.8
≥10	40.7	N	2 < 5 13.	3 2 3 101-	10 34.8	≥10	40.9
N=	5852	arr	4	3 3 (10 32	10 25.0	N=	6808
			≥10 50. N= 225	/ =10 23.3	= 132		
1 / 50/ W.	60:-		N= 225	2 N= 428 "			, ~ ~ )
VV (NA			<del></del>	<del></del>		Z 1	// } a
\(\sigma \)\(\sigma \)\(\sigma \)\(\sigma \)\(\sigma \)\(\sigma \)\(\sigma \)\(\sigma \)	5 1 TOTAL	2 VV (NM) -	•		N (NM) 2	VV (NAME)	1 2/59
1.5 <1	7 - 4 1.5	7.5	VV (NM) %	VV (NM)		2.5	ا کا لہا
1/2	7 31 3	A . 1 - T. (	3 <.5 3.	6 <.5 9.2		3, 101	1 3 100
2 <5	/// a l	7 0 1 9.7	.5 < 1 5.	6 .5 < 1 6.0		14 - 31	\0°
5 < 10 1	16 - 13 1	6 6 1 2 8.1	1<2 10.		. 7	2 3 22	ا کے
≥10 / N= 5;	J 31 1	7 1 5 9.3	2 < 5 14.	1 265 16.21		19 - 27 5. /	70 /]
55° 1 1 4	05 $-0$ $4$	1 5 23.0	5 < 10 17.		3 7	1460 N	
	N= 2	53	≧10 48.		2660	N= 1	
	+	N = 248	N= 180		N= 2000	1 manual 1	
1/		-					
1/	VV (NM)					VV (NM) 5.2	l
V	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	VV (NM)	VV (NM) %	VV (NM) 3	VV (NM)	1 4.5	\
	1 5 7.			1	<.5 3.	'   [ ] " ~	1
1	1<2 2.8	.5 <1 3.1		, i	1 5 61 3	152	$I_{c}$
1	- \	1 1 2 3 111	.5 <1 2. 1 <2 5.		1<2 4	41 / 2	<b>1</b> \
1	5 12.1	2 < 5 11 A		Y 1	1 7/7 1	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	6
1	345 34.0			~l	1 = 10 34	+.01 ~10 40	
500	N= 42.8 N= 3175	' ≤10 44.0 l	•	J   J	>10 4	3.31 1 45	
1	31/5	N= 3767	≥10 43. N= 350			405 N-	\
]	-		.1- 350	·   14- 30/.	1		\ 1
	1				T -	1	\
/	1	1					\ }
	1						\
E Walhiller The	vecholds			<del></del>			lanuar:
5 Visibility Thre	esnoias						January

Marine Area C

Marine Area B

<b>5</b> .9	Khetirka-In-Chukot  VISIBILITY (NM)  <.5	<u>*</u>	Ugol'neja VISIBILITY (NM)	<u> </u>	Buhta Providenja  VISIBILITY (NM)	7
5.9	]]	_	VISIBILITY (NM)	<u>%</u>	VISIBILITY (NM)	*
	<.5					•
7 7	11	5.5	{\frac{1}{2}}	12.6	<.5	4.6
7.3	.5 <1	2.7	.5 <1	7.1	.5 <1	3.9
6.0	1<2	6.3	1<2	10.6	1<2	6.7
11.4	2 <5	9.0	2 <5	12.5	2 <5	10.6
16.3	5 < 10	7.0	5 < i0	12.0	5 < 10	15.0
53.0	≥10	69.5	≥10	45.3	<u>≥</u> 10	59.2
5464	N=	3250	N=	4843	N=	4361
	Nome		Unalakleet		Cape Romanzof	
<b>%</b>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	3	VISIBILITY (NM)	3
3.7	<.5	3.4	<.5	2.6	<.5	8.4
4.1	.5 <1	3.3	.5 <1	2.5	.5 <1	8.2
8.6	1<2	4.4	1<2	3.0	1<2	6.5
14.8	2 <5	8.3	2 < 5	6.1	2 < 5	14.2
40.3	5 < 10	19.3	5 < 10	23.6	5 < 10	29.9
28.5	<u>≥</u> 10	61.4	≥10	62.2	≥10	32.7
8840	N=	20107	N=	13990	N=	16381
	King Salmon		Port Heiden		Cold Bay	
<u>z</u>	VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	ž
3.4	<.5	1.6	<.5	7.1	<.5	5.1
3.9	.5 <1	2.7	.5 <1	3.6	.5 <1	4.0
6.7	∬ 1<2	3.5	1<2	2.3	1<2	5.9
15.7	2 <5	6.1	2 <5	9.5	2 < 5	12.9
34.4	5 < 10	19.0	5 < 10	19.0	∫ 5 <10	38.7
35.9	≥10	67.1	≥10	58.6	≥10	33.4
17495	N=	17374	N=	2024	N=	12682
	St. Paul		Adak		Shemye	
<u> </u>	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	3
15.9	<.5	11.5	<.5	1.9	<.5	5.3
2.0	.5 <1	6.2	.5 <1	2.5	.5 <1	5.4
1.2	1<2	5.8	1<2	5.3	1<2	6.9
5.8	2 < 5	14.5	2 < 5	18.0	2 < 5	16.6
37.7	5 < 10	50.9	5 < 10	67.2	5 < 10	46.1
١٠,١	11 2 \ 10	20.2	) 3 1 10		11 2 10	- · · ·
37.7	1 ≥10	11.1	≥10	5.1	≥10	19.7
	16.3 53.0 5464 3.7 4.1 8.6 14.8 40.3 28.5 8840 3.4 3.9 6.7 15.7 34.4 35.9 17495	16.3   5 < 10   53.0   ≥ 10   N=      Nome	16.3	16.3	16.3	16.3

February

Marine Area D

VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	2	VIŞIBILITY (NM)	3	VISIBILITY (NM)	<u>z</u>
<.5	7.1	<.5	7.0	<.5	4.9	<.5	3.1
.5 <1	7.9	.5 <1	7.5	.5 <1	4.6	.5 <1	2.8
1<2	9.2	1<2	13.7	1<2	6.8	1<2	5.7
2 < 5	16.0	2 <5	17.3	2 < 5	12.2	2 < 5	12.8
5 <10	24.2	5 <10	20.2	5 <10	26.6	5 < 10	31.2
≥10	35.7	≥10	34.3	≥10	44.8	≥10	44.4
N=	1617	N=	6409	N:-	3929	N=	7088
Marine Area E	170	· 65°	189	170°	2	2160 Merine Aree F	
VISIBILITY (NM)	3 /			VV (NM) % VV (N	M) 3 1	VISIBILITION	D 2
<.5	3.9	الم الما الما الما الما الما الما الما	VV (NM) %	1		<.5	5.1
.5 <1	2.8 5.1		<.5 7.4	. 2.5 3.7	/	.5 <1	2.7
2 < 5	12.4	/	5 1.5 <1 10.		2 5.5 ( <sup>1</sup>	2 < 5	11.6
5 <10	34.8	a Mu	) 1<2 H. 2<5 17.4	2 0.0	(5 13.8)	5 < 10	33.2
≥10	41.0	N	2 < 5 17.4 5 < 10 15.9	' I - 1 - 1 - 2	10 34.9	≧10	42.7
N=	6105   / 		≧10 38.0		10 29.5	N=	6919
7			N= 969	N= 378 N	= 289		
D/VV (N)	M) 60:		1				<i>a</i> ~ 7 ]
1 5.5	2 1 xxx		<del></del>	+	-   v	V (NM)	// } 4
\\ \frac{1.5 < 1}{}	5.5	S VV (NM) %	VV (NM) %	VV (NM) 2	IV (NM)	∠s 3.9\ \\	1 /3
1/2	8.5 1.5 <1	<.5 7.8	<.5 6.2	<.5 7.6	<.5 5.2	5<1 3.6	1 2 /5
2 <5	6 ~ 1 ' ' \	8 0 1 1 1 1 1 4	.5 <1 7.2	•	5<1	1<2 3.7	المركز كر
< / ۱	21 1 1 - \ 1	9 0 2 2 0.8	1<2 13.	1<2 14.1		4 3 31	ا کم
1 / N= 4/	8.4	10.0	, , ,		2 < 5 13.8 5 < 10 25.6	19.2	// 97
55. 2	256 N- 45	.0/ ≥10 25.0	1	2 3 10 22.5	≥10 41.5	1288 W	
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	7	N= 283	N= 2251	N= 3753	,,	\	
1/	VV	-				, (MM) ×	į
1/	VV (NM)	VV (NM)	· . — —	Ţ	VV (NM)	5.11	
Y	15.3 5.2	1 / = 1	VV (NM) %	VV (NM) %	1 5 3.	4 2.5	\
	1<2 3.2	5<1 4.2	<.5 4.0		5/1 2.	91.5 4.9	1 1
1	2 < 5 . 7	.5 <1 3.2 1 <2 6.5	.5 <1 2.9		1 10 5	31 25 11.	21
$\perp$ $I$	5 13.7	1 2 < 5 11 6	1<2 5.9	`	265 12	.71 - 10 34.	1
1	≥10 30.1	30 71	2 < 5 12.5 5 < 10 34.5		1 - 10 31		8
500	$N = \frac{42.7}{2920}$	≥10 43 0	≥10 40.5		≥10 4-	1.0	~\
1	-320	N= 4022	N= 3515	, i —		788 N=	
1. /	-						\
1 /	1			+			\
1 /	- 1	1			ł	\	\
				1		\	\
5 Visibility Thr	resholds						February
							· Joinany

Marine Area C

Merine Area B

Marine Area A

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Nikol'skoe		Khatirka-In-Chukot		Ugol'neja		Buhta Providenja	
VISIBILITY (NM)	<u> 3</u>	VISIBILITY (NM)	ž	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3
<.5	4.3	<.5	3.7	<.5	9.6	<.5	4.3
.5 <1	5.1	.5 <1	2.3	.5 <1	5.2	.5 <1	3.0
1<2	8.4	1<2	6.4	1<2	9.3	1<2	5.7
2 < 5	11.2	2 < 5	7.1	2 < 5	13.4	2 < 5	9.9
5 <10	15.5	5 < 10	5.8	5 < 10	11.8	5 < 10	14.5
≥10	55.4	≥10	74.7	<u>≥</u> 10	50.5	≧10	62.5
N=	6021	N=	4081	N=	5299	N=	4900
Norheast Cape		Nome		Unelekteet		Cape Romanzof	
VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	2	VISIBILITY (NM)	3
<.5	5.3	<.5	3.2	<.5	1.8	<.5	8.8
.5 <1	4.8	.5 <1	3.1	.5 <1	1.7	.5 <1	9.7
1<2	7.1	1<2	4.5	1<2	2.3	1<2	6.1
2 < 5	13,9	2 < 5	9.3	2 < 5	6.3	2 <5	13.9
5 < 10	37.2	5 < 10	17.9	5 < 10	21.8	5 < 10	27.1
≥10	31.8	<u> </u>   ≥10	61.9	≧10	66.0	≥10	34.4
N=	9517	N=	21309	N=	14498	N=	18221
Cape Newenham		King Salmon		Port Heiden		Cold Bay	
VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	2	VISIBILITY (1)	7.
<.5	5.2	<.5	1.3	<.5	3.1	<.5	2.9
.5 <1	5.2	.5 <1	2.4	.5 <1	2.7	.5 <1	3.6
1<2	7.5	1<2	3.3	1<2	2.8	1<2	5.4
2 <5	14.8	2 < 5	5.9	2 < 5	7.3	2 < 5	12.2
5 < 10	32.0	5 < 10	18.1	5 < 10	13.4	5 < 10	40.2
≥10	35.4	<u>≥</u> 10	69.0	≥10	70.7	≥10	35.8
N=	19632	N=	19067	N=	2219	N=	13875
Nikolski		St. Paul		Adek		Shemya	
VISIBILITY (NM)	%	VISIBILITY (NM)	3	VISIBILITY (NM)	<u>7</u>	VISIBILITY (NM)	3
<.5	21.5	<.5	8.9	<.5	1.9	<.5	3.8
.5 <1	1.4	.5 <1	6.2	.5 <1	2.5	.5 <1	4.8
1<2	0.9	1<2	5.6	1<2	4.5	1<2	7.2
2 <5	4.9	2 < 5	13.9	2 < 5	19.2	2 < 5	16.1
5 < 10	32.5	5 < 10	47.9	5 < 10	66.0	5 < 10	45.9
≥10	38.8	≥10	17.5	≧10	5.8	≥10	22.1
N=	2228	N=	11597	N=	22123	N=	19367
March		JL		JL		5 Visibility	Thresh

March

VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)   \$   VISIBILITY (NAU)	Visibility (NAM)   5	Adamia a Assa A	Adada Assa B	7	11-113
Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scale   Scal	Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sec	Marino Area A	Marine Area B	Marine Area C	Marine Area D
1.5 < 1	1.5 < 1	VISIBILITY (NM)	Z VISIB(LITY (NM)	VISIBILITY (NM)	VISIBILITY (NM)
1 < 2	1 < 2	<.5 11.5	11.5 <.5 6.6	<.5 6.1	<.5 3.1
2 < 5	2 < 5	.5 <1 5.7	5.7   .5 < 1 4.9	.5 <1 3.4	.5 <1 2.9
5 < 10	5 < 10	1<2 6.4	6.4   1<2 9.3	1<2 6.1	1<2 5.3
\$\frac{\geq 10}{\geq 1257}   \$\frac{\geq 10}{\geq 1257}   \$\frac{\geq 10}{\geq 1257}   \$\frac{\geq 10}{\geq 10}   \$\geq	\$\frac{2}{10}	2 < 5 11.7	11.7   2<5 16.0	2 < 5 11.4	2 < 5 12.1
N=   1257	N=   1257   N=   5541   N=   4763   N=   8280   N=   170   N=	5 < 10 29.9	29.9   5<10 25.0	5 < 10 29.5	5 < 10 32.4
Marine Area E   170   58   180   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   1	Marine Aver E   170   65   180   170   170   180   Marine Aver E   170   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180   180	≥10 34.8	34.8 ≥10 38.1	∬ ≥10 43.5	≧10 44.1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N= 1257	N= 5541	N= 4763	N= 8280
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   Separation   S   S   S   S   S   S   S   S   S	Marino Area E	170 65	170°	160 Marino Area F
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		<ul> <li>&lt;.5 10</li> <li>5 &lt; 1 6</li> <li>1 &lt; 2 10</li> <li>2 &lt; 5 16</li> <li>5 &lt; 10 29</li> <li>≥10 26</li> <li>N= 30</li> <li>N= 30</li> <li>×v (NM)</li> <li>&lt;.5 4.0</li> <li>&lt;.5 4.0</li> <li>&lt;.5 4.0</li> <li>&lt;.5 5 6</li> <li></li> <li>&lt;.5 4.0</li> <li>&lt;.5 5 6</li> <li></li> <li>&lt;.5 4.0</li> <li>&lt;.5 5 6</li> <li></li>     &lt;</ul>	$\frac{1}{2}$ $\frac{\text{VV (NM)}}{\text{<.5}}$ $\frac{1}{2}$	
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	<.5 5 .5 <1 2 1 <2 7 2 <5 12. 5 <10 30. ≥10 42. N= 3450	N= 253 N= 14  NM) $\frac{2}{5}$ $\frac{\text{VV (NM)}}{\text{C.5}}$ $\frac{2}{3.6}$ $\frac{\text{VV (NM)}}{\text{C.5}}$ $\frac{2}{3.6}$ $\frac{\text{VV (NM)}}{\text{C.5}}$ $\frac{2}{3.6}$ $\frac{2.8}{5.61}$ $\frac{1.6}{4.0}$ $\frac{1.6}{5.61}$	14 N= 3712 N= 30.5 3 $\frac{\text{VV (NM)}}{\text{<.5}}$ $\frac{\text{Z}}{\text{<.5}}$ $\frac{\text{VV (NM)}}{\text{<.5}}$ $\frac{\text{Z}}{\text{<.5}}$ .4 .5 <1 3.1 .5 <1 2 .1 1 <2 5.9 1 <2 4 .1 1 <2 5.9 1 <2 4 .9 2 <5 11.8 2 <5 11 .9 2 <5 13.4 5 <10 32 .0 ≥10 44.1 ≥10 60	VV (NM)  √5  √5  √5  √5  √5  √5  √5  √5  √5  √

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- 11	• ]	1	C

Nikol'skoe		Khatirka-in-Chukot		Ugol'naja		Buhta Providenja	
VISIBILITY (NM)	<u>*</u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3
<.5	4.3	<.5	3.5	<.5	6.2	<.5	2.6
.5 <1	2.2	.5 <1	2.3	.5 <1	4.0	.5 <1	2.7
1<2	5.0	1<2	4.6	1<2	6.2	1<2	5.3
2 < 5	10.9	2 < 5	8.4	2 <5	9.2	2 < 5	10.4
5 < 10	13.2	5 < 10	6.4	5 < 10	11.7	5 < 10	13.4
≥10	64.4	≥10	74.7	≥10	62.8	<u>}</u>	65.7
N=	5629	N=	3804	N=	5 185	N=	4682
Norheast Cape		Nome		Unalakleet		Cape Romanzof	
VISIBILITY (NM)	3	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<b>%</b>	VISIBILITY (NM)	7
< <b>.</b> 5	4.7	<.5	2.0	<.5	1.4	<.5	7.3
.5 <1	5.2	.5 <1	3.7	.5 <1	1.9	.5 <1	8.3
1<2	9.8	1<2	5.0	1<2	1.8	! <2	6.7
2 <5	14.3	2 < 5	10.5	2 < 5	4.7	2 <5	14.7
5 < 10	31.6	5 < 10	16.3	5 < 10	15.0	5 < 10	30.0
≥10	34.4	≥10	62.5	≥10	75.2	≥10	33.0
N=	10105	N=	21334	N=	14615	N=	18729
Cape Newenham		King Selmon		Port Heiden		Cold Bay	
VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	2
<.5	4.6	<.5	0.8	<.5	3.4	<.5	1.9
.5 <1	5.0	.5 <1	1.5	.5 <1	3.0	.5 <1	2.6
1<2	7.5	1<2	2.9	1<2	2.7	1<2	4.8
2 < 5	17.1	2 < 5	6.0	2 < 5	8.4	2 < 5	14.8
5 < 10	30.8	5 < 10	16.8	5 < 10	13.2	5 < 10	39.7
≥10	35.0	≥10	72.0	≥10	69.3	<u>≥</u> 10	36.2
N=	19132	N=	18476	N=	2119	N=	13435
Nikolski		St. Paul		Adek		Shemye	
VISIBILITY (NM)	<u>7</u>	VISIBILITY (NM)	ž	VISIBILITY (NM)	ž	VISIBILITY (NM)	<u>"</u>
<.5	20.3	<.5	6.4	<.5	0.7	<.5	3.1
	1.5	.5 <1	5.0	.5 <1	1.4	.5 <1	5.0
.5 <1		1<2	5.7	1<2	4.0	1<2	7.4
.5 <1 1 <2	1.2			1.7		1.1	
1<2		2 < 5	15.1	2 < 5	19.8	2 < 5	15.6
1 < 2 2 < 5	4.9	2 <5		2 < 5	19.8 67.8	2 < 5	15.6 42.6
1<2		11	15.1	11		[ ]	

April

							11-117
Marine Area A		Marine Area B		Marine Area C		Marine Area D	
VISIBILITY (NM)	<u>z</u> .	VISIBILITY (NM)	<u>%</u>	VISIBILITY (NM)	7.	VISIBILITY INM	<u>3</u>
<.5	8.4	<.5	6.4	<.5	7.0	<.5	2.9
.5 <1	6.0	.5 <1	5.3	.5 <1	3.4	.5 <1	2.4
1<2	5.7	1<2	7.8	1<2	5.7	1<2	5.3
2 <5	10.5	2 < 5	13.2	2 < 5	13.4	2 < 5	13.0
5 < 10	25.5	5 <10	28.8	5 < 10	29.1	5 <10	32.6
≥10	43.9	≥10	38.5	≧10	41.4	≥10	43.7
N=	581	N=	4142	N=	6158	N=	7490
Marine Area E		65 %		130	~~	160   Marine Ares F	
	170	B	180	1700	L7	`~ \\	
VISIBILITY (NM)	4.5	5	VV (NM) Z	VV (NM) & VV (NA	<u>0</u> 3	<.5	4.6
.5 <1	2.9		<.5 4.4	130 (5	5.2	رب 1 > 5 < 1	2.7
1<2	5.5	: :	.5 <1 6.6	1 - 1 - 1	3.3	1<2	4.8
2 < 5	11.9	No.	5 1<2 5.8	1<2 6.5 1<	_	2 < 5	10.1
5 <10 <u>≥</u> 10	33.3		√ 2<5 10.9	2 < 5 13.4 2 <		5 <10 ≥10	29.0 48.9
N=	8652		5 < 10 27.	1 -4	~ A A A	N=	9565
<del></del>		~	≥10 44.	1 At-	213 12		
7 / N	60:_		N= 137	N= 232 N=	K		<i>τ</i> η
D VV CNM							1 } .
$\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} $	5 0 VINIO	Z VV (NM) Z			(Ma) ×	7 91	
1100	3.3/5	8 3	VV (NM) 2	AA (MW)	1.5	<.J ~ 71	1 2 12
1 2	8.7 [ ]	10.5 5<1		2 (.5 /.2)	3.2	.5 \ 5 4\	1 3 /5
15 -10	1.3 2<5	6.8/10	,	2 3 3	1 < 2 6.1	13.2	\o'\
/ >20 <	J. / # ~ .	3.8 2<5 16	, , , , , ,	1 1 2	2<5 13.8	28.7	
		2,015/10 -		J 2 (3 13.5)	31.01	4 /	/
55^		≥10 44.5			≥10 41.4	N= 4331 N	
1		N= 146	N= 757		N= 2186	1	
/			•			1	
/	VV (NM)			+	_	VV (NM)	
/	$\sqrt{\frac{5.5}{5.5}}$ 4.6	VV (NM)	VV (NM) %	VV (NM) 3	VV (NM)	7 <.5 4.0	•
j	3 2	' ! <.5 4 3 l	<.5 3.6		<.5 3.	1 - 11 2.7	•
, j		3.6	.5 <1 3.		.5 <1 2.	1 1 1 < 2	1
<b>/</b>	12.1	5.0	1<2 5.4		1 1 < 2		) <b>(</b>
<u> </u>	33.0	10	2 < 5 14.0		1 L	.6 5 .0 47.	0 /
	N. 41.7	1 340	5 < 10 34.7		5 <10 30 ≥10 45	71 EN 606	7
	3190	N= 42.0 N= 4531	≥10 39.2			25 N=	-
/~		+551	N= 4172	N= 4745	, "		
/	Γ				+	_	
1	1					\	\
/	1	1					
- 141 - 14 1314 - <b>- T</b> 1							
5 Visibility Thre	esnoids						Apr

1	1.1	1	8

Nikol'skoe		Khatirka-In-Chukot		Ugol'naja		Buhta Providenja	
VISIBILITY (NM)	3	VISIBILITY (NM)	ž	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	3
<.5	8.4	<.5	8.8	<.5	6.5	<.5	2.5
.5 <1	0.9	.5 <1	1.4	.5 <1	2.0	.5 <1	1.9
1<2	1.9	1<2	4.9	1<7	5.3	1<2	5.8
2 < 5	9.1	2 < 5	8.8	2 < 5	8.7	2 < 5	11.7
5 < 10	15.7	5 < 10	8.0	5 < 10	11.6	5 < 10	13.7
≥10	64.0	≧10	68.2	≥10	65.8	≥10	64.3
N=	5710	N=	3508	N=	5057	N=	4716
Norheast Cape		Nome		Unelekleet		Cape Romanzof	
VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	*	VISIBILITY (NM)	<u>:</u>
<.5	4.0	<.5	1.8	<.5	1.6	<.5	3.8
.5 <1	4.5	.5 < 1	2.2	.5 <1	1.3	.5 <1	4.2
1 < 2	6.8	1<2	3.7	1<2	1.2	1<2	4.8
2 < 5	13.1	2 < 5	6.8	2 < 5	3.0	2 < 5	10.6
5 < 10	30.2	5 < 10	12.2	5 < 10	7.7	∬ 5 < 10	27.0
≥10	41.3	≧10	73.3	≥10	85.2	≥10	49.6
N=	10469	N=	21321	N=	14942	N=	18927
Cape Newenham		King Salmon		Port Heiden		Cold Bay	
VISIBILITY (NM)	3	VISIBILITY (NM)	<u> 3</u>	VISIBILITY (NM)	3	VISIBILITY (NM)	<u>.</u>
. –	A C	<.5	1,4	<.5	2.1	<.5	• . •
<.5	4.5	11		11			
<.5 .5 <1	4.5	.5 <1	0.7	.5 <1	1.7	.5 <1	1.3
		11	0.7	11		.5 <1 1 < 2	1.3 2.4
.5 <1	4.1	.5 <1		.5 <1	1.7	<b>,</b>	
.5 <1 1 <2 2 <5	4.1 5.7	.5 <1 1 <2	1.2	.5 <1 1 < 2	1.7 2.1	1<2	2.4
.5 <1 1 <2 2 <5	4.1 5.7 11.1	.5 <1 1 <2 2 <5	1,2 3,4	.5 <1 1 < 2 2 < 5	1.7 2.1 5.4	1 < 2 2 < 5	2.4 9.6
.5 <1 1 <2 2 <5 5 <10	4.1 5.7 11.1 22.6	.5 <1 1 <2 2 <5 5 <10	1.2 3.4 13.6	.5 <1 1 < 2 2 <5 5 < 10	1.7 2.1 5.4 8.3	1 < 2 2 < 5 5 < 10	2.4 9.6 39.2
.5 <1 1 <2 2 <5 5 <10 ≧10	4.1 5.7 11.1 22.6 52.0	.5 <1 1 <2 2 <5 5 <10 ≥10	1.2 3.4 13.6 79.7	.5 <1 1 <2 2 <5 5 <10 ≥10	1.7 2.1 5.4 8.3 80.3	1 < 2 2 < 5 5 < 10 ≥10	2.4 9.6 39.2 46.4
.5 <1 1 <2 2 <5 5 <10 ≧10 N=.	4.1 5.7 11.1 22.6 52.0	.5 <1 1 <2 2 <5 5 <10 ≥10 N=	1.2 3.4 13.6 79.7	.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N=	1.7 2.1 5.4 8.3 80.3	1 < 2 2 < 5 5 < 10 ≥10 N=	2.4 9.6 39.2 46.4
.5 <1 1 <2 2 <5 5 <10 ≥10 N=.	4.1 5.7 11.1 22.6 52.0 19659	.5 <1 1 <2 2 <5 5 <10 ≥10 N=	1.2 3.4 13.6 79.7 18359	.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N=	1.7 2.1 5.4 8.3 80.3 2120	1 < 2 2 < 5 5 < 10 ≥10 N=	2.4 9.6 39.2 46.4 13153
.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N=.	4.1 5.7 11.1 22.6 52.0 19659	.5 <1 1 <2 2 <5 5 <10 ≥10 N=	1.2 3.4 13.6 79.7 18359	.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N=	1.7 2.1 5.4 8.3 80.3 2120	1 < 2 2 < 5 5 < 10 ≥ 10 N=  Shemye  VISIBILITY (NM)  < .5	2.4 9.6 39.2 46.4 13153
.5 <1 1 <2 2 <5 5 <10 ≥10 N=.  Nikolski  visibility (NM) <.5	4.1 5.7 11.1 22.6 52.0 19659	.5 <1 1 <2 2 <5 5 <10 ≥10 N= St. Paul  VISIBILITY (NM) <.5	1,2 3,4 13,6 79,7 18359	.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N= Adak  VISIBILITY (NM)  <.5	1.7 2.1 5.4 8.3 80.3 2120	1 < 2 2 < 5 5 < 10 ≥10 N=	2.4 9.6 39.2 46.4 13153
.5 <1 1 <2 2 <5 5 <10 ≥10 N=.  Nikoleki  visibility (NM)  <.5  .5 <1	4.1 5.7 11.1 22.6 52.0 19659 2 26.0 1.4	.5 <1 1 <2 2 <5 5 <10 ≥10 N=  St. Paul  VISIBILITY (NM)  <.5  .5 <1	1.2 3.4 13.6 79.7 18359	.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N=  Adak  VISIBILITY (NM)  <.5  .5 < 1  1 < 2	1.7 2.1 5.4 8.3 80.3 2120	1 < 2 2 < 5 5 < 10 ≥10 N= Shemye VISIBILITY (NM) < .5 .5 < 1 1 < 2	2.4 9.6 39.2 46.4 13153
.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N=.  Nikoleki  VISIBILITY (NM)  <.5  .5 < 1 1 < 2	4.1 5.7 11.1 22.6 52.0 19659 2 26.0 1.4 1.1	.5 <1 1 <2 2 <5 5 <10 ≥10 N=  St. Paul  VISIBILITY (NM)  <.5  .5 <1  1 <2	1.2 3.4 13.6 79.7 18359 	.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N= Adak  VISIBILITY (NM)  <.5 .5 < 1	1.7 2.1 5.4 8.3 80.3 2120	1 < 2 2 < 5 5 < 10 ≥10 N= Shemys VISIBILITY (NM) < .5 .5 < 1 1 < 2 2 < 5	2.4 9.6 39.2 46.4 13153 5.9 5.7 5.5
.5 <1 1 <2 2 <5 5 <10 ≥10 N=.  Nikoleki  visiBility (NM)  <.5  .5 <1  1 <2  2 <5	4.1 5.7 11.1 22.6 52.0 19659 26.0 1.4 1.1 4.6 30.5	.5 <1 1 <2 2 <5 5 <10 ≥10 N= St. Paul VISIBILITY (NM) <.5 .5 <1 1 <2 2 <5	1.2 3.4 13.6 79.7 18359 7.2 5.8 6.0 15.3 47.4	.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N=  Adak  VISIBILITY (NM)  <.5 .5 < 1 1 < 2 2 < 5	1.7 2.1 5.4 8.3 80.3 2120 3 0.2 0.6 2.6 19.2 70.9	1 < 2 2 < 5 5 < 10 ≥10 N=  Shemye  VISIBILITY (NM)  < .5  .5 < 1  1 < 2  2 < 5  5 < 10	2.4 9.6 39.2 46.4 13153 5.9 5.7 15.5 41.3
.5 <1 1 <2 2 <5 5 <10 ≥10 N=.  Nikoleki  visiBilitr (NM)  <.5  .5 <1  1 <2  2 <5  5 <10	4.1 5.7 11.1 22.6 52.0 19659 2 26.0 1.4 1.1 4.6	.5 <1 1 <2 2 <5 5 <10 ≥10 N= St. Paul VISIBILITY (NM) <.5 .5 <1 1 <2 2 <5 5 <10	1.2 3.4 13.6 79.7 18359 	.5 <1 1 < 2 2 < 5 5 < 10 ≥10 N=  Adak  VISIBILITY (NM)  <.5 .5 <1 1 < 2 2 < 5 5 < 10	1.7 2.1 5.4 8.3 80.3 2120	1 < 2 2 < 5 5 < 10 ≥10 N= Shemys VISIBILITY (NM) < .5 .5 < 1 1 < 2 2 < 5	2.4 9.6 39.2 46.4 13153 5.9 5.7 5.5

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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Marine Area A		Marine Area B		Marine Area C		Marine Area D	
5 < 1	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	3
1 < 2	<.5	10.7	<.5	10.2	<.5	10.4	<.5	4.2
2 < 5	.5 <1	4.1	.5 <1	4.7	.5 <1	2.6	.5 <1	2.0
\$\frac{\geq 10}{\geq 20}\$ 36.7  \frac{\geq 10}{\geq 36.3}\$  \frac{\geq 10}{\geq 36.7}\$  \frac{\geq 10}{\geq 36.7}\$   \frac{\geq 10}{\geq 36.9}\$    \frac{\geq 10}{\geq 44.6}\$                                                                                                                                                                                                                                                                                                  \qquad        \qquad  \qquad \qquad  \qquad \qquad \	1<2	7.2	1<2	5.9	1<2	5.0	1<2	3.9
210 36.7 N= 38.9 ≥10 41.7 ≥10 44.6 N= 8511    Martine Arter E	2 < 5	11.9	2 <5	12.0	2 < 5	14.1	2 < 5	10.5
N=   1035   N=   3825   N=   9116   N=   8511	5 < 10	29.4	5 <10	31.3	5 < 10	26.3	5 < 10	34.8
Mattine Area E   1/3   55   169   169   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170	≥10	36.7	≥10	35.9	≥10	41.7	≥10	44.6
Section 200   \$   \$   \$   \$   \$   \$   \$   \$   \$	N=	1035	N=	3825	N=	9116	N=	8511
Section 2019   Section 2			<u></u>		<u></u>			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Marine Area E	170	65	1896	170°	77	160 Marine Area F	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	VISIBILITY (NM)	3			7	W & L 20	\ H ====	
1	· ·	F1		2		. *	J 11	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11		\ 1	0 \.3 12.2	· • • /	!!	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	_	II.	•	ر ا ر		2 7.1 6	1 1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5 < 10	33.0	ر کالمر	11	$\frac{1}{2}$ $\frac{2}{5}$ $\frac{3}{2}$	<5 9.9 i	1 !	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			~ 1	,	1 - 10 /		F1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N=	10613	rr		3 ≥10 41.7 ≥	205 17	N=	10942
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7			N= 550	N= 115 N	= 390		100
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1) 5000			1			, il
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	<.5	18 - VV (NM)	2		+	- \ v		ف رُ ا
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\bigcap \int_{1}^{3} \zeta_{1}$	<b>7</b> - 1 110	12 2	VV (NM) %	VV (NM) 2	IV (NM)	, = 10.21 V	. A.Y.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1 2	5 1 1.0	481	4 <.5 8.	<.5 10.4	- 1	5 \	ା 🐔 🐧 🖔
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6 6	10 3 1 'S	5.9/1		21.5		122	- J - 10°
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	V / ≥10 '	3.0 1- 3	9.6		' •	1	25.7	چ <sup>ک</sup>
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	/ <sub>N-</sub> 46	23	3.9 5 4.6		_ 1	5<10 31.4	41.4	9
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	55.	$^{1}$ $N_{-}$ $+3$	· 1   ≥10 40 5		3 (3 (10 3 1.2 ]	≥10 36.8	6298 W	!
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	_ / 18		1		2010	N-	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1		14- 1091	N~ 2324		J	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	/	VV (NM)		<del> </del>			I WWO Z	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\mathbf{l}'$	1 < 5 2	VV (NM)	10/000			4.	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Y	15-1 1.3	1 <.5			1 5 4.	$0$ $\frac{1}{2}$	1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11-7 <./	1.5<1 30			1 = 11 2.		1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1		1 1/2 5 5 1	I	1	1<2 3	1 2 <5	<b>\</b>
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1	31.0	15 13.4			12<5	7 5 < 10	2 \
5529 N= 7675 N= 5389 N= 5972 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763 N= 7763	<b>1</b>	N- 42.7 1	\ <sub>10</sub> = 00.0			15 < 10 33	5 ≥10 €03	7
7675 N= 5389 N= 5972 N=	500	5529	38.2	≥10 39.9	≥10 44.7	≥10 40	63 N=	
5 Visibility Thresholds May			/675	N= 5389	N = 5972	N- ,,		
5 Visibility Thresholds May						4		
5 Visibility Thresholds May	/							\
5 Visibility Thresholds May	/							
5 Visibility Thresholds May								
	5 Visibility The	resholds						May

Nikol'skoe		Khetirke-In-Chukot		Ugol'naje		Buhta Providenja	
VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	7.
<.5	16.9	<.5	15.9	<.5	10.0	<.5	5.7
.5 <1	0.6	.5 <1	0.7	.5 <1	0.8	.5 <1	2.1
1<2	1.7	1<2	3.0	1<2	1.8	1<2	8.6
2 < 5	9.1	2 <5	8.3	2 < 5	5.1	2 < 5	12.0
5 < 10	15.9	5 < 10	8.1	5 < 10	8.6	5 < 10	10.4
≥10	55.9	≥10	64.0	≥10	73.7	≥10	61.3
N=	5502	N=	3448	N=	4902	N=	4534
Norheast Cape		Nome		Unelskieet		Cape Romanzof	
VISIBILITY (NM)	2	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>*</u>	VISIBILITY (NM)	3
<.5	7.4	<.5	2.7	<.5	1.6	<.5	5.5
.5 <1	3.9	.5 <1	2.4	.5 <1	1.6	.5 <1	4.6
1<2	4.9	1<2	3.4	1<2	1.4	1<2	3.5
2 < 5	11.0	2 <5	6.5	2 < 5	2.7	2 <5	10.7
5 < 10	26.8	5 < 10	11.9	5 < 10	9.3	5 <10	29.0
≥10	46.1	≥10	73.2	≥10	83.3	≥10	46.7
N=	9923	N=	20628	N=	14476	N=	17765
Cape Newenham		King Selmon		Port Heiden		Cold Bay	
VISIBILITY (NM)	ž	VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	<u>z</u>
<.5	5.1	<.5	1.8	<.5	1.2	<.5	1.3
.5 <1	3.4	.5 <1	1.3	.5 <1	2.1	.5 <1	1.2
1<2	5.7	1<2	1.5	1<2	2.4	1<2	3.1
2 < 5	13.7	2 < 5	4.1	2 < 5	8.0	2 <5	9.0
5 < 10	20.6	5 < 10	13.2	5 < 10	9.2	5 < 10	33.9
≥10	51.5	≥10	78.1	≟10	77.2	<u>≥</u> 10	51.5
N=	18410	N=	17756	   	2081	N=	12720
Nikolski		St. Paul		Adek		Shemya	
VISIBILITY (NM)	7.	VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	3
<.5	42.0	<.5	11.9	<.5	0.9	<.5	15.1
.5 <1	1.5	.5 <1	6.8	.5 <1	1.4	.5 <1	7.6
1<2	1.6	1<2	6.3	1<2	3.7	1<2	8.8
2 <5	6.3	2 <5	14.8	2 < 5	21.2	2 < 5	16.0
5 < 10	19.1	5 < 10	44.8	5 < 10	65.9	5 < 10	31.8
≥10	29.4	≥10	15.4	10 ≥10	6.8	≥10	20.5
N=	2200	N=	10026	N=	21504	N=	18421
• •		11				11	

9.8

Marine Area D

<.5

VISIBILITY (NM)

5	73.2	5	70.2	5 .4	2.6	5 41	2.5
.5 <1	2.8	.5 <1	3.6	.5 <1	2.6	.5 <1	3.5
1<2	3.3	1<2	5.7	1 < 2	4.1	1<2	5.6
2 < 5	7.6	2 <5	12.2	2 < 5	12.2	2 < 5	12.5
5 < 10	23.7	5 <10	29.3	5 <10	27.9	5 <10	32.4
≥10	47.3	≧10	33.0	≧10	38.0	≥10	36.3
N=	1692	N=	5590	N=	9920	N=	9820
		L					
Marine Area E	170	65.	189	170°	P	160 Marine Area I	F
VISIBILITY (NM)	<u>*</u>     /		~~	<del></del>	Very	VISIBILITY (	<u> </u>
<.5	10.6		Y VV (NM) X	1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	(NW) Z	) \ <.5	9.0
.5 <1	3.9		<.5 18.	41 (.)	<.5 13.4	.5 < 1	3.2
1<2	5.3		5 .5 <1 2.	5<1 1.8 .5	<1 3.6 A.2 A.2	1 < 2 2 < 5	4.4
2 <5 5 <10	12.3	Sh	) 1<2 2.	$7 \cdot 1 \cdot 1 \cdot 2 \cdot 3.9 \cdot 1$	1	5 < 10	28.7
≥10	36.2		2<5 7.		2	≥10	44.3
N=	11420		5 < 10 17.	*   J   1,0	0	N=	10485
Ĺ		~	<u></u> 10 51.	1	≥10 50.0 N= 590		
7	60:	/	N= 954	N= 383	K-		m
D/vv (M				1		2 L A	1
\(\sigma\) \(\sigma\) \(\sigma\).5	27.7 VV (NM)	Z VV (NM)			עע (אאז) אַ ל	IV CN	1 /3
\\ \sigma_{.5 < 1}	3 / \.5	21 0	VV (NM) Z	VV (NM) 3	16 9	<> 0.51	1 کا ہا
1/2	3 = 1.5	3 1 5	.9 <.5 16.		1	.5 \ 4 21	1 5 /54
5 < 10	6.6	5 0	3 .5 < 1 3.	8   .5 < 1 3.7	.5<1 2.8 1<2 4.5	122	\ ~\\\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
1 / >1-	19 5 1 - 3 1	4.4 7 26			991	26.1	
1 / 1/2 4	10 5 1 . 10 2:	3.0 5 210 27	1		5 < 10 33.4	38.6	5v \
55.	215   No 32	.6   ≥10 37	_	م م ۔ ۔	≥10 32.5	6443 N	
1	7	73 N= 698	_		1 3154	N= 0	
	7		B N= 249	5 N = 2553			\
1/	J var.		· <del> </del>	<del></del>		W (NM)	\
1/	VV (NM)	VV (NM)	•		VV (NM) 3	1 4 9.3	31
Y	15.3 12.3	31 75	VV (NM)	VV (NM) %	15 9.	71 3.4	21
	11-2 4.3	15/1 12.4			5 5 1 3	313 4	6 \
	1 2 6.5	1.5			4	.61 75 10.	.6
	15.7	2 < 5 14.9	1<2 6.		2 2 25 10	1.10 20	. /
I	>40	5 < 10 32.4	2 < 5 13.		15/10 32	$2.9  \sum_{10}^{2} 43$	.5
500	N= 49.5	≥10 29.0	5 <10 31. ≧10 32.	9 1 9	. 1 >10 38	3· 1 N- /	183
1	8432	N= 8892	≧10 32. N= 775	T 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		514	
1 /			//5	2 1 1 3 3			\ ]
/	- 1			+		\	\
] /	1					1	\
/	1					1	\
5 Visibility Th	resholds				<u> </u>		June
S VISIDINITY III	11 43110143						Vuile

Marine Area C

<.5

16.2

VISIBILITY (NM)

15.2

Marine Area B

<.5

15.2

VISIBILITY (NM)

Merine Area A

<.5

VISIBILITY (NM)

1	ı	. 1	ı	2	2

Nikol'skos		Khatirka-In-Chukot	· — · — · —	Ugol'neja		Buhta Providenja	
VISIBILITY (NM)	<u>*</u>	VISIBILITY (NM)	3	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3
<.5	25.3	<.5	22.4	. <.5	10.9	<.5	4.6
.5 <1	0.6	.5 <1	0.5	.5 <1	1.0	.5 <1	2.1
1<2	2.1	1<2	3.8	1<2	2.0	1<2	10.6
2 <5	12.8	2 < 5	8.5	2 < 5	5.5	2 < 5	12.6
5 < 10	13.7	5 < 10	8.3	5 < 10	8.4	5 < 10	12.0
≥10	45.5	≥10	56.5	≥10	72.3	≥10	58.1
N=	5409	N=-	3296	N=	4981	N=	4458
Norheast Cape		Nome		Unelekleet		Cape Romanzof	
VISIBILITY (NM)	<b>%</b>	VISIBILITY (NM)	<u> 3</u>	VISIBILITY (NM)	<u> </u>	VISIBILITY (I.11)	3
<.5	4.1	<.5	1.5	<.5	0.5	<.5	5.1
.5 <1	3.8	.5 <1	2.6	.5 <1	0.7	.5 <1	4.7
1<2	6.8	1<2	5.4	1<2	1.4	1<2	3.8
2 <5	14.6	2 < 5	9.9	2 <5	3.2	2 < 5	12.2
5 < 10	30.1	5 < 10	16.5	5 < 10	12.1	5 < 10	31.7
≥10	40.7	≥10	64.1	≥10	82.2	≥10	42.6
N=	10653	N=	21311	N=	15878	N=	18733
Cape Newenham		King Selmon		Port Heiden		Cold Bay	
VISIBILITY (NM)	7.	VISIBILITY (NM)	<u>%</u>	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3
<.5	5.4	<.5	2.4	<.5	2.9	<.5	2.6
.5 <1	4.9	.5 <1	1.3	.5 <1	4.7	.5 <1	2.6
1<2	8.1	1<2	3.0	1<2	3.5	1<2	5.6
2 <5	17.6	2 < 5	7.0	2 < 5	9.5	2 <5	13.7
5 < 10	23.0	5 < 10	16.4	5 < 10	10.5	5 < 10	37.0
≥10	41.0	≧10	69.9	≥10	68.9	≥10	38.7
N=	19518	N=	18345	N=	1990	N=	13868
Nikolski		St. Paul		Adek		Shemya	
VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	3
<.5	67.9	<.5	18.3	<.5	1.8	<.5	28.2
.5 <1	1.8	.5 <1	9.0	.5 <1	2.4	.5 <1	11.1
1<2	0.6	1<2	9.4	1<2	6.4	1<2	10.6
2 < 5	3.9	2 < 5	18.1	2 < 5	25.7	2 < 5	15.6
2 \ \ \ \ \	9.2	5 < 10	34.7	5 <10	57.4	5 < 10	21.8
5 < 10		1.1		11		11	
	16.5	≥10	10.6	∬ ≥10	6.3	[] ≥10	12.6

Marine Area D

VISIBILITY (NM)	3	VISIBILITY (NM)	7.	VISIBILITY (NM)	<b>%</b>	VISIBILITY (NM)	<u>z</u>
<.5	13.7	<.5	16.8	<.5	15.5	<.5	16.5
.5 <1	3.2	.5 <1	5.4	.5 <1	4.2	.5 <1	5.4
1<2	4.2	1<2	8.0	1<2	5.6	1<2	6.6
2 < 5	8.7	2 < 5	14.9	2 < 5	13.7	2 < 5	14.0
5 <10	24.3	5 <10	29.2	5 <10	28.0	5 <10	29.1
≥10	45.9	≥10	25.6	≥10	33.0	≥10	28.4
N=	3619	N=	5720	N=	9363	N=	8520
						L	
Merine Area E	170	65	1800	170°	Pa	160 Merine Area F	
VISIBILITY (NM)	2			VV (NM) % VV (N	M) Z	VISIBILITY (NM	
<.5	20.0		VV (NM) 3	-	~1	<.5	14.4
.5 <1 1 < 2	6.0		<.5 22. .5 <1 2.8	11 (.5 15.0)	1 3.5	.5 <1 1 < 2	4.9 5.3
2 < 5	13.4		1<2 5.0		2 3.8 <b>√</b> ८	2 < 5	10.6
5 < 10	28.0	بالر	2<5 10	0 2 < 5 10.7 2		5 < 10	28.3
≥10	26.3	N	5 < 10 21.	1 5 < 10 27.8 5 <		≥10	36.5
N=	11777	ar	≧10 39.	o ≥10 37.8 <sup>≥1</sup>	4613 ~	// N=	11314
			N= 1443	N= 698 N	= 1043		
VV (NM							, ~
5.5	18.7 VV (NM)	Z VV (NIII)	<del></del>	+	(V (NM) % V	V (NM)	// } 4
5 5 51	2 2 1 1.3	30 0	VV (NM) Z	VV (NM) 2 3	17 Q	<.5	
2<5	4.2	5 3 7 23.			\.\.	5 \ \ \ 8\	1 / /5
15-12	71.8   - >	6.8	1	3   .5 <	5<1 5.0	122 91 /	/ / \@
V 1312 2	2 = 1- 3 1	7.01 255 1.6	-	. 7	2 < 5 14.3	26.7	ا کم
\ \ \ N=\ \ 39	'·8'   \ \ - \ - \ \	0.8 5 < 10	_ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	_ 1	5<10 29.91	36.91	0 /
55. 306	$N = \frac{20}{19}$	• 1 1 >10		3 3 4 10 23 13	≥10 25.41	N= 4704 W	
V	_/ '9	N= 1140	N= 244		N= 4558		
1	7				_	January .	
	VV (NM)					VV (NM)	İ
<b>!</b> /	1 <.5 202	VV (NM)	VV (NM) %	VV (NM) 2	VV (NM)	1 ,5 14.7	, j
	1.0 \1 5 ~	<b>'   &lt;</b> .5 27 7	<.5 20.		<.5 16.	0 - 11 5.4	<i>\</i>
1	`~ 7 .	1.5 <1 6.7	.5 <1 6.6	- 1	1.5<1 4.	c 1 1<2	31
1	5 - 13.2	0.31	1<2 7.	1<2 6.3	13	01 4 7 28	2 ( 1
\ \ \frac{1}{1}	25.7	15 < 10	2 < 5 14.	3 2 < 5 14.0	1 - 10 29	815 35.	3 [
$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} dx$	21.2		5 < 10 27.		30	11 - 700	.o \
500	N= 5217	≥10 19.4 N= 6384	≥10 23.6		70	57 N= 78-	-
		5504	N= 6142	N= 6198			- \
/	T			<del></del>	+		\
/	1					\	\ 1
/					1		\
			<del>-</del>				
5 Visibility Thre	esholds						July

Marine Area C

Marine Area B

Marine Area A

Nikel'skee		Khetirke-In-Chukot		Ugol'neje		Buhta Providenja	
VISIBILITY (NM)	ž	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	*	VISIBILITY (NM)	<u>z</u>
<.5	15.2	<.5	15.0	<.5	8.4	<.5	2.7
.5 <1	0.4	.5 <1	0.3	.5 <1	0.7	.5 <1	1.3
1<2	2.5	1<2	3.9	1<2	3.2	1<2	7.0
2 < 5	10.9	2 < 5	10.6	2 <5	7.1	2 < 5	12.6
5 < 10	15.1	5 < 10	9.5	5 < 10	12.8	5 < 10	15.0
≥10	55.9	≧10	60.7	≥10	67.8	<u>≥</u> 10	61.5
N=	5334	N=	3318	N=	4877	N=	4520
Norheast Cape		Nome		Unalakiest		Cape Romanzof	
VISIBILITY (NM)	<b>%</b>	VISIBILITY (NM)	3	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	<u> 3</u>
<.5	3.3	<.5	0.8	<.5	0.3	<.5	2.9
.5 <1	3.0	.5 <1	2.1	.5 <1	0.6	.5 <1	4.8
1<2	7.4	1<2	5.1	1<2	1.6	1<2	4.3
2 <5	16.2	2 <5	10.7	2 <5	3.8	2 < 5	13.0
5 < 10	32.4	5 < 10	19.7	5 < 10	15.5	5 < 10	30.7
≥10	37.7	<u>≥</u> 10	61.5	≧10	78.3	≥10	44.3
N=	10877	N=	21799	lvi_	15788	N=	18816
Cape Newenhem		King Selmon		Port Heiden		Cold Bay	
VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3
<.5	4.0	<.5	2.5	<.5	3.6	<.5	1.8
.5 <1	5.0	.5 <1	1.6	.5 <1	3.9	.5 <1	3.4
1<2	7.2	1<2	3.3	1<2	4.0	1<2	7.0
2 < 5	17.4	2 <5	8.7	2 < 5	9.7	2 < 5	15.5
5 < 10	24.4	5 < 10	21.2	5 < 10	11.8	5 < 10	38.2
≥10	42.1	≥10	62.8	<u> </u>   ≥10	67.0	<u> </u>   ≥10	34.0
N=	20133	N=	18828	N=	2005	N=	14376
Nikolski		St. Paul		Adek		Shemya	
VISIBILITY (NM)	3	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	<u> </u>
VISIBILITY (IIII)	58.5	<.5	13.0	<.5	1,9	<.5	24.6
<.5	50.5			11		i i	10.0
	1.5	.5 <1	7.9	.5 <1	2.2	.5 <1	
<.5		.5 <1 1 <2	7.9 8.5	V 1	2.2 6.4	11	
<.5 .5 <1	1.5	11		1<2	6.4	1<2	9.0
<.5 .5 <1 1 <2 2 <5	1.5 1.3 3.8	1<2	8.5 17.1	1<2 2<5	6.4 25.4	1<2 2<5	9.0 14.5
<.5 .5 <1 1 <2	1.5 1.3	1 < 2 2 < 5	8.5	1<2	6.4	1<2	9.0

<b>*</b>	Marine Area	A	Marine Area B					
1	VISIBILITY	(NM)	Marine Area B		Marine Area C			11.
	<.5		VISIBILITY (NM)	3	11	1	Marine Area D	
1	.5 <1	9.2	<.5		VISIBILITY (NM)	<u>z</u>	1	
	1<2	4.0	.5 <1	13.9	<.5	11.9	VISIBILITY (NM)	*
	2 < 5	4.5	1<2	6.0	.5 <1	1	<.5	16.4
		10.7	2 < 5	7.3	1<2	4.0	.5 <1	4.8
	5 < 10	23.3	5 < 10	15.3	2 < 5	6.0	1<2	6.7
	≥10	48.3		26.5	5 < 10	16.8	2 < 5	12.5
	N=	3710	≥10	31.1	≥10	29.8	5 < 10	
<u> </u>			N=	3510	N=	31.5	≥10	29.4
M	erine Area E	7			IV	8097	N=	30.2
Ì	VISIBILITY (NM)	170°	65°	180			~~~	8585
	<.5	30.0	122	7	170°	7	160 Merina Australia	
1	.5 <1	20.2		J.,		5	160 Marine Area F	
	1<2	6.1	4	VV (NM) 3	AA CHM) & AA CHP	2 3	VISIB-LITY (NM)	3
	2 <5	12.7		<.5 12.5	<.5 9.9 <.5	8.4	<.5	15.8
=	5 <10	27.1	1 2		.5 <1 4.9 .5 <1	3.9	.5 <1	4.7
	≥10 N=	29.0		1<2 5.2 2<5 11 1	1<2 4.3 1<2	3.6	1<2	5.8
	-14	12900			2<5 13.9 2<5		2 <5 5 <10	11.8
	7		/ :			١	≥10	27.1
1/	D/ YV CMM			12.3	≥10 45.1 ≥10	49.81	N=	34.9
1/	7.5	3 1		N= 1896	N= 718 N=	1393		11192
$\sim$	1.5 <1	12.0 VV(NM)	1		•	X		
	1150	2.51. 1.3	VV (NM)				1	$\sim$
15	1285	2. a 1.3 <1	1 1.0 01 01	V (NM)	V (NM) Z VV (N	IM) × VV (NM		
$\nu$	10-1-	) < 1 /621	7515	<.5 12.0	<.5 15.1 <.5	1 , =	10.2	M. M.
1	≥10 17	14 15 -12 0	1 - 12 5 5 1	<1 5.8 5	<1 6.6 .5 <	1 4.8 5<1	3.2	J 12 1
55.		5 / 210 17 2	~ \3 1~ 1	6.61	<2 7.3 1<	2 6.8 1<2		5 /5
1000	2040	N= 47.2	23 212	<sup>5</sup> 13.7 2	<5 16.5 2 <	5 16.7 2 <		109
1 /	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	487	≥10 30.0 ≥10		<10 25.7 5 <1	0 32.6 5 < 10		\
[ /	1	1	202	) 34.6 ≥	10 28.9 ≥10	25.4 ≥10	2712 NI	V
//		VV.	- N=	1173 N	= 1885 N=	N	3/42	
/		S.5 3 VV	-		•			1
7	<i></i>	5.5 21.6 VV	(NM)				1	1
	$\int_{1}^{\infty}$	5.01	5 2 VV (NI	0 z vv	(NM) % VV (	NM) Z VV	(NM) ×	- 1
	15	~~ / \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1 4.6 <.5			- 1	5 16.21	1
	15 <	15 0 15	2 2.3 1.5 <1	5.7 5	.5 19.0 <. <1 4.7 .5 <		<1 4.9	- 1
	/ ≥10	1 42.0 1- 1-	13.4	7.0 1			<2 6.0	1
<b>b</b> •	N=	< A > 1 10	7~ ( ~ \)	12.9 2.		5 12.8 2	<5 12.1	1
_		3850 / ≤10	25.0 13 <10	27.3 150			<10 26.8	1
		N=	5900	27.4 ≥1			≥10 34.0 <b>1</b>	1
	/	- American	0309 N=	6465 N=			N= 7832	
	/	1 -	-					
	<i>f</i> .	$\cdot \cdot \cdot = \int_{-\infty}^{\infty} e^{-i\omega t} dt$	1					1
	1	1	1	1		1	/	1
/isibili	ty Thresho	lde				1		)
						1	1	- 1
							1	ì

Marine Area A

١	I	l	2	G

11-126							
Nikol'skoe		Khatirka-In-Chukot		Ugol'naja		Buhte Providenja	
VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	7	VISIBILITY (NM)	<u>3</u>
<.5	4.7	<.5	6.4	<.5	2.5	<.5	0.9
.5 <1	0.2	.5 <1	0.3	.5 <1	0.5	.5 <1	0.7
1<2	0.9	1<2	2.4	1<2	2.1	1<2	3.6
2 <5	7.3	2 <5	7.9	2 < 5	7.5	2 < 5	8.7
5 < 10	14.3	5 < 10	6.3	5 < 10	15.8	5 < 10	13.9
≥10	72.5	≥10	76.8	≥10	71.6	≥10	72.1
N=	5294	N=	3190	N=	4824	N=	4337
Norheast Cape		Nome		Unglakiest		Cape Romanzof	
VISIBILITY (NM)	2	VISIBILITY (NM)	ž	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3
<.5	1.7	<.5	0.3	<.5	0.2	<.5	1.2
.5 <1	2.6	.5 <1	1.0	.5 <1	0.2	.5 <1	2.5
1<2	4.9	1<2	2.4	1<2	0.5	1<2	3.2
2 <5	14.0	2 < 5	7.1	2 < 5	1.5	2 < 5	10.0
5 < 10	37.9	5 < 10	20.4	5 < 10	15.5	5 < 10	32.6
≥10	39.0	10 ≥10	68.7	≥10	82.1	≥10	50.6
N=	10867	N=	21074	N=	15346	N=	18226
Cape Newenhem		King Salmon		Port Heiden		Cold Bey	
VISIBILITY (NM)	3	VISIBILITY (NM)	<u>%</u>	VISIBILITY (NM)	<u> 3</u>	VISIBILITY (NM)	7
<.5	1.0	<.5	1.4	<.5	0.4	<.5	0.4
.5 <1	1.8	.5 <1	0.5	.5 <1	0.6	.5 <1	1.2
1<2	3.5	1<2	1.0	1<2	1.4	1<2	3.8
2 < 5	11.3	2 < 5	4.2	2 <5	6.1	2 < 5	10.0
5 < 10	29.5	5 < 10	20.1	5 < 10	16.5	5 < 10	44.0
≥10	53.0	≥10	72.8	≧10	74.9	≧10	40.5
N=	19786	N=	18216	N=	2103	N=	13918
Nikolski		St. Peul		Adak		Shemye	
VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	<u>\$</u>	VISIBILITY (NM)	3
<.5	32.8	<.5	5.1	<.5	0.3	<.5	5.3
.5 <1	0.9	.5 <1	3.5	.5 <1	1.3	.5 <1	4.3
1<2	0.7	1<2	4.6	1<2	4.1	1<2	5.5
2 < 5	4.7	2 < 5	11.1	2 < 5	21.0	2 < 5	11.4
5 < 10	23.3	5 < 10	57.5	5 < 10	65.8	5 < 10	41.2
≥10	37,5	≧10	18.1	≥10	7.5	≥10	32.3
N=	2382	N=	10315	N=	21505	N=	18936
				I I		f f	

September

Marine Ares D

VISIBILITY (NM)	2	VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	<u>z</u>
<.5	2.1	<.5	5.0	<.5	4.3	<.5	4.9
.5 <1	2.0	.5 <1	2.9	,5 <1	2.7	.5 <1	2.0
1<2	3.0	1<2	6.1	1<2	5.2	1<2	4.0
2 < 5	6.4	2 < 5	12.7	2 < 5	14.4	2 < 5	9.7
5 < 10	24.2	5 < 10	31.4	5 < 10	31.7	5 < 10	31.6
≥10	62.3	≥10	42.0	≥10	41.7	≥10	47.8
N=	2305	N=	2574	N=	8283	N=	7505
Marine Area E	170	65	189	170°	~	160 Marino Area F	1
VISIBILITY (NM)	3		7		- SV	VISIBILITY (NM)	3
<.5	6.3		VV (NM) &	VV (NM) & VV (N		<.5	5.6
.5 <1	2.6	1	<.5 2.5	5 <.5 2.6 <.		.5 <1	2.7
1<2	4.4	•	.5 <1 1.6	5 .5 <1 2.1 .5 <	- 6 1/ 1/	1<2	3.5
2 <5	10.6		3 1<2 2.6	1<2 2.8 1		2 < 5	9.0
5 < 10	32.3	in the second	/ 2<5 7.4	2<5 9.1 2		5 < 10	28.7
≥10 N=	43.6	~	5 < 10 24.	3 5 < 10 28.2 5 <		≥10 N=	50.4
14-	10003	N	≧10 61.		1035 67	/	1035
			N= 689	N= 529 N	= 1033		
/ / VY (M)	M)					<sup></sup> 1	,
1 5.5	3 / VV			+		IN (NM)	) } <b>4</b>
1.5 <1	3.5 / _=	NV (NM)	VV (NM) 3	VV (NM) 3 3	IV (NM)	J. S. O \ ∨ 7	
1/2	1.4 1.5 <1	<.8 \ <.5 5.4	4 <.5 2.	1 65 6.5	<.5 4.7	2.0	J 15
2 <5	67/1/2	3.41.5<1 2.5			5 <1 3.01	۲ ۱۰۱۵ ک	) \sa
1 >1 >	?? > /_ < \3	1<2		· ( ·	1<2 5.3	2<5 13.3	\V \\
≥10 N= 6.	301 70 2	261, 10.9	2 < 5 12.	1 2 < 5 12.9	2<5 15.0	20.0 V %	₹ \ <u>\</u>
55- 12	97 ( -10 66	20.0	5 < 10 34.		~ ~ ~ ~ ~	1 ~10 2 /	i J
To the	N= 4.	24	≥10 41.	5 ≥10 42.5	5022	N= 2500	
		N= 239	N= 730	N= 1560	N= 5922	1	
1/		-	1			-	1
$\mathbf{I}/$	VV (NM)			-		VV (NM)	į.
<b>/</b> /	\( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \langle \cdot \) \( \la	VV (NM)	VV (NM)	VV (NM) - 2	VV (NM) 2	7 <5 0.71	}
	1 7 7	<.5 7.3	<.5 6.6	1	<.5 5.	4 5<1 3.5	\ 1
	1 1 -	1.3 <1 2.9	.5 <1 2.4	~ (	.5<1 2.		1
1 /	- 13 0 6	4.3	1<2 4.6	· 1	1 \2	C 1 7 2 - A	. 1
1	29.3	2<5 10.8	2 < 5 10.	·	1 2 < 5	5 < 10	51
1	50.7	31.11	5 < 10 30.		5 < 10 32	0 ≥10 730	2
500	3139	43.6	≥10 45.5	5 ≥10 44.5	7	372 N=	
1	-	N= 5027	N= 4900	· .	1 N= /-		-
/				1	1		\
/	-						\
	1						\ }
/	1	1		1	\		\ <b>\</b>
5 Vigibility The	resholds			<del></del>	<del></del>		September
5 Visibility Thu	#3001G5					•	oahraiiingi

Marine Area C

Marine Area A

Marine Area B

Nikol'skoe		Khatirka-In-Chukot		Ugol'naja		Buhte Providenja	
VISIBILITY (NM)	3	VISIBILITY (NM)	7	VISIBILITY (NM)	7.	VISIBILITY (NM)	3
<.5	1.4	<.5	1.3	<.5	4.1	<.5	1.2
.5 <1	0.5	.5 <1	1.0	.5 <1	3.2	.5 <1	1.4
1<2	1.1	1<2	2.2	1<2	6.0	1<2	4.1
2 <5	5.9	2 <5	9.1	2 <5	11.3	2 < 5	8.8
5 < 10	18.6	5 < 10	5.5	5 < 10	13.6	5 < 10	19.6
≥10	72.5	10 ≥10	80.9	≥10	61.8	≥10	65.0
N=	5552	N=	3551	N=	5148	N=	4556
Norheast Cape		Nome		Unalakiest		Cape Romanzof	
VISIBILITY (NM)	<u>"</u>	VISIBILITY (NM)	3	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	3
<.5	1.3	<.5	0.7	<.5	0.6	<.5	2.3
.5 <1	1.9	.5 <1	1.5	.5 <1	1.0	.5 <1	3.8
1<2	5.0	1<2	2.8	1<2	1.4	1<2	3.1
2 <5	12.5	2 < 5	7.4	2 <5	3.2	2 < 5	9.2
5 < 10	44.7	5 < 10	20.5	5 < 10	18.7	5 < 10	33.6
≥10	34.6	≥10	67.1	≧10	75.2	≥10	47.9
N=	11097	N=	21813	N=	15781	N=	18667
Cape Newenham		King Salmon		Port Heiden		Cold Bay	
VISIBILITY (NM)	7,	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	<u>\$</u>	VISIBILITY (NM)	<b>%</b>
<.5	0.5	<.5	1.3	<.5	0.6	<.5	0.3
.5 <1	1.8	.5 <1	1.0	.5 <1	1.2	.5 <1	0.7
1<2	2.9	1<2	1.4	1<2	1.6	1 < 2	1.8
2 < 5	11.0	2 < 5	3.9	2 < 5	5.9	2 < 5	8.2
5 < 10	34.7	5 < 10	21.2	5 < 10	17.1	5 < 10	50.7
≥10	49.0	≥10	71.3	≥10	73.6	≥10	38.3
N=	20546	N=	18847	N=	2043	N=	14380
Nikolskí		St. Paul		Adek		Shemye	
VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	<u>*</u>	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	<u>3</u>
<.5	10.6	<.5	0.8	<.5	0.2	<.5	1.5
.5 <1	0.7	.5 <1	1.2	.5 <1	0.5	.5 <1	2.1
1<2	0.4	1<2	2.3	1<2	2.8	1<2	3.8
2 <5	6.3	2 < 5	9.4	2 < 5	16.0	2 <5	11.4
5 < 10	35.9	∬ 5 <10	67.6	5 < 10	72.9	5 < 10	49.6
		11		ł ł		11	31.5
≥10	46.1	≥10	18.6	≥10	7.6	<u>}</u>   ≥10	ر.از

Marine Area D

VISIBILITY (NM)	3	VISIBILITY (NM)	2	VISIBILITY (NM)	%	VISIBILITY (NM)	<u>z</u>
<.5	1,7	<.5	2.2	<.5	1.3	<.5	1.8
.5 <1	2.2	.5 <1	2.0	.5 <1	1.7	.5 <1	1.4
1<2	3.9	1<2	4.0	1<2	4.4	1<2	2.6
2 <5	10.3	2 <5	13.6	2 <5	14.2	2 <5	9.6
5 < 10	25.1	5 <10	36.3	5 < 10	37.2	5 < 10	31.8
≥10	56.8	≥10	41.8	≥10	41.1	≥10	52.6
N=	1374	N=	1795	N≔	4302	N=	6867
Marine Area E	173	65	180/	170°	2-1	160 Marine Area F	
VISIBILITY (NM)	ž				2 VSV	VISIBILITY INM	2 %
<.5	2.5		VV (NM) Z	VV (NM) % VV (NA		<.5	1.5
.5 <1 1 < 2	3.2		<.5 2.2		. 1 /	.5 <1	1.6
2 < 5	10.8		5 .5 <1 2.7		- c V K	2 < 5	3.0 9.3
5 < 10	33.5	Sh	1<2 4.4	1122 3.01		5 < 10	30.8
≥10	48.2		2 < 5 10.	2 3 13 15 15		≥10	53.9
N=	9001		5 < 10 26.	21.1-1	59.41	N=	9724
			≥10 53.1 N= 925	1 =10 40.5	278		
1 July	60.		N- 925	N= 233	<u> </u>	1 - 7	. 51
VV (MA			<del></del>	<del></del>		Z 1 / /	$A = \{a\}$
55 71	2.01	Z VV (NM) Z	•		V (NM) 3 V	V CAME	1 / 5
1152	1.0	2.0 < 5	VV (NM) Z		- 161	1.9	1 7 6
16 /2-6	~ · D   4	2.01.5<1		2.0	1.71	$3.5$ \ /2	
11 15	2<5	4.9 1 1/2	_	+ 1 . 3 ~ 1	1<2 4./	25 10.3	ا ۲۰ کم
10 5		2<5 12.1		) 1 1 2 1	2<5 15.4	13. 13. 1	
55. N= 11	~· ) / >1 ~ ~ /	.3 5 < 10 31.9	5 < 10 33.	3 2 3 12.0	5 < 10 38 . 3		``
120		.3 ≥10 50.5	≥10 43.8	_ 1	≥10 38.4	≥10 1076 V	
1 0		N= 182	N= 666		N= 3433	1	
1/		-	1				
1/	VV (NM)			+		VV (NM) Z	ľ
V	1 <.5	VV (NM)	VV (NM) %	VV (NM) 3	VV (NM)	1 75 1.71	·
	1.5 <1 2.1	1 <.5	<.5 2.6		<.5 2.	11 - 11	1
	1<2 1.8	1.5 <1 1.9	.5 <1 2.2	- 1	.5<1 1.	0 1 1 < 2	.\
1	10 0 ~	3.8	1<2 3.2	1<2 2.6	1<2 3.		7
1	`'' 70 ~	2 < 5 10.2	2 < 5 9.5		1 ~	6 5 < 10 52	3
500	54.4	31.5	5 < 10 31.5	5 5 < 10 32.7	5 < 10 33	31 = 665	,7 \
308	N= 3133	, JO.U I	≥10 51.	≥10 50.5	68	95 N=	
		N= 3939	N= 4293	N= 4680	N= 68		_ \
1 /							\
/				T = -			\ [
		1			1	\	\ \
5 Visibility Thr	resholds						October

Marine Area C

Marine Area A

Marine Area B

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	Khetirke-In-Chukot		Ugol'neje		Buhta Providenja	
*	VISIBILITY (NM)	7	VISIBILITY (NM)	%	VISIBILITY (NM)	7,
	<.5	-	<.5		<.5	2.7
	1 1		14		11	3.6
	k k		11		j j	7.8
	4.1		11		11	13.2
	11		iii		5 < 10	18.1
	≥10	72.8	1 1		} ≥10	54.6
5297	N=	3278	N=	5005	N=	4328
	Nome		Unelekieet		Cape Romanzof	
<u>z</u>	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	3	VISIBILITY (NM)	<u> </u>
3.8	<.5	2.4	<.5	1.4	<.5	5.2
4.7	.5 <1	4.0	.5 <1	2.2	.5 <1	5.5
9.6	1<2	5.1	1<2	2.3	1<2	4.7
19.0	2 < 5	9.7	2 < 5	5.6	2 < 5	13.4
45.7	5 < 10	24.6	5 < 10	22.2	5 < 10	34.1
17.1	≥10	54.1	11 ≥10	66.3	10 ≥10	37.2
10394	N=	21113	N=	15373	N=	17766
	King Selmon		Port Heiden		Cold Bay	
3	VISIBILITY (NM)	<u> 3</u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	2
2.8	<.5	2.5	<.5	2.9	<.5	1.1
4.5	.5 <1	1.9	.5 <1	1.9	.5 <1	1.8
5.6	1<2	2.7	1<2	1.7	1<2	2.9
14.6	2<5	4.7	2 < 5	6.2	2 < 5	10.1
35.9	5 < 10	21.3	5 < 10	14.8	5 <1C	50.7
36.7	≥10	67.0	≥10	72.4	≥10	33.4
19319	N=	18239	N=	1802	N=	13920
	St. Paul		Adek		Shemya	
3	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	3	VISIBILITY (NM)	3
13.8	<.5	1.4	<.5		<.5	2.0
1.1	.5 <1	2.1	.5 <1		l f	2.7
	1<2		14		11	4.8
5.7	2 <5	13.1	2 < 5	17.0	2 <5	14.0
	5 < 10	65.5	5 < 10	71.8	5 < 10	54.0
35.9	11 3 \ 10					
35.9 42.7	≥10	14.8	<u>≥</u> 10	6.0	10 ≥10	22.5
	3.8 4.7 9.6 19.0 45.7 17.1 10394 3.8 4.5 5.6 14.6 35.9 36.7 19319	2.2	X     VISIBILITY (NM)     X       2.2     <.5	\$\begin{array}{c c c c c c c c c c c c c c c c c c c	\$\begin{array}{c c c c c c c c c c c c c c c c c c c	\$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)   \$   VISIBILITY (NAM)

November

Marine Area A		Marine Area B		Marine Area C		Marine Area D	
VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u> </u>	VISIBILITY (NM)	7.	VISIBIL TY (NM)	<u>z</u>
<.5	2.6	<.5	1.4	<.5	1.9	<.5	2.0
.5 <1	4.1	.5 <1	2.7	.5 <1	2.6	.5 <1	2.2
1<2	8.8	1<2	5.2	1<2	5.4	1<2	3.7
2 < 5	15.8	2 < 5	11.1	2 <5	14.3	2 < 5	11.5
5 < 10	19.0	5 < 10	26.3	5 < 10	37.5	5 < 10	36.4
≥10	49.8	≥10	53.4	≥10	38.3	≥10	44.2
N=	1200	N=	2489	N=	30.5	N=	6565
11-	1200	IN-	2409	14—	3040	14-	0000
Merine Aire E	170	65°	180		~~	160 Marine Area F	
VISIBILITY (NW)	3		7	75-	Vev	VISIBILITY (NA	D <b>3</b>
<.5	2.2	( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )	VV (NM) %	VV (NM) 3 VV (NI	<u> </u>	<.5	2.0
.5 <1	2.3	ζ,	<.5 3.2	<.5 1.6 <.5	T /	1> 5.	1.9
1<2	3.9	,	.5 <1 3.3	5<1 6.3 .5 <1		1<2	3.5
2 < 5	12.1	Sh	5 1<2 7.7	1<2 14.2 1	<b>v</b>	2 < 5	10.7
5 <10 ≧10	36.0 43.4		2<5 16.6	5 2<5 16.6 2		5 < 10	33.1 48.7
1 N=	6684		5 < 10 17.	2 5 < 10 27.7 5 <		≥10 N=	8410
			≥10 52.0		07 17		
1			N= 908	N= 253 N	K		Ţ <sub>α</sub> ,
VV (NA	0		1				$n \geq n$
(5.5)	NV (NM)	,		+		IV (NM)	في فر
( ) 1.5 <1	5.0 <.5	Z VV (NM) Z	VV (NM) Z		V (NM)	<.5	1 2/2
1/52	3.6 5.5 5.9 153	2.4 <.5 0.9 5.4 5<1		1 <.5 1.9	<.5 2.0 5<1 2.8	.5 < 1 . 7	1 / /5
2 <5	11 . I ` ` <	5.4 .5 <1 4.3		1 5 < 1 3.1	5 < 1 2.0	1<2 3.51	، ه\ (مر <sup>الم</sup>
5 < 10		a - 1 - 0.0	1<2 6.0		1 - 2	2 2 21 7	الم المكي
\[ \int \geq \frac{\geq 10}{N=}  5;	7 . 1 . 10 . 7	3 11 - 10./	2 < 5 9.6	2 < 5 13.5	4	15 210 45 71	( )
55° / 1/2 6	75 1 40	7/ 2/.0	5 < 10 19.	4 5 < 10 32.8	3 \ 10	≥10 43.	,
The		67	≧10 61.		2568		
1 0	-	N= 233	N= 1350		N= 2500	1	
1/			l			-	
1/	VV (NM)		*- <del></del>	+	7	VV (NM) 2.1	
V	<.5 2.6	VV (NM) Z	VV (NM)	VV (NM) 3	VV (NM)	A 4.0	•
	3 4	?   <.5 > 5	<.5 2.4	1	<.5 2.	31.551 26	, <b>\</b>
i <i>i</i>	1<2 3.4	1.5 < 1 2.7	.5 <1 2.4	· · · · · · · · · · · · · · · · · · ·	1	1<2	3
1 1	~ \.) 1 ~	1 1<2 4 7	1<2 4.	' i ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' '	1 < 2	6 4 7 01	6
<b>1</b>	5 < 10 35 . 2	12.41	2 < 5 12.	- 1	1 2 < 5	6 5 < 10 17	11
1. /	0 30 0 I	35.2	5 < 10 36.0	'	5 < 10	2 8 1 = 10 55	B2\
500	N= 2886	€10 42.5	≥10 42.9	9 ≥10 44.6	≥10 4	652 N= 33	
1		N= 3548	N= 3516		N= 50		
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5 Visibility Thr	esholds						November
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## 11-132

Nikol'skoe		Khatirka-In-Chukot		Ugol'neje		Buhta Providanja	
VISIBILITY (NW)	<u>*</u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<u>z</u>	VISIBILITY (NM)	<b>Ž</b>
<.5	4.5	<.5	4.4	<.5	14.4	<.5	3.7
.5 <1	4.2	.5 <1	3.3	.5 <1	7.1	.5 <1	3.5
1<2	4.6	1<2	8.6	1<2	8.6	1<2	6.3
2 < 5	10.2	2 < 5	10.0	2 < 5	12.5	2 < 5	10.6
5 < 10	17.6	5 < 10	7.0	5 < 10	13.0	5 < 10	18.2
≥10	58.9	≥10	66.7	≥10	44.4	<u>≥</u> 10	57.7
N=	5460	N=	3282	N=	5218	N=	4476
Norheast Cape		Nome		Unalakleet		Cape Romanzof	
VISIBILITY (NM)	3	VISIBILITY (NM)	<u> 3</u>	VISIBILITY (NM)	<u>3</u>	VISIBILITY (NM)	5
<.5	3.3	<.5	3.5	<.5	2.2	<.5	7.8
.5 <1	4.6	.5 <1	3.6	.5 <1	2.0	.5 <1	ć.8
1<2	8.4	1<2	4.4	1<2	2.2	1<2	4.0
2 < 5	17.4	2 < 5	9.6	2 < 5	5.4	2 < 5	14.0
5 < 10	38.4	5 < 10	24.5	5 < 10	26.7	5 < 10	32.2
≧!0	27.8	_, ≥10	54.5	≥10	61.5	≥10	34.~
№=	9459	N=	21808	N=	15851	N=	16673
Cape Newenham		King Salmon		Port Heiden		Cold Bay	
- (SIB L ** (NM)	3	VISIBICITY (NM)	7	VISIBILITY (NM)	<u>.</u>	VISIBILITY INM	5
<.5	4.2	<.5	2.4	<.5	5.2	<.5	3
.5 <1	5.2	.5 <1	3.2	.5 < 1	3.5	.5 <1	3.3
1 < 7	7.5	1<2	3.8	1<2	2.2	1<2	4.8
2 <5	16.0	2 < 5	5.4	2 < 5	7.2	2 < 5	
5 < 10	35.2	5 < 10	24.0	5 < 10	23.6	5 < 10	46.Î
≥10	31.8	≥10	61.3	≥10	58.3	≥10	29.8
∱4 <u> =-</u>	19154	N=	18839	N=	1986	N=	.4385
Nikolski		St. Paul		Adak		Shemye	
VISIBILITY (NM)	<b>3</b>	VISIBILITY (NM)	7.	VISIBICITY (NM)	3	VISIBIC TY (NM)	<u> </u>
	12.4	<.5	4.4	<.5	1.4	<.5	2.8
<.5		1.1		11	2.0	.5 < 1	3.€
<.5 .5 <1	1.7	.5 <1	3.7	.5 < 1	2.0		ં . '્
		.5 <1 1 <2	3.7 4.1	1 1<2	4.8	1<2	5.9
.5 <1 1 <2	1.7	1.1		1<2	4.8	1<2	
.5 <1 1 <2 2 <5	1.7 1.5	1<2	4.1	1	4.8 17.9	1 < 2 2 < 5	5.9
.5 <1 1 <2 2 <5 5 <10	1.7 1.5 7.0 39.2	1 < 2 2 < 5 5 < 10	4.1 14.9 60.8	1 < 2 2 < 5 5 < 10	4.8 17.9 69.9	1 < 2 2 < 5 5 < 10	5.9 '6.7 52.
.5 <1 1 <2 2 <5	1,7 1.5 7.0	1 < 2 2 < 5	4.1 14.9	1<2 2<5	4.8 17.9	1 < 2 2 < 5	5.9 .6.

December

Marine Area D

S.5   6.2   S.5   4.8   S.5   3.4   S.5   2.9	VISIBILITY (NM)	7.	VISIBILITY (NM)	3	VISIBILITY (NM)	3	VISIBILITY (NM)	<u>z</u>
5 < 1	<.5	6.2	<.5	4.8	<.5	3.4	<.5	2.9
1	Į.			5.2	.5 <1	3.9		
S < 10	1<2		1<2	10.5	1<2	6.2	1	4.4
≥10	2 < 5	16.7	2 < 5	13.1	2 <5	14.2	2 < 5	11.2
N=   2045   N=   3267   N=   346   N=   6226	5 < 10	14.7	5 <10	22.4	5 < 10	31.4	5 < 10	35.0
Marine Area E   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170   170	≥10	40.1	≥10	44.0	≥10	40.9	≥10	44.3
\$\( \frac{5}{5} \) 2.6 5 \( \frac{1}{2} \) 2.7 1 \( \frac{1}{2} \) 4.7 2 \( \frac{1}{3} \) 3.3 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1} \) 3.5 5 \( \frac{1} \) 3.5 5 \( 1	N=	2045	N=	3267	N=	346 *	M=	6226
\$\( \frac{5}{5} \) 2.6 5 \( \frac{1}{2} \) 2.7 1 \( \frac{1}{2} \) 4.7 2 \( \frac{1}{3} \) 3.3 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1}{3} \) 3.5 5 \( \frac{1} \) 3.5 5 \( \frac{1} \) 3.5 5 \( 1			<u></u>					
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5 < 1		- 11			7	w a V	`	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1	11		VV (NM) Z	- 1	_	4	
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Marine Area C

Marine Area A

Marine Area B

## Map 6. Cloud amount

BLACK LINE – Percent frequency of total cloud amount  $\leq 2/8$ .

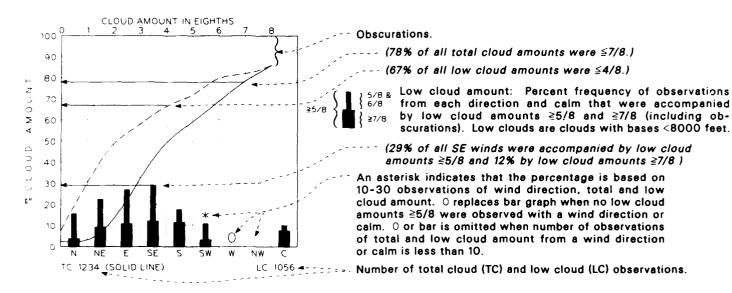
BLUE LINE – Percent frequency of low cloud amount  $\geq 5/8$ .

Albers Equal—Area Conic Projection

# Graphs: Cloud cover/wind direction

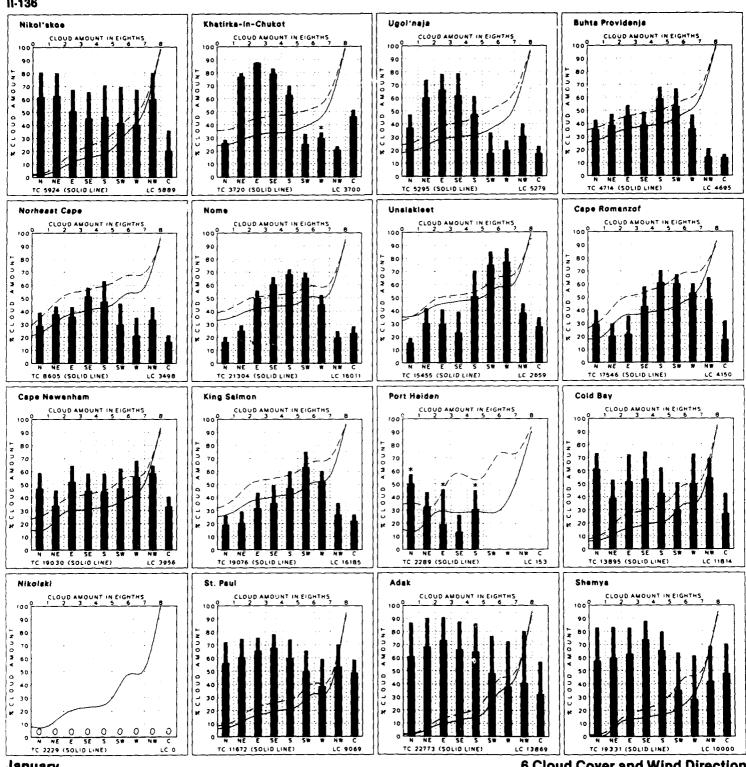
Total Cloud Amount }

Cumulative percent frequency of indicated cloud amount equal to or less than the amount intersected by the curve.



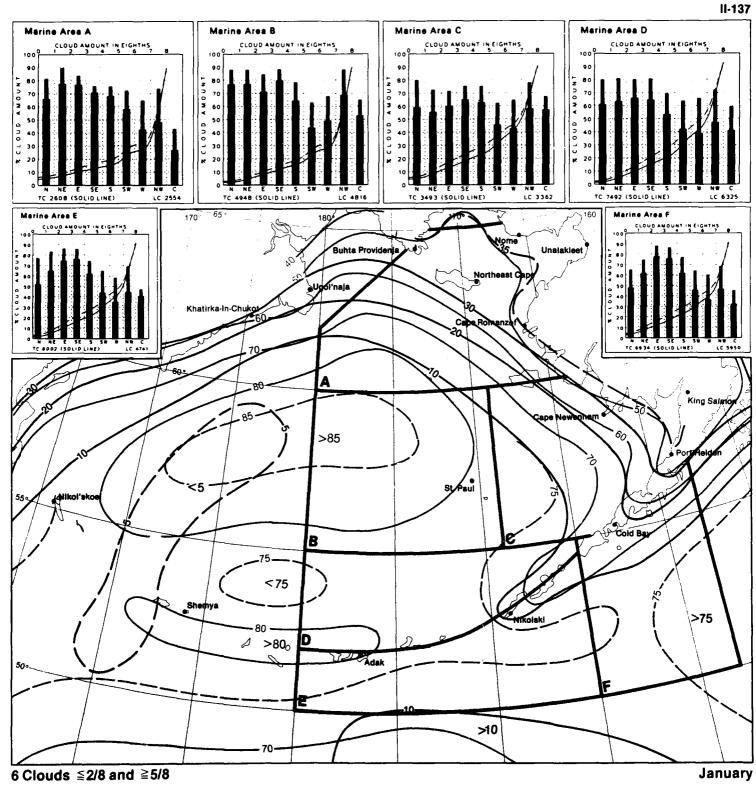
A survey of the cloud data (total and low cloud amounts) from the marine data base shows the number of total cloud reports significantly greater than that of low cloud amounts. This is because many of the early marine observations contain only total cloud amounts. Therefore, somewhat different samples may be used to compute the two curves on the graph. This may lead to inconsistencies where the low cloud amount appears higher than the total cloud amount. Where this occurred, the graph was adjusted in favor of the total cloud by making the curves coincide. The frequency of obscured conditions may be determined from the graph by subtracting the cumulative percent frequency on the curve corresponding to 8/8 coverage from 100%. In computing the bar graph, obscurations are considered as 8/8 coverage.

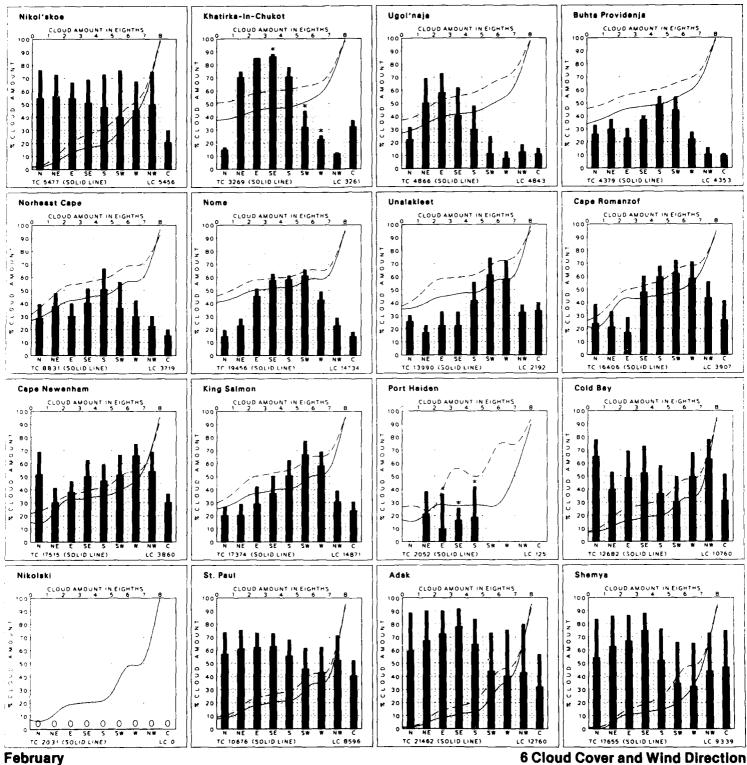
For the two isopleth presentations (total cloud amount  $\leq$  2/8 and low cloud amount  $\geq$  5/8), only those observations reporting both total and low cloud amounts were summarized. This helps eliminate problems introduced as a result of different size data sets. A comparison of total cloud analyses based on satellite data by the U.S. Department of Commerce and U.S. Air Force (1971) shows a fairly close agreement with, and bolsters the confidence in, the marine cloud statistics presented in this atlas. Refer to the texts in Sets 3 and 4 for additional information on clouds.

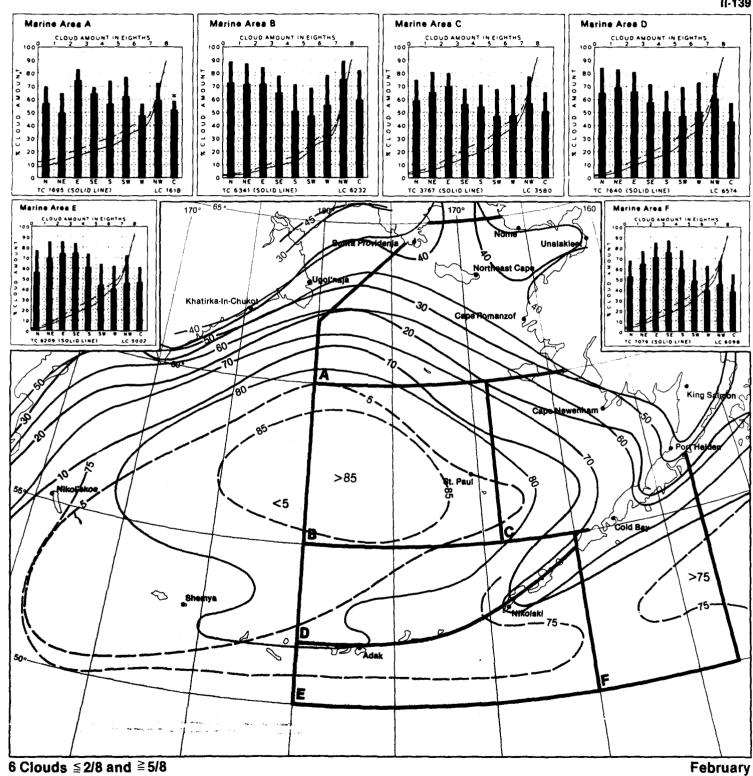


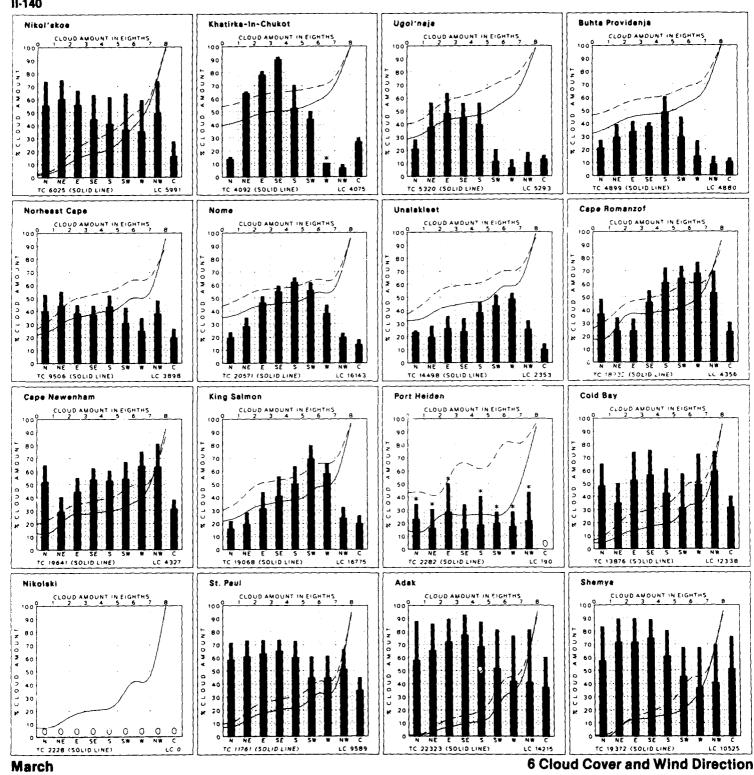
January

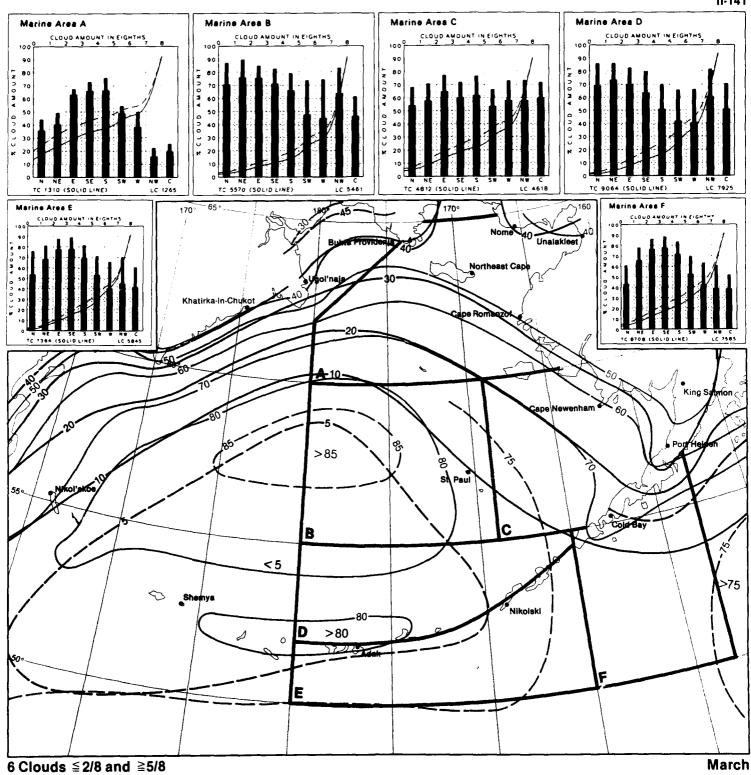
**6 Cloud Cover and Wind Direction** 



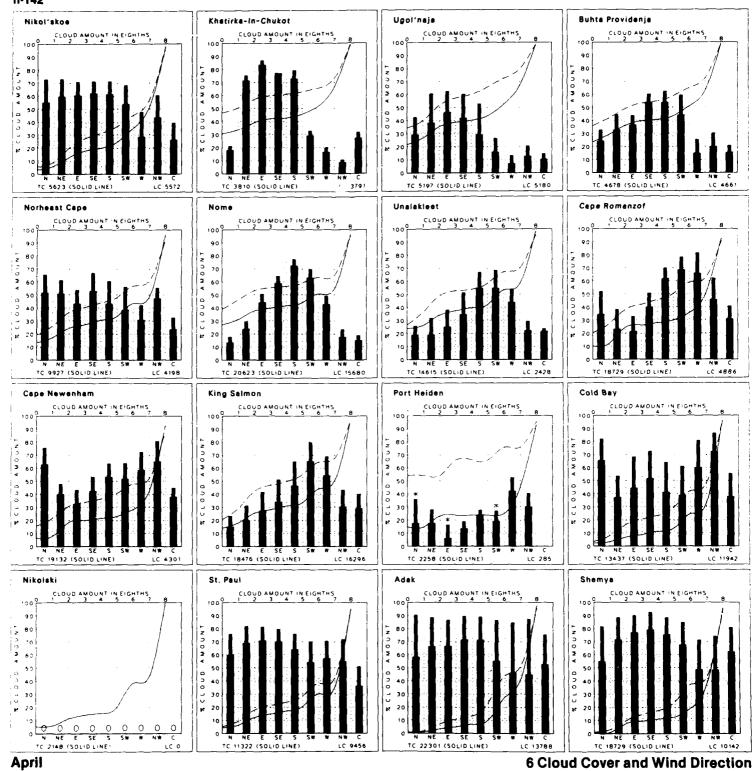


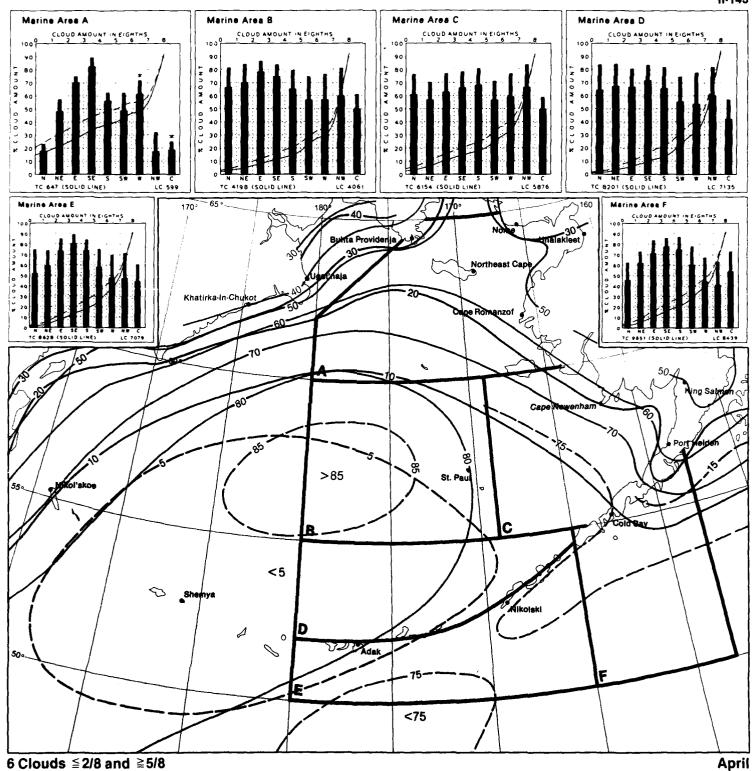




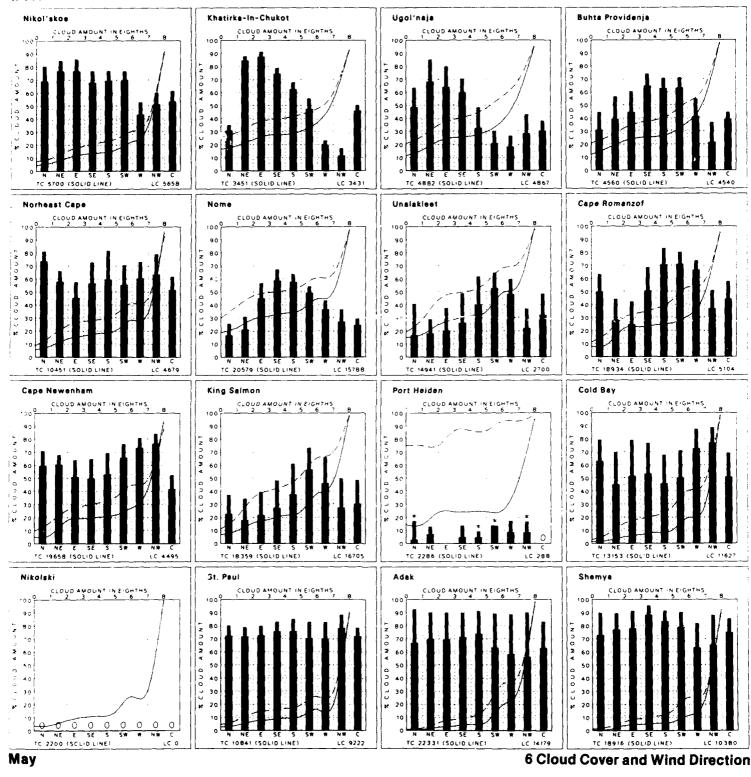


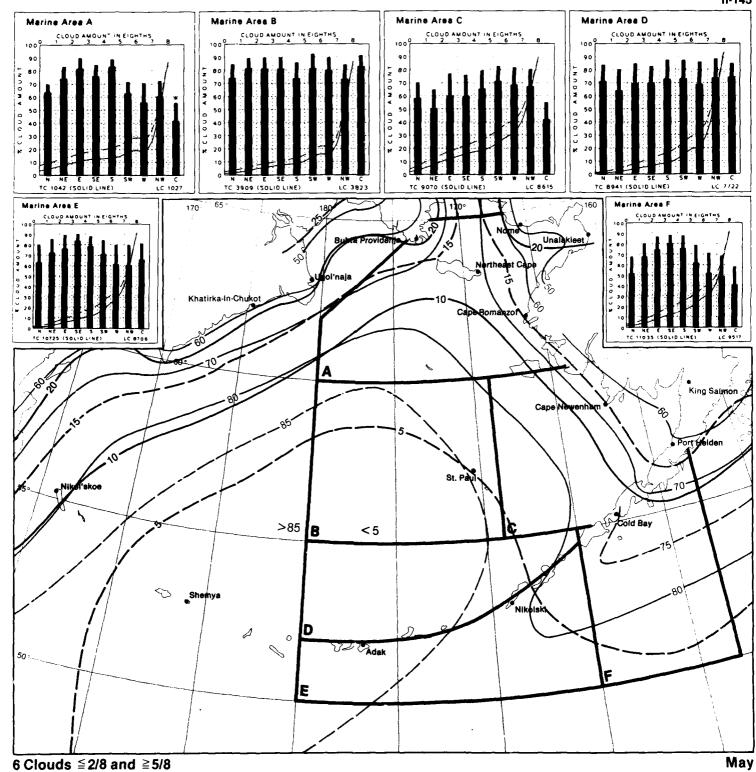
#### 11-142

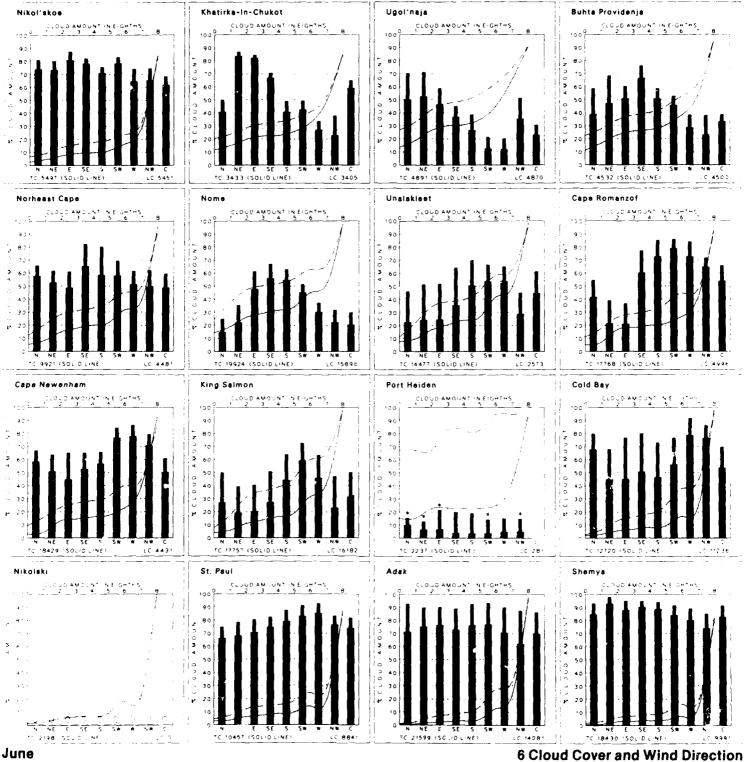


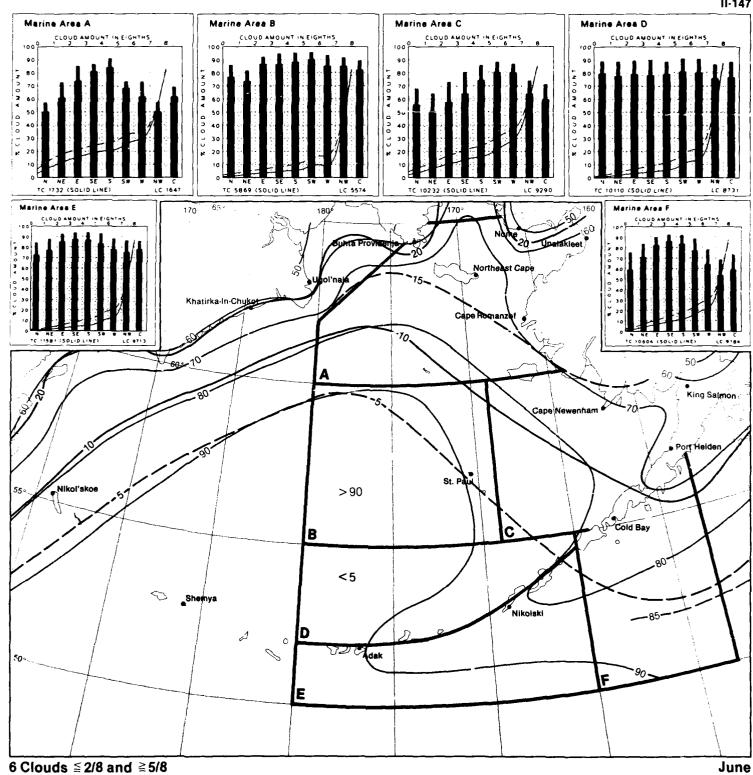


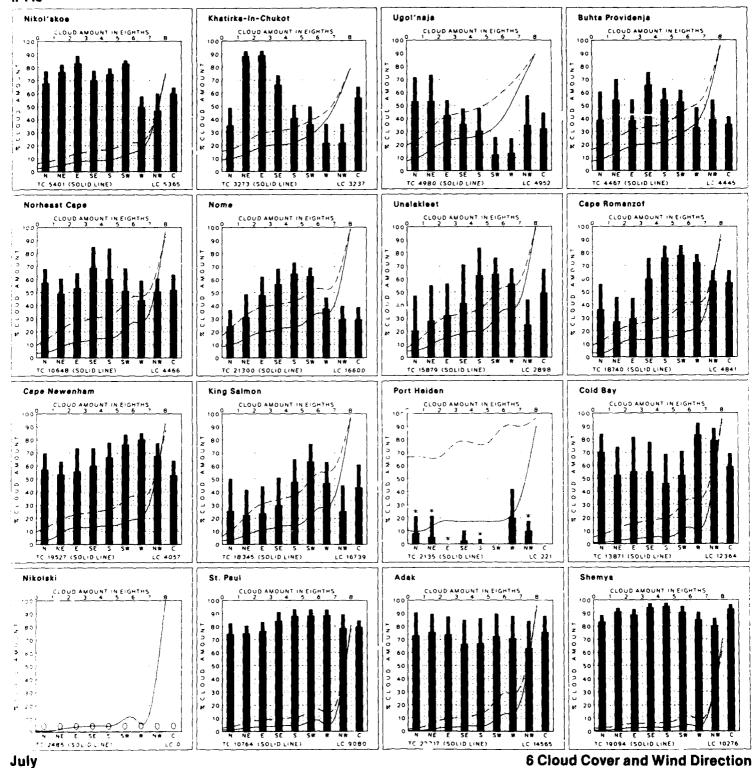
### 11-144

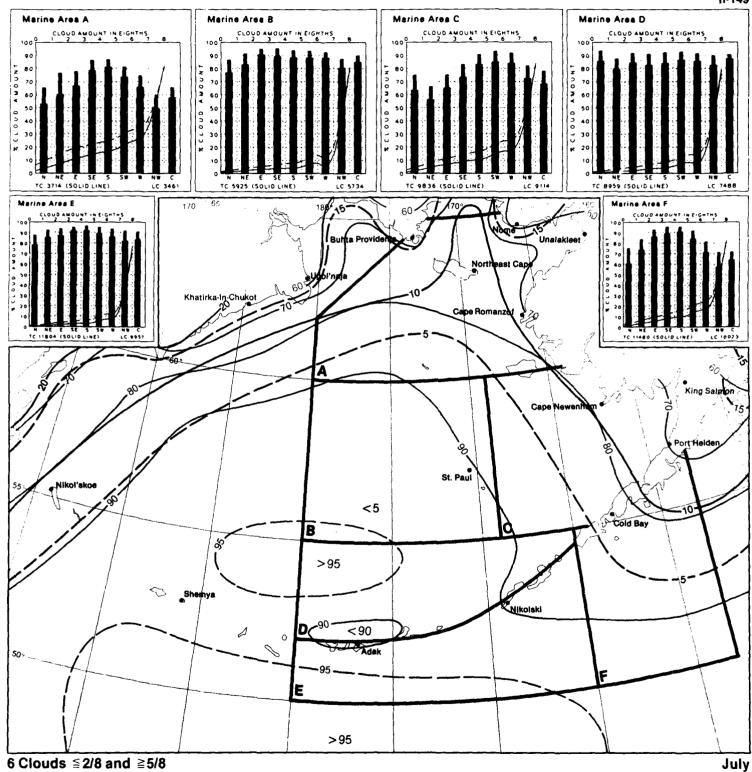


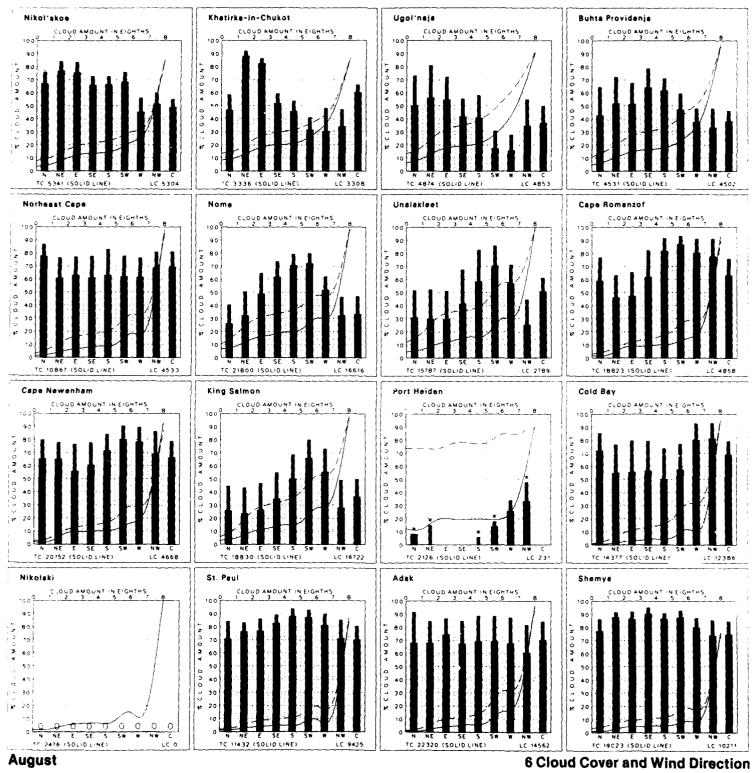


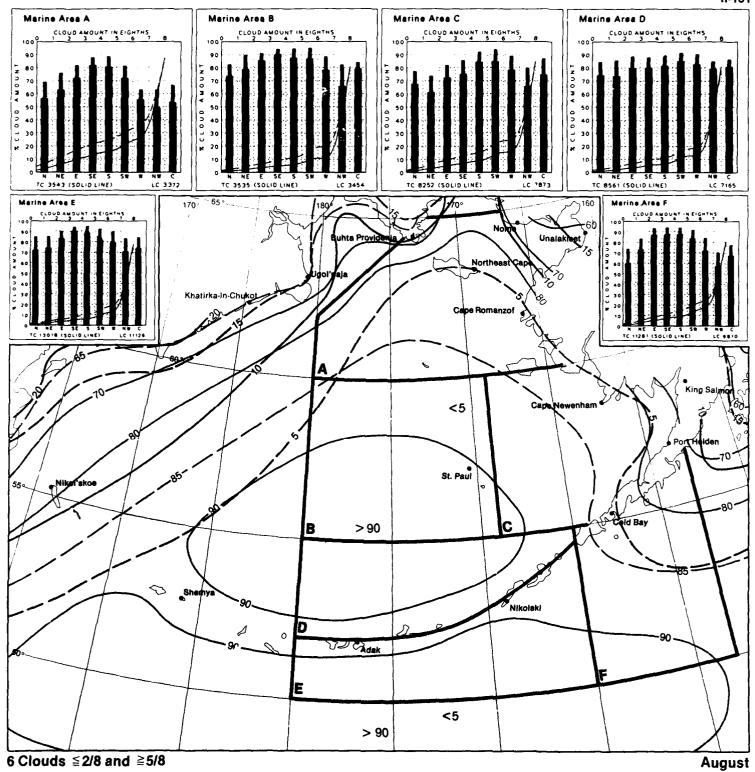




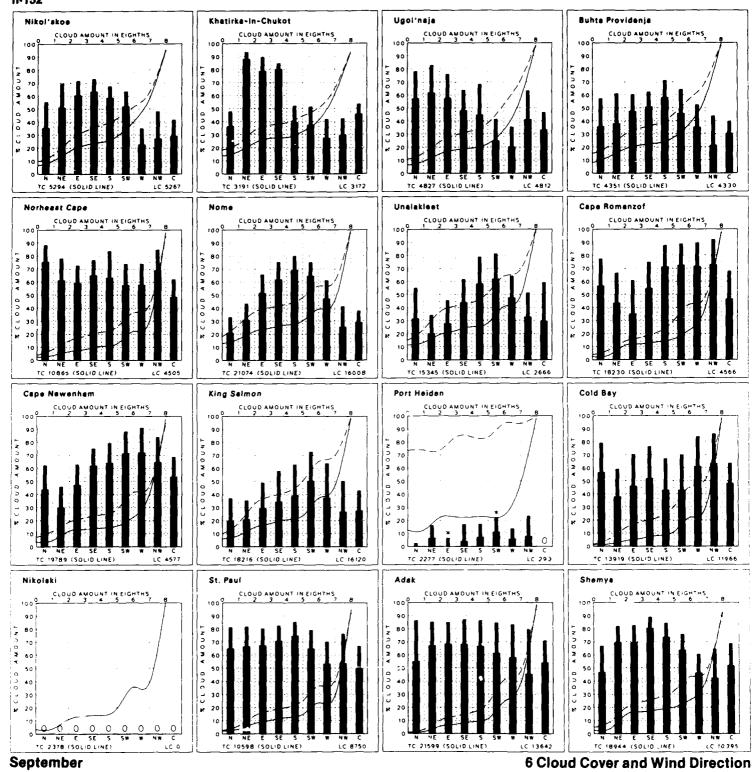


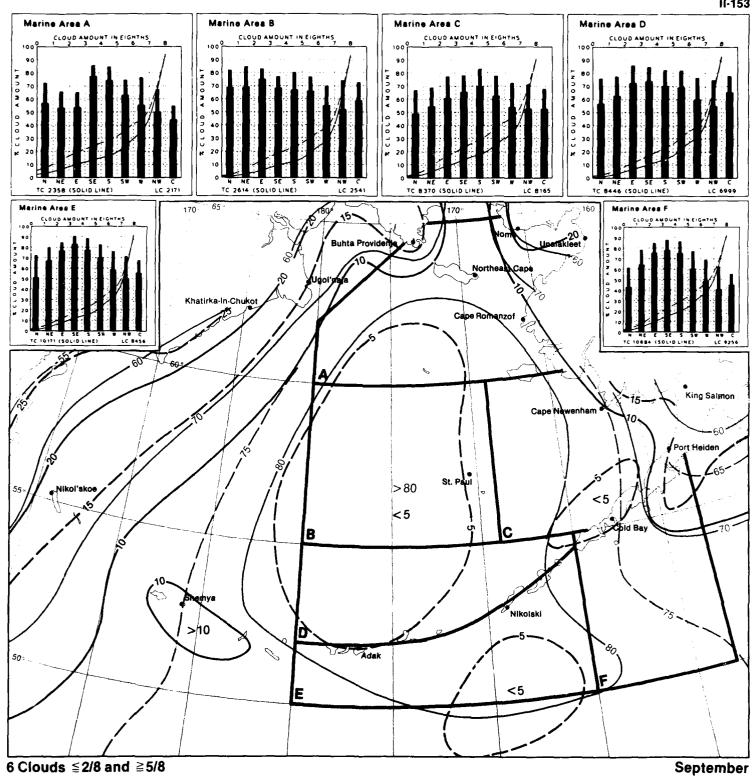


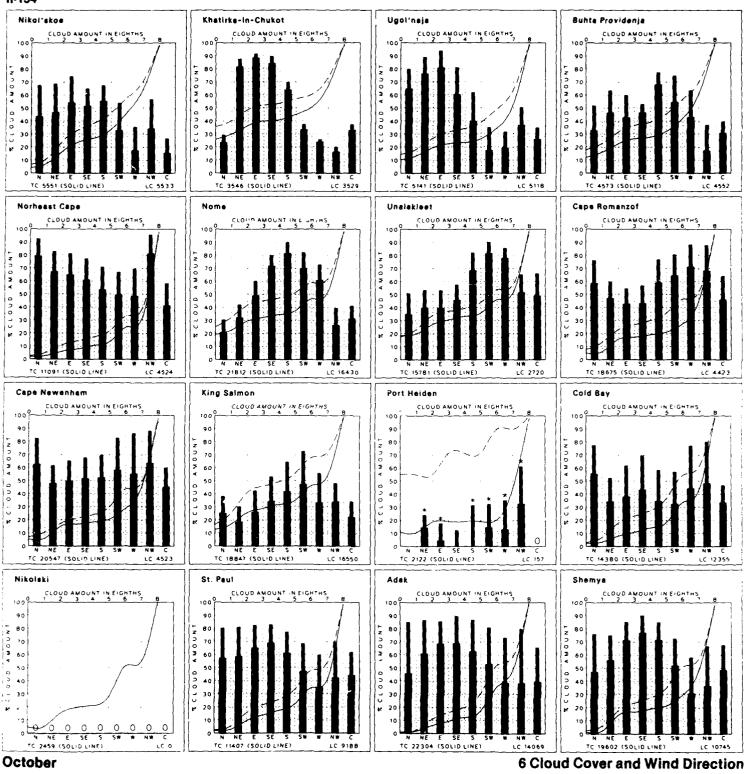


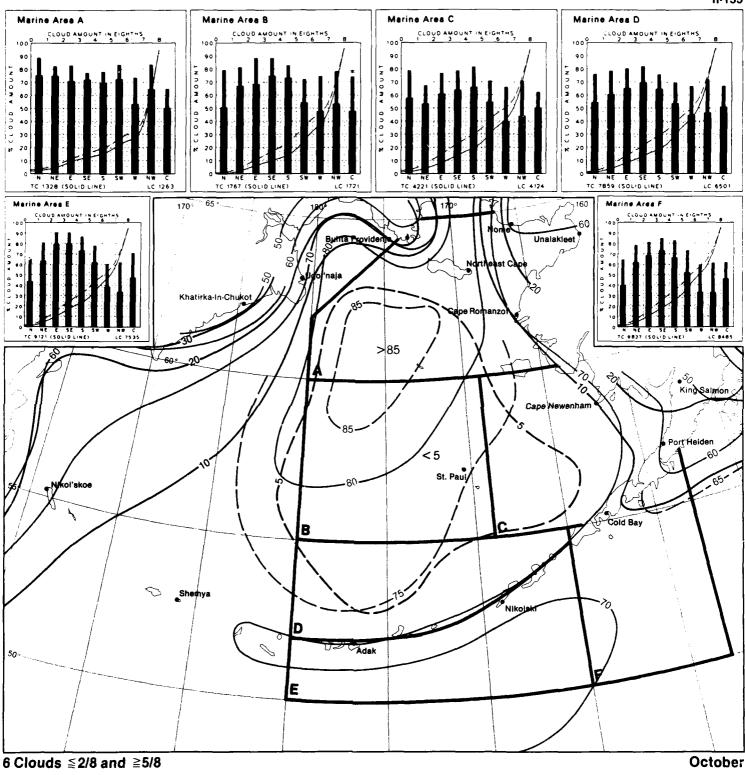


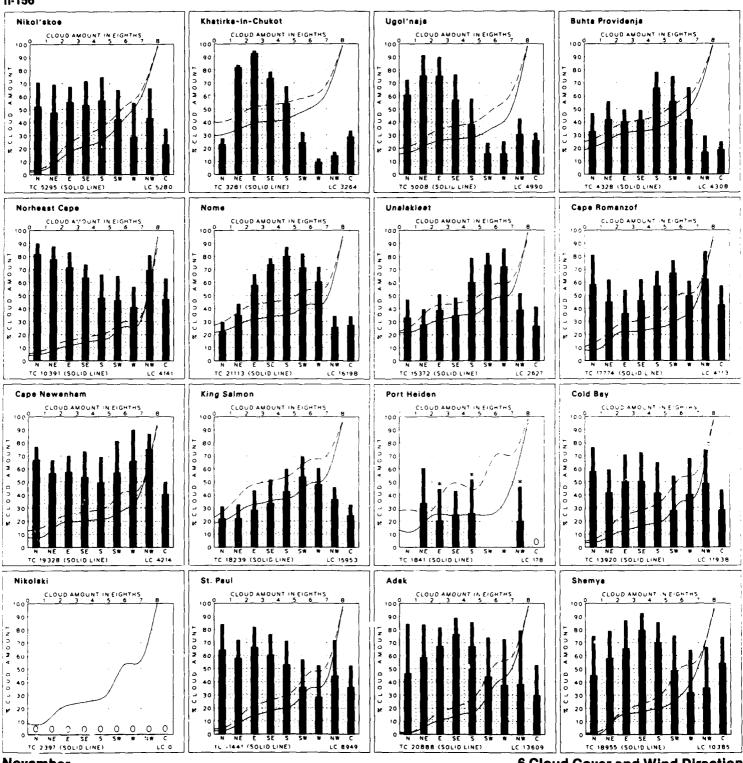
#### II-152





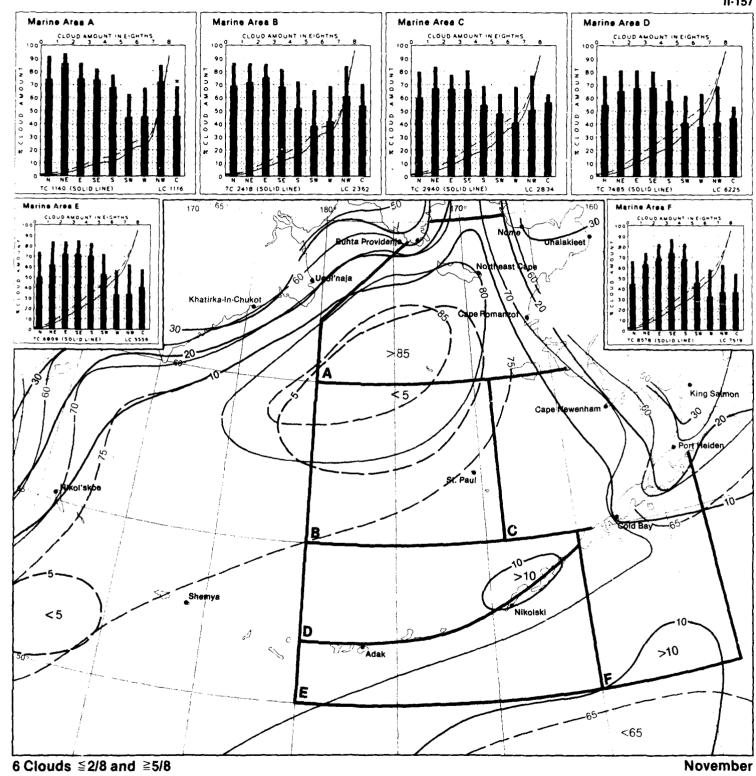


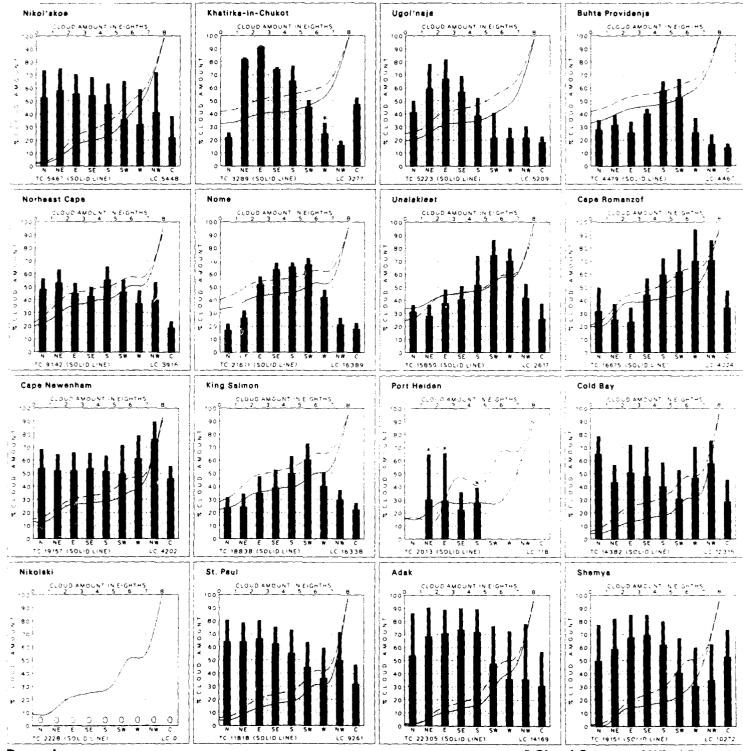




November

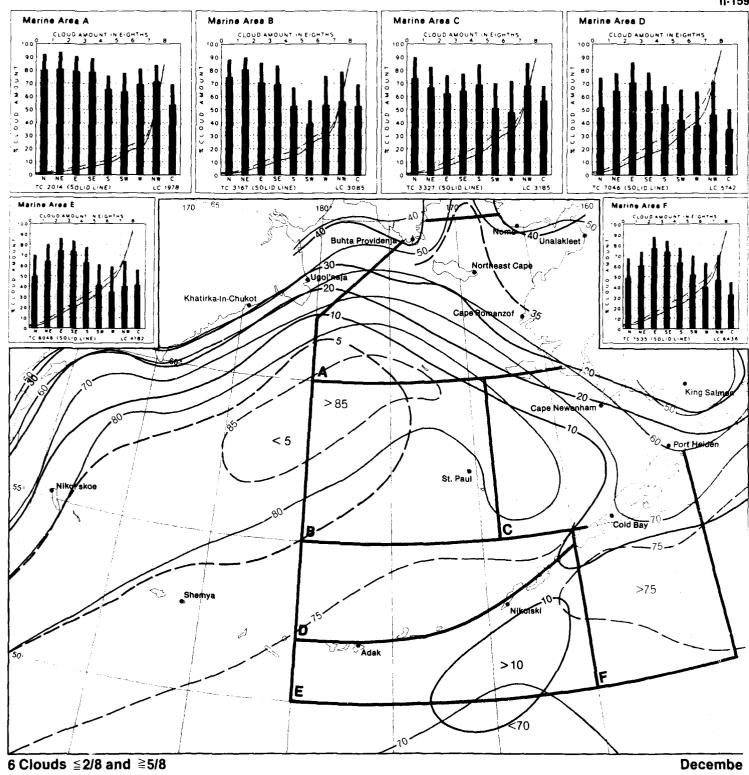
6 Cloud Cover and Wind Direction





December

6 Cloud Cover and Wind Directio



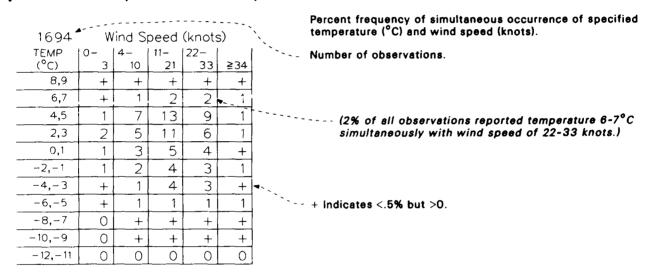
# Map 7. Air temperature extremes (°C)

BLACK LINE — Maximum (99%) air temperature (1% of temperatures were greater than the given value).

BLUE LINE — Minimum (1%) air temperature (1% of temperatures were equal to or less than the given value).

Albers Equal-Area Conic Projection

# **Graphs:** Air temperature/wind speed



Air temperature is one of the elements most frequently observed by mariners. On many ships, the heating effect of the ship's structure has a tendency to produce higher than actual ambient air temperature readings because of instrument exposure. This is especially true under calm, sunny conditions. Despite the inaccuracies, the large-scale patterns and mean gradients of the isopleth analyses are relatively accurate.

The temperature scale of the graphs varies in both range and class interval. The graph can be used to determine the extent of human discomfort from the combined effects of extreme heat or cold and winds, or to estimate the likelihood of superstructure icing. Refer to Section I of this atlas for detailed information on superstructure icing and wind chill.

7 Legend

Legend 7

Nikol'akoe	1				
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TEMP	0-	4-	11-	22 -	1 1
(°C)_	3	10	21	33	≥ 34
≩6	0	0	0	0	0
4,5	0	+	0	+	0
2,3	+	+	1		1
0,1	+	2	5	3	1
-2,-1	1	5	11	6	3
-4 - 3	1	5	8	5	2
-6,-5	2	5	7	3	2
-8,-7	2	4	5	2	1
-10,-9	1	1	2	+	+
-12,-11	+	1	1	+	+
≦~13	+	+	+	+	+

K	Khatirka-in-Chukot								
	3669	Wil	nd Sp	eed	(kno	ts)			
	TEMP	0-	4 ~	11-	22 -	1 1			
	(°C)	3	10	21	33	≥34			
	≩-4	5	5	7	3	+			
	-6,-5	2	2	2	_ 1	+			
	-8,-7	1	1	3	1	1			
	-10,-9	1	1	2	-	+			
	-12,-11	1	1	1	2	1			
•	-14,-13	1	1	2	2	1			
	-16,-15	1	1	2	2	1			
	-18,-17	1	,	3	3				
	-20,-19	1	•	2	2	+			
	-22,-21	1	1	3	1	1			
,	≨-23	1	4	8	3	1			

U	Boj, uaja					
	5256	Wis	nd Sp	eed	(kno	ts)
	TEMP	0 -	4 -	111-	22-	
	(°C)	3	10	_21	3.3	≩34
	≩ -6	3	4	7	7	3
ľ	-8,-7	2	2			+
	-10,-9		+	1	1	+
	-12,-11	1	1		1	2
	-14,-13	1	1	1	2	_ 2
	-16,-15	1	1	1	2	2
	-1817		1	1	2	3
	-20,-19	1	+		2	2
	-22,-21		1		2	2
	-24,-23	1	1	1	2	2
•	≨-25	3	2	2	4	5

hte Prov	(IGER	•								
4678	Wil	Wind Speed (knots)								
TEMP	0-	4 -		22 -						
(°C)	3	10	21	33	≥34					
≥-4	2	6	8	2	+					
-6,-5	1	2	_4_	4	. +					
-8,-7	1	2	5_	1	+					
-10,-9	1	1	2	1	+					
-12,-11	1	2	3		+					
-14,-13	2	2	2	1	+					
-16,-15	2	2	3	لكا	+					
-1817	3	3	_ 3		+					
-20,-19	2	1	1	+	+					
-2221	3	2	1	+						
§-23	12	3	1	+	+					

Norheast (	Cape				
8544	Wir	nd Sp	eed	(kno	ts)
TEMP	0 -	4	11-	22-	1
(°C)	3	10	21	3 3	≥34
≥-4	1	3	7	5	1
-6,-5	1	_2	2	, ,	+
-8,-7	1	_ 2	3	1	+
-10,-9	1	1	3	1	+
-12,-11	1	2	2	+	+
-14,-13	1	3	3	1	+
-16,-15	1	2	3	+	+
-18,-17	2	4	3	1	+
-20,-19	2	4	3	1	+
-22,-21	.2	_ 2	2	+	0
≦-23	8	6	4	+	0

N	ome					
	22017	Wi	nd Sp	eed	(kno	ts)
	TEMP	0 -	4 -	11 -	22 -	1 1
	(°C)	3	10	_21	33	≥34
	≥-4	1	4	12	3	+
	-6,-5		2	3	1	+
	-B,-7		2	3	1	+
	-10,-9	1	3	_3	1	+
	-12,-11	,	2	2	1	+
	-14,-13	2	2	3	1	+
	16,- :5	1	2	.2	+	+
	-18,-17	2	2	2	1	+
	-20,-19	2	_ 2	_2	+	+
	-22,-21	Ĩ	2	1	+	+
	≦-23	12	9	2	+	+

15434 Wind Speed (knots)    TEMP
(°C) 3 10 21 33≥34 ≥-6 1 4 10 4 +
≥-6 1 4 10 4 +
-B,-7 + 1 3 2 +
-10,-9 + 2 3 2 +
-12,-11 + 1 2 2 +
-14,-13 1 2 3 2 +
-16,-15 1 2 2 2 +
-18,-17 1 2 3 2 +
-20,-19 1 2 2 1 +
-22,-21 1 2 1 1 +
-24,-23 1 2 2 1 +
≦-25 5 12 4 1 +

Cape Rom	enzof				
17446	w:	nd Sp	eed	(kno	(2)
TEMP	0-	4 -	11-	22~	
(°C)	3	10	21	33	≩ 34
<b>≩</b> 0	1	2	_8_	_2	
-21	1	2	5	[ _2]	+
-4,-3	2	3	6	2	•
-6,-5	2	1	3	1	+
-8,-7	2	2	3	1	+
-10.~9	2	1	2	,	+
-12,-11	1	1	:	•	+
-14,-13	2	1	1	2	1
-16,-15	2	1	2	1	
-18,-17	1	1	2	1	+
<u>s</u> -19	3	3	6	6	3

18410	Wil	nd Sp	eed	(kno	ts)
	0 -	4-	111-	22-	i
(°C)	3	10	21	3 3	≥34
≩ 2	+	1	6	4	+
0.1	1	4	9	3	+
-2,-1	2	_ 3	5	2	+
-4,-3	3	3	4	1	+
-65	2	1	,	1	+
-B7	3	2	1	1	+
-109	3	2	1	+	+
-12,-11	2	1	1	1	+
-14,-13	2	1	1	+	+
-16,-15	2	1	1	+	+
<u>≨</u> -17	6	5	6	1	0

KI	ng Saimi	o n				
	19078	Wi	nd Sp	eed	(kno	ts)
	TEMP	0 -	4-	11-	122-	1 1
	(°Ç)	3	10	_21_	. 33	≥34
	≥0	1	9	11	5	+
	-2,-1	1	4	2	+	+
	~4,-3	,	4	2	+	+
	-6,-5	1	3	1	+	0
	-87	2	3	1	+	0
	-109	2	3	1	+	0
	-12,-11	1	2	. 1	+	0
	-14,-13	_2	2	1	+	0
	-16,-15	1	2	1	+	+
	-18,-17	1	2	1	+	0
•	<u>≤</u> -19	6	11	7	1	+

St. Paul

Port Heide	n				
6361	wi	nd Sp	eed	(kno	ts)
1EMP (°C)	0 - 3	10	11- 21	22~	≥ 34
≥6	+	+	1	+	+
4,5	+	1	2	1	+
2,3	1	4	9	4	1
C,1	2	8	9	2	+
-2,-1	2	8	3	+	0
-4,-3	2	5	2	+	0
-6,-5	1	3	2	+	+
-8,-7	1	2	1	+	0
-10,-9	1	2	1	+	0
-12,-11	+	2	1	0	0
≦-13	1	5	7	1	0

Cold Bay					
13894	Win	nd Sp	eed	(kno	ts)
TEMP	0~	4 -		22 -	
(°C)	3	10	21	3.3	≥ 34
≹Β	0_	+	+	+	0
6,7	+	+	+	1	+
4,5	+	+	3	3	1
2.3	+	2	10	6	1
0.1	1	8	1.1	4	1
-2,-1	1	4	4	1	+
-4,-3	1	4	4	1	+
-6,-5	1	3	2	1	+
-B,-7	+	ز ا	3	2	+
-10,-9	+	2	3	,	+
≦-11	+	2	3	1	+

Nikoleki					
2113	Wis	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11-	22 -	1 1
(°C)		10	21	33	≥34
≥ 10	0	0	0	0	0
8,9	0	0	0	0	0
6,7	+	+	+	+	+
4,5	+	+	_ 2_	1	0
2,3	1	4	9	4	+
0,1	3	13	20	6	+
-21	3	6	7	3	+
-4,-3	1	3	4	2	+
-6,-5	1		2	1	+
-8,-7	+	+	1	+	0
\$-9	0	0	1	+	0

11604	Wi	nd Sp	eed	(kno	ts)
TEMP	10 -	4 -	11-	22~	í
_(°C)	. 3	10	_21	_33	₹34
≧6	0	0	+	+	+
4,5	_0	+	_ +	1	+
2,3	+	2	8	5	+
0,1	1	6	15	6	1
-2,-1	1	3	6	2	+
-4,-3	_ 1	2	5	2	+
-6,-5	1	2	3	3	+
-8,-7	+	2	_ 3	3	+
-10,-9	+	1	3	2	+
-12,-11	+	7	2	1	+
≨-13	+	1	2	2	+

22766	Wii	nd Sp	eed	(kno	(s)
TEMP	0-	4 -	111-	22-	ł
(°C)	3	10	21	33	≥ 34
≥ 10	0	0	0	0	0
8,9	0	+	+	+	+
6,7	+	1	1	1	+
4,5	1_	_3	3	_ 1	+
2,3	3	_9	12	4	+
0,1	4	10	14	5	+
-2,-1	3	4	5	1	+
-4,-3	3	3	3	1	+
-6,-5	1	1	+	+	0
-8,-7	1	+	+	+	O
≨-9	1	+	0	0	0

Adak

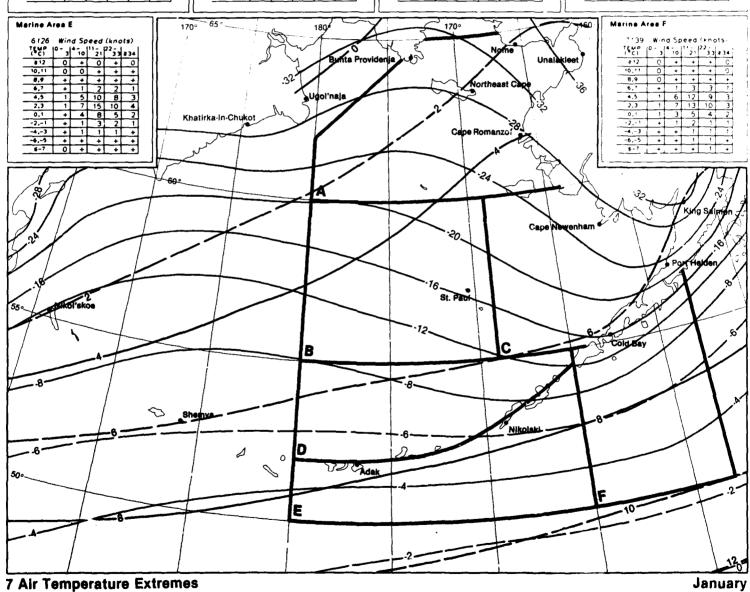
Shemye						
19232	Wii	nd Sp	eed	(knc	(s)	
TEMP	10 -	4 -	11-	122 - 1	1 1	
(°C)	3	10	21	33	≥ 34	
≥8	0	0	0	+	_0	
6,7	0	+	0	0	+	
4,5	+	+	+	1	+	
2,3	1	_2	7	6	1	
0,1	3	7	16	9	2	
-2,-1	2	.5	10	5	1	
-4,-3	2	4	7	3	+	
-6, 5	!	-	1	1	+	
-8,-7	+	+	+	+	+	
-10,-9	+	+	+	0	+	
≦-11	+	+	0	+	_0]	

Marine A	ea A	•			
2807	Wi	nd Sp	eed	(kno	ts)
TEMP	0 ~	[4-	11-	22-	1 1
(°C)	3	10	21	33	≩34
≩4	+	_ +	_ 1	+	+
2,3	+	1	3	1	+
0.1	+	3	8	5	1
-2,-1	1	3	7	4	1
-4,-3	1	2	5	4	1
-6,-5	+	1	3	3	1
<b>-6,-</b> 7	+	1	3	3	-
-10,-9	+	1	2	3	1
-12,-11	+	1	2	3	1
-14,-13	+	1	2	1	1
5-15	_	1		1	<u> </u>

М	Marine Area B							
	4949	Wi	nd Sp	eed	(kno	ts)		
	TEMP	0-	4-	11-	22 -	1 1		
	(°C)	_3	_10	21	_33	≥34		
	≥8	+	+	+	+	+		
	6,7	0	+	+	+	+		
Ī	4,5	+	1	2	2	+		
Ī	2,3	1	3	9	5	1		
	0,1	1	_5	12	8	2		
•	-2,-1		2	_6	4	1		
	-4,-3	+	2	5	3	1_		
	-6,-5	+	1	4	2	+		
•	-8,-7	+	_1	3	2	+		
•	-10,-9	+	1	2		+		
-	≦-11	+	1	2	2	1		
•								

М	arine A	ea C				
	3884	Wi	nd Sp	eed	(kno	ts)
	TEMP	0-	4 -	11 -	22 -	
	(°C)	3	10	21	3 3	≥34
	≩10	0	+	0	0	0
	8,9	0	+	+	+	0
	6,7	+	+	+	4	+
	4,5	+	2	6	3	1
	2.3	1	5	14	7	2
	0,1	1	5	10	5	1
	-2,-1	1	2	4	2	+
	-4,-3	1	1	2	2	_:]
	-6,-5	+	1	2	2	+
	-8,-7	+	1	2	2	1
	≦-9	+	+	2	2	1
•						

Marine Area D								
75. <sup>7</sup> 6	Wi	na Sp	eec	(kno	ts)			
TEMP	0 -	4 -		22 -	1			
(°C)	] 3	10	21	33	≥ 34			
0¹ ≤ِ	+	+	+	+	+			
0,9	+	+	+	+	+			
6.7	+	1	1	1	+			
4.5	+	3	7	6	2.]			
2,3	1	6	13	10	3			
0.1	1	4	10	8	3			
-2,-1	+	1	4	3	1			
-4,-3	+	1	2	2	1			
-6,-5	+	+	1	1	+			
-8,-7	+	+	+	+	+			
≨ -9	0	+	+	+	+			



N	kol'skoe	)				
	5438	Wi	nd Sp	eed	(kno	ts)
	TEMP	0 -	4-	11-	22-	1 1
	(°C)_	3	10	21	33	≩34
	≩6	0	0	0	0	0
	4,5	0	0	+	0	0
	2,3	+	+	1	+	+
	0,1	+	2	4	2	1
	-2,-1	1	4	9	7	31
	-4,-3	1	5	9	5	3
	-6,~5	2	5	8	4	1
	-8,-7	2	4	6	3	1
	-109	1	1	2	1	+
	-12,-11	+	1	ī	+	+
	£-13	+	+	+	+	+

KI	atirka-i	n-Chi	ıkot			
	3223	wi	nd Sp	eed	(kno	ts)
	TEMP	0 -	4 -	11-	122 - 1	
	(°C)_	3	10	21	33	≩34
	≩-8	5	5	6	3	
	-10,-9	1	1	1	1	+
	-12,-11	1	1	2	1	1
	-14,-13	1	1	2	2	1
	-16,-15	1	1	3	2	_ T
	-18,-17	1	2	5	4	2
	- 20,-19	1	1	2	2	+
	-22,-21	1	1	5	3	1
•	-2423	1	2	4	2	1
	-26,-25	1	2	3	1	1
	≤-27	1	4	4	1	1

ol'naja					
4832	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	14 -	11-	22 -	
(°C)	3	10	21	33	≥34
≩-8	3	3	5	5	2
-10,-9	1	1	1	+	+
-12,-11	1	1	1	1	1
-14,-13	1	1	1	1	1
- i6,-15	1	1	1	2	2
-18,-17	2	1	. 2	3	3
-20,-19	1	+	1	2	2
-22,-21	1	1	1	3	4
-24,-23	2	1	2	3	4
-26,-25	2	1	2	_3	3
<u>≤</u> -27	3	2	3	3	5
	4832 TEMP (°C) ≥ -8 -10,-9 -12,-11 -14,-13 -i6,-15 -18,-17 -20,-19 -22,-21 -24,-23 -26,-25	4832 Winterpretation of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control	4832 Wind Sp TEMP 0 - 4 - (°C) 3 10 ≥ -8 3 3 3 - 10, -9 1 1 - 12, -11 1 1 1 - 14, -13 1 1 1 - 16, -15 1 1 1 - 20, -19 1 + -22, -21 1 1 1 - 24, -23 2 1 - 26, -25 2 1	4832 Wind Speed  TEMP   0 -   4 -   11 -   (°C)   3   10   21  æ-8   3   3   5 -10,-9   1   1   1 -14,-13   1   1   1 -16,-15   1   1   1 -18,-17   2   1   2 -20,-19   1   +   1 -24,-23   2   1   2 -26,-25   2   1   2	4832 Wind Speed (kno TEMP   0 -   4 -   11 -   22 -   (°C)   3   10   21   33   2 - 8   3   3   5   5   5   10 - 9   1   1   1   1   1   1   1   1   1

uhta Providenja							
4327	Wi	nd Sp	eed	(kno	15)		
TEMP	0 -	4 -	11-	22-	1		
(°C)	3	10	21	33	₹34		
<u>₹</u> -8	2	5	9	2	+		
-10,-9	1	1	2	+	+		
-12,-11		2	3	1	+		
-14,-13	1	2	4	1	+		
-16,-15	2	3	4	1	+		
-18,-17	3	3	4	1	+		
-20,-19	2	2	1	+	0		
-22,-21	4	3	2	+	+		
-24,-23	5	2	1	+	9		
-26,-25	4	2	1	+	0		
€-27	8	2	+	+	+		

Norheast (	Cepe				
8799	Wi	nd Sp	eed	(kno	ts)
TEMP (°C)	0 - 3	4 -	11- 21-	22~	≥34
≩~8	2	5	10	6	1
-10,-9	ī	2	2	1	+
-12,-11		2	_2	+	0
-14,-13	1	2	2	1	+
- 16, - 15	2	2	2	+	0
-18,-17	2	3	3	+	+
-20,-19	2	4	2	+	+
-22,-21	2	3	2	+	0
-24,-23	4	4	_2	+	+
-26,-25	3	3	2	+	+
<u>≰</u> -27	7	7	2	0	0

H	om e					
	20105	Wi	nd Sp	eed	(kno	ts)
	TEMP	0-	4-	(11-	22~	1 1
	(°C)_	3	10	21	33	≥ 34
	≧-6	3	دء	11	3	+
	-8,-7	1	2	3	1	+
	-10,-9	1	2	3	1	+
	-12,-11	1	2	2	+	+
	-14,-13	2	2	3	1	+
	-16,-15	1	2	1	1	+
	-18,-17	2	3	.2	+	+
	-20,-19	2	3	2	+	+
-	-22,-21	2	2	1	+	+
_	-24,-23	3	3	1	+	+
	≨-25	13	8		+	+

Unelakies	<b>!</b>				
13972	w;	nd St	beed	(kno	ts)
TEMP	10 -	4-	11-	22~	1
(°C)	3	10	21	3 3	≥ 34
≩ -8	1	6	12	4	+
-109	+	1	3	2	+
-12,-11	1	1	2	2	+
-14,-13	, 1	2	3	3	+
-16,-15	1	1	2	1	+
-18,-17	1	2	2	2	+
-20,-19	1	2	2	1	+
-22,-21	1	2	1	+	+
-24,-23	1	2	1	+	+
-26,-25	1	2	1	+	+
≦-27	6	12	2	+	v

16317	Wi	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	[22 - ]	
(°C)	3	10	21	3 3	≥ 34
≥4	3	5	12	3	+
-65	2	1	_2		+
-87	2	1	2	1	+
-109	2	1	2	2	+
-12,-11	1	1	1	1	+
-14,-13	2	1	2	2	1
-16,-15	1	1	2	2	7
-18,-17	1	1	2	2	1
-20,-19	1	1	2	2	,
-22,-21	1	1	2	2	1
≦-23	1	3	5	4	

Cape New	enha	m			
17474	Wi	nd Sp	seed	(kno	ts)
TEMP	0	4 -	11 -	22 - 1	1
(°C)	3	10	21	33	≩34
≥2	+	1	4	2	+
0,1	1.	_3_	9	2	+
-2,-1	2	3	5	1	+
-4,-3	2	3	3	1	+
-6,-5	1	2	2	1	+
-8,-7	2	1	1	+	+
-10,-9	2	2	1	+	+
~12,-11	2	2	1	+	+
-14,-13	2	2	2	+	+
~16,-15	1	2	1	+	0
<b>≨</b> ~17	6	8	9	2	+

Ki	ng Salme	o n				
	17369	Win	nd Sp	besi	(kna	(5)
	TEMP	0-	4-	11-	22- 1	
	(°C)	3	₹0	21	33	≩34
	≧-2	2	11	13	_ 3	+
	-4,-3	1	4	2	+	0
	-6,-5	1	2	1	+	0
	-8,-7	1	3	2	+	0
	~10,-9	1	3	1	+	0
	~12,-11	1	2	1	+	0
	~14,-13	1	3	2	+	0
	~16,-15	1	2	1	+	0
	-18,-17	1	2	2	+	0
	-20,-19	1	3	2	+	0
	≦-21	4	10	6	+	+

5709	Wi	nd Sp	eed	(kno	ts)
TEMP	10-	4 -	11-	22-	1
(°C)	3	10	21	33	≥34
≥4	+	1	_ 3	2	+
2,3	1	_ 2	_ 6	3	+
0,1	1	6	6	1	+
-2,-1	3	5	3	+	0
-4,-3	1	4	2	+	0
-6,-5	1	3	2	+	0
-8,-7	1	2	2	+	0
-10,-9	1	3	2	+	٥
-12,-11	1	2	2	+	0
-14,-13	1	2	3	+	0
≨~15	1	9	10	2	0

12682	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11-	22 -	
(°C)	3	10	21	33	≩ 34
≩6	+	+	+	+	+
4.5	+	+	1_	1	+
2,3	+	3	8	5	
0,1	1	7	11	4	1
-2,-1	1	4	5	1	+
-4,-3	1	5	5	1	+
-6,-5	+	2	4	1	+
-8,-7	1	2	5	2	+
-10,-9	+	2	3	2	+
-12,-11	+	1	1	1	+
≦-13	+	1	2	1	+

Nikoleki					
1947	wi	nd Sp	eed	(kno	ts)
TEMP (°C)	0 - 3	10	11-	22 - 33	≥ 34
≥8	0	0	0	0	0
6,7	0	0	0	0	+
4,5	+	+	1	1	0
2,3	1	3	5	2	+
0,1	5	12	14	6	+
-2,-1	3	7	9	3	+
-4,-3	1	6	7	4	+
-6,-5	+	1	3		+
-8,-7	0	1	1	1	0
-109	0	+	+	+	0
5-11	0	0	0	0	Ö

St. Paul					
10600	Wi	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22-	1 1
(°C)	3	10	21	33	≧ 34
≩4	0	+	+	+	+
2,3	+	1	3	2	+
0,1	+	4	14	4	1
-2,-1	+	3	6	3	+
-4,-3	1	2	5	2	+
-6,-5	. ±	1	3	3	+
-8,-7	+	2	3	3	1
-10,-9	+		4	3	17
-12,-11	+	1	2	2	+
-14,-13	+	1	2	2	+
<b>≦</b> -15	+	2	6	3	+

21407	Wii	nd Sp	eed	(kno	ts)
TEMP (°C)	0-3	4 -	11-	22-	≥ 34
≥ 10	ő	0	0	0	0
8,9	+	+	+	+	0
6,7	+	+	1	+	+
4,5	+	2	2	1	+
2,3	2	8	10	4	1
0,1	5	11	13	5	1
-2,-1	2	5	7	2	+
-4,-3	2	3	4	1	+
-6,-5	1	1	1	+	+
-8,-7	1	+	+	+	0
≨-9	1	+	+	+	Ō

Adek

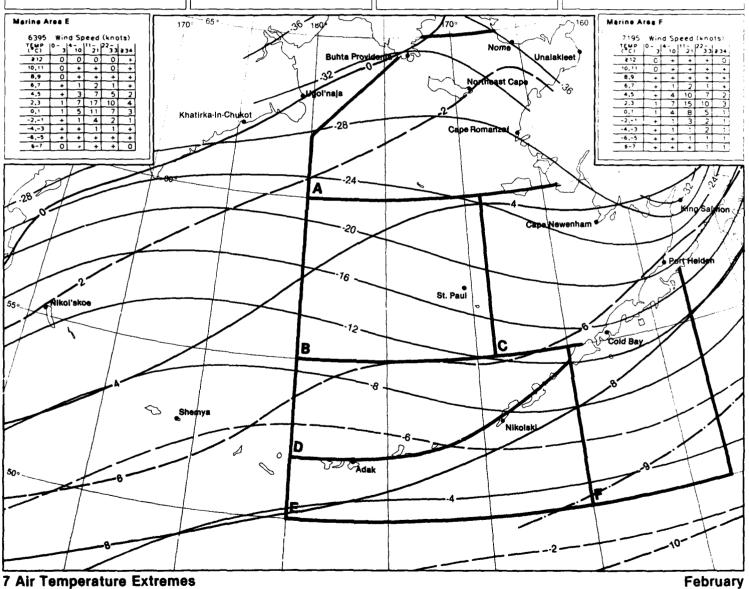
emye					
17572	w;	nd St	eed	(kno	ts)
TEMP	10 -	4-		22-	
(°C)	3	10	21	3 3	≩34
≥8	0	0	0	0	0
6,7	0	0	+	+	Ō
4,5	+	+	+	+	+
2,3	1	1	5	3	1
0.1	3	7	15	9	- 2
-2,-1	2	6	12	6	, 1
-4,-3	3	4	8	4	1
-6,-5	1	1	1		+
-8,-7	+	+	+	+	0
-10,-9	+	+	0	0	Ü
<u></u> = 11	+	+	0	0	0

Marine Area A								
1630	wi	nd Sp	eed	(kno	ts)			
TEMP (°C)	0 - 3	4-	11- 21	22- 33	≥34			
₹0	1	2	5	3	1			
-2,-1	+	3	7	3	_1			
-4,-3	+	2	4	2	+			
-6,-5	+	2	3	2	+			
-8,-7	+		3	3	+			
-109	+	1	2	2	+			
-12,-11	+	1	4	4	1			
-14,-13	+	1	5	4	1			
-1615	+	1	5	4	1			
-18,-17	+	1	3	2	_1			
<u>\$</u> -19	+	1	3	2	1			

6145 Wind Speed (knots)  TEMP 0- 4- 11- 22- (°C) 3 10 21 33 \(\frac{21}{3}\)	- 1
(°C) 3 10 21 33 ≩:	
	+
≧4 [ +	
2.3 + 1 3 2	1
0.1 + 2 6 4	1
-2,-1 + 2 4 3	1
-4,-3 + 2 4 2	1
-6,-5 + 2 4 3	1
-8,-7 + 2 5 4	1
-10,-9 + 2 5 4	1
-12,-11 + 1 4 3	1
-14,-13 + 1 3 2	1
≦-15 + 1 3 2	1

М	Marine Area C								
	4298	wii	nd Sp	eed	(kno	ts)			
	TEMP (°C)	0 - 3	4 - 10	11- 21	22 - 33	≥ 34			
	≥8	0	+	+	+	+			
	6,7	+	+	+	+	+			
	4.5	+	1	2	1	+			
	2,3	+	4	11	6	1			
	0,1	1	5	12	6	1			
	-2,-1	+	2	5	3	1			
	-4,-3	+	1	3	2	1			
	-6,-5	+	2	3	_3	1			
	-8,-7	+	1	3	_2	1			
	-10,-9	+	1	1	_ 1	1			
	≦-11	+	1	3	4	1			

Marine Area D								
7683	Wie	nd Sp	eed	(kno	ts)			
TEMP	0 -	4 -	111~	122 -	1 1			
(°C)	]3	10	.21	33	≩ 34			
≩ 10	+	+	+	+	+			
8,9	+	+	+	+	+			
6,7	+	1	1	1	+			
4,5	+	3	6	4	1			
2.3	1	6	14	10	3			
0.1	1	4	10	7	3			
-2 -1	+	2	4	4	1			
-4,-3	+	1	3	2	1			
-6,-5	+	+	2	2	1			
-8,-7	+	+	+	1	+			
<u>\$-9</u>	+	+	+	+	+			



N'k	ol'sko	)					
	5985	Wie	nd Sp	eed	(kno	ts)	
	TEMP	0-	4 -	11-	22-	1 1	ľ
	(°C)	3	10	21,	33	≩ 34	
	≩6	0	0	0	+	0	ĺ
	4,5	0	0	+	0	0	ĺ
_	2,3	+	+	1	1	+	
	0,1	+	2	5	2		i
_	-2,-1	1	_ 5	12	7	3	ì
_	-4,-3	2	6	10	4	3	i

K	Khatirka-In-Chukot							
	4034	Wi	nd Sp	eed	(kno	ts)		
	TEMP	0 -	4-	11-	22-	1		
	(°C)	3	10	21	33	≩ 34		
	≧-6	4	4	5	2	+		
	-8,-7	1	1	3	5	+		
	-10,-9	1	1	1	1	+		
	-12,-11	1	2	3	2	+		
	-14,-13	1	2	4	2	1		
	-16,-15	1	3	4	2	1		
	-18,-17	1	4	6	3	1		
	-20,-19	1	2	3	1	+		
	-22,-21	1	3	4	1	+		
	-24,-23	1	2	3	1	+		
	<u>≨</u> -25	1	3	3	1	0		

uhta Providenja							
4858	wi	nd Sp	eed	(kno	ts)		
TEMP	0 ~	4 -	11~	22 -			
(°C)	3	10	21	33	≥34		
≩-6	3	5	6	_ 1	+		
-8,-7	2	_2	3	_ 1_	+		
-10,-9	1.	2	4	+	+		
-12,-11	2	3	4	1	+		
-14,-13	3	3	3	1	+		
-16,-15	3	4	3	1	+		
-18,-17	4	4	3	+	+		
-20,-19	3	2	_2	+	+		
-22,-21	4	2	1	+	0		
-24,-23	4	_ 2	1	+	0		
≨-25	8	1	1	0	0		

Norheast Cape								
9426	Wit	nd Sp	eed	(kno	ts)			
TEMP	0-	4 -	11-	22-	1			
(°C)	3	10	21	33	≥34			
≩-4	2	4	7	3	_1			
-6,-5	1	1	1	1	+			
-8,-7	1	2	2	1	+			
-10,-9	1	2	2	1	+			
~12,-11	2	2	_2	+	+			
-14,-13	_ 3	_ 4	_ 3	_ 1_	+			
-16,-15	3	3	2	+	0			
-18,-17	3	4	3	+	0			
-20,-19	3	4	2	+	0			
-22,-21	2	2	1	+	0			
≨-23	7	6	2	+	0			

iom •					
21305	Wie	nd Sp	eed	(kno	ts)
TEMP	0 -	4-	11-	22 -	
(°C)	3	10	21	3.3	≩ 34
₹-4	1	5	9	2	+
-6,-5	1	2	2	1	+
-8,-7	1	3	3	1	+
-10,-9	2	3	3	1	+
-12,-11	1	3	2	+	+
-14,-13	2	4	3	1	+
-16,-15	2	3	2	+	+
-18,-17	2	3	2	+	0
-20,-19	3	3	1	+	0
-22,-21	2	2	1	+	0
≨-23	11	6	1	+	0

14470	Wi	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22-	1
_(°¢)	3	10	21	33	≥ 34
≩-4		6	10	3	+
-65	+	2	3	1	+
-8,-7	+	2	4		+
-109	1	3	4		+
-12,-11	1	2	3	1	+
-14,-13	1	3	4	1	+
-16,-15	1	2	2	1	+
~1817	1	3	2	1	+
-20,-19	1	3	1	+	+
-22,-2:	1	2	1	+	0
≨-23	5	8	3	+	+

	18136	Wii	nd St	eed	(kno	ts)
	TEMP	10 -	4-	111-	22-	
	(°C)	3	10	21	33	≥ 34
	<u>₹</u> 0	1	3	5	1	+
_	~21	1	2	6	_ 2	+
_	-4,-3	2	3	5	2	+
	-6,-5	1	1	2	1	+
	-8,-7	2	2	3	1	+
-	-109	2	2	3	2	+
	-1211	2	1	2	2	+
Ξ	-14,-13	2	2	3	3	1
-	-16,-15	2	1	_ 2	1	1
_	-18,-17	2	1	2	1	+
	≦-19	2	3	6	3	+

Cape New	ennai	T)			
19576	Win	nd Sp	eed	(kno	ts)
(°C)	0-3	4 - 10	11-	22 - 33	≥ 34
₹4	+	+	+	+	+
2,3	1	1	3	1	+
0,1	3	6	10	2	+
-2,-1	3	5	6	2	+
~4,-3	3	4	4	1	+
-6,-5	2	2	2	1	+
-8,-7	2	3	2	+	+
-109	2	3	2	+	+
-12,-11	1	2	1	+	+
-14,-13	2	2	2	+	+
<u>≨</u> -15	3	4	5	1	+

King Salmon										
19064	Wi	nd Sp	eed	(kno	ts)					
TEMP	0~	4 -	11-	22~	1 1					
(°C)	1_3	10	21	33	≥34					
≥4	+	2	3	1	+					
2,3	1	4	_5	_2	+					
0,1	1	7	6	1	+					
-2,-1	1	5	3	+	+					
-4,-3	2	5	3	+	+					
-6,-5	1	3	1	+	0					
-87	1	4	2	+	0					
-109	1	3	2	+	+					
-12,-11	1	2	1	+	+					
-14,-13	1	3	2	+	0					
<b>≨</b> − '5	4	9	5	+	0					

6377	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11-	22-	
(°C)	3	10	21	33	≥34
≥8	+	+	+	+	٥
6,7	+	1	1	+	0
4,5	+	2	3	1	+
2,3	1	5	8	5	1
0,1	2	9	9	2	+
-2,-1	2	7	5	1	+
-4,-3	1	5	4	+	+
-6,-5	1	3	2	+	0
-8,-7	+	2	3	+	0
-10,-9	+	2	2	+	0
<u>≨</u> -11	1	5	4	1	Ö

old Bay					
13876	Wie	nd Sp	eed	(kno	ts)
TEMP	0 -	(4 -		22-	i
(°C)	3	10	21	33	≥ 34
≥8	_ 0	+	+	+	+
6,7	+	+	+	+	. ÷
4,5	+	1	2	_ 2	+
2,3	+	4	9	5	1
0,1	1	8	12	6	1
-2,-1	t	4	5	2	+
-4,-3	1	4	5	2	+
-6,-5	+	2	4	. 1	+
-8,-7	+	2	3	1	+
~10,-9	+	1	2	1	+
≦-11	+	2	3	1	+

Nikolski					
2057	Wit	nd Sp	eed	(kno	ts)
TEMP	0-	4-		22-	
(°C)	3	10	21	33	≥34
≥ 10	0	0	+	0	0
8,9	+	0	0	0	0
6,7	+	+	0	+	0
4,5	+	1	2	+	0
2,3	2	6	8	3	+
0,1	4	12	19	7	+
-2,-1	2	4	8	3	+
-4,-3	1	3	5	3	+
-6,-5	+	1	2	1	+
-8,-7	+	1	1		0
≨-9	0	0	0	+	0

11595	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11-	22-	
(°C)	3	10	21	33	_
≥4	0	+	+	+	0
2,3	+		2	1	+
0,1	+	5	14	6	+
~2,-1	+	4	7	3	+
-4,-3	1	3	6	3	+
-6,-5	+	2	4	2	+
-87	+	2	5	2	+
-10,-9	+	1	3	2	+
-12,-11	+	1	2	1	+
-14,-13	+	1	2	2	+
≨-15	+	2	3	2	+

22293	Wit	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22 - 1	
(°C)	3	10	21	33	≥ 34
≩ 10	0	+	_0	0	0
8,9	0	+	+	+	+
6,7	+	1	1	+	+
4,5	1	3	4	_2	+
2,3	3	_10	14	4	1
0,1	4	11	15	6	1
-2,-1	2	4	4	1	+
-4,-3	2	2	2	_ 1	_+
-6,-5	1	+	+	+	+
-8,-7	+	+	+	0	0
≨-9	+	+	0	0	0

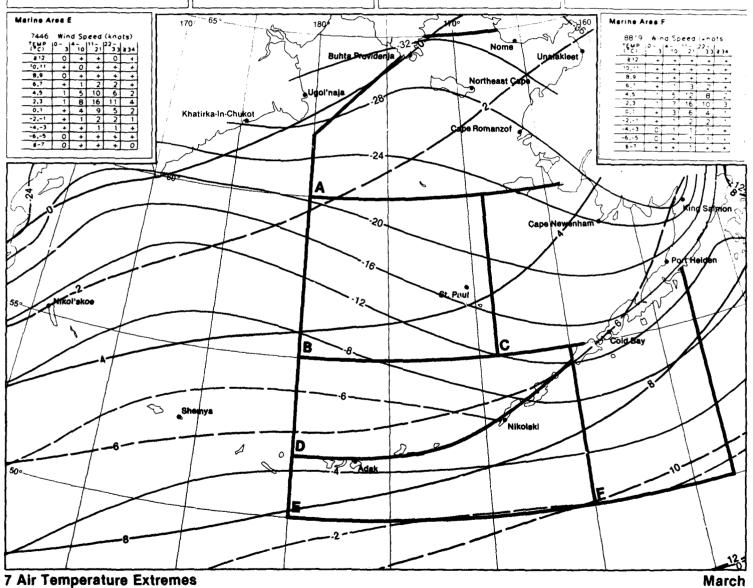
amya					
19308	Wit	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22-	
(°C)	3	10	21	33	≥34
≥ 10	_0	0	0	Ö	0
8,9	_0	0	0	0	0
6,7	0	0	0	+	0
4,5	+	+	+	+	+
2,3	1	. 2	7	5	1
0.1	4	8	18	12	2
-2,-1	2	6	9	6	1
-4,-3	1	3	5	_2	+
-6,-5	+	1	1	+	+
-8,-7	+	+	+	+	0
≨-9	+	+	+	0	Ō

Marine Area A											
	1218	Wir	nd Sp	eed	(kno	ts)					
	TEMP (°C)	0 - 3	4-	11-	22 - 33	≥34					
	<b>≩</b> 0	+	1	4	2	1					
}	-21	+	4	- 8	4	1					
	-4,-3	+	_2	4	2	_ 1					
i	-6,-5	+	1	2	3	1					
	-6,-7	+	2	3	2	1					
	~10,~9	+	2	2	3	_ +					
	~12,~11	1	3	4	3	2					
	~14,~13	1	2	2	2	1					
	~16,~15	+	2	4	2	+					
	~18,-17	1	2	3	1	+					
	≦-19	+	2	2	1	1					

M	Marine Area B										
	5571	Win	nd Sp	eed	(kno	ts)					
	TEMP	0-	4-	111-	22-	l j					
	(°C)		_10	_21	33	≩34					
	<b>≩</b> 6	+	+	+	+	+					
	4,5	+	+	_ 1	1	+					
	2,3	+	2	5	3	+					
	0,1	1	4	9	5	1					
	~2,-1	1	4	8	4	1					
	-4,-3	1	2	5	3	1					
	~6,-5	+	2	4	3	1					
	-87	+	2	3	2	+					
	-10,-9	+	1	3	2	+					
	-12,-11	+	1	2	2	+					
·	<u>≨</u> –13	+	1	3	2	+					

Marine Area C										
5089	Wil	nd Sp	eed	(kno	ts:					
TEMP (°C)	0 - 3	4-	21	22-	≥ 34					
- ₹8	+	+	+	5						
6.7	+	,—,·	+	+	0.1					
4,5	+	1	2	,	-					
2,3	1	6	12	6						
0.1	1	6	12	5						
-2,-1	1	5	5	3	<del>,</del>					
-4,-3	1	3	4	2	+					
-6,-5	+	1	3	2	+					
-8,-7	+	1	2	1	+					
-109	+	1	2	1	+					
<u>s</u> -11	+		_ 2	1	+					

М	Marine Area D											
	906	W	nd Sp	eed	(kno	ts)						
		0 -	4 -	11-	22 ~							
	(°C)	3	10	21	33	≩ 34						
	≩12	_ +	+	+	+							
	10,11	+	+	+	+	+						
	8,9	+	+	+	+	+						
	6.7	+	1	2		+						
	4,5	,	3	6	6	· ·						
	2,3	1	6	15	1 :	4						
	0.	1	4	9	7	3						
	-2,-1	+	2	3	3							
	-4,-3	+	•	2	2	<b>-</b>						
	-65	+	+	•	1	+						
	<b>≤</b> - 7	+	+	··								



N	kol'skos	•				
	5567	Wi	nd Sp	eed	(kno	ts)
	TEMP	10-	4-	71-	22-	1 1
	(°C)	] 3	10	21	33	≩34
	≩8	0	0	+	0	0
	6,7	_+	+	0	0	0
	4,5	+	+	+	+	0
	2,3	1	3	4	_ 2	+
	0.1	2	7	12	4	1
	-2,-1	3	1.1	15	6	2
	-4,-3	2	6	6	3	1
	-6,-5	1	2	2	1	+
	-8,-7	1	1	1	+	+
	-10,-9	+	+	+	+	+
	≦-11	+	+	0	0	0

3758	Wii	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22~	l
(°C)	3	10	21	33	≥34
₹0	1	1	+	+	0
-2,-1	3	3	3	+	+
-4,-3	3	3	2	1	+
-6,-5	3	3	2	1	+
-6,-7	3	4	5	3	,
-109	2	2	3		+
-12,-11	3	4	3	2	1
-14,-13	2	4	3	1	1
-16,-15	2	3	3	1	+
-1817	2	3	3	1	+
≦-19	2	2	1	+	+

U	gol'naja					
	5150	Wi	nd Sp	eed	(kno	ts)
	TEMP	0 -	4 -	[11-	(22-	1
	(°C)	3	10	21	33	≥ 34
	≩-2	2	2	3	2	+
	-4,-3	2	2	_ 2	1	+
	-6,-5	2	2	2	1	1
	-8,-7	3	3	2	1	1
	-10,-9	2	1	2	2	1
	-12,-11	3	2	3	2	2
	-14,-13	3	_ 2	3	2	2
	-1615	3	2	4	3	2
	-18,-17	2	2	3	3	2
	-20,-19	+	1	1	1	1
	≨-21	1	1	1	1	1
	-12,-11 -14,-13 -16,-15 -18,-17 -20,-19	3 3 3 2 +		3 4 3	2 2 3	2 2

4616	₩ii	nd Sp	eed	(kno	ts/
TEMP	0-	4 -	11 - 1	22-	1
(°C)	3	10	21	3.3	≥ 34
₹0		2	_2	+	+
-2,-1	1	4	2	+	+
-4,-3	2	5	2	+	C
-6,-5	2	4	3	+	0
-8,-7	4	5	3	1	+
-10,-9	2	3	2	+	+
-12,-11	4	4	3	+	+
-14,-13	4	4	_ 2		+
-16,-15	5	4	2	+	0
-18,-17	5	3	1	+	0
≦-19	6	1	+	+	0

,	forheast (	Cape				
	9853	Win	nd Sp	seed	(kno	ts)
	TEMP .	10-	4 -	11-	122	)
	(°C)_	3	10	21	33	≩ 34
	<b>≩</b> 0	. 1	3	6	3	1
	-21	1	3	4	1	+
	-4,-3	1	3	5	1	+
	-6,-5	1	2	2	1	+
	-8,-7	2	_3	3	+	+
	-109	2	_ 3	3	1	+
	-12,-11	1	3	2	+	0
	-14,-13	3	4	4	+	0
	-16,-15	2	3	2	+	0
	-18,-17	3	3	2	+	+
	≨-19	4	3	1	+	+

J 111 W					
21332	Wii	nd Sp	eed	(kno	ts)
TEMP	0 -	4-	11-	22 -	l
(°C)	3	10	21	33	≥ 34
₹2	+	1	2	+	0
0,1		4	6	_ 1	+
-2,-1	1	4	_ 5_	_ 1	+
-4 - 3	2	5	5	1	+
-65	2	3	3	1	+
-8,-7	2	4	3	1	+
-10,-9	2	4	3	+	+
-12,-11	2	3	1	+	+
-14,-13	2	4	2	+	+
-15,-15	2	2	1	+	0
≤-17	7	6	1	+	0

U	nelekleel	t				
	14583	Win	nd Sp	eed	(kno	ts)
	TEMP	0-	4 -	111-	22-	) (
	(°C)	3	,0	21	33	≩ 34
	≥4	+	2	3	+	0
	2,3	1	3	4	+	+
	0,1	1	6	5		+
	-2,-1	1	4	4	1	+
	-4,-3	2	5	4	1	+
	-6,-5	1	4	3	+	+
	-8,-7	2	4	3	1	+
	-10,-9	1	3	2	+	0
	-12,-11	1	3	2	+	+
	-14,-13	1	3	2	+	+
	≨~15	4	9	2	+	+

18673	₩i	nd Sp	eed	(+00	ts:
TEMP	10 -	4 -	11-	22-	i
(°C)_	3	10	21	33	234
≥4	+	1	1	+	0
2.3	1	2	2	+	0
0.1	1	4	7	2	-
-2,-1	2	4	7	2	+
-4,-3	2	4	6	2	+
-65	1	2	4		•
-8,-7	1	2	3		•
-109	2	2	3		
-12,-11	1	2	2	1	+
-14,-13	2	. 2	3	2	-
≦-15	2	3	5	2 .	+

Cape New	enhei	m			
19052	Win	nd Sp	eed	(kno	ts)
TEMP	10-	4 -	11-	22-	
_ ( <u>°</u> C)	3	10	21	33	≥ 34
≩6	+	+	+	+	0
4,5	3	1	1	+	+
2,3	2	3	5	2	+
0,1	5	9	9	2	+
-2,-1	4	6	5	1	+
-4,-3	_ 3	5	4	1	+
-6,-5	1	3	3	+	+
-8,-7	1	3	3	+	+
-10,-9	1	5	ū	+	0
-12,-11	1	1	2	+	0
≨-13	1	2	2	+	0

Ķi	ng Salm	no				
	18473	Win	nd Sp	eed	(kno	ts)
	TEMP	0	4-		22- 1	
	(°C)	3	10	21	33	≥34
	<b>≩</b> 8	+	2	2	+	+
	6.7	+	3	3	1	+
	4,5	1	4	3	1	+
	2,3	1	7	6	1	+
	0.1	3	1.1	6	+	O
•	-2,-1	2	7	3	+	0
	-43	2	6	3	+	0
	~6,-5	1	3	2	+	0
	~B,-7	1	4	2	+	0
	-10,-9	1	2	1	+	0
	<u>¥</u> -11	1	4	2	+	0

Pc	it Heide	n				
	6547	Wi	nd Sp	eed	(kno	ts)
	TEMP	0-	4-	111	22 -	1 !
	(°C)	3	10	21	33	≩34
	≧8	+	1	1	1	0
	6,7	+	2	3	1	+
	4,5		3	4	1	+
	2,3	1	7	6	1	0
	0.1	3	11	6	1	+
	-2,-1	2	7	3	+	0
	-4,-3	2	7	4	+	+
	-6,-5	1	_ 3	4	+	0
	-8,~7	+	1	2	+	0
Ī	-10,-9	+	1	1	+	0
	≦-11	+	_2	2	+	0
•						

13437	Wil	nd Sp	eed	(kno	ts!
TEMP	10	4 -	11-	22-	1
(°C)	3	10	21	33	≥ 34
≥ 10	+	+	+	+	0
9,9	0	+	+	+	0
6,7	+	1	1	!	+
4,5	+	2	4	3	+
2,3	+	5	1.1	6	1
0,1	1	7	13	4	+
-2,-1	+	4	6	2	+
-4,-3	+	3	8	2	+
-6,-5	+	2	3	1	+
-8,-7	+	1	2	i	+
≨-9	+	,	1	+	0

Nikolski					
2086	Win	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11~	22-	1
(°C)	3	10	21	33	≥34
≩ 10	+	+	0	0	_ 0]
8,9	+	+	+	0	0
6,7	+	+	+	+	0
4,5	+	1	3	1	0
2,3	1	7	14	4	7
0.1	3	10	21	9	+
-2,-1	1	3	5	4	+
-4,-3	+	1	4	3	+
-6,-5	0	+	1	+	0
-8,-7	0	0	+	+	0
≨-9	0	0	0	0	0

St. Paul					
11095	Wii	nd Sp	eed	(kno	ts)
TEMP	10-	4 -		22 -	
(°C)	3	10	21	_33	≥ 34
<b>≩</b> 6	0	0	0	_ 0	0
6,7	0	+	+	+	0
4,5	+	+	1	+	+
2,3	+	2	6	2	+
0.1	1	7	19	5	+
-2,-1	1	5	а	. 3	+
-4,-3	+	3	6	3	+
-6,-5	+	2	3	2	+
-8,-7	+	2	4	2	+
-10,-9	+	1	3	1	+
≨-11	+	1	2	1	+

22294	Wis	nd Sp	eed	(kno	ts)
TEMP	10 -	4 ~	11-	22-	
(°C)	3	_10	_ 21	33	≥ 34
≩12	0	0	0	+	0
10,11	0	+	+	+	0
8,9	+	+	+	+	+
6,7	+		3	1	+
4,5	1	6	9	3	+
2,3	3	13	18	5	1
0,1	3	9	1.1	3	1
-2,-1	1	2	2	1	+
-4 -3	+	+	+	+	+
-6,-5	+	+	0	0	0
<b>≦</b> -7	+	0	0	0	0

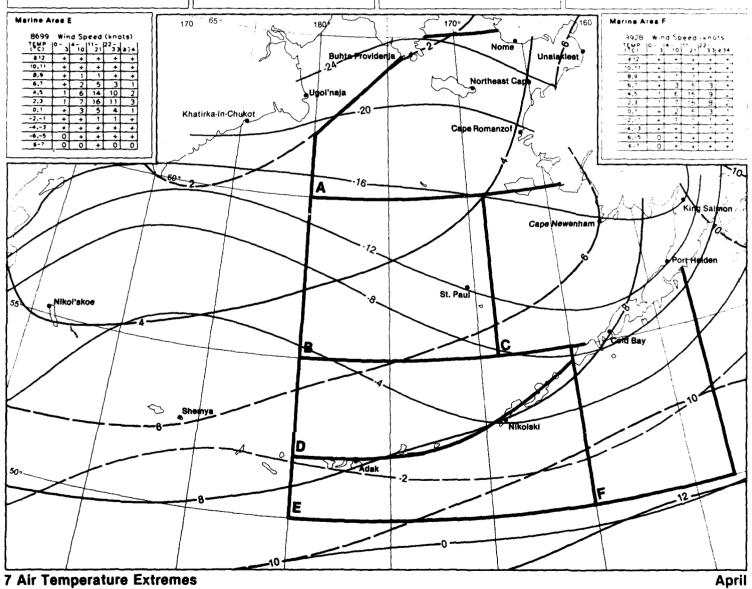
nemya					
18679	Wit	nd Sp	eed	(kno	ts)
	10 -	4-	11-	22~	1
(°C)	( 3	10	21	33	≥ 34
≥10	0	0	0	0	0
8.9	0	0	0	0	0
6,7	0	+	+	Ç	0
4.5	+	+	2		٠,
2,3	2	7	20.	9	1
1,0	4	11	20	9	1
-21	1	. 3	4	2	+
-4,-3	+	1	+	+	+
-6,-5	+	+	+	+	0
-8,-7	+	0	0	+	0
≨-9	0	0	0	0	0

Marine A	A ser				
608	wi	nd Sp	eed	(kno	ts)
TEMP (°C)	0-3	4-	21	22 - 33	≥34
₹4	0	0	0	0	+
2,3	0	1	+	+	0
0,1	+	3	15	6	+
-2,-1	1	2	6	3	1
-4,-3	1	2	_4	2	+
-6,-5	+		_2	2	0
-8,-7	+	2	3		+
-10,-9	1	3	2	2	+
-12,-11	+	2	6	1	+
-14,-13	1	2	5		0
≨~15	1	4	_5	2	+

M	Marine Area B								
	4380	wi	nd Sp	eed	(kne	ts)			
	TEMP	0~	4 -	111 -	22 -	1 1			
	_(° <u>C</u> )	3	10	21	33	≥34			
	<b>≩8</b>	+	+	+	0	0			
	6,7	0	+	+	+	0			
	4,5	+	1	2	1	+			
	2,3	+	4	11	4	1			
	0,1	1	6	12	5	1			
•	-2,-1	1	4	9	5	1			
	-4,-3	1	3	5	3	+			
	-6,-5	1	2	4	2	+			
	-8,-7	+	1	2	1	+			
	-10,-9	+	1	2	1	+			
	<u>≨</u> -11	+	+	1	+	+			

Marine A	rea C				
6548	Wi	nd Si	oeea	.kno	ts.
TEMP	0 -	4 -	11-	22 -	1 1
(°C)	3	10	21	33	≥ 34
≥ 10	0	+	+	+	0
8,9	+	+	+	+	0
6.7	+	1	1	+	+
4,5	1	3	4	2	+
2.3	1	8	14	6	1
0.1	1	6	12	5	
-2,-1	1	3	7	4	1
-4,-3	1	- 2	4	2	1
-6,-5	+	1	2	1	+
-8,-7	+	+	1		+
≨-9	+	+	+	+	+

М	arine Ai	es D				
	8247	Wir	id Sp	eed	(kno	(5)
	TEMP		4		22 -	
	(°C)	3	10	21	33	<u> 34</u>
	æ 12	+ 1	+1	+	_ +	0
	10.11	+ 1	_+		_ •	0
	8, ₃	+		!	•	+
	6,7	+	2	2	•	7
	4.5	,	4	9	7	2
	2.3	2	6	16	10	3
	0.1		4	9	5	2
	-2,-1	+ 1	1	3	2	•
	-4,-3	+ ;			•	+
	-6,-5	+	+ 1	+	+	+
	<b>≤</b> ~ 7	0	+	+	+	0



Nikol'akos	1				
56 <b>u</b> 5	Wi	nd Sp	eed	(kno	ts)
	0 -	4 -	11-	22 -	1
(°C)	3	10	21	33	₹34
<u> </u>	0	0	0	_0	0_
10,11	0	0	_0_	0	$\begin{bmatrix} 0 \end{bmatrix}$
8,9	+	+	+	+	0
6,7	+	1	+	+	0
4,5	1	4	4	+	+
2,3	4	17	25	7	1
0,1	3	10	11	3	1
-2,-1	2	3	2	1	+
-4,-3	+	+	+	+	+
-6,-5	0	0	0	+	+
<b>≤</b> - 7	0	0	0	0	0

Kha	tirka-l	n-Chu	ikot			
	3396	Wii	nd Sp	eed	(kno	ts)
	TEMP	0-	4 -	11-	22-	
_	(°C)	3	10	21	33	≩34
	≥8	+	+	+	0	0
	6,7	+	+	+	+	0
	4,5		1	1	+	0
	2,3	7	- 5	4	1	0
	0,1	10	7	3	+	+
	-2,-1	15	10	5	2	+
	-4,-3	5	4	2		+
	-6,-5	2		1	+	+
_	-8,-7	1	1	1	+	+
	10,-9	1	1	+	+	+
_	<u>≤</u> -11	1	1	1	+	+

1 <b>g</b> a	il'naja					
	4857	Wi	nd Sp	eed	(kno	ts)
	TEMP	0-	4 -	11 -	22-	
	(°C)	3	10	21	33	≥ 34
	≥8	+	+	+	0	0
_	6.7	+	1	+	+	Ò
	4,5	1	1	1	+	0
	2,3	3	5	4	1	+
	0,1	3	5	6	2	+
_	-2,-1	5	8	10	4	1
	-4,-3	3	5	6	3	1
	-6,-5	2	2	2	1	3
	-8,-7		1	2	2	1
-	10,-9	+	+	1	1	1
_	≨-11	1	1	2	1	+

ihta Providenja							
4519	Wi	na Sp	eed	(kno	ts)		
TEMP (°C)	0 - 3	10	11-	22 - 3 3	<b>≩</b> 34		
₹8	+	1	+	+	0		
6.7	1	2	1	+	0		
4,5	1	4	2	+	0		
2.3	5	9	. 3		0		
0,1	5	10	3	+	+		
-2,-1	8	12	4	•	+		
-4,-3	5	5		+	0		
-6,-5	2	3		+	٥		
-8,-7	2	2	1	+	0		
-10,-9	1	1	+	0	C		
<u>s-11</u>	1	1	+	+	0		

Norhesst	Cape				
10440	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11-	22-	) )
(°C)	_ 3	10	21	3.3	≩ 34
≩θ	+	+	+	0	0
6,7	+	+	+	+	+
4,5	1	1	1	+	+
2,3	3	6	3	1	+
0,1	6	15	11	3	1
-2,-1	4	8	7		+
-4,~3	3	6	4	+	0
-6,-5	1	2	1	+	0
-87		2	1	+	0
-10,-9	1	1	1	+	0
<u>\$-11</u>	1	1	1	+	0

N	om e					
	21320	Wi	nd Sp	eed	(kno	ts)
	TEMP	0 -	4 - '	11-	22-	1 1
	(OC)		10	21	33	≥34
	≥12	+	1	2	+	0
	10,11	+	2	2	+	0
	8,9	+	3	2	+	0
	6,'	1	5	3	+	[ _ე]
	4,5	1	5	4	+	0
	2,3	2	9	6	+	+
	0.1	3	12	7	1	+
	-2,-1	2	6	2	+	4
	-4,-3	2	4	1	+	
	6,-5	1	1	1	+	Ō
	<b>≤</b> − 7	2	3	)	+	0
•						

Unalakiee	1				
14933	Wil	nd Sp	eed	(kno	ts)
	0 -	4 -		22-	1
(°C)	3	10	21	33	≥ 34
≥ 12	+	2	3	+	J
10,11	+	3	2	+	0
8.9	1	4	3	+	0
6,7	2	8	4		0
4.5	2	7	4	+	0
2.3	3	11	5	+	0
0.1	3	1.1	3	+	0
~2,-1	1	4	1	+	0
-4,-3	1	3	1	+	0
-6,-5	+	1	1	0	0
<u>\$</u> ~ 7	1	2	1	+	0

18892	Wi	nd Si	eed	(kno	15/
FEMP	10-	4 -	11-	22-	
(°C)_	3	10	21	3.3	≥ 3.4
≥10	+	1	1	+	
8.9		2	1	+	
6,7	2	5	3	+	
4,5	2	5	4	+	
2.3	3	6	6	•	
0.1	4	8	9		
-21	3	5	6		
-4,-3	2	4	3	•	
-6,-5	,	1	,		
-8,-7	+	1	,	+	
<u>s</u> 9	+		1	+	

Cape Romanzot

Сер	. New	enhei	m			
1	9580	Wi	nd Sp	eed	(kno	(s)
1	EMP	10 -	<b>4</b> -	11-	122- 1	1
	(°C)	3	10	21	33	≥ 34
	≥ 12	+	1	+	0	0
	10.11	1	1	+	0	0
	8.9	2	2	1	+	0
	6,7	4	5	3	+	+
-	4.5	5	7	5	1	+
	2.3	7	9	7	1	+
	0.1	6	9	7	1	+
	2,-1	2	4	3	+	0
_	4,-3	1	2	2	+	0
	-6,-5	+	+	1	+	0
~	ş7	+	+	1	+	0

King Salm	on				
18357	w.	nd Sp	eed	(kno	ts)
TEMP	10 -	4 -	11 -	[22 - ]	1
(°C)	3	10	21	3 3	≩ 34
≩ 14	+	2	1	+	0
12,13	+	3	2	+	0
10,11	1	4	4	1	+
8.9	1	5	4	1	+
6,7	2	9	7	1	+
4.5	2	8	.5	1	+
2,3	3	10	4	+	+
0,1	2	8	3	+	0
-2,-1	1	3	1	+	0
-4,-3	T	1	+	+	0
<u>≤</u> -5	+	1	+	0	0

Port Hei	den				
632	6 Wii	nd Sp	eed	(kno	ts)
TEMP	10 -	4-	11~	22 -	
(°Ç)	3_	[ 10	21	33	≥ 34
≥ 14	+	+	+	+	0
12,13	+	1	1	+	0
10,11	+	2	3	1	0
8.9	+	3	4	1	+
6,7	1	7	8	2	+
4,5	2	8	7	1	0
2,3	3	11	6	1	C
0.1	3	9	4	+	+
-2,-1	1	3	3	+	0
-4,-3	1	1	1	0	0
≨-5	+	1	+	0	0

Cold Bay					
13153	Wie	nd Sp	eed	(kno	ts)
TEMP	0 -	4 ~	117-	22-	
(°⊂;	3	10	21	33	≥ 34
≥ 14	0	+	+	0	0
12,13	+	+	+	+	0
10.11	+	1		+	0
8,9	+	2	2	+	•
6,7	+	5	9	.4	+
4.5	1	7	12	5	-
2,3	1	9	14	4	-
0,1	1	6	8	2	+
-2,-1	+	2	1	+	3
-4,-3	+	1	1	+	9
£-5	+	+	+	C	3

Wir	nd Sp	eed	(kno	ts)
0 -	4-	11-		1 1
3	10	21	33	≥ 34
0	+	0	0	0
0	+	+	0	0
+	+	+	0	0
+	2		+	0
2	8	7	1	0
4	16	20	6	+
2	6	13	5	1
+	. 1	2	2	+
0	+	+	+	+
_ 0	0	0	0	0
0	0	0	0	0
	0 0 0 + + 2 4 2 + 0	0 - 3 10 0 + 0 + + + 2 2 8 4 16 2 6 + 1 0 + 0 + 0	0 - 3 4 - 11 - 21 0 + 0 0 + + + + + + + + + + + + + + +	3 10 21 33 0 + 0 0 0 + + 0 + + + 0 + 2 1 + 2 8 7 1 4 16 20 6 2 6 13 5 + 1 2 2 0 + + + 9 0 0 0

St. Paul			•		
10507	Win	nd Sp	eed	(kno	ts)
TEMP (°C)	0 - 3	10	11-	22- 33	≥ 34
≩10	0	+	+	+	0
8,9	0	+	+	+	0
6,7	+	1	2	+	0
4,5	+	3	_ 5	1	0
2,3	1	10	19	3	+
0,1	1	12	18	3	+
-2,-1	1	5	6	2	
-4,-3	+	_ 2	2	1	+
-6,-5	+	+	+	+	+
- <b>0</b> ,-7	+	+	+	+	0
≨-9	+	+	+	+	0

Adek					
22328	Win	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22-	, ,
(°C)	3	10	21	33	≥ 34
≩ 14	+	+	+	0	0
12,13	+	+	+	+	0
10,11	+	+	+	+	0
9,9	+	1	1	+	+
6.7	1	9	9	2	+
4,5	3	15	14	4	1
2,3	5	12	12	3	+
0,1	2	2	2	+	+
-2,-1	+	+	+	0	0
-4,-3	+	+	0	0	0
≨-5	+	0	0	0	0

Shemya					
18837	wii	nd Sp	eed	(knņ	ts:
TEMP (°C)	0 - 3	<b>4</b> -	11 - 21	22 - 3 3	≥ 34
≥12	0	0	C	0	0
10,11	0	+	0	C	0
8,9	+	+	+	0	0
6,7	+	1	2	+	+
4,5	2	7	15	4	+
2,3	5	15	29	8	+
0,1	1	3	4	2	+
-2,-1	+	+	+	+	+
-4,-3	+	0	+	0	0
~6,-5	0	0	0	0	O
<u>≤</u> - 7	0	0	0	0	0

Marine Area A	Marine Area B	Marine Area C	(I-171 Marine Area D
1440 Wind Speed (knots)  1EMP 0-   4-   11-   22-   (°C1   3   10   21   33   234   2 0	4350 Wind Speed (knots)  TEM, 0-   4-   11-   22-   (°C)   3   10   21   33   234  212   0   + 0   0   0  10,11   + + + 0   0   0  6,7   + 2   2   + + +  4.5   1   6   8   2   +  2,3   2   11   15   4   +  0,1   2   8   13   4   1  -2,-1   1   4   5   2   +  -4,-3   + 1   2   1   +  -6,-5   + + + + + 0  8-7   + + + + + 0	9790 Wind Speed (knots)	9357 Wind Speed (Fnots)  TEMP 0- 4- 11- 127- (*C1 3 10 2! 33) 834,  **14 0 + + 0 0  12,13 + + + + +  10,11 + 1 1 + +  8.9
10875 Wind Speed (knots)  [(w) 0 - 3  4 - 10  17   12 23 3   234   214	B Buhte Provi	Northeast Cape 2  A Cape Romanzon  St. Paul  C  Mikglakt	Merine Area F  1300 Wind Speed (knots)

7 Air Temperature Extremes

Nikol'sko	•				
5456	Wi	nd Sp	eed	(kno	ts)
TEMP	10 -	4 -	11-	22 -	
(°C)	3	10	21	33	≥34
≥ 14	L ±	+	_+	0	
12,13	+	+	+	+	0
10,11	+	1	+	+	0
8,9	1	2	2	+	0
6,7	2	10	10	2	+
4,5	4	16	19	3	+
2,3	4	10	10	_2	+
0,1	+	1	1	+	+
-2,-1	+	0	+	0	0
-4,-3	0	0	_0	0	0
<u>s</u> -5	0	0	0	0	0

hetirke-In-Chukot									
3364	Wind Speed (knots)								
TEMP	0 -	4 -	11-	22-	1				
(°C)	3	10	21	_33	≩34				
≥ 14	•	1	1	+	0				
12,13	+		1	+	0				
10,11	1	1	+	+	0				
8,9	2	2	1	+	0				
6,7	5	4	2	+	0				
4,5	13	10	5	1	+				
2,3	!6	10	6	+	0				
0,1	6	3	1	+	ಾ				
-2,-1	3	1	+	+	+				
-4,-3	+	+	0	+	+				
<u>s</u> -5	0	0	Ö	0	0				

Ųg	ol'naja					
	4856	Wii	nd Sp	eed	(kno	ts)
	TEMP	(0 -	4 -	11-	22-	
	(°C)	3_	10	21	33	≩34
-	<u>≥</u> 14		2	1	+	+
_	12,13	1	1	1	+	+
_	10,11	1	2	1	+	+
_	8,9	2	3	2	1	+
_	6.7	2	5	4	1	+
	4,5	4	7	6	1	+
	2,3	5	12	9	_2	+
	0,1	3	4	4	1	+
_	-2,-1	1	3	2	1	+
_	-4,-3	+	+	+	+	+
_	<b>≨</b> -5	+	+	+	0	+

4473	Wil	nd Sp	eed	(kno	15)
	10-	4 -		22 -	į
(°C)	3	10	21	3 3	≥ 34
≥ 14	+	1	+	0	0
12,13	1	2	+	0	0
10.11	1	2	+	_0	<u></u> <u></u>
8.9	3	4	1	0	0
6.7	5	8	2	0	0
4,5	9	13	3	+	0
2,3	_11	15	4	+	+
0,1	5	5	1	0	0
-2,-1	3	2	+	0	0
-4,-3	1	+	+	0	0
§-5	+	+	0	0	Ç

Norheast	Cape				
9923	wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11 -	22 -	1 1
(°C)	3	10	21	33	≥ 34
≥ 14	+	+	+	+	0
12,13	+	1	1	+	0
10,11	1	2	_1	_ +	0
8,9	Ţ	3	_2	+	0
6.7	4	8	.5	1	+
4,5	4	9	5	1	+
2,3	7	13	6	1	+
0,1	6	11	3	-	0
-2,-1	2	2	1	0	0
-4,-3	+	+	+	_ 0	0
<u>s</u> - 5	0	0	0	0	_ o

20628	Wil	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11-	22 - 1	l
(°C)	3	10	21	3 3	₹34
≥ 16	+	3	2	+	0
14,15	+	2	1	+	0
12,13	1	5	2	+	0
10,11	1	8	3	+	0
8,9	1	7	4	+	0
6,7	3	11	5	+	0
4,5	2	9	5	+	0
2,3	2	8	4	+	0
0,1	1	4	2	+	0
-21	+	1	+	0	0
§-3	+	+	0	0	0

Unalakleet	t				
14458	Wii	nd Sp	eed	(kno	ts)
TEMP	0-	4-		22-	1
(°C)	3	10	21	33	≥ 34
≩ 18	+	1	1	+	+
16,17	+	2	1	+	+
14,15	+	3	2	_+	0
12.13	1	8	4	+	+
10,11	3	13	5	÷	+
8.9	3	10	4	+	0
6,7	3	11	4	+	0
4,5	2	6	2	+	0
2,3	1	5	1	+	0
0,1	1	2	+	C	0
≦-1	+	+	+	0	0

apa Romanzof ∠								
17725	Win	nd Sp	eed	(±no	ts/			
	0-	4 -	11-	22 -				
(°C)	3	10	21	3.3	₹34			
≥ 16	+	1	1	+	0			
14,15	+	1	1	+	0			
12,13	1	3		+	0			
10,11	2	5	3	+	0			
В.9	2	5	4	+	0			
6,7	4	9	6	1	0			
4,5	3	9	6	+	0			
2.3	3	9	5	+	Q			
0.1	2	3	_3	+	0			
-21	+	1	1	+	0			
<b>≨</b> -3	+	+	+	+	0			

Cape Nev	venha	m			
18313	w:	nd Sp	peed	(kno	ts)
TEMP	10-	4 -	11 -	22-	1 1
(°C)		10	21	3 3	≥ 34
≩ 16	+	+	+	0	0
14,15	+	1	+	+	0
12.13	2	2	1	+	Ö
10,11	4	6	2	+	0
8.9	5	8	4	+	0
6,7	9	14	7	1	+
4.5	6	8	5	+	+
2,3	3	5	3	+	+
0.1	1 1	1	1	+	+
-2,-1	+	+	+	0	0
≨-3	0	0	0	0	O

17756	Wil	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11~	22 -	ļ
(°C)	3	10	21	33	≥ 34
≥ 20	+	2	_ 1	+	0
18,19	+	1	1	+	0
16,17	+	3	2	+	0
14,15	+	4	3	+	+
12.13	1	7	4	1	+
10,11	2	_40	6	1	+
8,9	2	01	4	+	+
6,7	3	12	5	+	+
4,5	1	6	2	+	+
2.3	1	3	1	+	0
<b>≤</b> 1	+	1	+	0	0

6135	Wil	nd Sp	eed	(kno	ts)
TEMP	10 -	4 - 3	11-	22 - !	
(°C)	3	10	21	_ 33	≥ 34
≥ 18	+	+	+	0	-0
16.17	0	+	1	+	0
4,15	+	1	1	+	+
12,13	+	3	4	1	0
10,11	1	8	7	1	+
8,9	2	9	6	1	+
6,7	5	14	_8	_ 1	+
4,5	3	7	3	+	0
2,3	2	5	2	+	0
0,1	1	1	,	0	0
≨-1	+	+	0	0	0

old Bay					
12720	Wil	nd Sp	eed	(kno	ts.
TEMP	10-	4-	111-	22 -	
_(°C)	3	10	21	3 3	≥ 34
≥ 16	0	+	+	0	0
14,15	0	+	+	+	0
12,13	+	1	_2	+	0
10,11	+	5	7	2	+
8,9	1	6	10	3	-
6,7	1	11	18	6	•
4,5	1	6	9	_ 2	+
2,3	+	2	4		+
0,1	+	+	1	+	Ĝ
-2,-1	+	0	0	C	C
<b>≤</b> - 3	0	0	0	0	C

Nikolski					
2200	Wi	nd Sp	oeed	(kno	ts)
TEMP	0 -	4 -	11 -	22-	1 1
(°C)	3	10	21	33	≥ 34
₹ 14	0	+_	0	0	0
12,13	+	+	0	0	0
10,11	+	1	+	+	0
8,9	+	1	1	+	0
6.7	2	11	.0	1	0
4,5	3	18	16	4	+
2,3	2	10	12	3	+
0,1	+	+	1	1	0
-21	0	0	0	0	Q
-4,-3	0	0	0	0	0
£-5	0	_0	0	0	0

10026	Wii	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22 -	1
(°C)	3	10	21	33	≥ 34
≥ 14	0	+	_0	0	0
12,13	0	+	+	+	0
10,11	0	1	1	+	0
8.9	+	2	3	+	0
6,7	+	10	14	1	+
4,5	1	13	15	1	O
2,3	1	10	14		+
0,1	+	4	_ 3	1	0
-2,-1	+	+	+	+	0
-4,-3	+	+	+	0	0
\$-5	0	+	0	0	0

21571	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11~	22-	
(°C)	3	_10	_21	_ 33	≩34
≥ 16	+	+	+	0	0
14,15	+	+	+	+	0
12,13	+	1	+	+	+
10,11	1	_ 3	2	+	+
8,9	1	7	5	1	+
6,7	5	22	16	2	+
4,5	4	12	9	2	+
2,3	1	2	1	+	0
0,1	+	+	+	0	0
-2,-1	+	0	0	٥	0
<b>≨</b> ~3	0	0	0	0	0

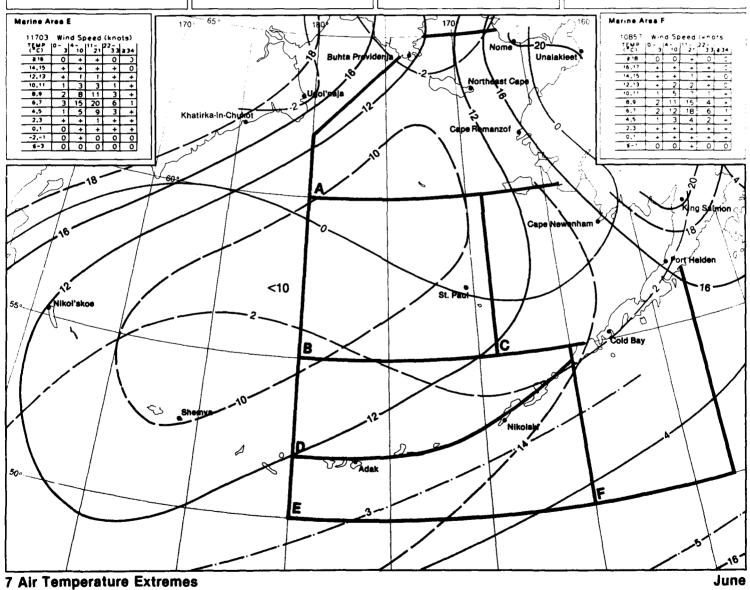
She	my4					
1	18373	Wii	nd Sp	eed	(kno	ts)
	TEMP	0 -	4 -	11~ ,	22-	;
	(°C)	3	.0	21	33	≥ 34
	≥ 14	0	0	0	0	0
	12,13	+	+	+	0	0
	10,11	+	+	_+	+	0
_	8,9	+	1	1	+	0
	6,7	3	11	15	_ 2	+
	4,5	5	18	24	3	+
	2,3	2	6	- 6	+	+
	0,1	+	+	+	0	0
_	-2,-1	+	0	0	0	0
_	-4,-3	0	0	0	0	0
_	<b>≨</b> -5	0	0	0	0	0

M	Marine Area A									
	2656	Wi	nd Sp	eed	(kno	ts)				
	TEMP	10-	4-	11-	22-	1				
	(°C)	_3	10	21	33	≩34				
	≩14	+	+	+	0	0				
	12,13	+	1	+	+	0				
	10,11	T	2	2	+	0				
•	8,9	1	3	3	1	0				
	6,7	2	7	6	1	+				
	4,5	2	13	10	2	1				
•	2,3	3	12	10	2	+				
•	0,1	1	7	4	+	0				
	-2,-1	+	1	1	+	0				
•	-4,-3	+	+	0	0	0				
	≨-5	0	0	0	0	0				

Marine A	Marine Area B								
6364	Wie	nd Sp	eed	(kno	ts)				
TEMP	0-	4-	11-	122 -	l i				
(°C)	3	10	21	33	<u>₹</u> 34				
≧ 14	0	0	0	0	0				
12,13	+	+	+	0	+				
10,11	+	1	+	+	+				
8,9	1	4	2	+	+				
6,7	3	13	14	3	+				
4,5	3	14	17	3	+				
2,3	2	6	7	1	+				
0,1	1	2	2	+	+				
-2,-1	+	+	+	+	0				
-4,-3	0	0	+	0	0				
≨-5	0	0	0	0	0				

Marine Ar	'88 C				
10565	Wii	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11 -	22-	l
(°C)	3	10	_ 21	33	≩34
≥ 16	+	+	+	0	0
14,15	+	+	+	+	0
12,13		7	+	+	_+
10,11	2	4	2	+	+
8,9	3	8	6	1	+
6,7	3	12	1.1	2	+
4,5	2	10	1.1	2	•
2,3	1	4	6	1	+
0,1	+	1	2	1	+
-2,-1	+	+	+	+	+
≨-3	0	0	0	+	+

Marine Ar	Marine Area D								
10871	Wir	nd Sp	eed	(kno	ts)				
TEMP	0 -	4 -		22-					
(°C)	3	_ 10	21	_ 33	≩34				
≩ 16	+	+	0	0	0				
14,15	+	+	+	+	0				
12,13	+	1	1	+	0				
10,11	7	3	3	+	+				
8.9	2	7	8	2	<del>+</del> ]				
6,7	3	15	19	5	+				
4.5	2	_ 8	1.1	3	+				
2.3	+	1	1	1					
0.1	0	+	+	+	+				
-21	+	+	+	+	0				
<u>s</u> - 3	0	0	0	0	0				



N	ikol'skos	)				
	5353	Wil	nd Sp	eed	(kno	ts)
	TEMP	10 -	4-	111-	22-	1
	_(°C)_	3	10	21	33	≥ 34
	≩18	0	+	0	0	_ 0
	16,17	+	+	_ 0	٥	0
	14,15	+	+	+	0	0
	12,13	1	3	1	+	0
	10,11	2	6	5	1	0
	8,9	5	14	17	3	+
	6.7	4	12	14	4	_ +
	4.5	1	2	3	1	0
	2,3	+	+	0	0	0
	0.1	+	0	0	0	0
	S-1		0	0	0	

3221	Wil	nd Sp	eed	(kno	ts)
TEMP	0 -	4-	11-	22 -	l
(°C)	. 3	10	21	_33	≩ 34
≩ 18	+	+	+	0	0
16,17	+		+	+	0
14,15	1	_ 1	1	+	0
12,13	2	_ 2	2	+	+
10,11	3	2	1	+	0
8,9	11	8	4	+	+
6,7	16	12	5	+	+
4,5	10	7	4	+	0
2,3	2	1	+	+	0
0,1	+	0	+	0	0
<u>§</u> - 1	0	+	0	0	0

U	gol'naja					
	4945	Wii	nd Sp	eed	(kno	ts)
		0-	4 -	11-	22-	i i
	(°¢)	3	10	21	33	≩34
	≥ 18	+	1	1	+	0
	16,17	1	1	1	+	+
	14,15	1	2	2	+	0
	12,13	2	5	4	1	+
	10,11	2	5	3	1	+
	8,9	4	9	6	1	+
	6,7	4	9	. 8	2	+
	4,5	3	6	6	1	+
	2,3	1	2	2	+	+
	0,1	ŧ	+	+	+	0
	≦ – 1	0	+	0	0	+

Buhte Prov	Buhte Providenje										
4421	Wie	nd Sp	eed	(kno	ts)						
7EMP (°C)	0 - 3	4 -	11-	22 - 33	≥ 34						
≥ 18	+	+	+	0	0						
16,17	+	+	+	0	0						
14,15	1	2	1	Ũ	_0						
12,13	2	5	i	+	+						
10,11	3	6	1	0	C .						
8,9	8	14	3	0	0						
6.7	10	16	3	0	_0 ,						
4,5	6	9	2	+	0						
2,3	2	2	1	0	_0						
0.1	+	0	+	0	0						
≨-1	0	0	0	0	_0						

N	Norheast Cape											
	10595	Wil	nd Sp	eed	(kno	ts)						
	TEMP	0-	4 -	11- :	22-	1						
	(°C)	3	10	21	33	≥34						
	≥ 18	+	+	+	+	0						
	16,17	+	+	1	+	0						
	14,15	+	1	1	+	0						
	12,13	1	3	3	+	0						
	10,11	3	8	6	1	+						
	8,9	4	9	7	1	+						
	6,7	5	13	1.1	1	+						
	4,5	2	6	4	1	+						
	2,3	1	2	2	+	0						
	0,1	+	+	+	0	0						
Ī	<u>5</u> - 1	0	0	0	0	0						

Nome					
21311	Wil	nd Sp	eed	(kriu	ts)
	0 -	4 -	11-	22 -	1
(°C)	_3,	10	21	3.3	≥ 34
≥ 20	+	1	1	+	0
18,19	+	1	1	+	0
16,17	+	3	2	+	0
14,15	1	4	2	+	0
12.13	2	10	4	+	0
10,11	3	14	6	+	+
8,9	2	11	6	+	0
6,7	2	10	6	+	0
4,5	1	3	1	+	0
2,3	+	1	+	+	0
<u> </u>	+	+	+	+	0
			<u> </u>		

Unelakleet	Unelskieet										
15859	Wii	nd Sp	eed	(knn	te)						
TEMP	0 -	4-	111-	122~	1						
(°C)	3	10	21	33	≥34						
≥22	+	+	+	0	0						
20,21	+	1	1	+	0						
18,19	+	2	1	+	0						
16,17	1	6	2	+	0						
14,15	2	9	3	+	0						
12,13	4	15	7	+	+						
10,11	3	14	8	1	0						
8,9	1	5	3	+	C						
6,7	1	3	2	+	0						
4,5	+	1	+	+	0						
≦ 3	+	+	+	0	0						

18686	18686 Wind Speed (knots)									
TEMP	10-	4 -	11-	22 -						
(°C)	3	10	_21_	33	≥ 34					
≥ 18	+	1	+	0	Ü					
16,17	1	, ,	1	+	_ 0					
14,15	1	2	1	+	_ 0					
12,13	2	5	3	+	С					
10.11	4	10	_6	+	_ 0					
8,9	5	1.1	_ 7	+	0					
6,7	5	13	7	+	0					
4,5	2	4	3	+	0					
2,3	+	1	1	+	0					
0.1	+	+	+	0	0					
≦-1	0	0	0	0	0					

Cape New	Cape Newenham											
19391	19391 Wind Speed (knots)											
TEMP	0-	4-	115-	22~	. 1							
(°C)	3	10	21	33	≩34							
≥ 18	+	+	+	+	0							
16,17	1	1	+	+	0							
14,15	2	2	1 .	+	0							
12,13	4	5	3	+	0							
10,11	7	12	6	+	0							
8,9	7	13	8	+	+							
6,7	6	10	7	+	0							
4,5	1	2	1	+	0							
2,3	+	+	+	0	0							
0.1	0	0	+	0	0							
<b>≨</b> − 1	0	0	0	0	0							

18345	Wii	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22-	1
(°C)	]3	10	21	33	≥34
≩22	+	2	_1	+	0
20,21	+	2	_ 1	+	0
18,19	+	3	1	+	0
16,17	1	5	3	+	0
14,15	1	6	_3	+	0
12,13	_2	11	_5	+	_0
10,11	4	16	6	+	+
9,9	3	10	3	+	+
6,7	2	5	2	+	0
4,5	+	1	+	0	0
≨ 3	+	+	+	0	0

King Salmon

Port Heiden										
5917	Wie	nd Sp	eed	(kno	ts)					
TEMP	0 -	4 -	11- 1	22 -	i					
(°C)	3	_10	21	_33	≥34					
<i>≩2</i> 0	+	+	1	+	0					
18,19	+	1	1	+	+					
16,17	+	2	2	+	+					
14,15	+	3	2	1	+					
12,13	2	7	5	1	+					
10,11	3	14	7	1	+					
8.9	3	11	8	1	+					
6,7	3	9	6	+	0					
4,5	2	2	+	0	0					
2,3	+	+	+	0	0					
≦ 1	+	+	0	0	υ					

13871	₩i	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11 ~	22 -	l
(°C)	3	10	21	33	≥34
≩ 18	0	+	+	+	0
16,17	+	+	- 1	+	0
14,15	+	1	1	+	0
12,13	+	3	_6	1	+
10,11	1	10	16	5	+
8,9	1	9	15	4	+
6,7	1	7	11	2	+
4,5	+	1	1	+	0
2.3	+	+	+	0	0
0,1	0	+	0	0	٥
≦-1	0	0	0	0	0

Nikolski					
2484	Wi	nd Sp	eed	(kno	ts)
	10 -	4 -		22-	1
(°C)		10	21	33	≥34
≩ 16	C	0	0	0	0
14,15	+	+	+	0	0
12,13	+	1	1	0	0
10,11	1	4	4	+	0
8,9	1	9	6	1	0
6,7	2	23	19	2	+
4,5	1	В	10	2	0
2,3	+	1	1	+	0
0,1	0	+	+	0	0
-2,-1	0	0	0	0	0
€-3	0	0	0	0	0
			_		

t. Paul					
10306	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11-	22-	1
(°C)	3	10	21	33	≥ 34
≩ 16	+	+	+	0	0
14,15	0	+	+	0	0
12,13	+	1	+	+	0
10,11	+	3	4	+	0
8,9	1	10	13	1	_0
6,7	2	24	24	1	0
4,5	1	7	_ 5	+	0
2,3	+	2	1	+	0
0,1	+	+	+	0	0
-2,-1	+	+	0	0	٥
<b>≨-3</b>	0	0	0	0	0

A	dek					
	22239	Wie	nd Sp	eed	(kno	ts)
	TEMP	0 -	4-	11-	22-	1 1
	(°C)	3	10	21	33	≩34
	≥ 18	+	+	+	+	0
	16,17	+	+	+	+	+
	14,15	+	1	1	+	+
	12,13	1	4	4		+
	10,11	3	11	9	1	+
	8,9	4	14	9	-	+
	6,7	6	14	9	1	+
	4,5	1	2	1	+	0
	2,3	+	+	+	+	0
•	0,1	+	0	0	0	0
	≨-1	0	0	0	0	0
_						

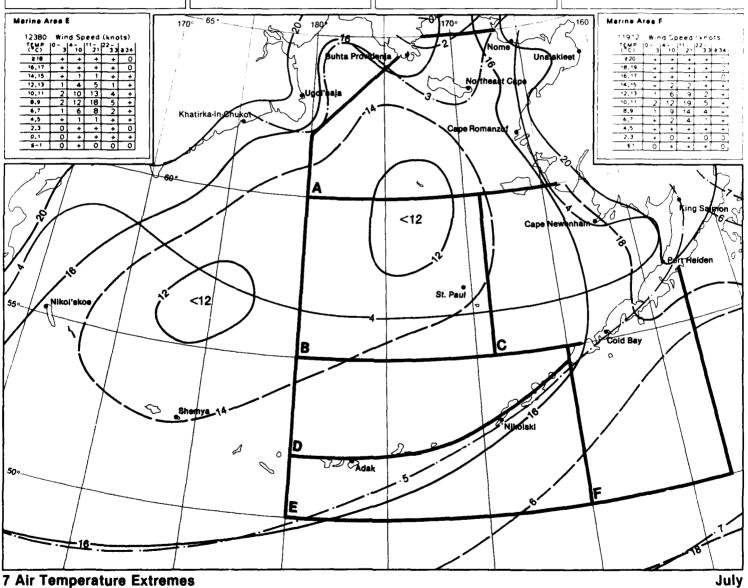
S	hemye					
	18976	Wii	nd Sp	eed	(kno	ts)
	TEMP	10-	4-	11-	22~	1
	(°c)	] 3	10	21	33	≩ 34
	≥ 16	0	0	0	0	0
	14,15	<u> </u> +	+	+	0	0
	12,13	+	+	+	+	0
	10,11	1	4	4	+	+
	8,9	3	13	13	2	+
	6,7	_ 6	20	23	2	+
	4,5	1	3	3	+	0
	2,3	+	+	+	0	0
	0,1	0	0	0	0	0
	-2,-1	0	0	0	0	0
	≨-3	0	0	0	0	0
	<b>≨</b> −3	0	0	0		<u> </u>

Marine Area A										
4770 Wind Speed (knd	its)									
TEMP  0-  4-  11-  22-	1 1									
(°C) 3 10 21 33	≥ 34									
≥18 + + + +	0									
16.17 + 1 1 0	0									
14.15 + 1 1 +	+									
12.13 1 2 2 +	+									
10,11 2 5 6 1	+									
8.9 2 10 11 2	+									
6.7 3 12 16 2	+									
4.5 1 5 6 1	+									
2,3 + 1 1 +	+									
0.1 + + + +	0									
<b>≨</b> -1 + 0 + 0	0									

М	Marine Area B										
	6134	Wis	nd Sp	eed	(kno	ts)					
		0 -	4 -	11-	22-	1 1					
	(°C)	3	10	21	33	<u>≥</u> 34					
	≩ 18	0	0	0	0	0					
	16,17	0	0	+	0	0					
	14,15	+	+	+	0	0					
	12,13	+	1	1	+	0					
	10,11	1	4	4	+	+					
	8,9	3	13	16	3	_ +					
	6,7	3	16	20	4	+					
	4,5	1	4	4	+	+					
	2,3	+	+	+	+	0					
	0,1	+	+	+	0	0					
	≦-1	0	0	0	0	0					

M	Marine Area C										
	10077 Wind Speed (knots)										
	TEMP	0 -	4 -	11 -	22 -						
	(°¢)	3	10	21	3.3	₹34					
	≥ 18	+	+	+	0	0					
	16,17	+	+	+	+	0					
	14,15	1	1	+	+	0					
	12,13	2	3	1	+	0					
	10,11	3	9	8		+					
	8,9	3	13	14	3	+					
	6,7	2	11	12	2	7					
	4,5	1	2	_3	1	+					
	2,3	+	+	+	0	0					
	0,1	+	+	+	0	0					
	≦~1	+	+	0	0	0					

M	Marine Area D											
	9609	wi	nd Sp	eed	(kno	ts)						
	TEMP	0 -	4 -		22 -							
	(°C)	3	,0	2:	33	≥ 34						
	≥ 18	+	+	+	+	0						
	16,1	+	+	+	+	+						
	14,15	+	1		+	•						
	12,13	1	2	2	+	+						
	10.11	2	7	9	2	+						
	8,9	3	13	18	4	+						
	6,7	2	9	13	3	+						
	4,5	+	1	1	+	+						
	2,3	+	+	+	+	+						
	0.1	+	+	+	+	0						
	<u>≤</u> – 1	0	+	0	0	0						



N	ikol'sko	)				
	5308	Wi	nd Sp	eed	(kno	ts)
	TEMP (°C)	0~	10	11-	22 ~ 3 3	≥34
	≩20	+	0	0	0	+
	18,19	+	+	+	0	+
	16,17	+	+	+	0	0
	14,15	+	1	+	0	0
	12,13	4	10	7	+	+
	10,11	4	14	13	_2	+
	8,9	6	13	14	4	1
	6,7	1	2	1	1	+
	4,5	+	+	+	0	0
	2,3	0	0	0	_0	0
	≰ 1	0	0	0	0	0

Khatirka-In-Chukot									
3285 Wind Speed (knots)									
TEMP	10-	14-	11-	122~					
(°C)	_ 3	10	21	33	≩34				
≩ 18	+	+	+	+	0				
16,17	+	1	+	+	0				
14,15	1	1	1	+	0				
12,13	2	3	2	+	0				
10,11	3	3	2	+	+				
8,9	15	11	5	1	+				
6,7	17	12	6	1	+				
4,5	5	3	1	+	+				
2.3	1	1	+	+	0				
0,1	+	0	0	+	0				
≨-1	0	0	0	0	0				

Jgoi naja					
4852	wi	nd Sr	heed	(k	•=)
TEMP	0 -	4-	111-	22-	i
(°C)_	3	10	21	33	≩34
≩ 18	_+	+	+	+	0
16,17	+	1	+	+	+
14,15	1		1	+	+
12,13		3	2	1	÷
10,11	2	4	3	1	+
8,9	4	10	9	2	+
6,7	5	11	12	4	+
4,5	3	5	5	3	1
2,3		1	1	1	+
0,1	+	+	+	0	+
≨-1	0	+	+	+	0

В	Buhta Providenja											
	4490 Wind Speed (knots)											
	TEMP	0 -										
	(°C)	3	10	21	33	≩ 34						
	≩ 18	+	+	+	0	0						
	16,17	+	+	+	+	0						
	14,15	+	1	+	0	0						
	12,13	2	4	1	0	0						
	10,11	3	7	Z	+	0						
	8,9	8	15	4	+	0						
•	6.7	1.1	15	4	+	+	l					
	4,5	7	7	2	+	+						
	2,3	_ 3	2	+	+	0						
	0,1	+	+	0	0	0	ĺ					
•	<u>≨</u> -1	+	0	0	0	0						
-												

Norheast Cape										
10869	w;	nd Sp	eea	(kno	ts)					
TEMP	0-	4 -	111-	22 -	) )					
(°C)	3	10	21	33	≩34					
≥ 18	0	+	+	0	0					
16,17	+	+	+	+	+					
14,15	+	+	+	+	0					
12,13	+	2	2	+	+					
10,11	2	8	7	1	+					
8,9	4	13	11	1	+					
6,7	4	14	11	2	+					
4,5	2	4	5	1	0					
2,3	1	1	1	+	+					
0,1	+	+	+	_0	0					
≦ - 1	0	0	0	0	0					

21802	Wi	nd Sp	eed	(kno	ts)
	0-	4-	11-	22-	
(°C)	3	10	21	3 3	≩ 34
≥ 20	+	+	+	C	0
18,19	+	+	+	0	0
16,17	+	1	1	+	0
14,15	+	3	2	+	0
12,13	1	8	5	+	0
10,11	2	15	10	1	+
8,9	2	12	8	1	+
6,7	2	8	5	1	+
4,5	1	2	1	+	0
2,3	1	2	+	+	0
≤ 1	+	1	+	0	0

Unelskiest										
15786	Wi	nd Sp	eed	(kno	ts)					
TEMP	0 -	14 -	11- 1	122 -	1 1					
(°C)	]3_	10	21	33	₹34					
≥ 20	+	1		+	0					
18,19	+		1	+	0					
16,17	1	4	2	+	0					
14,15	1	6	3	+	0					
12,13	3	13	7	+	0					
10,11	4	16	11	1	+					
8,9	2	7	4	+	0					
6,7	1	4	2	+	0					
4,5	+	1	+	+	0					
2,3	+	1	+	0	0					
≤ 1	+	1	+	0	0					

Cape R	Cape Romanzof						
187	64	wi	nd Sp	eed	(kno	ts)	
7 E M (°C		- 3	4-	11-	22 - 3 3	≥ 34	
≥ 1	8	+	1	+	+	0	ļ
16,	17	+	1	+	+	О	1
14.	15	1	2	1	+	+	
12.	13	2	6	. 3	+	0	1
10.	11	4	11	.8	+	+	i
В,	9	4	13	10	1	+	1
6,	, I	5	12	8		+	•
4,	5	1	2	1	+	+	
2.	3	+	1	+	+	0	
0.	1	+	+	+	+	0	
≦ -	1	0	0	0	0	0	Ì

20043	Wi	nd Sp	oeed	(kno	ts)
TEMP	0-	4-	-11	22-	ſ
(°C)	3	10	21	33	≩34
<b>≥</b> 20	0	+	+	_0	0
18,19	+	+	+	+	0
16,17	+	+	+	+	0
14,15	1	1	1	+	0
12,13	3	6	5	1	0
10,11	8	17	11	1	+
8,9	6	16	10	_ 1	+
6,7	3	5	4	+	0
4,5	+	+	+	+	0
2,3	0	+	+	0	0
<u>≰</u> 1	0	0	0	0	0

KI	King Salmon								
	18824	wi	nd Sp	oeed	(kno	ts)			
	TEMP	0 -	4-	111-	122-	1			
	_(°C)	3	10	21	33	≥34			
	≩22	+	1	+	+	0			
	20,21	+	1	1	+	0			
	18,19	+	2	1	+	0			
	16,17	+	4	_3	+	+			
	14,15	1	6	4	1	+			
	12,13	2	13	_7	1	+			
	10,11	4	16	7	+	+			
	8,9	2	8	3	+	0			
	6,7	2	4	_1	+	0			
	4,5	1	1	+	0	+			
	≨3	1	1	+	0	0			
-									

5631					
5631		ua 2t	eea	(kno	(S)
TEMP	10-	4 -	11 -	22-	
(°C)	3	10	_21	3.3	≩34
≥ 20	+	+	+	+	0
18,19	+	1	1	+	0
16,17	+	2	2		0
14,15	1	3	3	1	0
12,13	2	9	8	1	+
10,11	4	16	12	1	+
8,9	4	10	8	1	+
6,7	_ 2	3	1	+	0
4,5	1	1	+	0	0
2,3	+	+	_0	0	0
≦ 1	+	+	0	0	0

14377	Wi	nd Sp	eed	(kno	(s)
TEMP	0 -	4 -	11~	22 -	ļ
(°C)	3	10	21	3 3	≥ 34
≥20	0	+	+	+	0
18,19	+	+	+	+	0
16,17	+	+	1	+	0
14,15	+	1	2	1	+
12,13	+	4	8	4	+
10,11	1	12	22	7	+
8,9	1	8	14	2	+
6,7	1	4	4	+	0
4,5	+	+	+	0	0
2,3	+	+	0	. 0	0
≨ 1	0	0	0	0	С

Nikolski					
2464		nd Sp	eed	(kno	ts)
7 <b>EMP</b> (°C)	0-3	4-	11-	22 - 33	≥34
≥ 16	0	0	0	0	0
14,15	0	+	0	0	0
12,13	+	1	1	+	0
10,11	1	5	6	1	0
8.9	2	11	10	2	+
6,7	4	22	21	4	+
4,5	. 1	4	4	1	+
2,3	+	+	+	0	0
0,1	0	0	0	0	0
-2,-1	0	0	0	0	0
€-3	0	0	0	0	0

st. Paul							
1108	39	Wi	nd Sp	oeed	(kno	ts)	
TEM		0 -	4-	11-	22-		1
(°C	)	3	10	21	33	≥34	ļ
≥ 1	9	0	0	0	0	0	l
16,1	7	0	+	+	0	0	Ì
14,1	5	+	+	+	+	0	1
12,1	3	0	+	1	+	0	1
10,1	1	+	5	10	1	+	١
8,9		1	17	≥6	_ 3	+	l
6,7		1	14	14	2	+	1
4,5		+	1	1	+	0	1
2,	1	+	+	+	0	0	1
0,1		+	+	0	0	0	1
<b>§</b> -	1	+	+	0	0	0	Ì
							•

22299	Wi	nd Sp	eed	(kno	ts)
TEMP	10-	4-	11-	22-	1
(°C)	3	10	21	33	≥ 34
<b>≩20</b>	+	+	_+	+	+
18,19	+	+	+	+	+
16,17	+	1	1	+	+
14,15	1	2	2	1	+
12,13	2	7	. 8	2	+
10,11	5	14	14	2	+
8,9	4	11	10	2	+
6,7	2	5	3	+	+
4,5	+	+	+	+	0
2,3	+	+	0	0	0
≨1	+	+	+	0	O

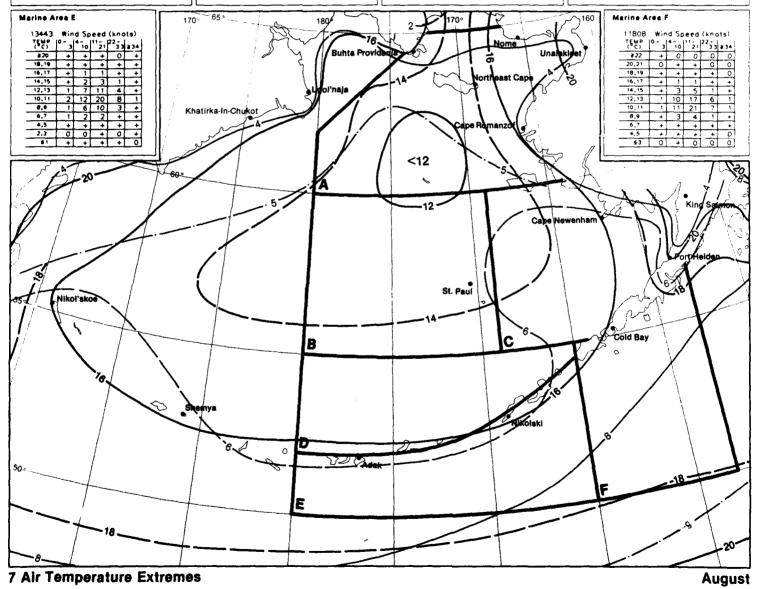
1011174					
18894	Wi	nd Sp	eed	(kno	ts)
	10-	4 -	111-	22-	
(°C)		10	21	33	≥34
₹18	0	0	0	0	0
16,17	+	0	+	С	0
14,15	+	+	+	0	C
12,13	+	2	2	+	0
10,11	2	13	14	2	+
8,9	5	19	25	4	+
6,7	2	5	4	+	+
4,5	+	+	0	0	0
2,3	0	0	0	0	0
0.1	0	0	0	0	0
≨~1	0	0	0	0	0

M	Marine Area A						
	4677	Wi	nd Sp	eed	(kno	ts)	
	TEMP	0~	4-	11-	22-	1 1	
	(°C)	3	10	21	33	≩ 34	
	≩ 18	+	+	+	0	0	
	16,17	+	1	+	0	0	
	14,15	+	1	+	+	0	
	12,13	1	3	2	+	+	
	10,11	T 7	6	8	1	+	
	8,9	2	12	17	4	+	
	6,7	3	13	13	3	+	
	4,5	+	_2	2	1	+	
	2,3	+	+	+	+	0	
	0,1	+	+	+	_0	0	
	≨-1	0	0	0	+	0	

М	Marine Area B						
	3683	Wi	nd Sp	eed	(kno	ts)	
		0 -	4~	11-	22-	1 1	
	(°C)	3	10	21	33	≩34	
	≥ 18	0	0	0	0	0	
	16,17	0	+	+	+	Ü	
	14,15	+	+	+	+	0	
	12,13	+	1	_ 2	+	U	
	10,11	1	7_	_13	_ 3	+	
	8,9	_2	12	29	9	1	
	6,7	_1	5	7	3	+	
	4,5	+	+	+	+	0	
	2,3	_0	+	+	0	0	
	0,1	_0	0	0	0	0	
	≦-1	0	0	0	0	0	

Marine Area C						
8537	Wi	nd Sp	oe <b>e</b> d	(kno	ts)	
TEMP	0-	4-	11-	22 -	1 1	
(°C)	3	10	21	33	≩34	
≥ 20	1 +	+	+	_ 0	+	
18,19	+	+	+	0	0	
16,17	+	+	+	+	0	
14,15	+	1	1	+	+	
12,13	1	4	3	1	+	
10,11	2	12	17	5	+	
8,9	2	14	22	6	+	
6,7	+	2	4	1	+	
4,5	+	+	+	+	0	
2,3	0	+	+	0	0	
<u>≨</u> 1	0	0	0	0	0	
					ت	

Marine A	rea D	•			
9657	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4-		22-	
(°C)_	3	10	21	33	≩ 34
₹20	<u>+</u>	+	0	+	0
	+	+	+	0	0
16.1	+	+	+	+	0
14,15	+	1	1	+	+
12,13		4	. 5	1	+
10,11	3	11	15	5	+
8,9	3	12	19	6	+
6.7	1	3	4	1	+
4,5	+	+	+	+	+
2,3	_+	+	+	+	0
<u>≤</u> 1	+	+	+	0	0



# Nikol'skos

5265	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4-	11-	22-	1 1
(°C)	3	10	21	33	≩34
≩ 18	0	0	0	0	0
16,17	0	+	+	0	0
14,15	0	+	0	0	0
12,13	+	3	2	1	+
10,11	2	8	111	3	+
8,9	5	15	17	4	3
6,7	4	7	6	3	+
4,5	2	2	2	1	+
2,3	+	+	+	+	0
0,1	+	+	+	0	0
<b>≨</b> – 1	+	+	0	0	+

### Khetirke-In-Chukot

3160 Wind Speed (knots)								
TEMP (°C)	0~3	10	21	22 - 33	≥34			
≥ 14	+	+	+	0	0			
12,13	+	1	+	+	.0			
10,11	1	1	1	+	Ö			
8,9	5	4	2	+	0			
6,7	13	10	7	7	+			
4,5	9	7	6	. 2	+			
2,3	6	5	5	2	+			
0,1	2	1	1	1	+			
-2,-1	,	1	1	+	+			
-4,-3	+	1	+	+	+			
≨-5	+	+	+	+	0			

# Ugol'naja

4796 Wind Speed (knots)								
TEMP	0-	4-		22-	1			
(°C)	3	10	21	3.3	≥ 34			
≩ 14	+	+	_+	0	+			
12,13	+	1	+	+	0			
10,11	+	1	1	+	+			
8,9	1	2	3	1	+			
6,7	4	7	7	2	+			
4,5	4	7	10	3	1			
2,3	4	7	9	4	. 2			
0,1	1	2	3	2	1			
-2,-1	1	1	2	2	1			
-4 -3	+	1	1	1	+			
≨-5	+	+	1	+	+			

#### Buhte Providenja

4314	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -		22-	l . i
(°C)	3	10	21	3.3	≥ 34
≥ 14	0	0	0	0	0
12,13	+	+	+	0	0
10,11	+	2	_+	+	0
8,9	2	4	2	+	0
6.7	5	1.1	4	+	0
4,5	9	13	5	+	Q
2,3	9	11	5	+	0
0,1	4	3	2	+	_ 0
-2,-1	3	2	7	+	0
-4,-3	1	1	+	+	0
≦-5	+	+	+	0	0

#### Norheast Cape

10867	Wii	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11-	22 - 1	
(°C)	3	10	21	33	≩34
≥ 14	0	0	0	0	0
12,13	+	+	+	+	0
10,11	+	1	1	+	+
8,9	1	4	4	1	+
6,7	4	1.1	15	2	+
4,5	3	_8	1.1	1	+
2,3	. 3	7	1.1		+
0,1	1	3	4	1	+
-2,-1	+	+	1	+	0
-4,-3	+	+	+	+	0
<u>⊊</u> -5	0	+	0	0	0

#### Nome

21073 Wind Speed (knots)								
TEMP	0 -	4-		22~				
(°C)	3	10	21	33				
<u>₹</u> 16	0	_+	L ±	+	0			
14.15	_ +_	+	+	+	0			
12,13	+	2	2	+	0			
10,11	1	6	4	+	0			
8,9	1	8	7	1	+			
6,7	2	12	11	_1	+			
4,5	1	7	4	+	+			
2,3	2	6	4	+	+			
0,1	2	5	3	+	_ +			
-2,-1	1	2	1	+	0			
≦-3	1	2	+	+	0			

#### Unalakieet

15343	wi.	nd Sp	eed	(kno	ts)
TEMP	0 - 3	4-	11- 21	22 - 3 3	≥ 34
≥ 16	+	1	1	+	0
14,15	+	1	1	+	0
12,13	+	3	3	+	0
10,11	1	7	6	+	0
8,9	2	8	7	+	+
6,7	2	12	9	1	+
4,5	2	6	4	1	0
2,3	1	5	3	+	+
0.1	1	4	2	+	+
-2,-1	1	2	1	+	0
<b>≨</b> -3	1	2	+	+	0

# Cape Romanzof

18176	Wil	nd Sp	eed	(kno	ts)
TEMP	10 ~	4 -	11	122 -	
(°C)	3	10	21	33	≥34
≥ 16	+	+	_ +	0	0
14,15	+	+	+	0	O
12.13	+	1	1	+	C
10.11	2	5	3	+	+
8,9	2	7	7		-
6,7	3	13	_13	2	•
4,5	2	8	7	1	-
2.3	2	5	5	1	+
0,1	1	2	2	1	-
-2,-1	+	+	!	+	+
<u>s</u> -3	+	_+	+		( )

#### Cape Newenham

19728	Win	nd Sp	eed	(kno	ts)
TEMP	0-	4 -		22 -	ł
(°C)	3	10	21	33	≥34
≥ 18	0	0	+	0	0
16,17	+	+	+	0	٥
14,15	+	+	+	_0	0
12,13	1	1	1	+	0
10,11	4	9	6	1	+
8,9	5	15	10	1	+
6,7	4	13	1.1	1	+
4,5	1	4	3	+	0
2,3	1	2	2	+	0
0.1	+	1	+	+	0
<u>≨</u> – 1	+	+	+	0	0

### King Salmon

18211 Wind Speed (knots)								
TEMP	0-	4 -	11-	22~	] ]			
رەت)	3	10	21	33	≥ 34			
≥ 18	+	_+	+	+	0			
16.17	+	1	1	+	0			
14,15	+	2	2	+	+			
12,13	1	_6	_ 5	1	_ +			
10,11	2	11	8	1	+			
8,9	2	10	5	+	+			
6,7	3	12	4	+	+			
4,5	2	5	1	+	0			
2,3	1	4	1	+	0			
0.1	1	3	1	+	0			
≦ - 1	1	2	+	+	0			

### Port Heiden

6205	We	ug St	peed	(kno	ts)
TEMP	0 -	4 -	11-	22-	
(aC)	3	10	21	3 3	≥ 34
<u>≥</u> 18	0	0	<u>+</u>	+	0
16,17	+	+	+	+	+
'4,15	+	1	1	+	+
12,13	1	4	4	.1	+
10,11	2	8	10	2	0
8,9	2	12	12	2	+
6,7	2	10	8	_ 1_	0
4,5	1	5	2	+	0
2,3	1	3	1	+	0
0,1	+	2	+	0	0
≦-1	+	+	+	0	0

### Cold Bay

13918	Wir	nd Sp	eed	(kno	ts)
TEMP	0 - '	4 -	11 -	22-	
(°C)_	3	10	21	33	≥34
≥ 18	0	+	+	+	J
16.17	Ç	0	+	+	0
14,15	+	+	+	+	0
12,13	+	2	3	1	+
10,11	1	7	14	4	+
8,9	1	8	15	4	+
6,7	1	9	14	_3	+
4,5	1	3	3	_+	+
2,3	+	2	1	+	0
0,1	+	+	+	0	0
≦-1	+	+	С	0	0

#### Nikolski

2356	Wi	nd Sp	eed	(kno	ts)
TEMP	0-	4 -		22-	
(°C)	3	10	21	33	₹34
≥ 16	0	0	0	0	0
14,15	0	Q	0	0	0
12,13		+	+	0	C
10.11	+	_ 2	2	+	0
8,9	1	8	8	1	0
6,7	4	21	22	3	+
4,5	1	7	10	4	+
2.3	+	1	2	1	+
0,1	0	0	+	0	0
-2,-1	0	0	0	0	0
<b>5-3</b>	0	0	0	0	0

# St. Paul

10316	Win	nd Sp	eed	(kno	ts)
TEMP	10-	4-	11-	22-	]
(°C)	3	10	21	33	≥ 34
≥ 16	0	0	0	0	0
14,15	0	+	+	0	0
12,13	0	+	+	+	0
10,11	+	1	3	1	0
8,9	+	8	18	3	+
6,7	1	14	22	5	+
4,5	1	5	5	2	+
2,3	+	3	2	. 1	<b>+</b>
0,1	+	2	+	+	0
-2,-1	+	+	+	0	0
≨-3	+	+	0	0	0

# Adek

21540	Win	nd Sp	eed	(kno	ts)
TEMP	10-	4-	111-	22 -	1 1
(°C)	_ <u>3</u>	10	21	_33	≥ 34
≱ 1B	0	+	+	_+	0
16,17	+	+	+	+	+
14,15	+	_+	+	+	+
12,13	+	2	3	1	+
10,11	2	11	11	2	+
8,9	3	14	14	_ 3	+
6,7	5	11	9	2	+
4,5	1	1	1	+	+
2,3	1	+	+	+	0
0,1	+	+	0	0	0
<b>≶</b> -1	+	0	0	0	0

# Shemya

18865	Wir	nd Sp	eed	(kno	ts)
TEMP	0- 1	4 -	11-	22-	
(°C)	3	10	21	33	≥ 34
≩ 18	0	0	0	0	0
16,17	0	0	0	0	0
14,15	+	0	+	0	0
12,13	+	1	1	+	+
10,11	1	7	11	3	+
8,9	4	14	23	6	+
6.7	4	8	10	2	+
4,5	1	1	1	+	+
2,3	+	+	+	+	0
0,1	+	0	0	+	0
≨-1	0	0	0	0	0

September

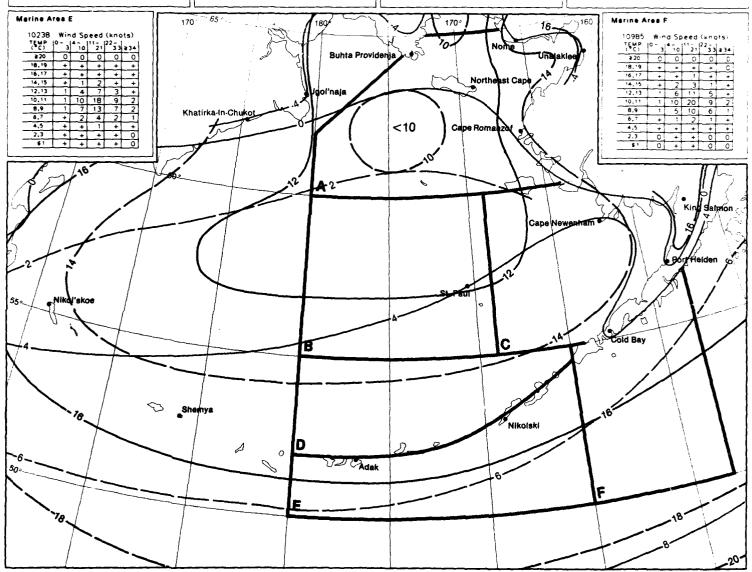
7 Air Temperature and Wind Speed

	Marine Area A									
	3705	Win	nd Sp	eed	(kno	ts)				
	TEMP (°C)	0-3	4- 10	11-	22 <i>-</i> 33	≥34				
	≥ 16	+	+	0	0	0				
1	14,15	+	+	_ +	+	0				
	12,13	+	1	1	+	0				
í	10,11	1	3	3	1	+				
1	8.9	1	5	10	3	+				
İ	6,7	2	10	16	4	1				
	4,5	2	7	10	4	+				
	2.3	1	3	5	2	+				
	0,1	+	1	1	1	+				
	-2,-1	0	+	+	+	+				
	≦-3	+	0	0	0	+				

М	Marine Area B										
	2800	Wie	nd Sp	eed	(kno	ts)					
	TEMP	0-	4-	11-	22-	1 4					
	(°C)	3	10	21	3.3	≥ 34					
	≩ 16	0	0	0	0	0					
	14,15	0	0	+	0	0					
	12,13	+	+	+	+	+					
	10,11	1	3	5	2	+					
	8,9	2	8	18	7	1					
	6,7	2	9	17	7	2					
	4,5	1	3	5	3	1					
	2,3	+	1	1		+					
	0,1	+	+	+	+	0					
	-2,-1	0	0	0	+	0					
	≦-3	0	Ö	0	0	0					

9055 Wind Speed (knots)  TEMP  0-  4-  11-  22-     (°C)   3   10   21   33 ≥34
(9c)   3  10  31  33  34
(°C) 3 10 21 33 ≥34
≥18 C + + O O
16,17 + + + 0 0
14,15 + + + +
12,13 + 1 1 + +
10.11 1 6 8 3 +
8.9 1 11 23 10
6.7 1 6 13 6
4.5 + + 2 1 +
2.3 + + + + +
0.1 0 + + + 0
≦-1 0 0 0 0 0

erine Area D											
8731	Wi	nd Sp	eed	(kno	ts)						
TEMP	0 -	0 -  4 -  11 -  22 -									
(°C)	3	10	21	33	≩34						
₹18	+	+	+	+	_ 0						
16,17	+	+	+	+	0						
14,15	+	+	1	+	+						
12,13	1	3	3	1	+						
10.11	2	7	11	4							
8,9	2	10	18	9	2						
6,7	1	6	10	5	1						
4,5	+	1	î	+	+						
2,3	+	+	+	+	+						
0,1	+	+	+	+	+						
≦-1	0	0	0	0	C						



7 Air Temperature Extremes

September

N	kol'skos	•					
	5517	Wil	nd Sp	eed	(kno	ts)	
		0-	4-	11-	22-	1 }	
	(°C)		10	21	33	≩34	
	≩ 14	0	0	0	0	0	
	12,13	0	0	0	+	0	
	10,11	+	+	1	+	0	
	8,9	+	2	3	1	+	
	6,7	2	6	10	5	1	
i '	4,5	3	9	10	4	1	
	2,3	5	9	9	4	1	
	0,1	1	2	3	1	+	
	-2,-1	1	1	1	+	+	
	-4 - 3	+	+	+	+	+	
	£-5	0	0	+	0	0	

Khatirka-li	(hatirka-in-Chukot								
3497	Wi	nd Sp	eed	(kno	ts)				
TEMP	Ju-	4-	11-	22-	i i				
(°C)	3	10	21	33	≩ 34				
<b>≩</b> 6	+	+	1	+	0				
4,5	2	2	2	1	+				
2,3	3	3	4	2	+				
0,1	3	3	3	1	+				
-2,-1	3	4	5	2	+				
-4,-3	3	3	5	2	+				
-6,-5	2	3	5	2	+				
~8,-7	1	3	5	3	1				
-10,-9	1	1	2	1	+				
-12,-11	1	1	2	1	+				
≦-13	1	1	2	1	+				

U	gol'neja					
	5114	Wit	nd Sp	eed	(kno	ts)
	TEMP	0-	4-	11-	22-	ł
	(°C)	3	10	21	33	≩34
	≩6	+	+	+	+	+
	4,5	+	1	2	1	+
	2,3	1	3	_ 3	2	. 1
	0,1	2	2	3	2	1
	-2,-1	1	3	5	4	3
	-4,-3	1	2	5	4	2
	-6,-5	2	2	3	4	2
	-8,-7	2	2	3	3	2
	-109	1	1	1	2	1
	~12,-11	1	1	2	2	1
	≦-13	1	2	2	2	2

4540	Wi	nd Sg	eed	(kno	ts)
TEMP	0 - 3	10	11- 21	22 ~ 33	≩ 34
≩6	0	+	+	+	0
4,5	+	2	1	0	0
2.3	2	6	4	1	0
0,1	3	7	3	1	+
-2,-1	5	8	6	1	+
-4,-3	5	8	5	1	+
-6,-5	4	6	4	1	+
-8,-7	4	3	1	+	0
-10,-9	1	1	+	+	0
-12,-11	2	1	1	+	0
≦-13	1	+	+	+	0

Norheast Cape									
11066	Wi	nd Sp	eed	(kno	ts)				
TEMP	0 -	4-	11-	22 -	1				
( °C )	3	10	21	33	≥34				
<b>≩</b> 8	0	+	+	+	0				
6,7	+	1	2	+	+				
4,5	+	2	4	1	+				
2.3	1	_3	8	2	+				
0,1	1	6	16	5	+				
-21	2	6	11	3	+				
~4,~3	1	5	9	2	+				
~6,~5	1	2	3	+	+				
~8,~7	+	1	2	+	+				
-10,-9	+	+	+	+	Ö				
≦-11	+	+	+	0	0				

Nome					
21813	Wi	nd Sp	eed	(kno	(s)
	0~	4-	11-	[22 - ]	
(°C)	3	10	21	33	≩34
<b>≩</b> 8	+	+	+	+	0
6,7	+	1	1	+	+
4,5	+	3	3	1	+
2,3	1	5	6	1	+
0,1	2	9	8	1	+
-2,-1	2	7	4	1	+
-4,-3	_ 2	8	5	1	+
-6,-5	1	5	2	+	+
-8,-7	2	5	2	+	+
-10,-9	1	3	1	+	0
≦~11	2	3	+	+	0

U	Unalakiees									
	15772		nd Sp	eed	(kno	ts)				
	TEMP	0-	4 -	11-	22-					
	(°C)_	3	10	21	3.3	₹34				
	≩6	+	2	3	+	0				
	4,5	+	2	2	+	+				
	2,3	1	4	5	1	+				
·	0.1	2	7	7	1	+				
	-2,-1	2	6	4		0				
	-4,-3	2	6	. 5	1	+				
	-6,-5	1	4	3	1	_+				
	~87	2	4	4	1	+				
	-10,-9	1	3	2	+	+				
	-12,-11	+	2	1	+	+				
	≨-13	1	3	ī	+	0				

18620 Wind Speed (knots)										
TEMP	10-	0- (4- (11- (22- )								
(°C)	3	10	21	33	≩34					
≩Β	+	+	+	+	0					
6,7	+	2	1	+	0					
4,5	1	3	3	+	+					
2,3	2	6	6	1	+					
0,1	3	7	10	2	+					
-2,-1	3	6	8	2	+					
-4,-3	2	5	7	2	+					
-6,-5	2	3	4	1	+					
-8,-7	1	1	2	1	+					
-10,-9	+	+	+	+	+					
≦-11	+	+	+	+	+					

20493 Wind Speed (knots)  TEMP 0- 4- 11- 12- (°C) 3 10 12- 133 334  \$12	C	Cape Newenham									
(°C) 3 10 21 33 ₹34 ₹12 0 + + + 0 10,11 + + + + + 0 8,9 1 1 1 2 + + 6,7 1 5 5 + + 4,5 2 7 6 1 + 2,3 3 9 9 1 + 0,1 3 8 7 1 + -2,-1 1 4 4 1 + -4,-3 1 3 4 1 +		20493	Wii	nd Sp	eed	(kno	ts)				
₹12     0     +     +     +     0       10,11     +     +     +     +     +     0       8,9     1     1     2     +     +       6,7     1     5     5     +     +       4,5     2     7     6     1     +       2,3     3     9     9     1     +       0,1     3     8     7     1     +       -2,-1     1     4     4     1     +       -4,-3     1     3     4     1     +			0-	4-	11-		1 1				
10,11 + + + + + 0 8,9 1 1 2 + + 6,7 1 5 5 + + 4,5 2 7 6 1 + 2,3 3 9 9 1 + 0,1 3 8 7 1 + -2,-1 1 4 4 1 + -4,-3 1 3 4 1 +		(°C)	3	10	21	3 3	3 34				
8,9 1 1 2 + + 6,7 1 5 5 + + 4,5 2 7 6 1 + 2,3 3 9 9 1 + 0,1 3 8 7 1 + -2,-1 1 4 4 1 + -4,-3 1 3 4 1 +		≩12	0	+	+	+	0				
6,7 1 5 5 + + 4,5 2 7 6 1 + 2,3 3 9 9 1 + 0,1 3 8 7 1 + -2,-1 1 4 4 1 + -4,-3 1 3 4 1 +		10,11	+	+	+	+	0				
4,5 2 7 6 1 + 2,3 3 9 9 1 + 0,1 3 8 7 1 + -2,-1 1 4 4 1 + -4,-3 1 3 4 1 +		8,9	1	1	2	+	+				
2.3 3 9 9 1 + 0.1 3 8 7 1 + -21 1 4 4 1 + -43 1 3 4 1 +		6,7	1	5	5	+	+				
0,1 3 8 7 1 + -2,-1 1 4 4 1 + -4,-3 1 3 4 1 +		4,5	2	7	6	1	+				
-2,-1 1 4 4 1 + -4,-3 1 3 4 1 +		2,3	3	9	9	1	+				
~43 1 3 4 1 +		0,1	3	8	7	1	+				
		-2,-1	1	4	4	1	+				
36 5 1 1 2 4 4		~4,-3	1	3	4	1	+				
		-6,-5	1	1	2	+	+				
<b>≨</b> -7 + 1 1 + +		≨-7	+	1	1	+	+				

cing Saimon									
18846	Wi	nd Sp	eed	(kno	ts)				
TEMP	0 -	4-	11~	22-					
(°C)	э	10	21	33	≩34				
≥10	+	1	2	+	+				
8,9	+	2	2	1	+				
6,7	1	5	5	1	+				
4,5	1	6	4	1	+				
2,3	5	8	4	+	+				
0,1	2	10	4	+	0				
-2,-1	2	5	2	+	0				
-4,-3	2	5	2	+	0				
-6,-5	1	3	1	+	+				
-8,~7	1	3	1	+	0				
≨-9	2	4	1	+	0				

6048	Win	nd Sp	eed	(kno	ts)
TEMP	0-	4-	11-	22~	ı
(°C)	3	10	21	33	≩34
≥12	+	+	+	+	0
10,11	+	1	2	+	0
8,9	+	2	4	1	+
6,7	1	6	8	2	+
4,5		7	9	1	+
2,3	1	7	8	1	0
0,1		8	6	+	+
-2,-1	1	5	2	+	0
-4,-3	1	3	2	+	0
-6,-5	+	2	1	+	0
€-7	+	2	1	+	0

Port Heiden

Adek

Co	ld Bay					
	14379	Wir	nd Sp	eed	(kno	ts)
	TEMP	10-	4 -	[11- ]	22-	1
	(°C)_	3	10	21	33	≩ 34
	≥ 14	0	.0	4	+	+
	12,13	+	+	+	+	+
	10.11	+	1	1	1	+
	8.9	+	1	4	2	+
	6,7	+	5	12	5	+
	4,5	1	5	10	3	+
	2,3	1	8	12	4	+
	0,1	1	7	7	2	+
	-2,-1	+	2	1	1	+
	-4,-3	+	1	+	+	+
•	≨~5	+	+	+	+	0

Wi	nd Sp	eed	(kno	ts)
0-	4-	11-	72-	
				_
0	0	_ 0	0	0
<u> </u>	0	+	_ 0	0
0	+	1	+	0
+	4	7	2	+
_ 2	9	14	6	+
1	7	14	7	_ 1
1	4	8	_ 5	1
+	1	1		+
0	0	+	+	0
0	0	0	0	0
0	0	0	0	. 0
	0 0 0 0 + 2 1 1 + 0	0 0 0 0 0 0 0 0 + + 4 2 9 1 7 1 4 + 1 0 0 0	0 4 - 1 11 - 1 1	3 10 21 33 0 0 0 0 0 0 0 + 1 + 4 7 2 2 9 14 6 1 7 14 7 1 4 8 5 + 1 1 1 0 0 + + 0 0 0 0

11311	Wi	nd Sp	eed	(kno	ts)
TEMP (°C)	0-3	10	11-	22 - 33	≩34
₹12	0	0	0	0	0
10,11	0	+	+	0	0
8,9	+	+	1	+	+
6,7	+	3	11	4	+
4,5	+	4	12	5	+
2,3	_ 1	6	13	5	1
0,1	_1	7	10	4	1
~2,-1	+	2	2	1	+
-4,-3	+	1	1	+	0
-6,-5	+	+	+	0	0
<b>6</b> -7	+	+	0	0	0

St. Paul

22296	Wi	nd Sp	eed	(kno	ts)
TEMP	0-	4 -	11~	22-	1 1
(°C)	3	10	21	33	≥ 34
₹16	0	0	0	+	0
14,15	0	0	0	+	+
12,13	0	+	+	+	+
10,11	+		2	1	+
8,9	1	4	6	2	+
6,7	3	12	16	5	1
4,5	3	9	10	3	+
2,3	3	6	5	1	+
0,1	2		1	+	0
-2,-1	+	+	+	0	0
≨-3	+	0	0	0	0

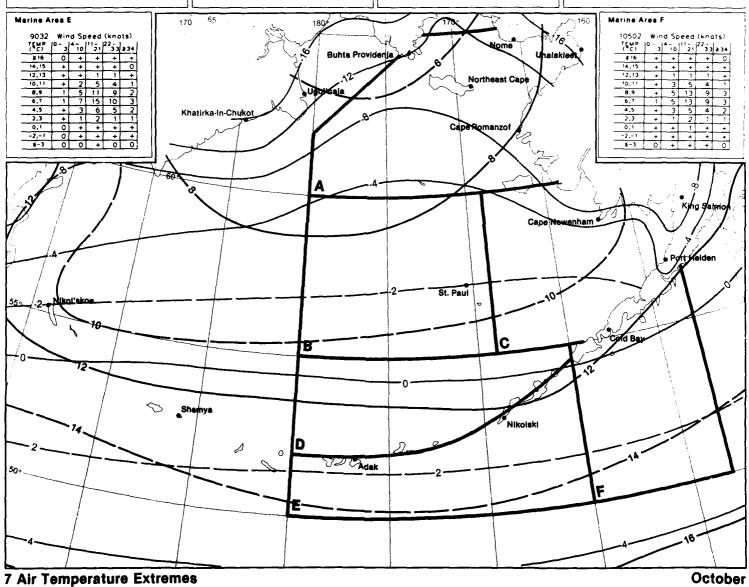
21	16MYE						
	19529	Wi	nd Sp	eed	(kno	ts)	
	TEMP	0-	4-	111-	22~		
	(°C)	3	10	21	33	≩34	
	≩14	0	0	0	0	0	
	12,13	0	0	+	0	0	
	10,11	+	+	+	+	+	
	8,9	+	2	5	2	1	
	6,7	2	- 8	18	8	2	
	4,5	3	7	13	6	1	
	2,3	2	5	7	3	1	
	0,1	1	1	1	+	+	
	-2,-1	+	+	+	+	+	}
•	-4,-3	+	+	+	+	0	}
•	≨-5	+	0	0	0	0	
							_

Marine Area A								
2532	Wi	nd Sp	eed	(kno	ts)			
TEMP	0-	4-	11-	22 -	1			
(°C)	<u>3_</u>	10	_21	33	≩34			
≩12	0	0	_ +	0	0			
10,11	+	+	+	+	0			
8,9	+	+	+	+	+			
6.7	+	2	5	_ 3	+			
4,5	1	4	_10	6	+			
2,3	1	6	11	5	1			
0,1	2	8	13	6	1			
-2,-1	+	2	3	2	+			
-4,-3	+	+	. 1	1	+			
-6,-5	+	+	1	+	+			
≦-7	0	+	+	+	+			

Marine Area B								
1939	Wi	nd Sp	eed	(kno	ts)			
	0 -	4-	11-	22~				
(°C)	3	10	21	33	≥34			
<u>≩</u> 14	_0	0	0	_+	0			
12,13	0	0	+	0	0			
10,11	0	+	1	+	+			
8,9	+	1	2	1	+			
6,7	+	3	9	6	1			
4,5	1	4	13	10	2			
2,3	1	6	10	8	2			
0,1	1	3	6	4	1			
-2,-1	0	+	1	1	+			
-4,-3	0	+	+	+	0			
<u>≨</u> -5	0	0	+	+	0			

M	Marine Area C								
	5124	Wi	nd Sp	eed	(kno	ts)			
	TEMP	0-	4-	11-	22 - 1		ı		
	(°c)	3	10	21	33	≩ 34	ļ		
	≥ 14	+	+	+	0	+			
	12,13	+	+	+	+	+			
	10,11	+	+	1	+	+	1		
	8,9	+	2	5	3	1			
	6,7	+	5	13	8	2			
	4,5	1	6	15	9	2			
	2,3	+	3	9	5	7			
	0,1	+	1	3	2	+			
	-2,-1	+	+	+	+	+	1		
	-4,-3	+	+	+	+	+			
	≨-5	0	0	0	0	0			
					<u> </u>		•		

Marine Area D								
8215	Wi	nd Sp	peed	(kno	ts)			
TEMP (°C)	0-	4-		22-				
	3	10	21	33	≥34			
≩ 16	0	+	+	+	+			
14,15	+	+	+	+	+			
12,13	+	+	+	+	+			
10,11	1	2	2	1	+			
8.9	1	5	8	5	1			
6,7	1	8	18	10	3			
4,5	1	5	11	6	2			
2,3	+	1	3	2	1			
0,1	+	+	+	+	+			
-21	0	+	+	+	+			
≨~3	+	+	+	0	0			



# II-182

Nikol'skoe	)				
5268	Wi	nd Sp	eed	(kno	ts)
TEMP	0-	4-		22 -	1 1
(°C)	3	10	21	33	≩ 34
≥ 10	0	0	0	0	0
8,9	_0	0	0	0	+
6,7	_0	+	+	+	+
4,5	+	1	3	1	1
2,3	1	4	8	6	3
0,1	1	5	8	4	1
-2,-1	2	7	10	4	2
-4, -3	2	_5	_ 7	3	1
-v, s	_ 1	2	2	1	+
-8,-7	+	+	1	+	+
≨-9	0	0	0	0	0

Kh	Khatirka-In-Chukot							
	3240	Wi	nd Sp	oeed	(kno	ts)		
	TEMP	0 -	4 -	11-	22-	1		
_	(°C)	3	10	21		≥34		
	≩-2	2	5	6	4	1		
Ī	-4,-3	1	1	2	2	+		
_	-6,-5	1	1	2	3	+		
	-8,-7		2	4	3	1		
_	-10,-9	1	2	2	1.	+		
	-12,-11	1	2	3	2	1		
	-14,-13	1	2	3	2	1		
	-16,-15	1	2	3	2	1		
_	~18,-17	1	2	4	3	1		
_	-20,-19	+	1	1	1	+		
_	≦-21	1	2	3	1			

igol'naja					
4983	Wi	nd Sp	eed	(kno	ts)
TEMP	0-	4-	111-	22-	ł
(°C)	3_	10	21	33	≥ 34
≩-2	1	1	5	6	4
-4,-3	_ 1	1	_ 2	2	2
-6,-5	1	2	2	2	2
-0,-7	1	2	2	3	2
-10,-9	1	1	1	1	1
-12,-11	1	1	1	2	3
-14,-13	1	1	2	2	2
-16,-15	1	1	1	2	2
-18,-17	1	2	1	2	4
-20,-19	1	1	1	1	2
≦-21	2	2	2	3	3

Buhta Prov	riden	je			
4295	wi	nd Sp	eed	(kno	ts)
	10 -	4 -		22-	i 1
(°C)	3	10	21	3.3	≥ 34
₹2	+	1	_2	1	+
0,1	+	2	_ 3	+	+
-2,-1	1	3	5	1	+
-4,-3	1	4	5	1	+
-65	1	4	5		+
-67	2	5	6	1	+
-109	2	3	2	1	+
-12,-11	3	4	3	1	+
-14,-13	2	3	3	+	+
-16,-15	2	3	1	+	0
<b>≨</b> -17	5	4	1	0	0

Norheast (	Cepe				
10289	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -		22~	1
(°C)	3	10	21	33	≥34
≥4	0	0	0	0	+
2,3	+	+	1	1	+
0,1	+	_ 2	_ 7	4	+
-2,-1		3	8	3	+
-4,-3	1	4	11	5	+
-6,-5	1	2	7	3	+
-87	_ 1	3	7	3	+
-10,~9	1	2	5	2	+
-12,-11	+	1	2	+	+
-14,-13	+	1	1	+	+
<u>s</u> - 15	+	1	2	+	+

01114					
21112	Wi	nd Sp	eed	(kno	ts)
TEMP	10-	4 -	11-	22 -	
(°C)	3	10	21	33	≥ 34
≥0	+	3	6	2	+
-2,-1	+	3	4	1	+
-4,-3	1	4	6	1	+
-6,-5	1	3	4	1	+
-8,-7	2	5	5	1	+
~10,-9	2	6	4	1	0
-12,-11	1	4	2	+	+
-14,-13	2	4	2	+	+
-16,-15	1	2	1	+	0
-13,-17	2	2	1	+	0
≦~19	4	5		+	0

	•				
15355	wi	nd Sp	oeed	(kno	ts)
TEMP	10 ~	4 ~	11~	22~	
(°C)	3	10	21	33	≥ 34
≥~2	1	4	8	_2	+
-4,-3	+	2	5	_2	+
-6,-5	1	2	4	1	+
-8,-7	1	4	5	2	+
-10,-9	1	4	5	2	+
-12,-11	1	3	3	1	+
-14,~13	1	3	4	1	+
-16,-15	1	2	_ 2	,	+
-18,-17	1	2	1	1	+
-20,-19	1	2	1	+	+
£-21	2	7	1	+	+

17739	Wi	nd Sp	eed	(kno	ts)
TEMP	0-	4	11-	22 -	
(°C)	3	10	21	33	≥ 34
≥4	+	+	+	+	0
2,3	+	j	_2	1	+
0,1	1	3	7	2	+
-2,-1	2	3	6	1	+
-4,-3	3	4	6	. 2	+
-6,-5	3	4	5	2	+
-8,-7	_3	4	4	3	+
-10,-9	2	2	3	2	1
-12,-11	1	1	2	1	+
-14,-13	1	1	2		+
<u>≤</u> -15	1	1	2	1	1

٠.	Cape Newsnnam							
	19267	wi	nd Sp	eed	(kno	ts)		
	TEMP	10-	4-	11-	22 -			
	(°C)	3	10	21	33	≥ 34		
	₹8	0	+	+	_ 0	0		
	6,7	+	+	1		+		
	4,5	+	1	3		+		
	2,3	1	5	8	1	+		
	0,1	4	9	8		+		
	-2,-1	3	4	4		+		
	-4,-3	3	4	5	1	+		
	-6,-5	2	3	3	1	+		
	-87	2	2	2		+		
	-109	1	2	2	1	+		
	<u></u> ≤-11	2	3	3	1	+		

ing Saim	J.,				
18239	Wi	nd Sp	oe <b>e</b> d	(kno	ts)
TEMP	10 -	4	11-	22~	1
(°C)	3	10	21	33	≩ 34
₹4	+	2	6	2	+
2,3	1	4	6	1	+
0,1	2	9	4	+	+
-2,-1	1	5	_2	+	0
-4,-3	2	5	2	+	0
-6,-5	1	3	1	+	0
-8,-7	2	5	2	+	0
-10,-9	2	4	_ 1	+	0
-12,-11	1	2	1	+	0
-14,-13	1	3	2	+	+
≦-15	3	. 7	3	+	0

Port	Port Heiden							
5	524	Wi	nd Sp	eed	(kno	ts)		
	MP	0 -	4		22 -	. 1		
(	()		10	23	_33	≥ 34		
	<b>8</b> ≨	+	+	+	1	+		
	5.7	+	+	1		+		
- 4	1,5	+	1	3	1	+		
	2,3	1	6	8	3	1		
	1,0	2	9	6	1	+		
-:	2,-1	2	9	5	1	+		
-4	1,-3	2	6	4	+	0		
-6	5,-5	1	5	2	+	0		
6	3,-7	+	3	2	+	0		
- 10	),-9	+	2	1	+	0		
_ ≤	-11	+	3	2	+	0		

C	old Bay					
	13919	Wi	nd Sp	eed	(kno	ts)
	TEMP (°C)	0-3	4-	11-	22 - 33	≥ 34
-	≥ 10	+	+	+	+	+
	8,9	Ü	+	Ŧ	+	+
	6,7	+	1	3	2	1
	4,5	+	3	ń	3	,
-	2,3	1	8	13	5	1
	0,1	1	10	11	3	+
_	-2,-1	1	4	4	2	+
	-4,-3	1	3	4	2	+
	-6,-5	+	1	1	+	+
	-8,-7	+	1	+	+	+
	≦-9	+	+	+	+	0

Nikolski					
2077	Wi	nd Sp	eed	(kno	ts)
TEMP	0	4 -		22-	
(°C)	3	10	21	33	≥ 34
₹12	Lo	0	0	0	_ 0
10,11	0	0	0	0	0
8,9	0	0	+	0	+
6,7	O	+	2	1	+
4,5	+	4	5	2	+
2,3	2	9	14	6	1
0,1	2	11	17	10	1
-2,-1	1	2	3	2	1
-4,-3	+	+	i	1	+
-6,-5	0	+	+	+	0
<b>≤</b> - 7	0	0	Ô	0	0

St	t. Paul					
	11380	Wi	nd Sp	eed	(kno	ts)
	TEMP	0 -	4	11-	22-	1 1
	(°C)		10	21	33	≩34
	≥ 10	0	0	0	0	_0
	8,9	0	+	_+	_+	0
	6,7	0	+	1	1	+
	4,5	+	1	6	4	+
•	2,3	+	4	15	7	1
	0,1	1	8	14	7	1
	~2,~1	1	4	6	_ 2	+
	-4,-3	1	3	4	2	+
	-65	+	1	1		+
	-8,-7	+	1	1		+
	≨-9	+	+	+	+	0

20880	Wit	nd Sp	eed	(kno	ts)
TEMP	10-	4-	11-	22-	ŀ
(°C)	3	10	21	33	≥ 34
≥12	0	+	+	+	+
10,11	0	+	+	+	+
8,9	+	+			+
6,7	+	3	5	2	+
4,5	1	6	9	4	1
2,3	3	12	16	5	1
0,1	5	8	8	2	+
-2,-1	2	2	1	+	+
-4,-3	1	+	+	+	0
-6,-5	+	+	+	0	٥
<b>≦</b> -7	+	+	0	0	0

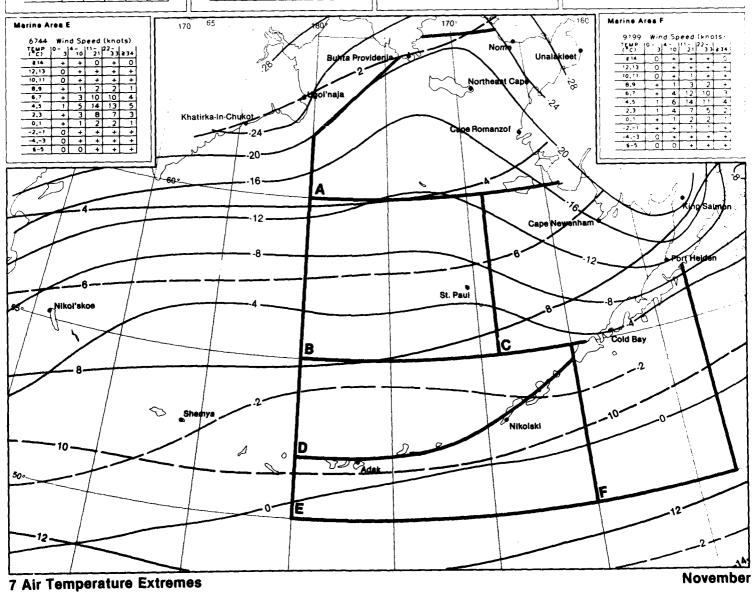
hemya					
18861	Wii	nd Sp	eed	(kno	ts)
TEMP	10-	4 -	11-	22-	
(°C)	3	10_	21	33	≥ 34
≥12	0	0	0	0	0
10,11	0	0	0	0	0
8,9	0	0	0	+	+
6.7	+	+	1	2	1
4,5	1	2	7	5	1
2.3	2	6	16	11	_ 3
0.1	2	6	14	7	1
-2,-1	1	2	4	2	+
-4,-3	1	1	1	+	+
-6,-5	+	+	+	+	+
≦-7	+	+	0	0	0

Marine Ar	Marine Area A							
1959	Wie	nd Sp	eed	(kno	ts)			
TEMP	0 -	4-	11-	22-	1			
(°C)	3	10	21	33	₹34			
<b>≥8</b>	0	+	+	+	0			
6.7	0	+	1	+	(+)			
4,5	0	1	4	2	+			
2,3	+	4	10	5	1			
0,1	1	7	13	10	1			
-2,-1	+	2	6	4	1			
-4,-3	+	1	4	3	1			
-6,-5	+	1	3	2				
-8,-7	+	1	2	1	+			
-10,-9	+	1	2	1	+			
<u>≤</u> -11	0	+	+	+	[ +]			

М	Marine Area B							
	2701	Wii	nd Sp	eed	(kno	ts)		
		0 -	4 -	11-	22-	1 (		
	(°C)_	3	10	21	33	≥ 34		
	≥ 10	0	+	+	+	0		
	8,9	0	+	+	+	+		
	6,7	+	+	1	1	+		
	4,5	+	3	6	_ 3	1		
	2,3	1	_5	12	_ 8	2		
	0,1	1	5	12	7	2		
	-2,-1	+	2	6	4	1		
	-4,-3	+	1	4	2	1		
	-6,-5	+	1	3	1	0		
	-8,-7	+	+	1	+	+		
	≦-9	0	+	+	0	+		

М	Marine Area C							
	4139	Wir	nd Sp	eed	(kno	ts)		
	TEMP (°C)	0 - 3	4 - 10	11 - 21	22 - 3 3	≩ 34		
	≥12	0	+	0	+	0		
	10,11	0	+	0	0	0		
	8.9	+	+	+	+	0		
	6,7	+	1	2	3	1		
	4,5	1	6	14	9	3		
	2,3	1	7	13	7	2		
	0,1	+	4	7	5	1		
	-21	+	1	3	_2	1		
	-4,-3	+	+	1	_1	+		
	-6,-5	0	+	1	+	+		
	<u>≤</u> -7	0	+	+	+	+		

Marine Area D						
7858	7858 Wind Speed (knots)					
	0 -	4-	11-	22-	1	
(°C)	3	10	21	33	≥34	
≥ 14	+	+	+	0	0	
12,13	+	+	+	+	+	
10,11	+	+	+	+	+	
8,9	+	1	T 1	1	+	
6.7	1	3	6	5	2	
4,5	1	7	15	11	4	
2,3	1	5	10	8	3	
0.1	+	2	4	4	1	
-2,-1	+	+	1	1	+	
-4,-3	+	+	+	+	+	
≦-5	0	+	+	+	+	



#### Nikoliekoa

Nikol'skoe	•				
5423	Wil	nd Sp	eed	(kno	ts)
TEMP	0-	4-	11-	22-	1
(°C)	3	10	21	33	≥34
≩6	0	0	0	0	0
4,5	0	+	+	+	+
2,3	+	1	3	2	1
0,1		4	6	3	1
-2,-1	2	6	10	5	3
-4,-3	2	6	9	4	2
-6,-5	2	5	7	3	1
-8,-7	2	_3	4	_	+
-109	+	1	+	+	+
-12,-11	+	+	+	+	0
≦-13	0	0	0	-0	_0

Kı	hatirka-ii	n-Chi	ıkot			
	3264	Wi	nd Sp	eed	(kno	ts)
	TEMP	0-	4-	11-	22-	1 1
	(°C)_	3	L_10	_ 21	33	≥34
	<u>₹</u> -6	4	5	6	3	1
	-8,-7	1	,	2	1	1
	-10,-9	1	1	1	1	+
	-12,-11	1	1	2	2	+
	-14,-13	+	1	3	3	1
	-16,-15	1	1	5	3	1
	-18,-17	1	2	5	4	2
	-20,-19	1	1	2	2	1
	-22,-21	1	2	3	1	+
				_		

U	gol'neja					
	5188	wi-	nd Sp	eed	(kno	ts)
	TEMP (°C)	0 - 3	4-	11 - 21	22 - 33	≥34
	≥-6	3	4	7	6	4
	-87	1	1	2	2	. 1
	-10,-9	+	1	1	1	1
	-12,-11	1	1	1	1	1
	-14,-13	1	1	1	2	2
	-16,-15	1	1	1	2	3
	-18,-17	2	1	1	2	3
	-20,-19	1	1	1	2	2
	-22,-21	1	1	1	2	3
	-24,-23	1	1	1	1	3
	<b>≨</b> −25	2	2	3	4	4

4438	Wi	nd Sp	eed	(kno	ts)
	0 -	4 -	11	22~	(
(°C)	3	10	21	33	≥ 34
≥-4	1	4	5	1	_ +
-6,-5	1	2	2	+	+
-8,-7	2	2	3	1	+
-10,-9	1	2	2	+	+
-12,-11	2	3	3	1	+
-14,-13	2	3	4	1	+
-16,-15	2	3	3	1	+
-18,~17	4	4	4	1	+
-20,-19	3	2	1	+	1
-22,-21	4	3	1	+	+
≦-23	10	3	1	+	0

Norheast (	Cepe				
9400	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	[11-	22-	
(°C)	3	10	21	33	≥34
≥-4	1	3	10	4	1
-6,-5	+	1	3	1	+
-8,-7	1	2	4	1	+
-10,-9	1	3	4	2	+
-1211	1	2	3	1	0
-14,-13	_1	_2	4	+	+
-16,-15	1	2	2	+	+
-18,-17	2	3	4	+	0
-20,-19	3	3	4	+	+
-2221	1	2	1	+	0
≨-23	6	_ 5	3	1	0

21808	Wii	nd Sp	eed	(kno	ts)
	0 ~	4 -	11-	22 -	1
(°C)	3	10	21	33	≥ 34
≧-6	1	6	11	3	+
-0,-7	1	3	4	1	+
-10,-9	1	3	2	1	+
~12,-11	1	2	2	+	+
-14,-13	2	4	3	+	+
-16,-15	1	3_	2	1	+
-18,-17	2	4	2	+	+
-20,-19	2	3	_ 2	+	+
-22,-21	_ 2	2	1	+	0
-24,-23	2	2	+	+	+
≨-25	10	6	1	+	0

Nome

Jnaieki						
1583	3	Wie	nd Sp	eed	(kno	ts)
TEMP	, 1	0 -	4 -	11-	22-	
(°C)		3	10	21	33	≥34
≥-8		1	_ 5	12	5	+
-10,-	•	1	2	4	2	+
-12,-	11	+	2	3	1	+
-14,-	13	1	3	3	5	+
-16,-	15	1	2	2	1	+
-18,-	17	1	2	2	1	+
~20	19	1	3	2	1	+
-22,-	21	1	2	2	1	+
~24,-	23	1	3	2	. 1	+
-26,-	25	1	2	1	+	+
≦-27		5	14	2	+	+

Cape Rom	Bnzof				
16634	Wij	nd Sp	eed	(kno	15)
TEMP (°C)	0-	4-		22-	
	3	10	21		≥ 34
≥-2	1	3	8	3	+
-4,-3	2	3	4	. 2	+
-6,-5	1	2	2	_ 1	_ +
-8,-7	2	2	_3	1	+
-10,-9	2	2	3	2	+
-12,-11	2	1	2	2	+
-14,-13	2	2	3	2	1
-16,-15	2	1	_2	2	•
-18,-17	1	1	3	. 2	
-20,-19	1	1	2	-	· ·
§-21	1	2	4	3	

Cape New	nnai	n			
19087	Win	nd Sp	eed	(kng	ts)
TEMP	0 -	4	111-	122-	( )
( o C )	3	10	21	3.3	≥ 34
₹2	+	2	_ 5	3	+
0,1		4	7	2	+
-21	2	3	4	1	+
-4,-3	3	4	3	1	+
-6,-5	2	2	2	1	+
-8,-7	3	2	2	1	+
10,-9	. 3	2	2	1	±
-12,-11	_2	1	1	+	+
-14,-13	2	2	2	+	+
-16,-15	2	2	1	+	+
<b>≤</b> -17	. 5	4	6	1	0

King Salmo	o n				
18840	Wi	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	111-	22 -	i I
(°C)	3	10	21	33	≩ 34
2-2	2	13	13	3	+
-4,-3	1	4	2	+	0
-6,-5	1	3	1	+	0
-8,-7	1	4	1	+	+
-10,-9	1	3	1	+	0
-12,-11	1	2	1	+	0
-14,-13	1	3	1	+	0
-16,-15	1	2	7	+	0
-18,-17	1	2	1	+	0
-20,-19	2	3	2	+	0
≦-21	7	9	5	+	+

5839	Wi	nd Sp	eed	(kno	ts)
TEMP	10 -	4 -	11-	22 -	į
(°C)	3	10	21	3.3	≥ 34
≩4	+	1	3	2	+
2,3	+	3	8	3	+
0,1	1	7	8	2	+
-2,-1	1	6	5	1	_ +
-4,-3	1	5	4	1	+
-6,-5	1	3	2	+	+
-8,~7	+	2	1	+	0
-10,-9	1	2	1	+	0
-12,~11	+	2	2	+	0
-14,~13	+	3	3	+	0
<u>≤</u> – 15	+	4	8	1	0

14359	Wil	nd Sp	eed	(uno	S
TEMP	10 -	4 -		22	1
(°C)	3	10	21	33	≥ 34
.₹8	0	0	+	+	
6,7	+	+		1	-
4,5	+	1	2	3	+
2,3	+	4	9	5.	
0,1	T	10	12	4	
-2,-1	1	5	6		
-4,-3	1	5	6	2	Ü
-6,-5	+	3	3	•	
-87	1	2	3	,	+
-10,-9	+	7	1		•
≦-11	+		+	,	-

Ni	Nikolski							
	2182 Wind Speed (knots)							
	TEMP (°C)	0 - 3	4-10	11-	22-	≥34		
-	≩ 10	0	0	0	0	0		
,	8.9	0	0	0	0	0		
	6,7	0	+	+	+	0		
	4,5	1		2	2	+		
	2,3	1	4	6	3	+		
-	0.1	4	13	18	8	1		
	-2,-1	3	6	8	4	1		
_	-4,-3	1	2	5	М	+		
	-6,-5	0	1	1	1	+		
	~B,-7	0	+	+	+	0		
	<b>≨</b> -9	0	0	0	0	0		

St. Pa	ul					
1.1	11798 Wind Speed (knots)					
	MP C)	0-,	10	11- 21	22-	≩ 34
	<u>≥</u> 8	0	Ö	0	0	0
6	.7	0	0	+	+	0
4	,5	0	+	1	1	+
2	, 3	+	2	10	5	1
	,1	1	6	13	6	1
-2	1	+	2	6	3	1
-4	3	1	4	7	4	1
-6	,-5	1	2	5	2	1
-8	,-7	1	2	4	2	+
~10	,-9	+	1	1	1	+
<u>\$</u> .	- 1 1	+	+	1	2	+

22273	Wis	nd Sp	eed	(kno	ts)
TEMP	0 -	4 -	11-	22-	l
(°C)	3	10	21	33	≩34
≥ 10	0	+	+	+	_ +
8,9	0	+	+	+	+
6,7	+	1	1	1	+
4,5	1	3	4	2	1
2,3	3	9	12	4	1
0,1	5	11	13	5	1
-2,-1	3	4	4	2	+
-4,-3	3	1	1	+	+
-6,-5	1	+	+	+	0
-8,-7	1	+	+	0	0
≨-9	+	+	0	0	0

19053	W.	nd Sa	eed	(kno	(2)
TEMP	10 -	4 -	11-	22 -	
(°C)	3	10	21	33	≥ 34
<b>≥</b> 10	0	0	С	0	0
8.9	0	0	0	0	0
6,7	+	+	+	+	+
4,5	+	+	1	1	
2,3	2	2	10		2
0.1	3	7	17	1.1	3
-2,-1	2	6	_ 9	4	
-4,-3	1	3	4	2	+
-6,-5	+	1	1	+	+
-87	+	+	+	+	0
<b>≨</b> −9	+	+	+	0	0

December

Marine Area A	Marine Area B	Marine Area C	Marine Area D
2465 Wind Speed (knots)  TEMP 0-3 4-0 11- 22- 33 ₹34  ₹4 0 + + 1 + 1  2.3 + + 2 2 2 + + 1  0.1 1 4 10 7 1  -21 + 2 3 2 1  -43 + 2 3 2 + - 65 + 2 4 3 1  -10,-9 + 1 3 3 1  -12,-11 + 1 3 4 2  -14,-13 + 1 3 3 2   €-15 + 1 3 3 2	3321 Wind Speed (knots)  TEMP   0-   1-   11-   22-   23   234    28	4161 Wind Speed (knots)  TEMP 0-   4-   11-   22-   (°C)	7381 Wind Speed (knots)  75MP 0- 4- 111- 122- (°C) 3 10 21 33 234  2 12 + + + + + +  10,11 + + + + + +  8,9 + + + + + +  6,7 + 11 2 2 1  4,5 1 4 10 9 4  2,3 1 6 13 10 4  0,1 1 4 7 6 2  -2,-1 + 1 3 2 1  -4,-3 + 1 1 + +  5-7 0 + + + +  0
Marine Area E 170	0 54 180	170	Marino Area F
5-2 Nikol'skos A	Buhta Provi	Cape Romanizof  St. Paul  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape  Cape	1846et  79.79 Wind Speed Linois.  1860 - 3 - 9 - 12 - 23 3 2 3 4 3 4 3 4 5 4 5 6 5 6 4 4 11 4 4 5 5 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7

7 Air Temperature Extremes

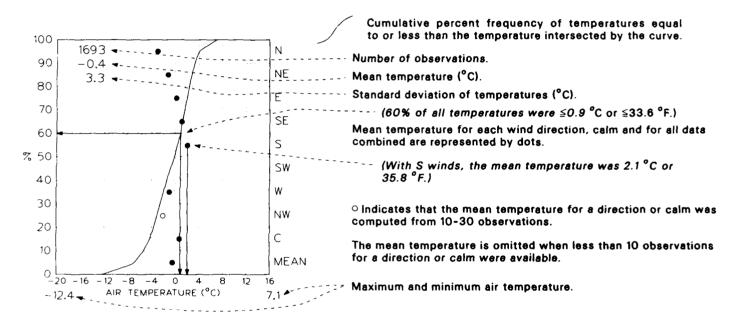
## Map 8. Air temperature mean and frequency ≤0°C

BLACK LINE - Mean air temperature (°C).

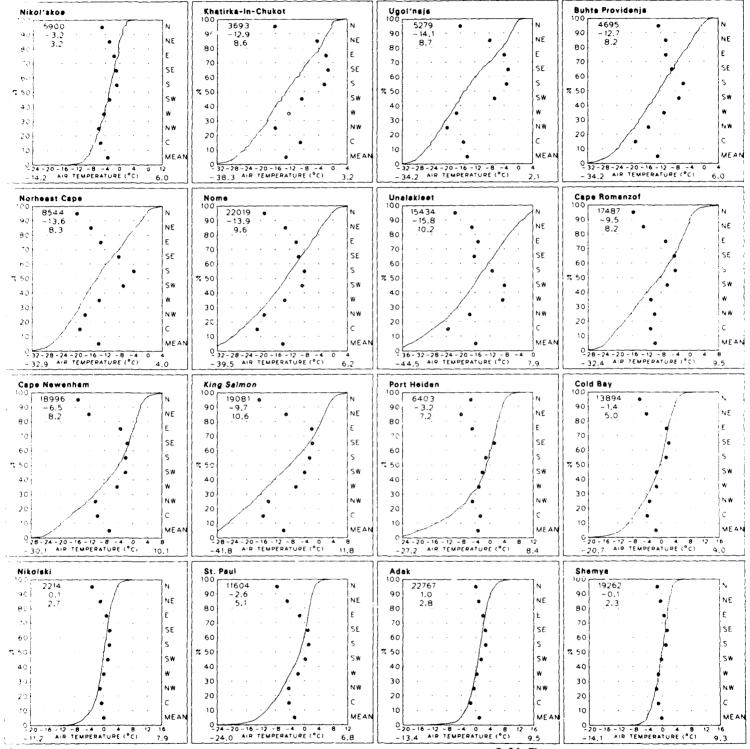
BLUE LINE - Percent frequency of temperature ≤0°C (≤32°F).

Albers Equal—Area Conic Projection

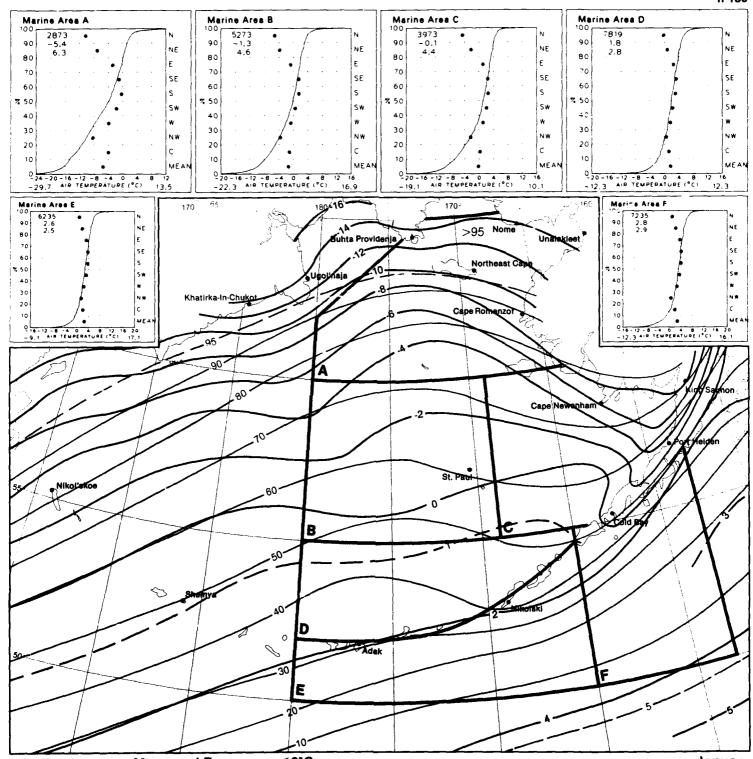
### Graphs: Air temperature/wind direction



The temperature scale of the graphs varies in both range and class interval. The percent frequency of temperature observations greater than a given value can be obtained by subtracting the cumulative percent frequency of that value from 100%. The number of observations and the standard deviation, plus the plotted points on the graphs, are based on those observations reporting both temperature and wind direction. The cumulative curve is based on all observations reporting temperature with or without wind direction.

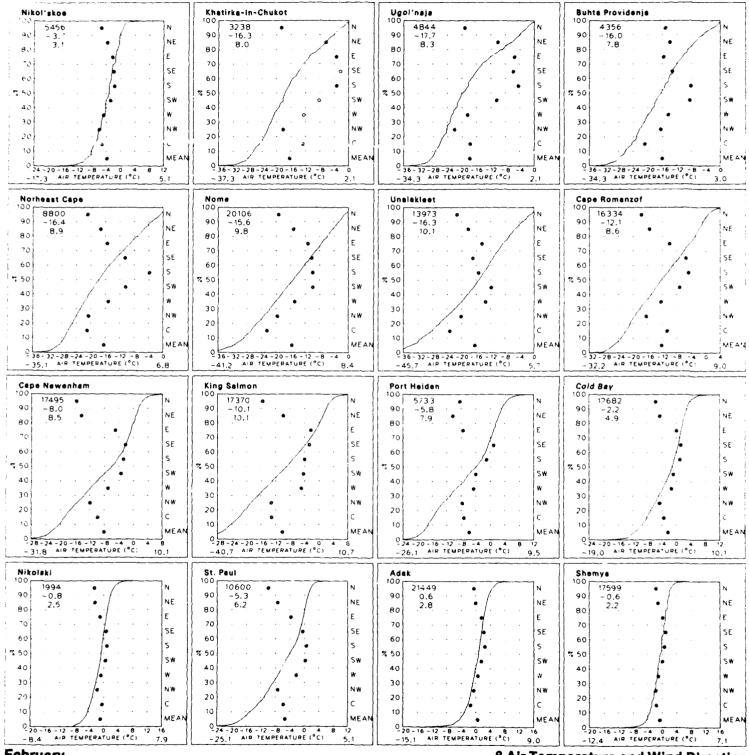


January 8 Air Temperature and Wind Direction



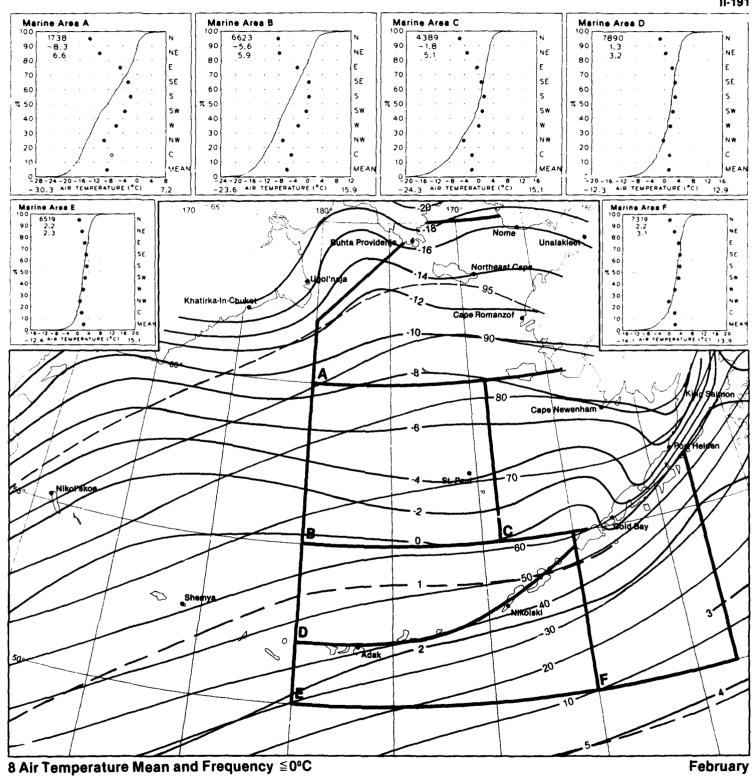
8 Air Temperature Mean and Frequency ≤0°C

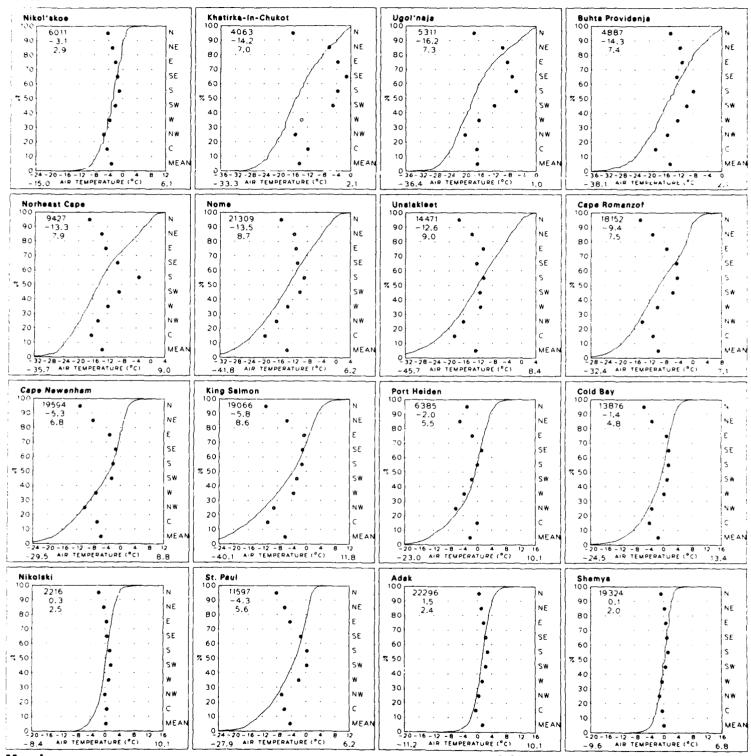
January



**February** 

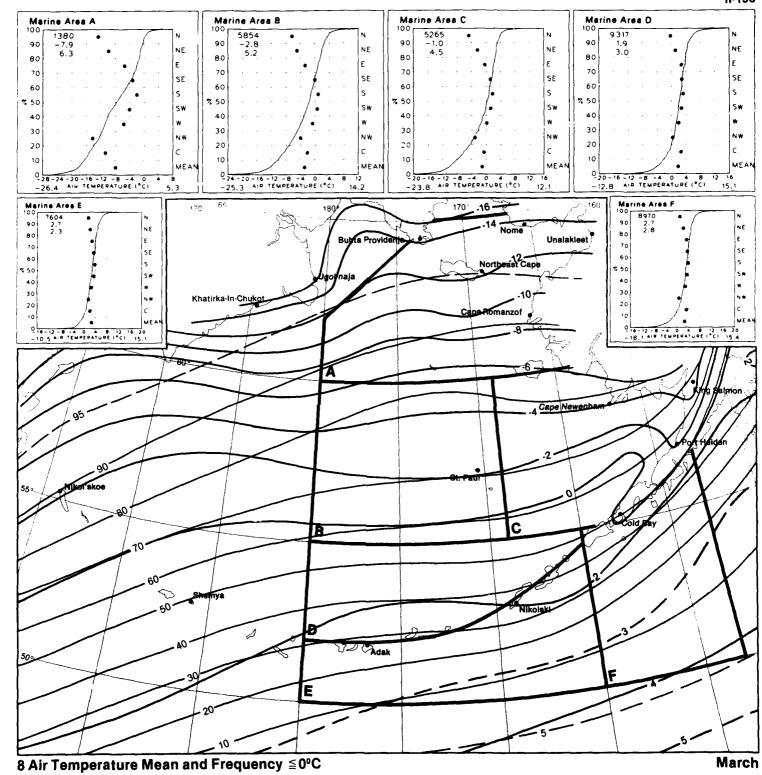
8 Air Temperature and Wind Direction

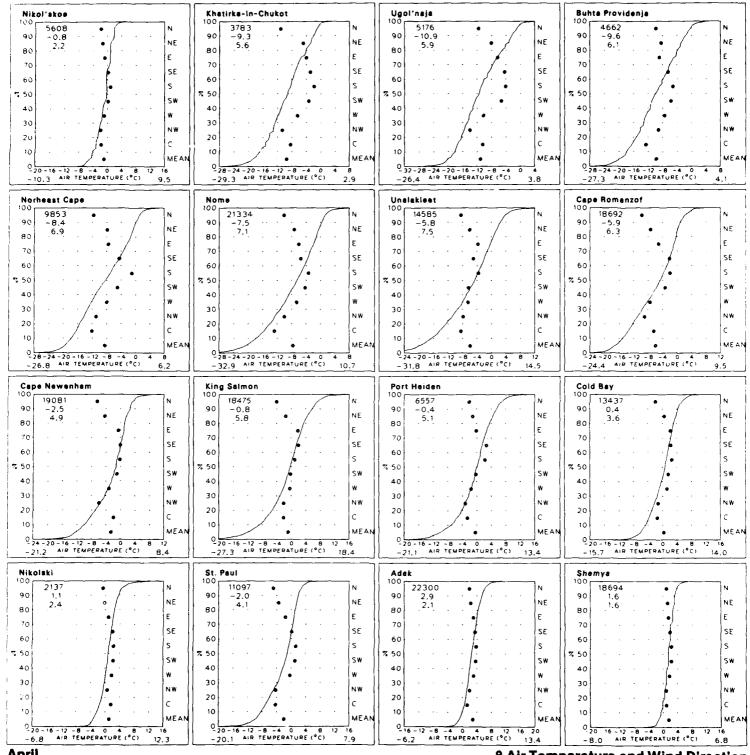




March

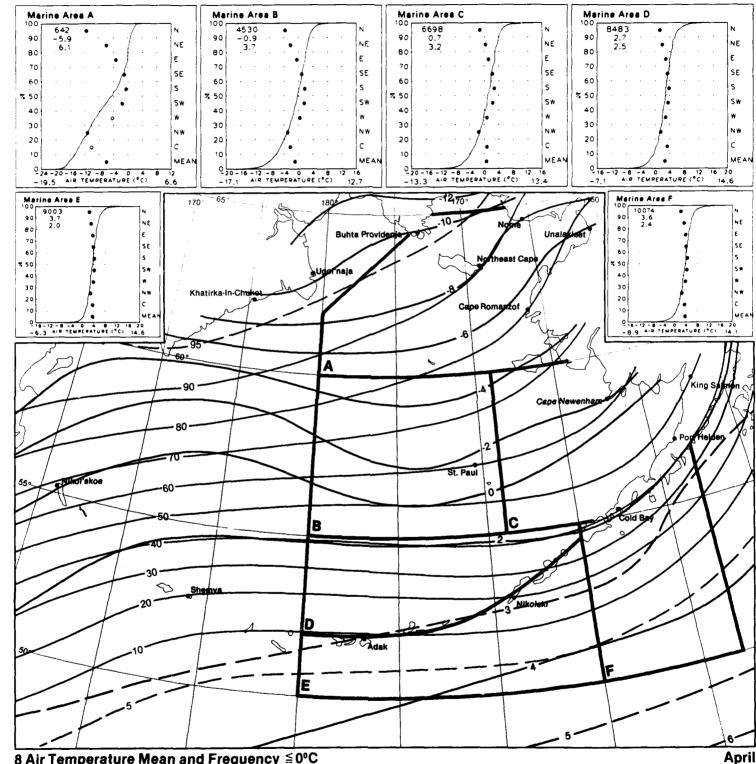
8 Air Temperature and Wind Direction



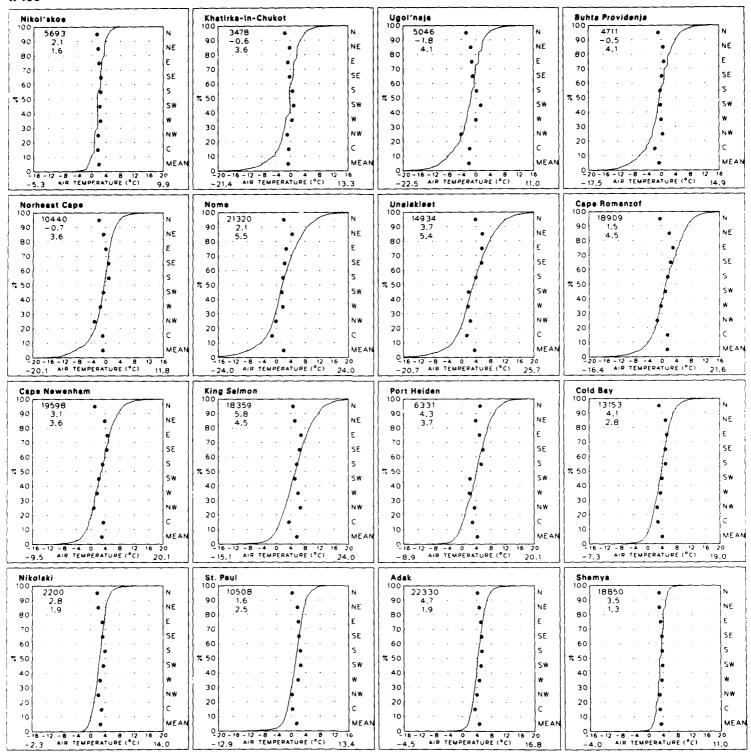


**April** 

8 Air Temperature and Wind Direction

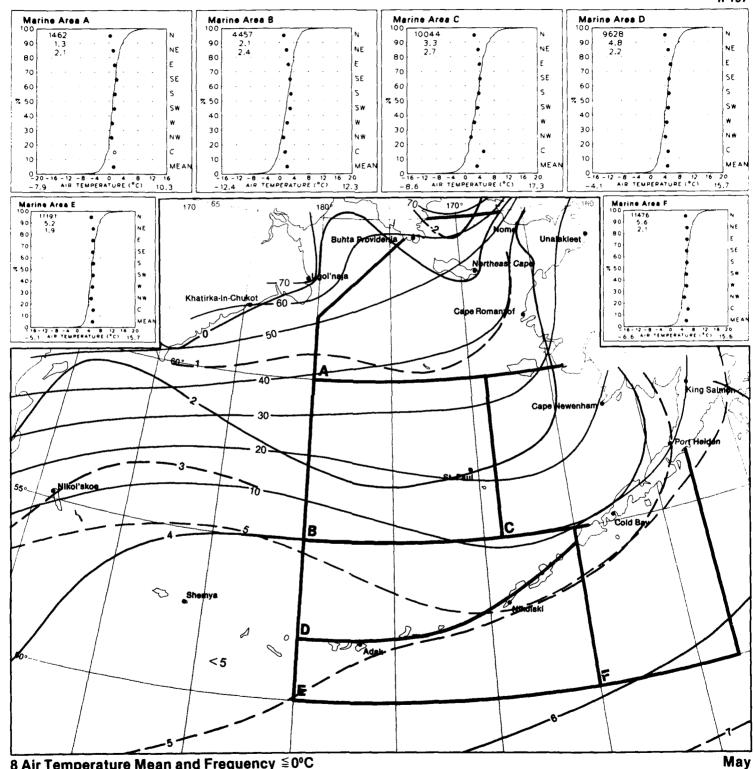


8 Air Temperature Mean and Frequency ≤ 0°C

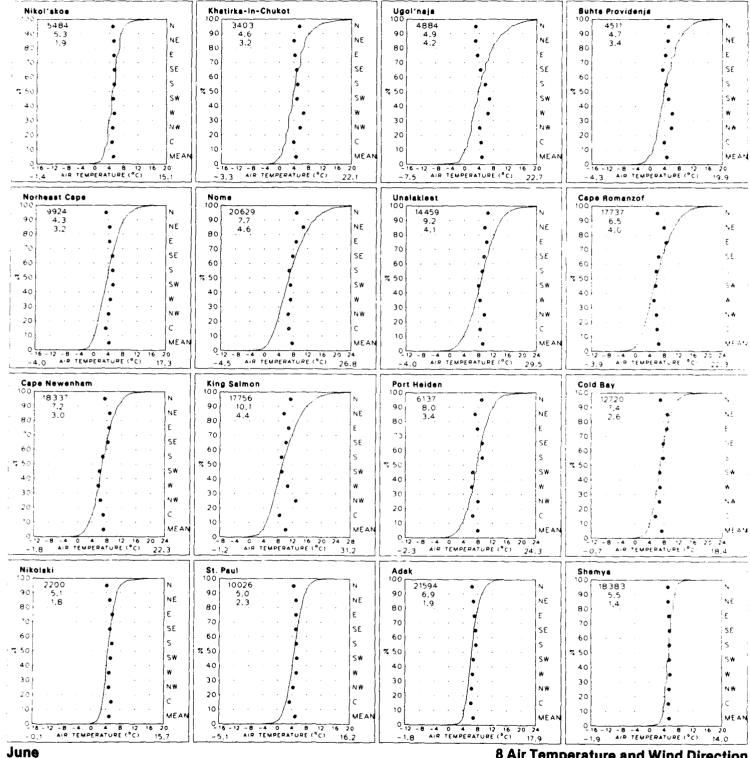


May

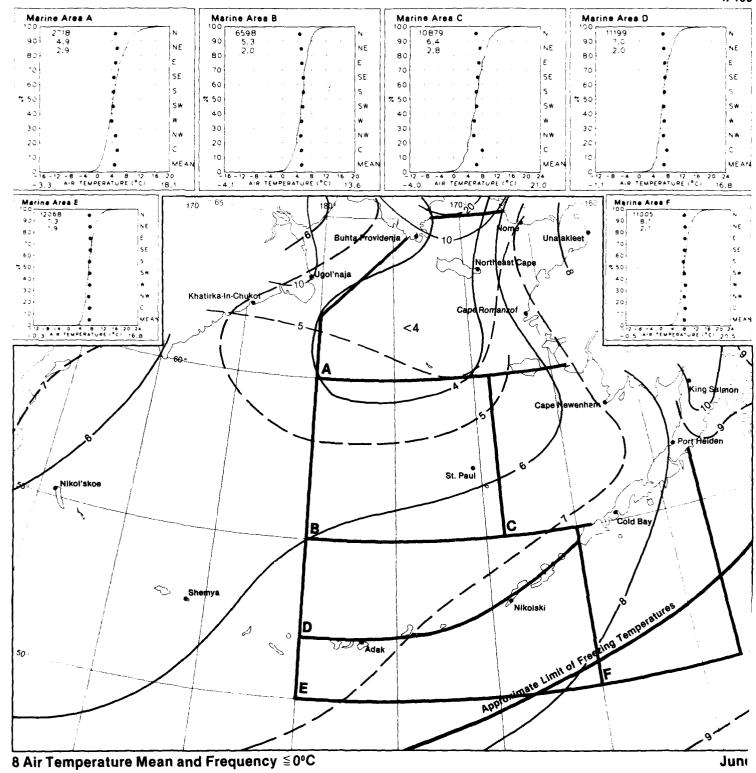
8 Air Temperature and Wind Direction

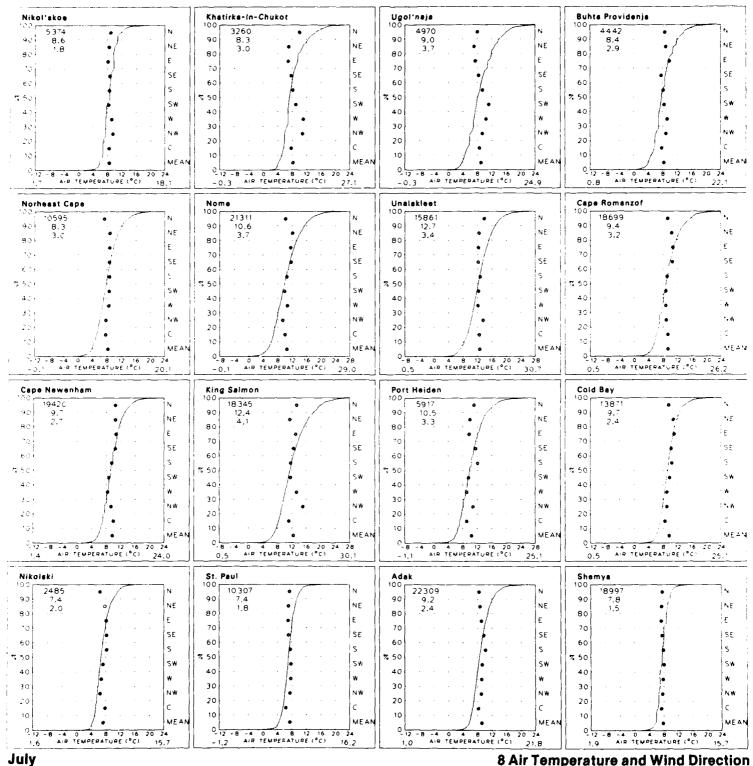


8 Air Temperature Mean and Frequency ≦0°C

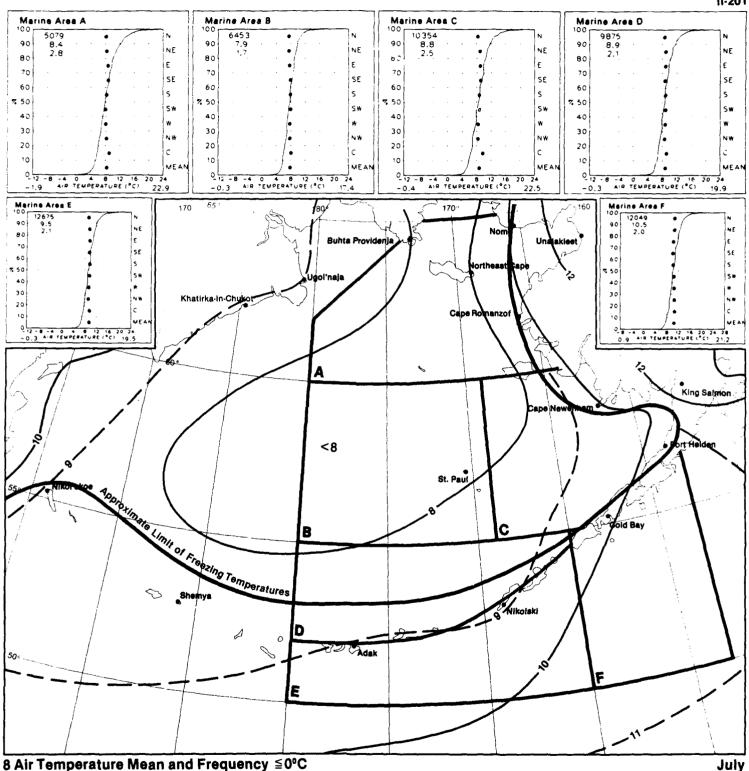


8 Air Temperature and Wind Direction

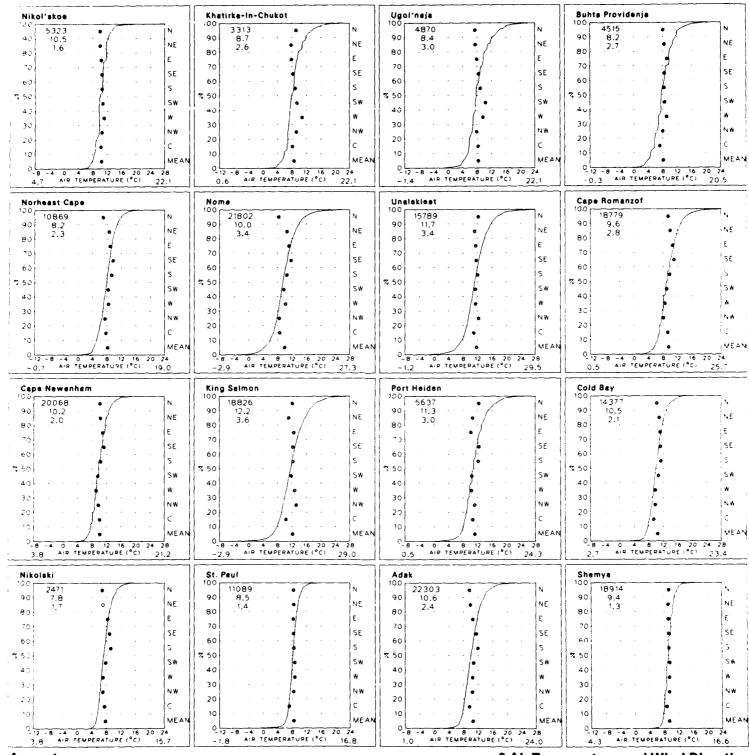




8 Air Temperature and Wind Direction

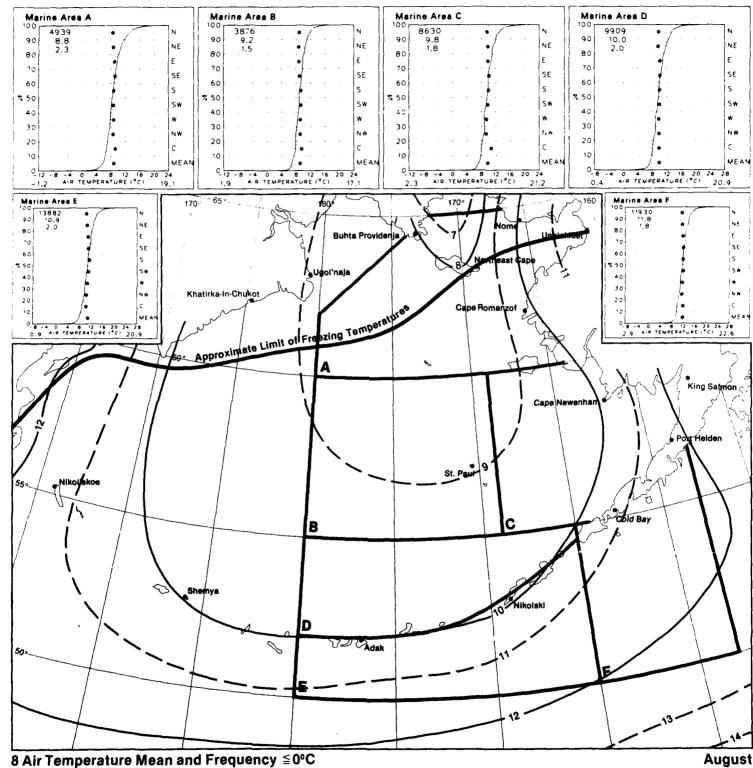


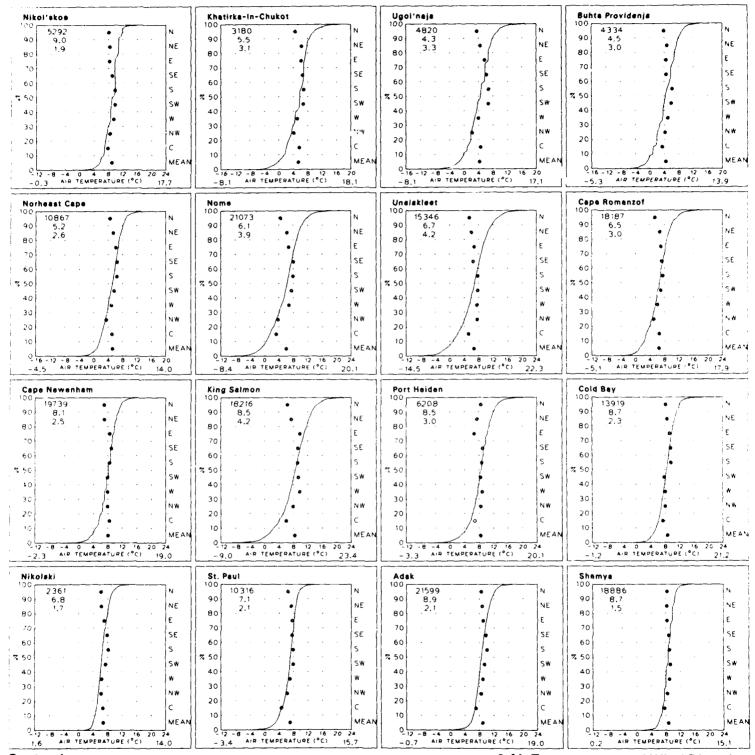
8 Air Temperature Mean and Frequency ≤0°C



August

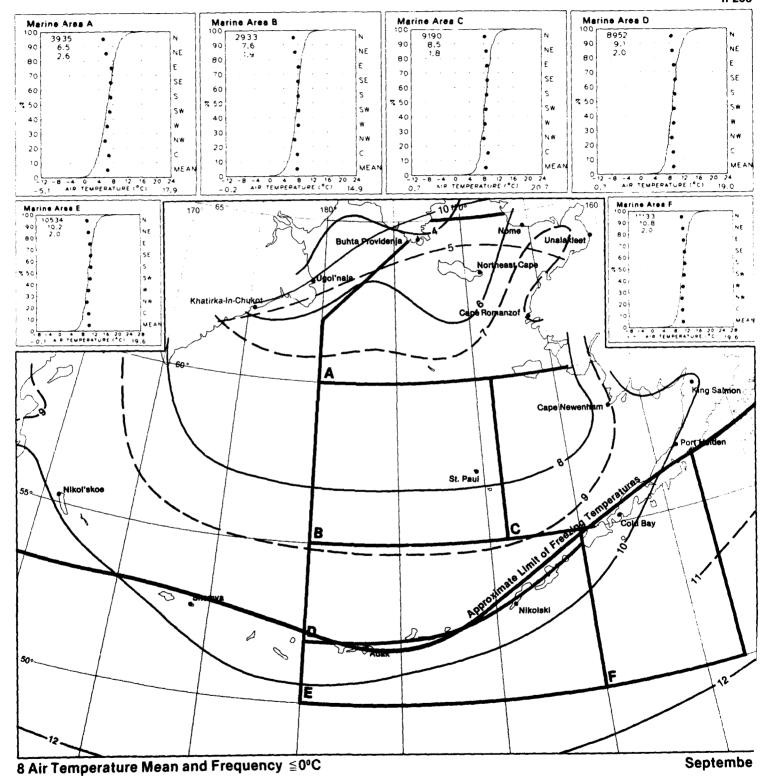
8 Air Temperature and Wind Direction

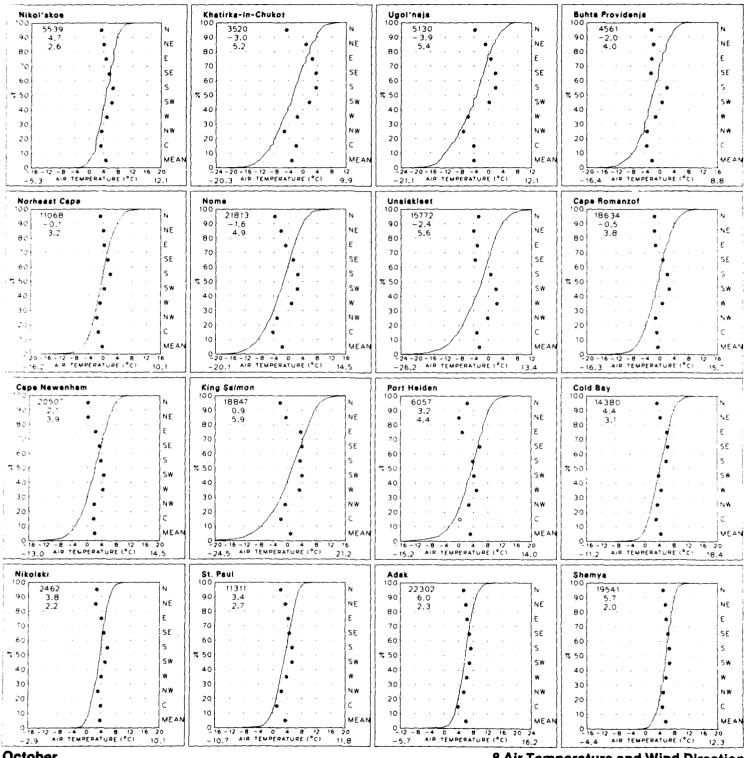




September

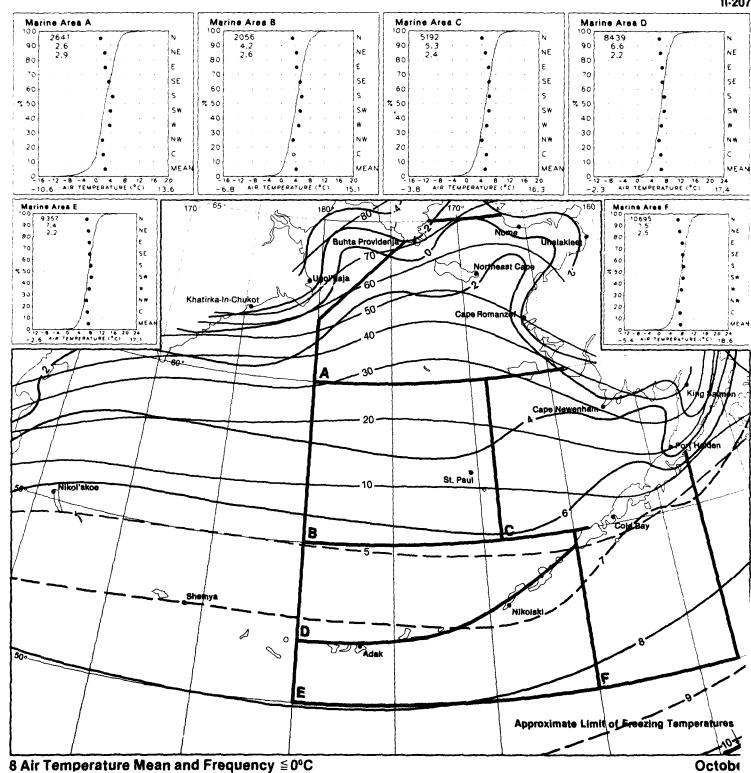
8 Air Temperature and Wind Direction

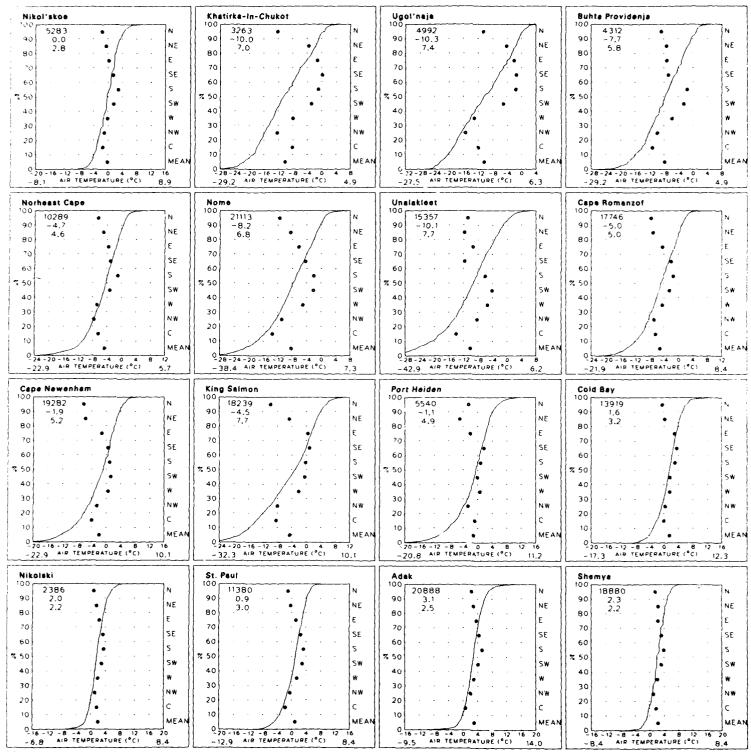




October

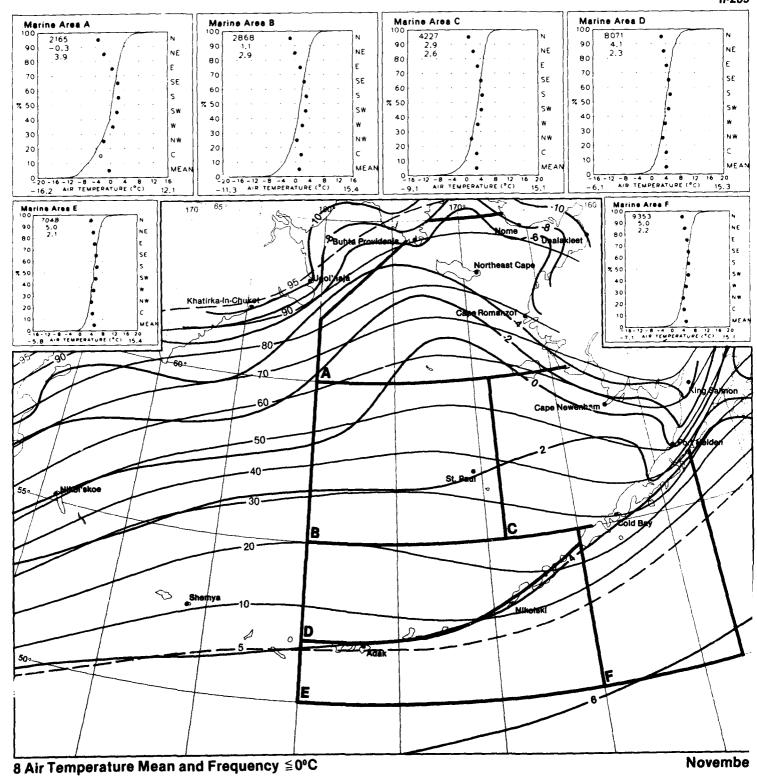
8 Air Temperature and Wind Direction

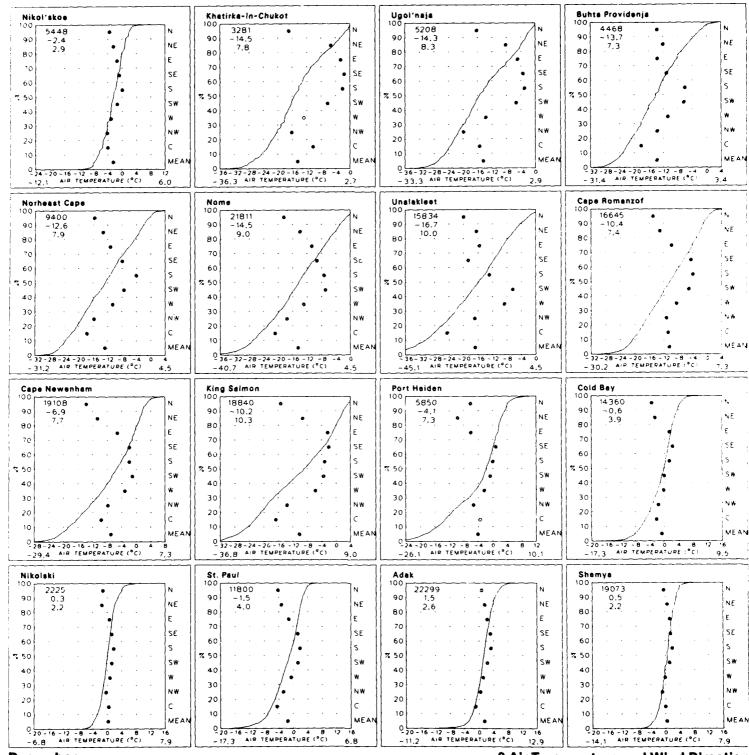




November

8 Air Temperature and Wind Direction





December

8 Air Temperature and Wind Direction

Legend

# Map 9. Dew point temperature extremes (°C)

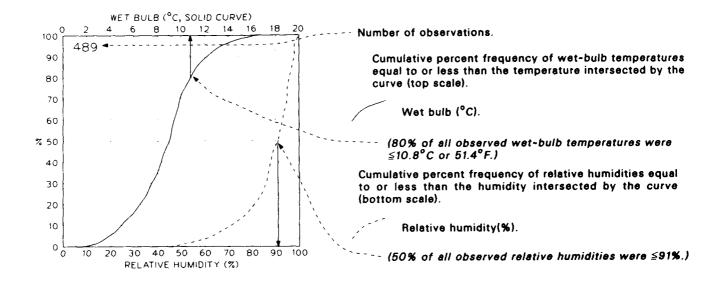
BLACK LINE - Maximum (99%) dew point temperature (1% of temperatures were greater than the given value).

BLUE LINE - Minimum (1%) dew point temperature (1% of temperatures were equal to or less than the given value).

Albers Equal—Area Conic Projection

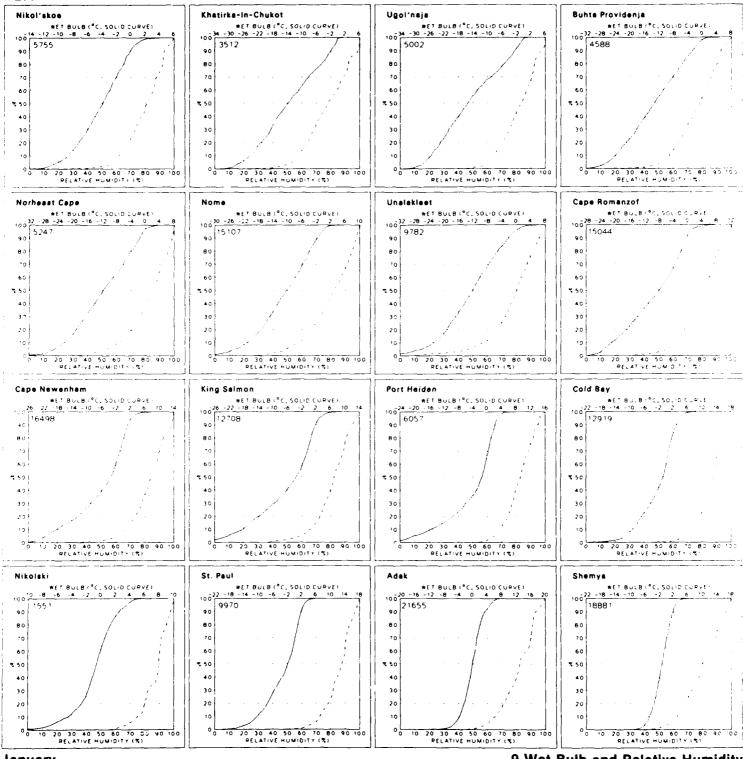
9 Legend

### Graphs: Wet bulb/relative humidity



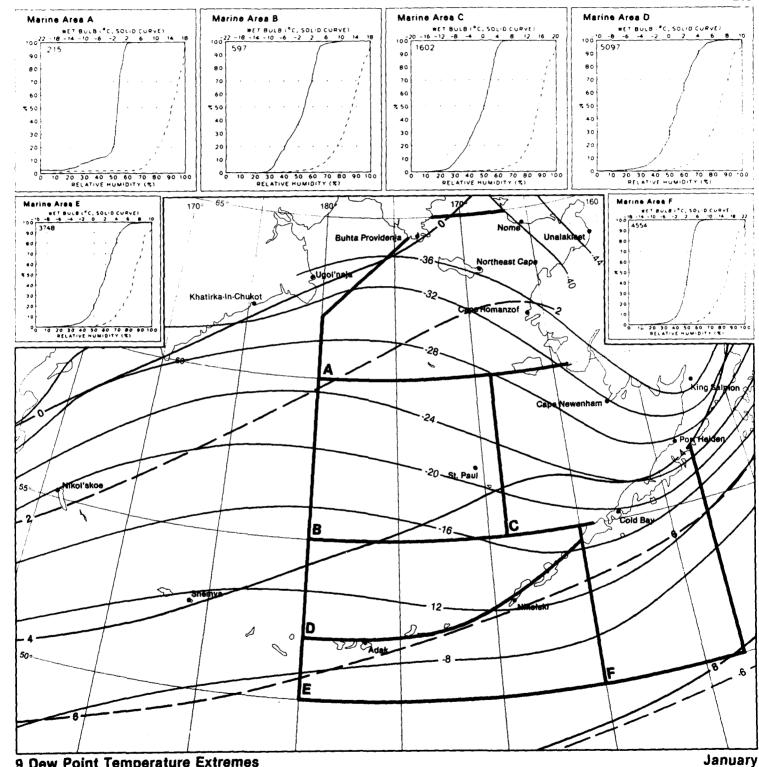
The observation count for the graph reflects those observations containing both dry and wet bulb temperatures; both are r quired in computing the relative humidity. The percentage of observations of either element greater than a given value can b

obtained from the graph by subtracting the cumulative percent frequency of that value from 100%.

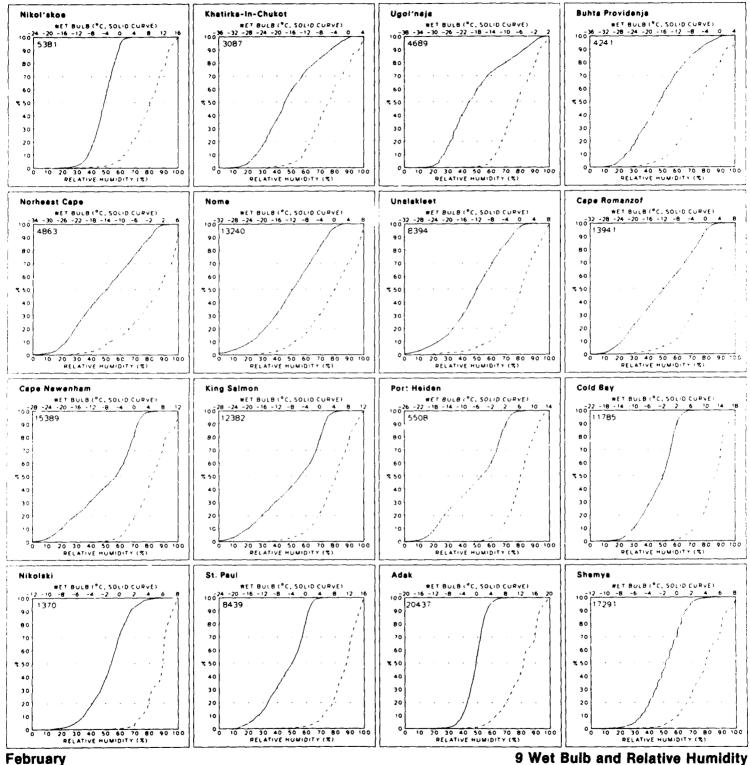


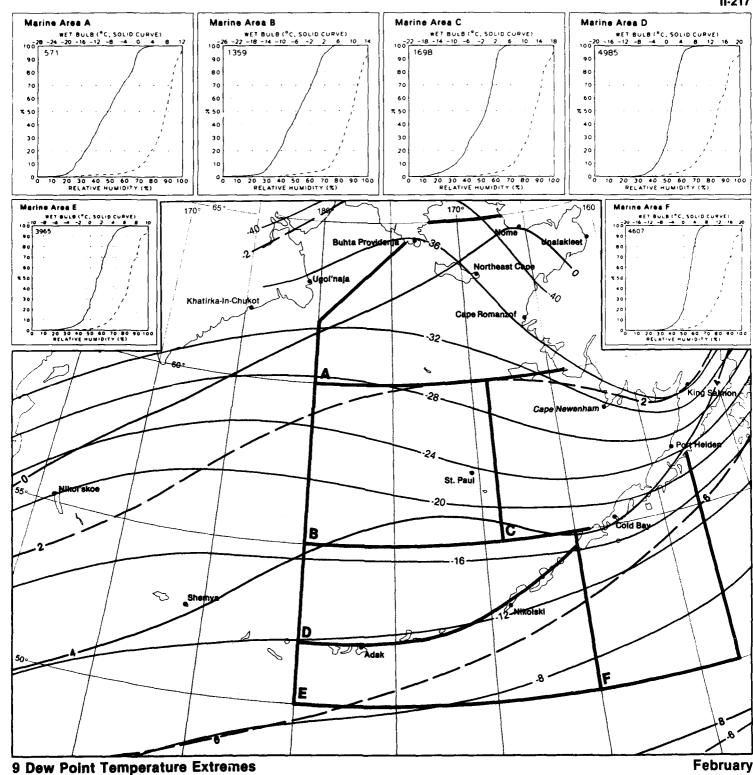
January

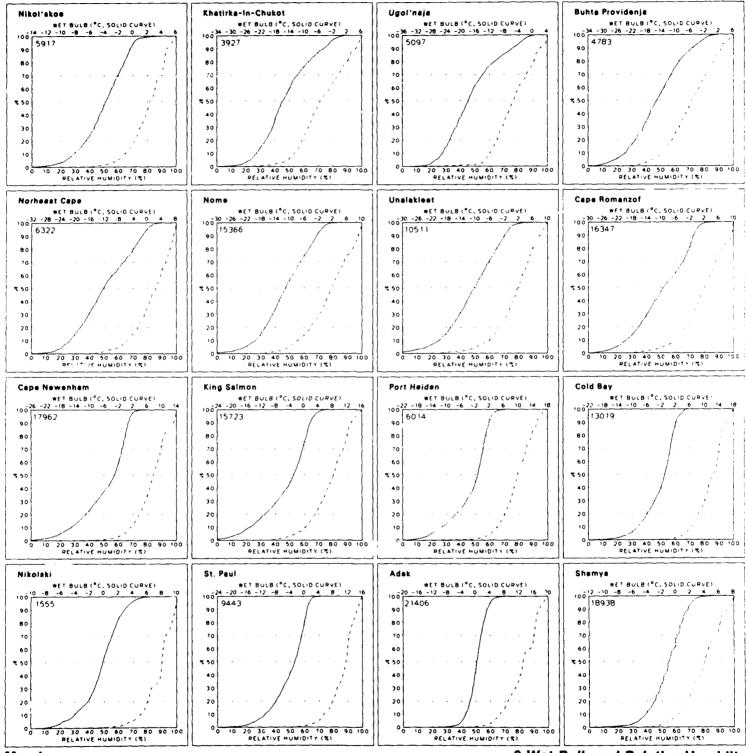
9 Wet Bulb and Relative Humidity



9 Dew Point Temperature Extremes

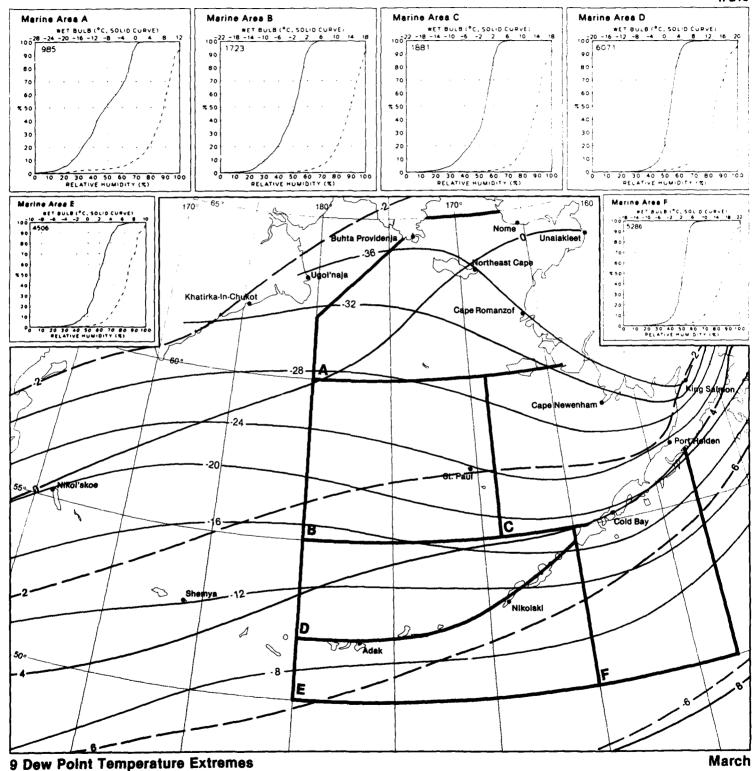


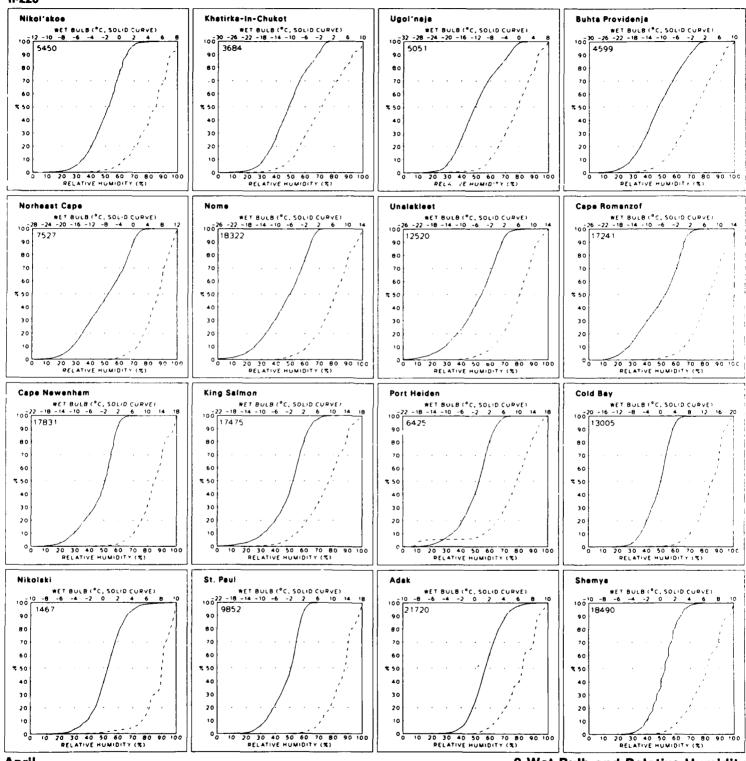




March

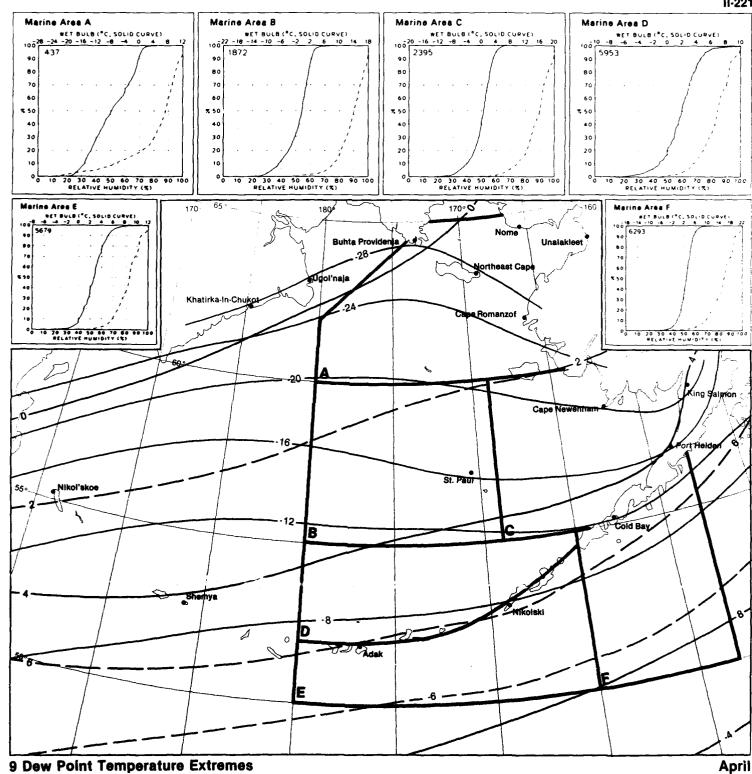
9 Wet Bulb and Relative Humidity



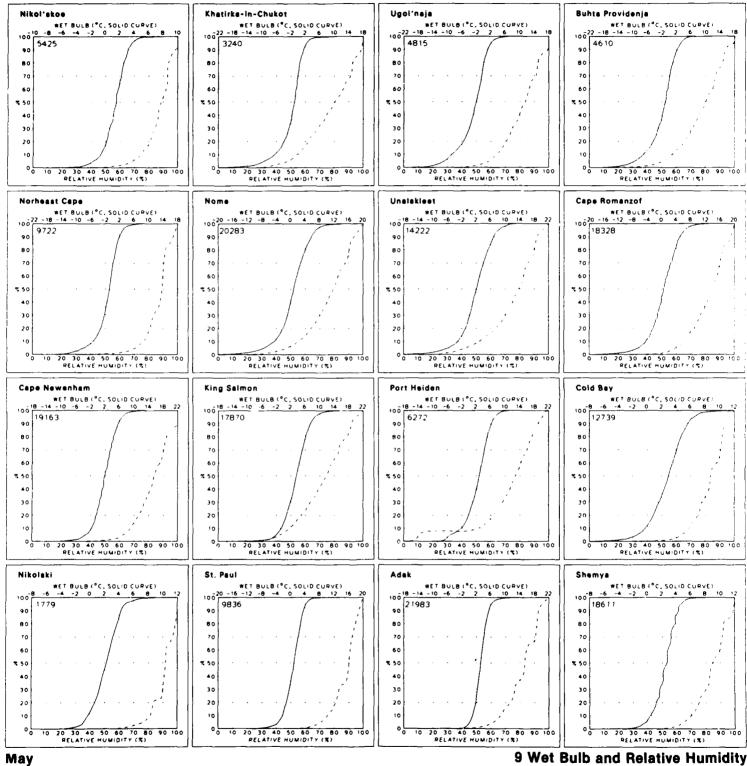


April

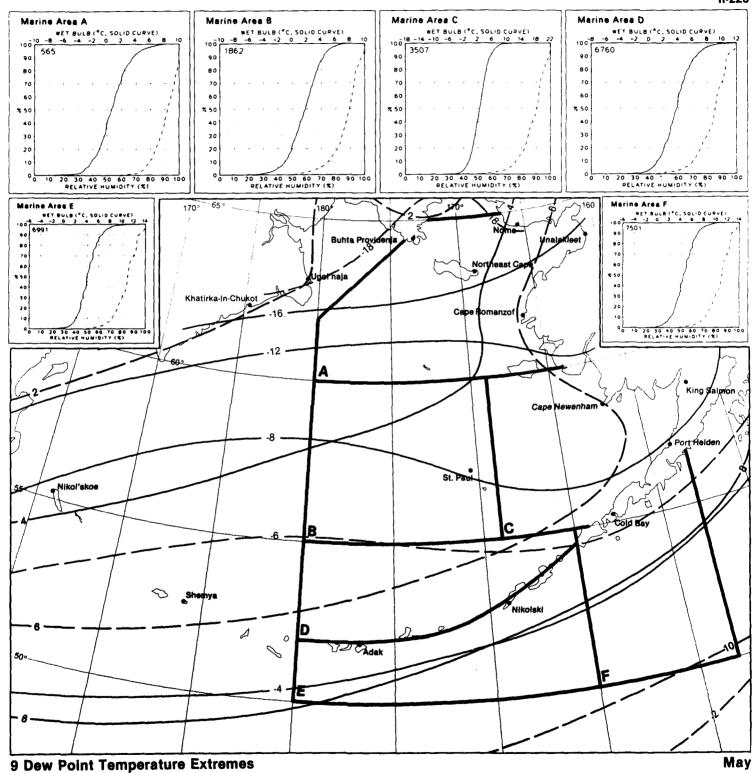
9 Wet Bulb and Relative Humidity

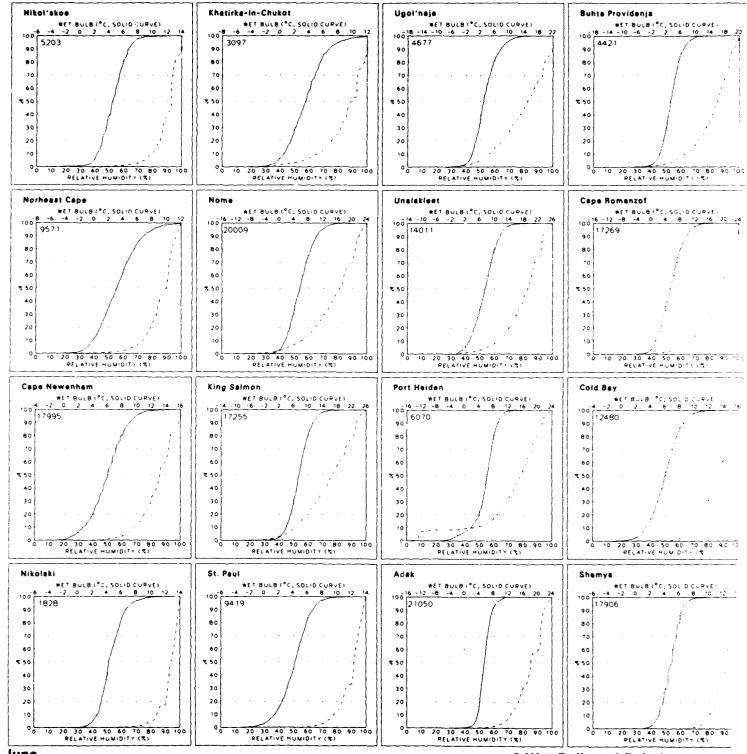


9 Dew Point Temperature Extremes



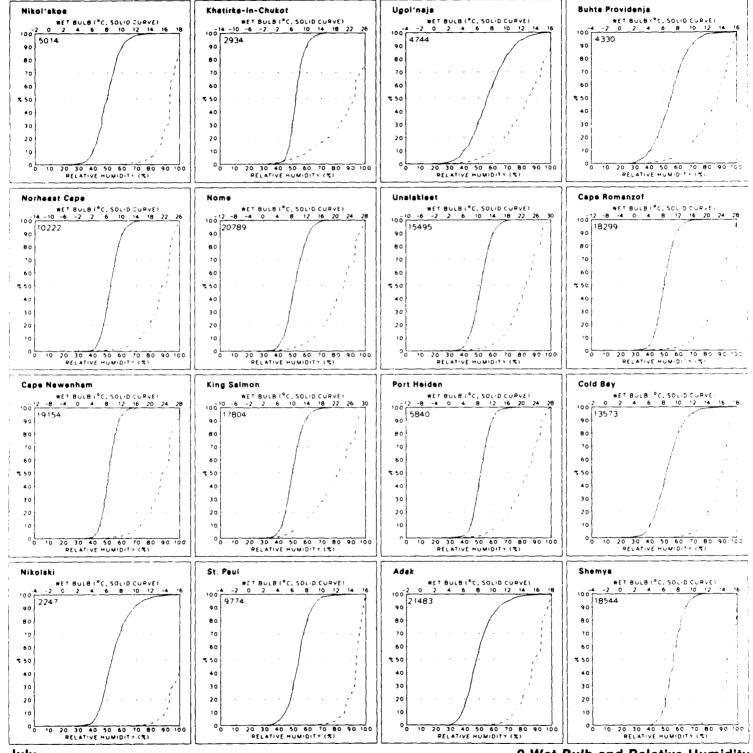
9 Wet Bulb and Relative Humidity





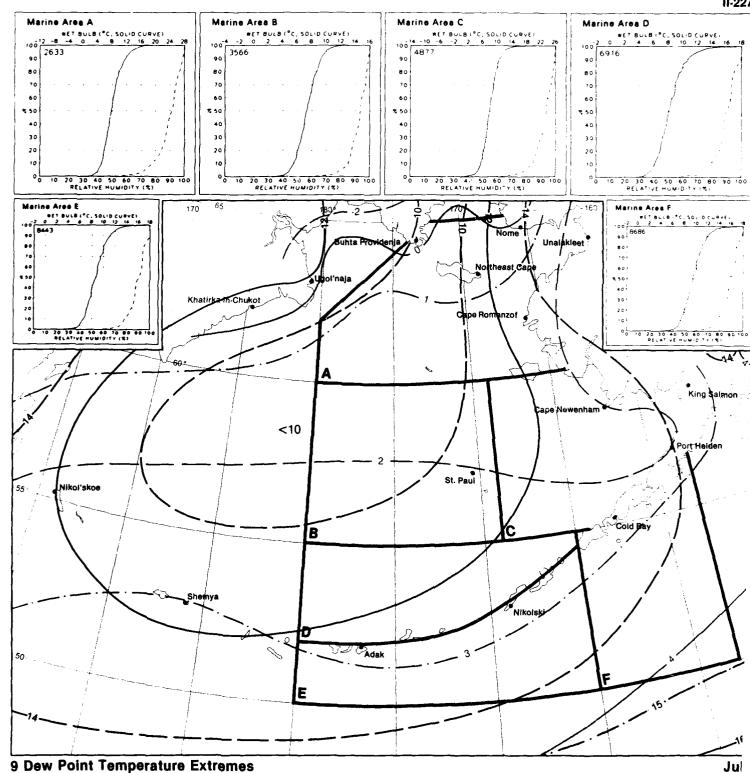
June

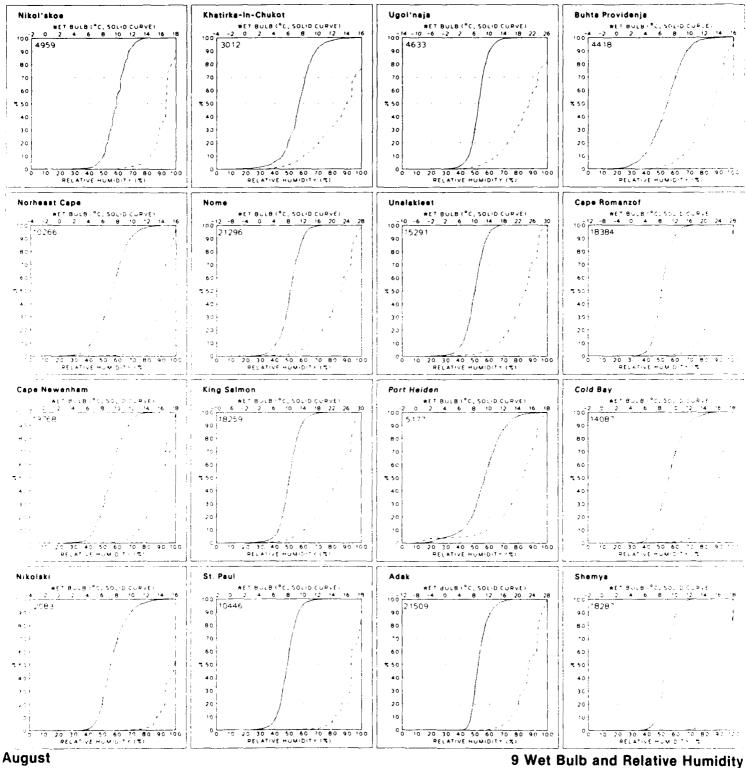
9 Wet Bulb and Relative Humid

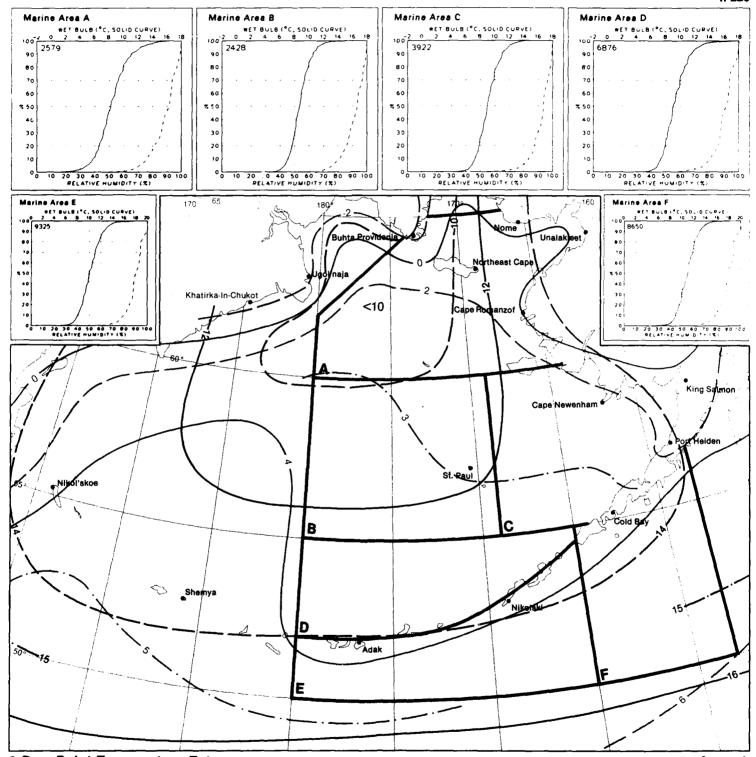


July

9 Wet Bulb and Relative Humidity

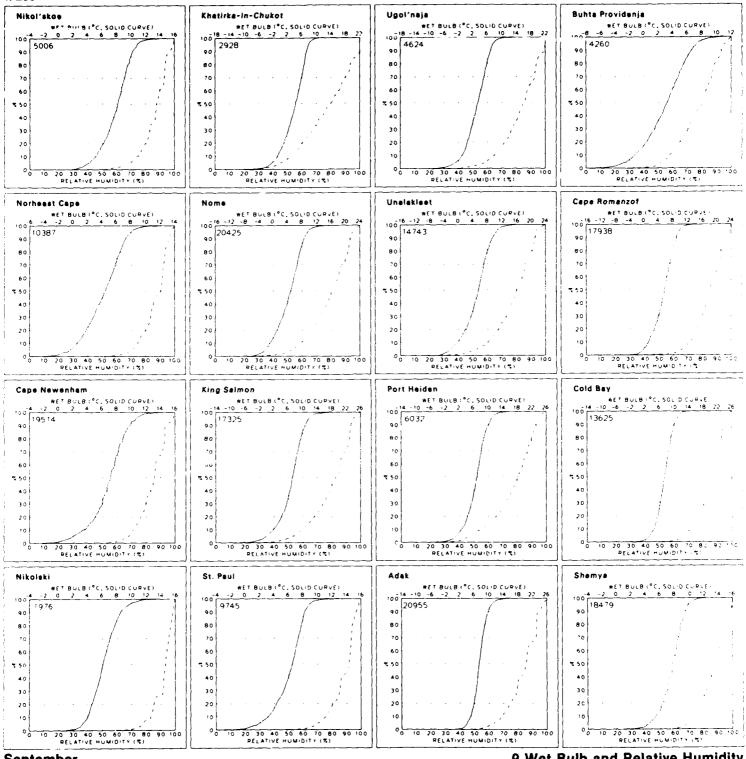






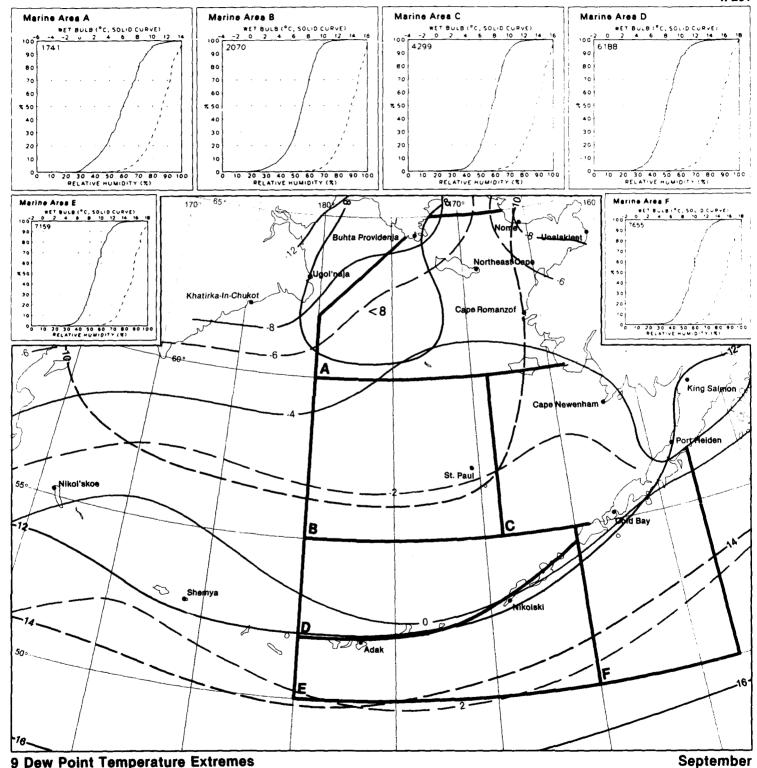
9 Dew Point Temperature Extremes

August

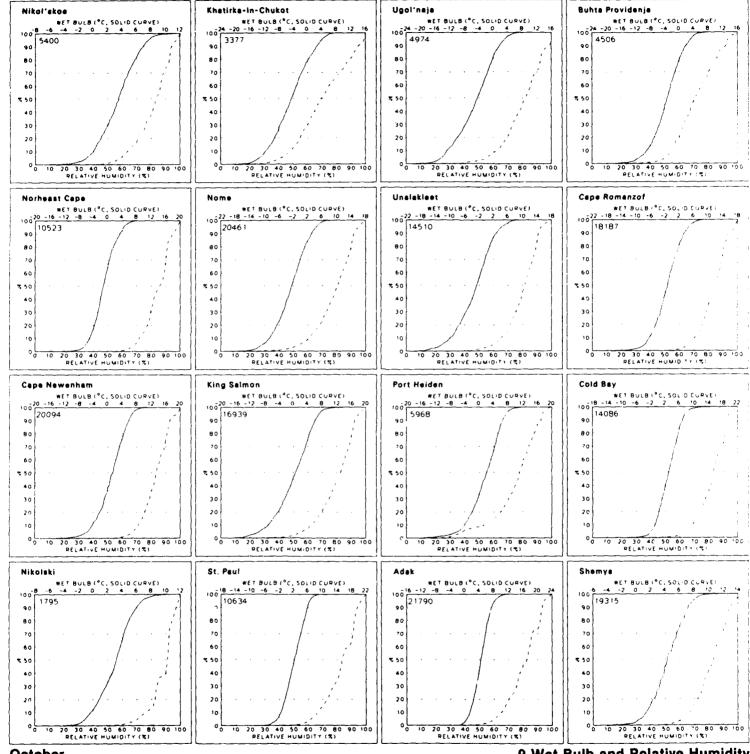


September

9 Wet Bulb and Relative Humidity

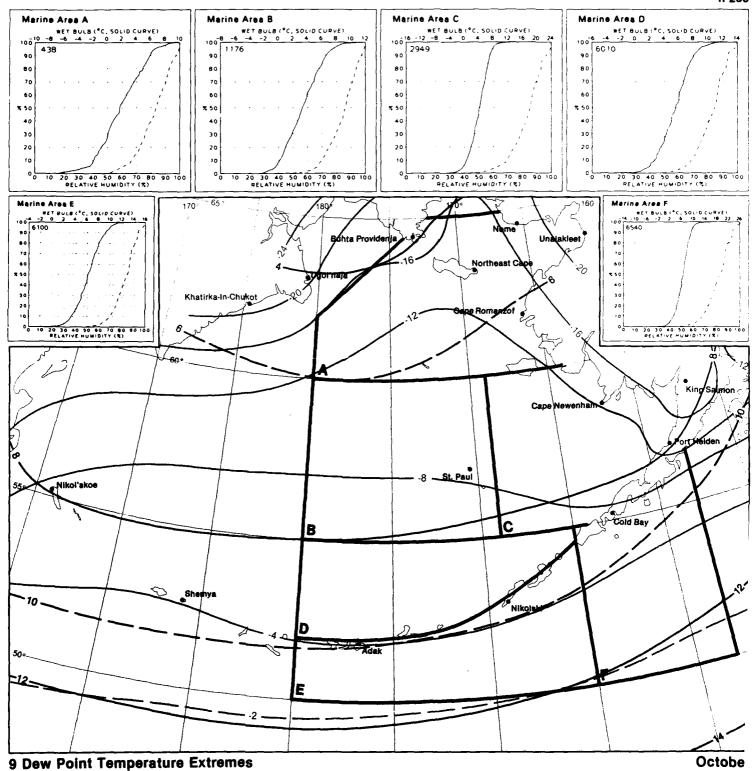


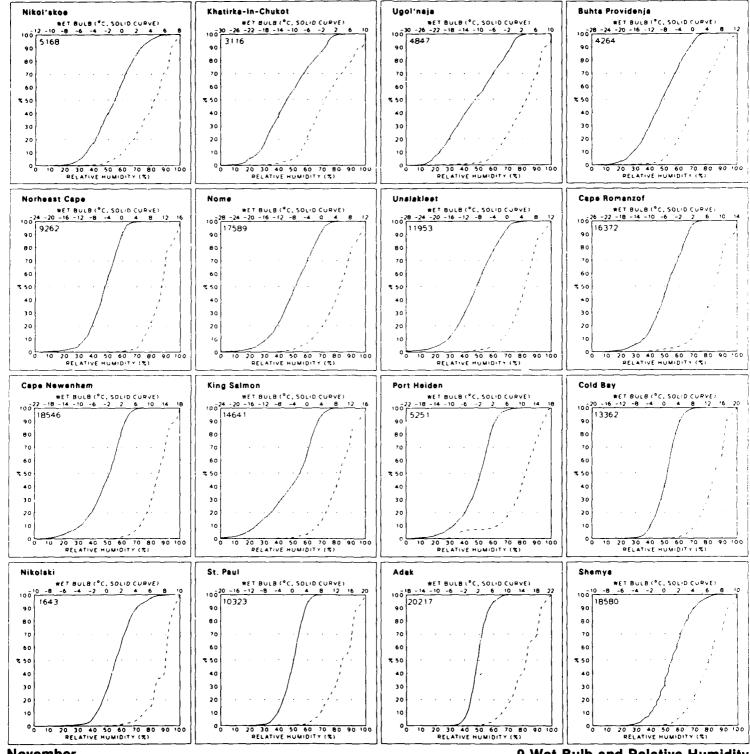
9 Dew Point Temperature Extremes



October

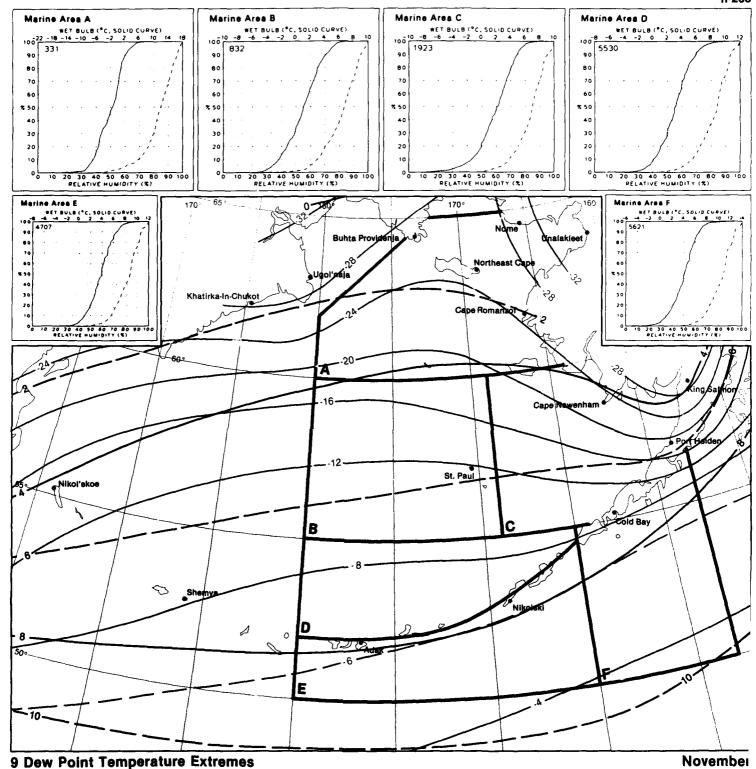
9 Wet Bulb and Relative Humidity



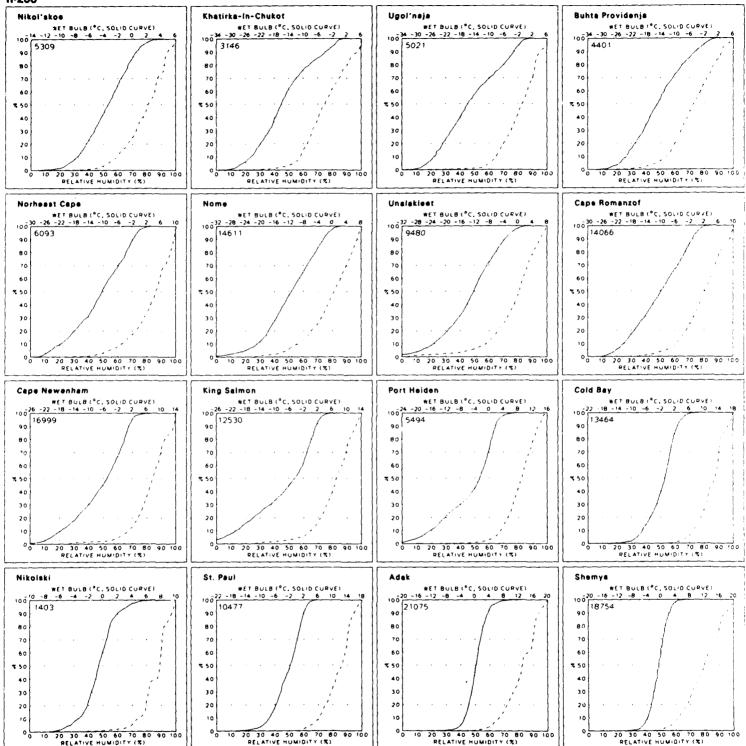


November

9 Wet Bulb and Relative Humidity

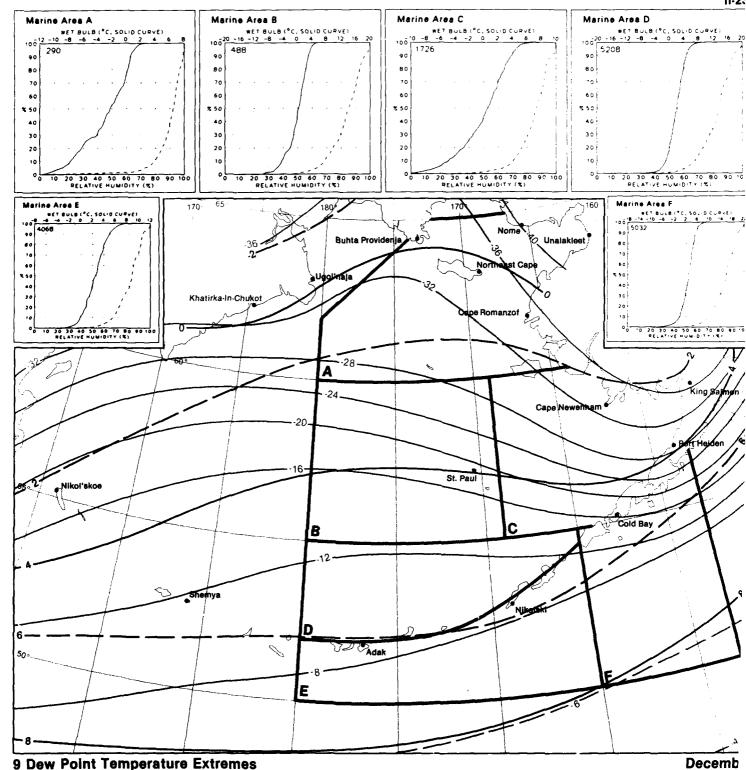






December

9 Wet Bulb and Relative Humidit



## Map 10. Mean sea level pressure and vector mean wind

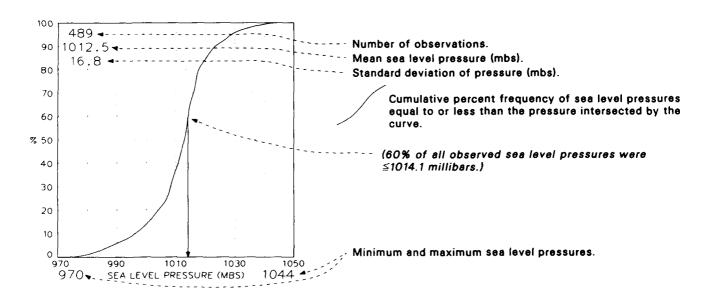
BLACK LINE - Mean sea level pressure (millibars).



Direction of flow toward station dot; vector magnitude in knots (example: vector mean wind is from northeast at 10.2 knots or 11.7 mph).

Albers Equal-Area Conic Projection

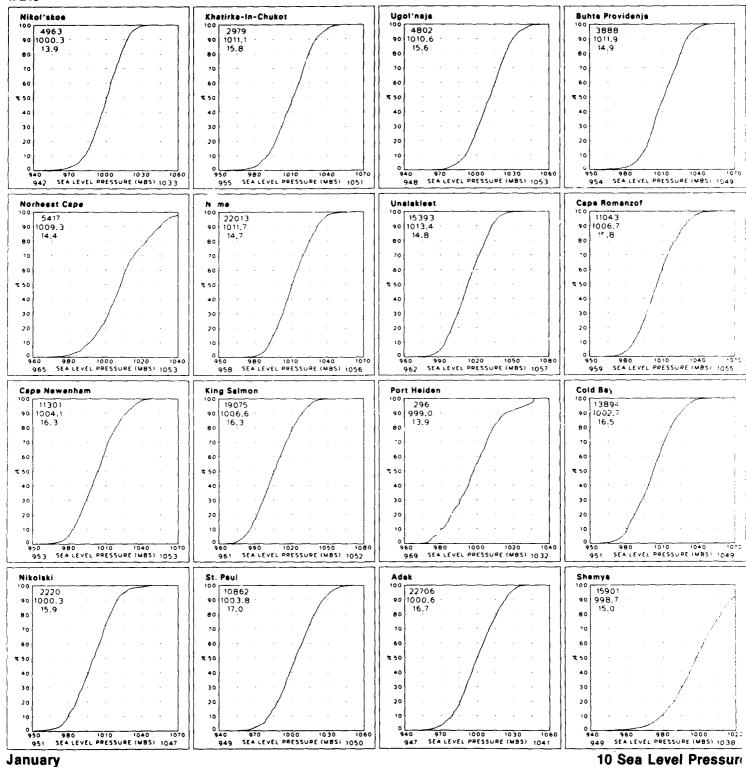
## **Graphs:** Sea level pressure

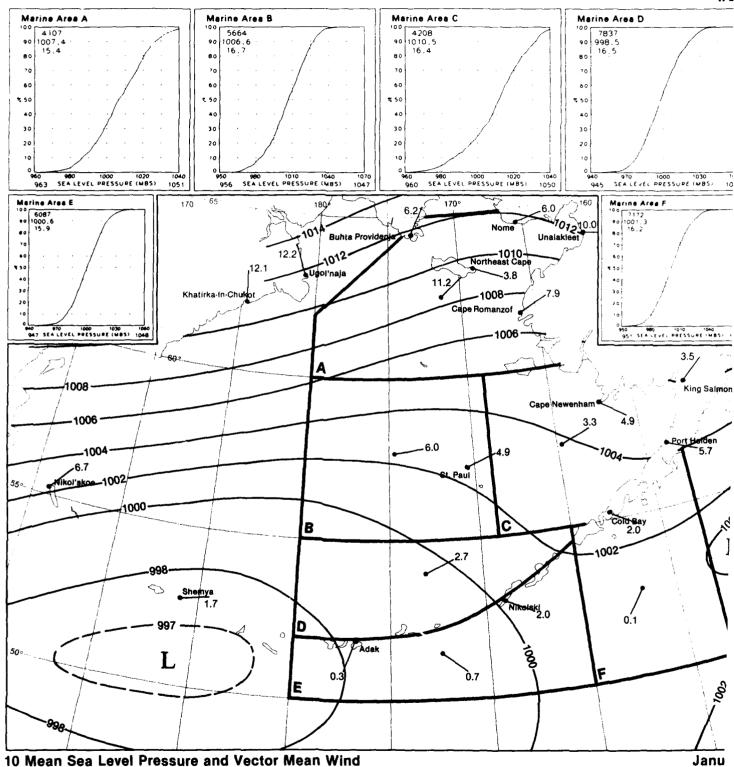


Sea level pressure is one of the most frequently recorded elements, but one of the least accurate because of instrumer calibration and coding errors. Despite the inaccuracies of the individual readings, the large-scale patterns and mean gradien of the isopleth analyses are relatively accurate. The percentage of sea level pressure observations greater than a given value of be obtained from the graph by subtracting the cumulative percent frequency of that value from 100%.

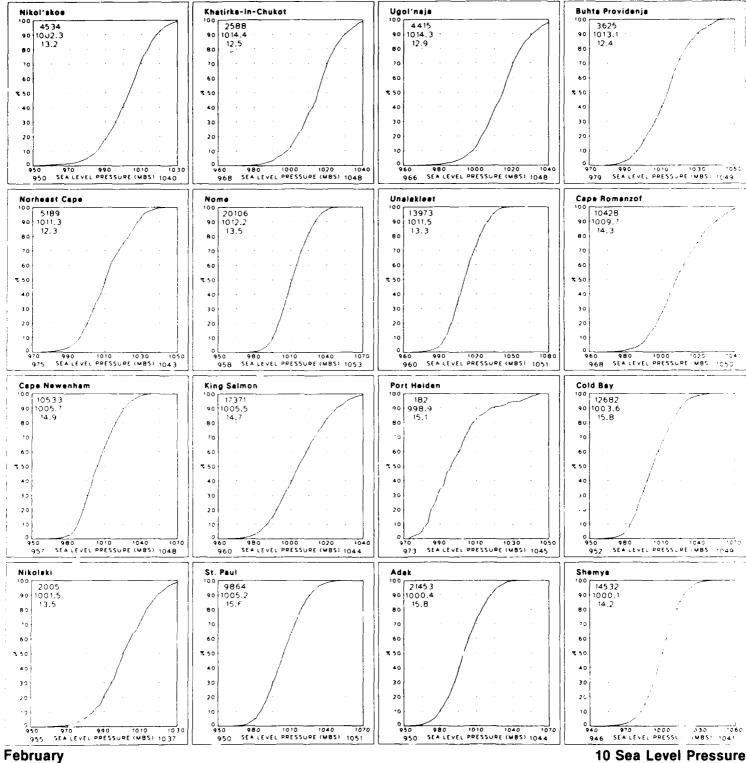
In areas of high persistence (also called constancy, steadiness) of direction, the magnitude of the vector mean wind (Set 1 should closely approach that of the scalar mean wind (Set 13).

10 Legend Legend

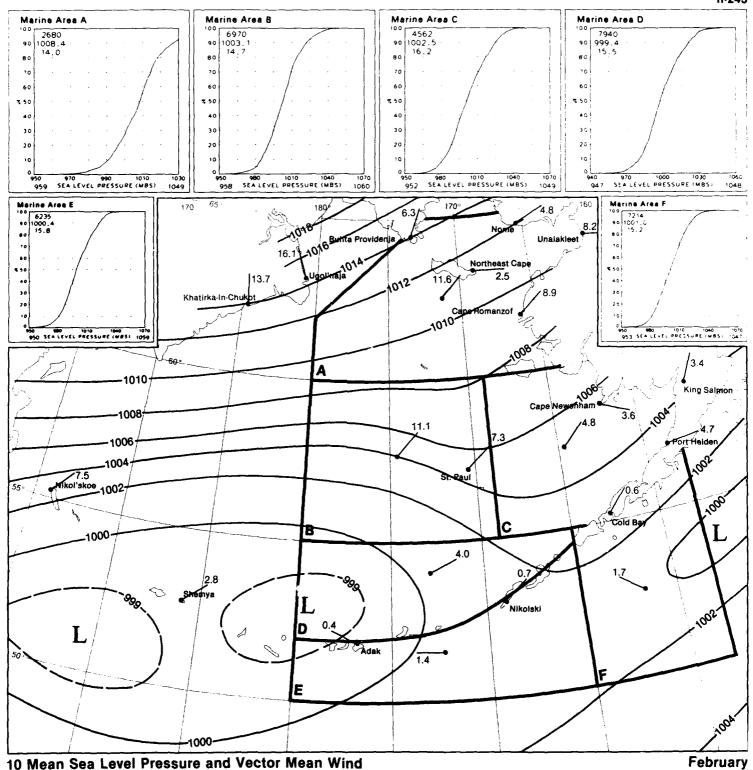


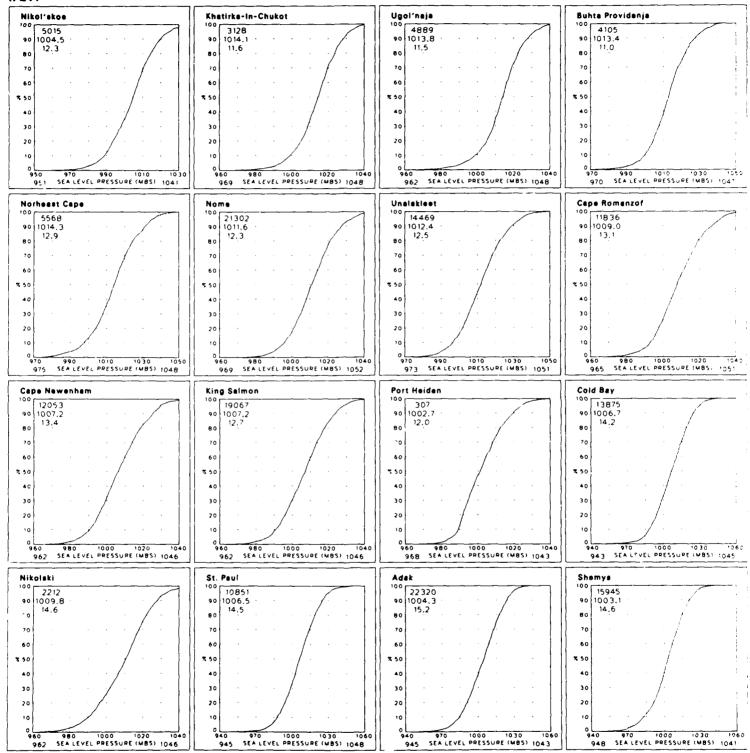


10 Mean Sea Level Pressure and Vector Mean Wind



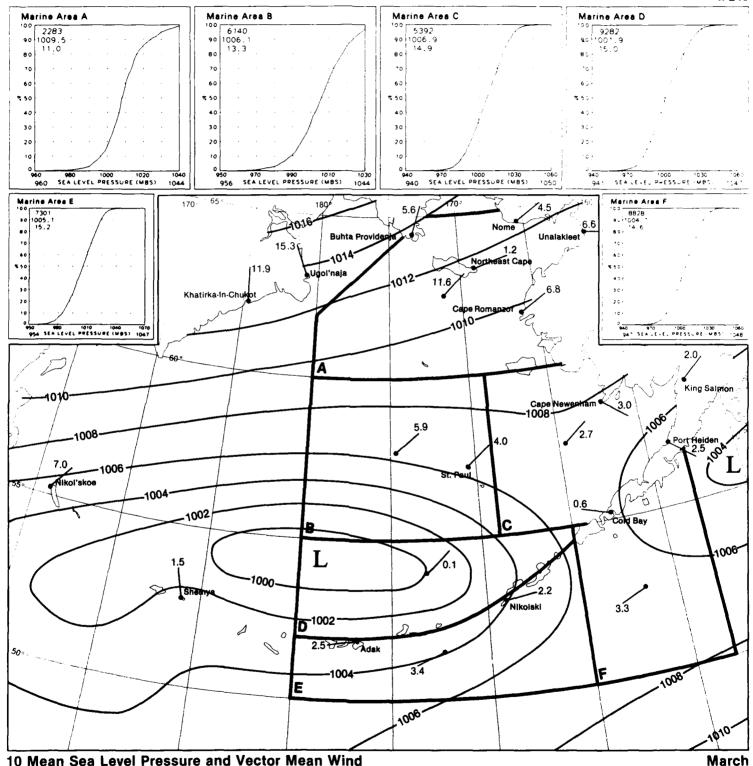
February



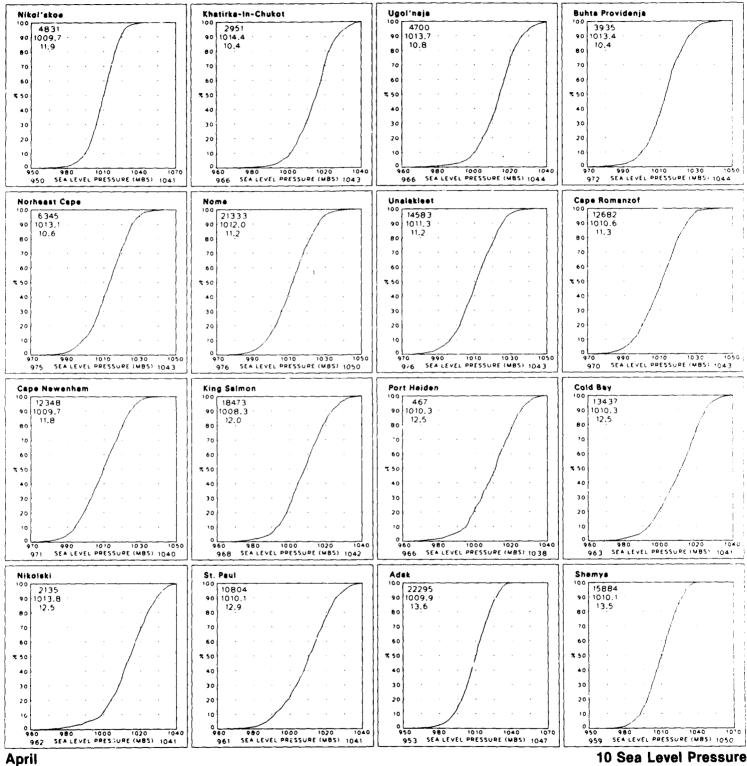


March

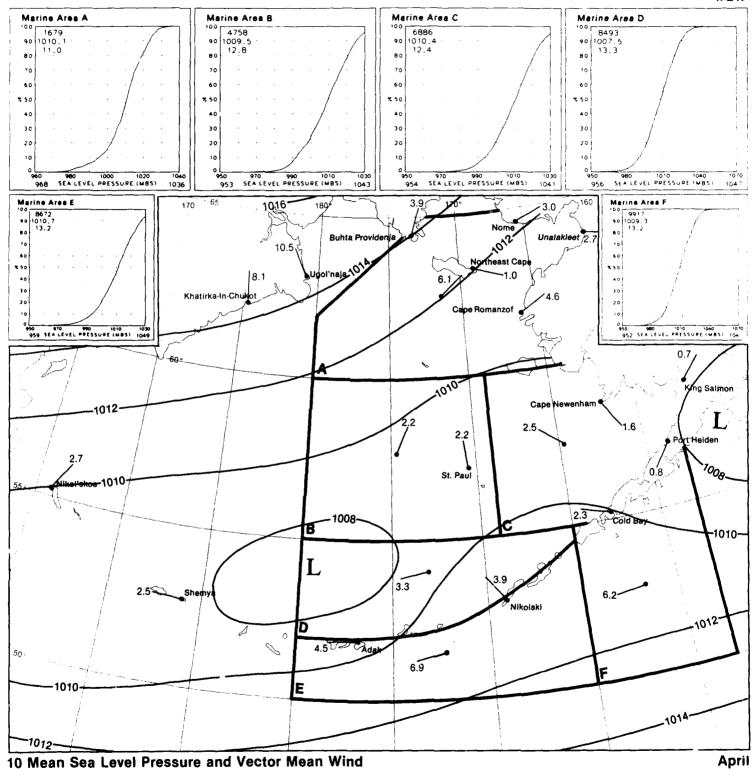
10 Sea Level Pressure



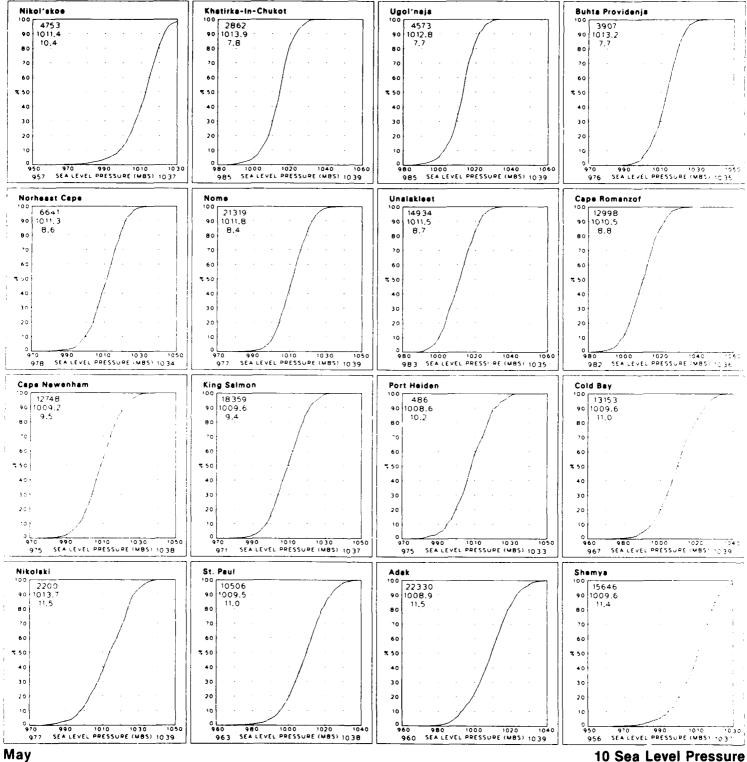
10 Mean Sea Level Pressure and Vector Mean Wind



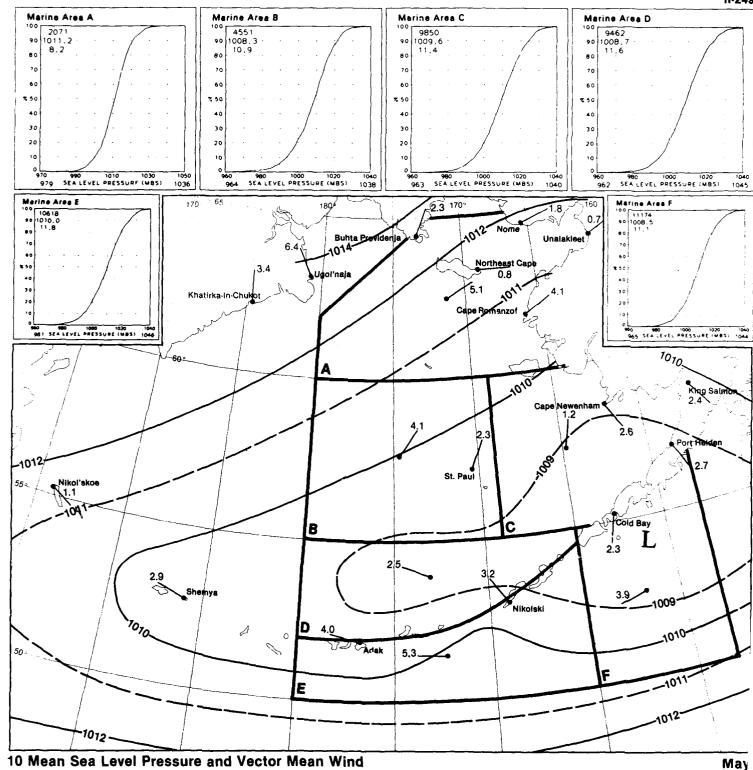
10 Sea Level Pressure



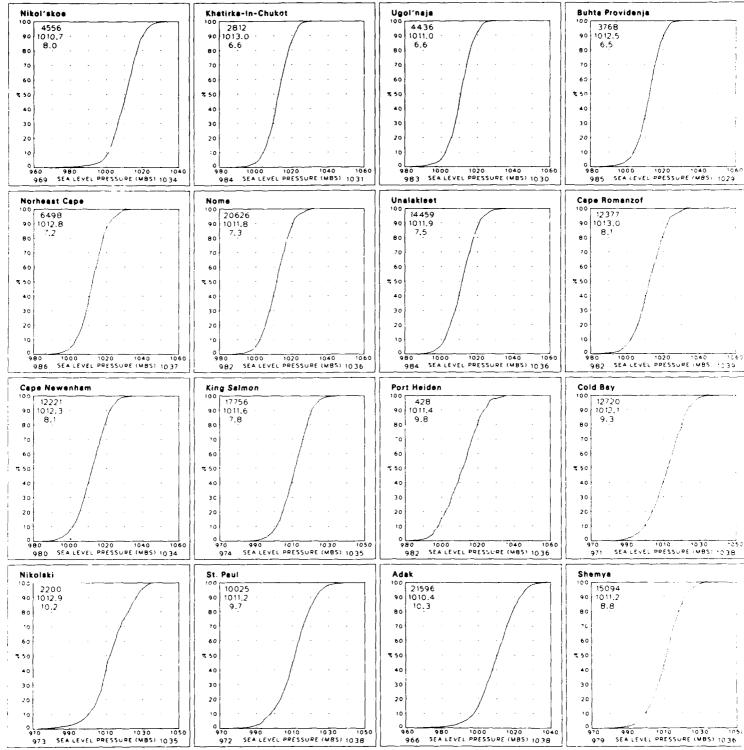
10 Mean Sea Level Pressure and Vector Mean Wind



10 Sea Level Pressure

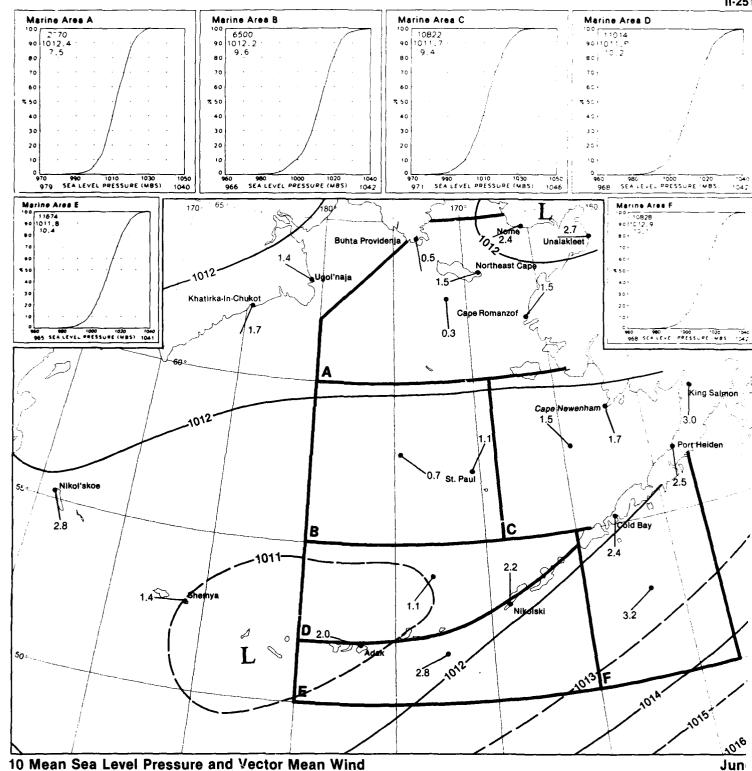


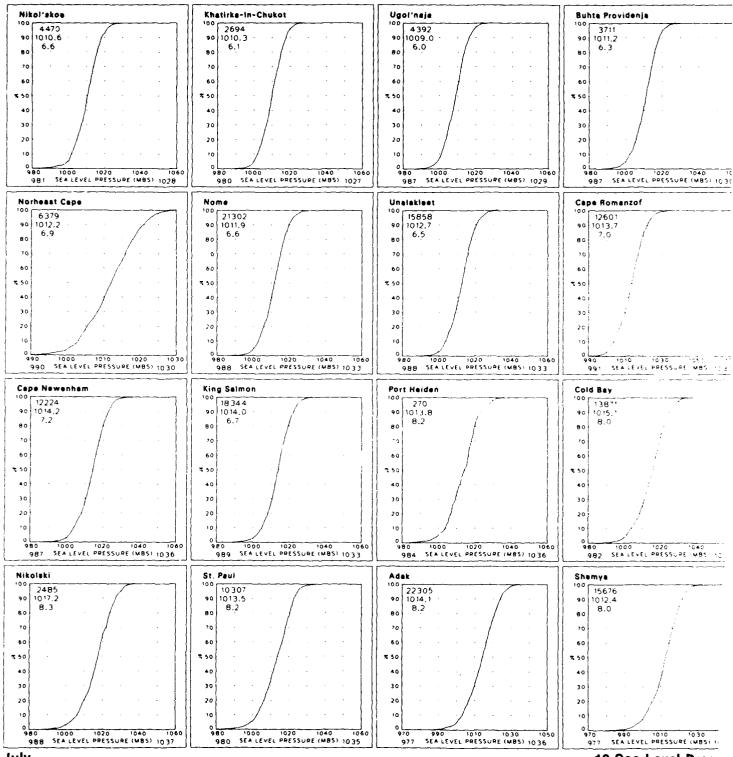




June

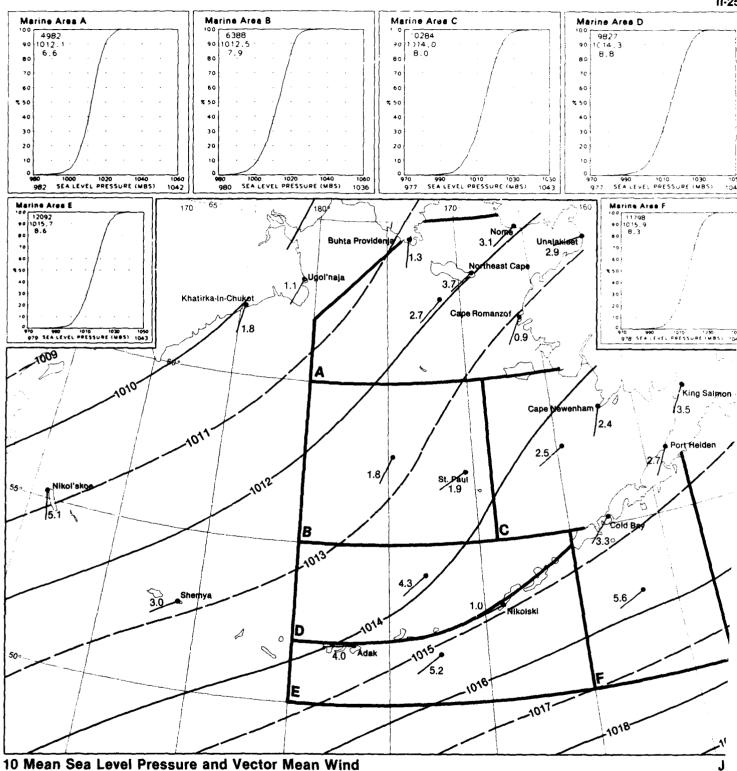
10 Sea Level Pressur



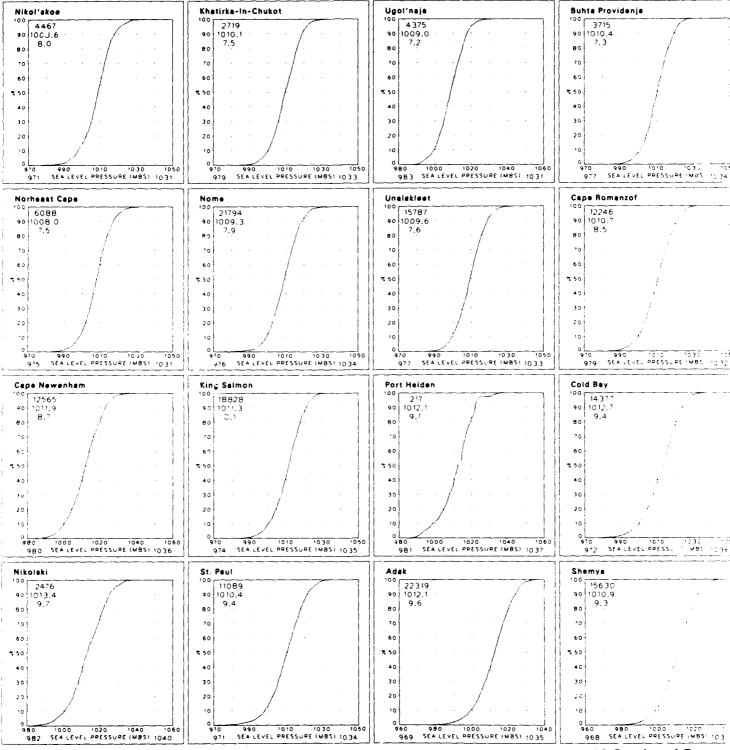


July

10 Sea Level Press

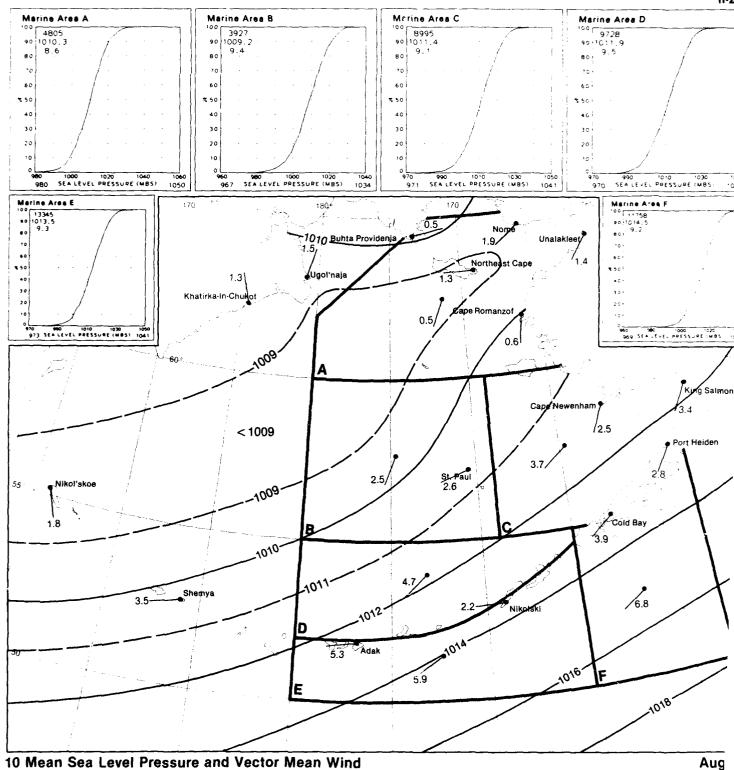






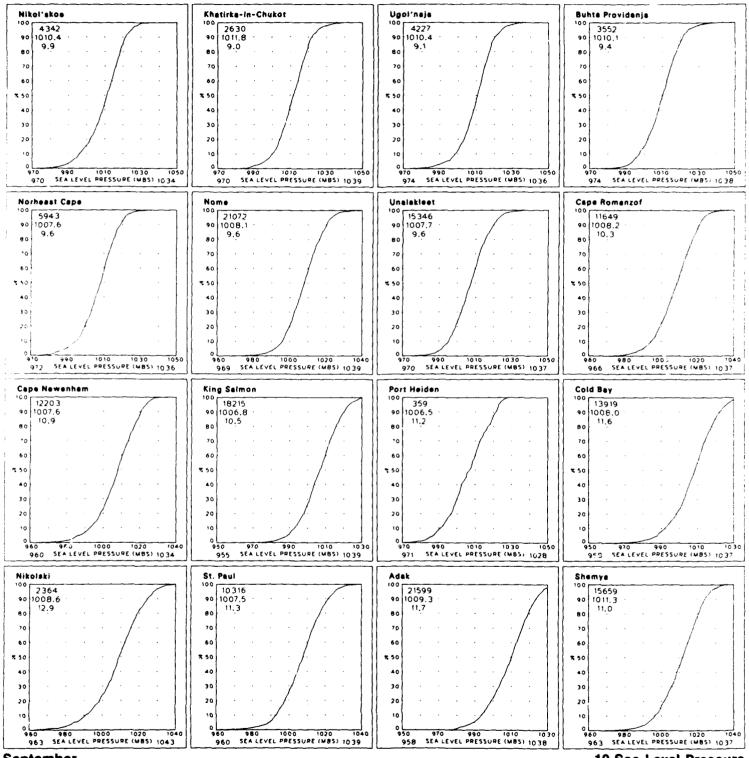
**August** 

10 Sea Level Pressu



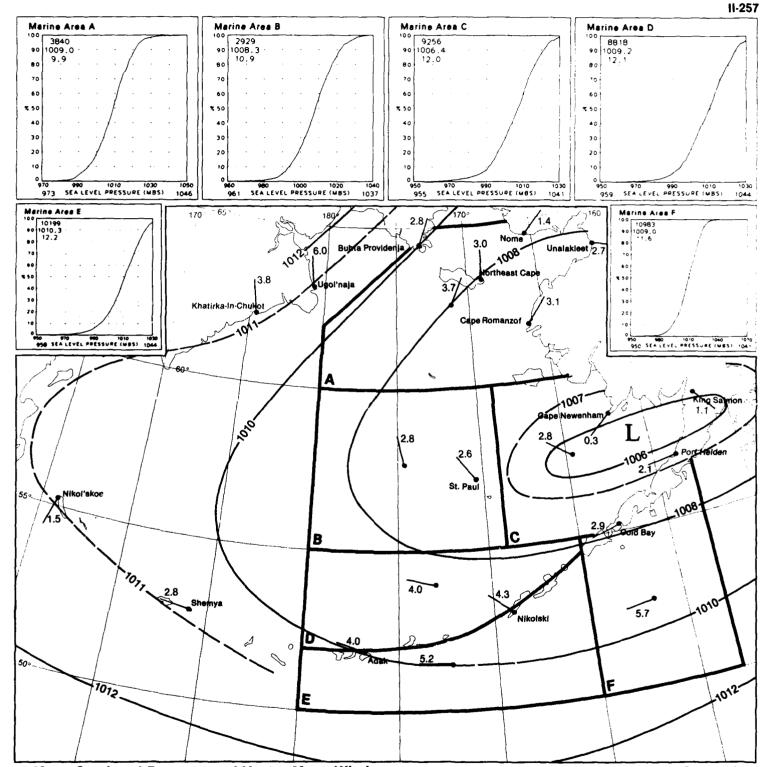
10 Mean Sea Level Pressure and Vector Mean Wind





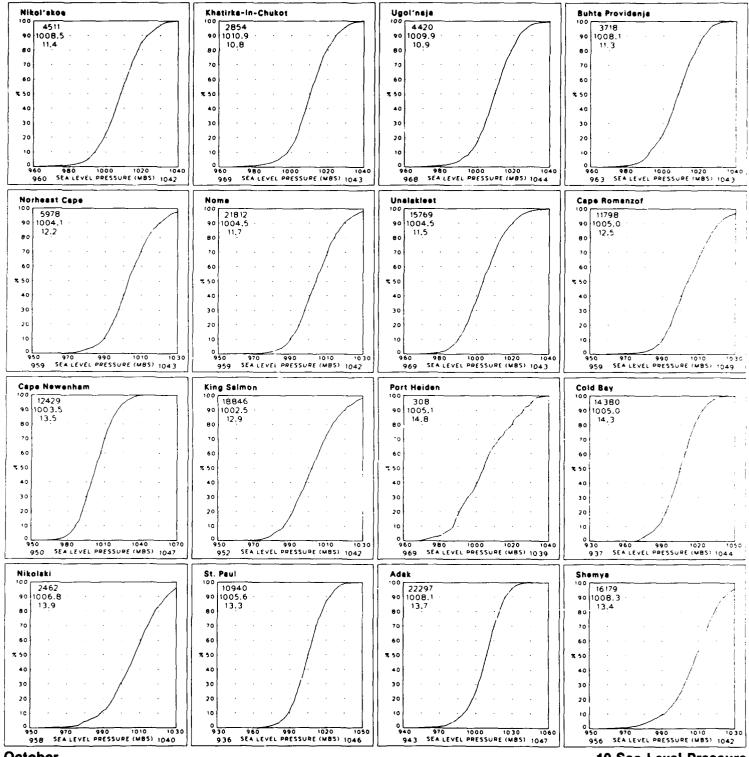
September

10 Sea Level Pressure



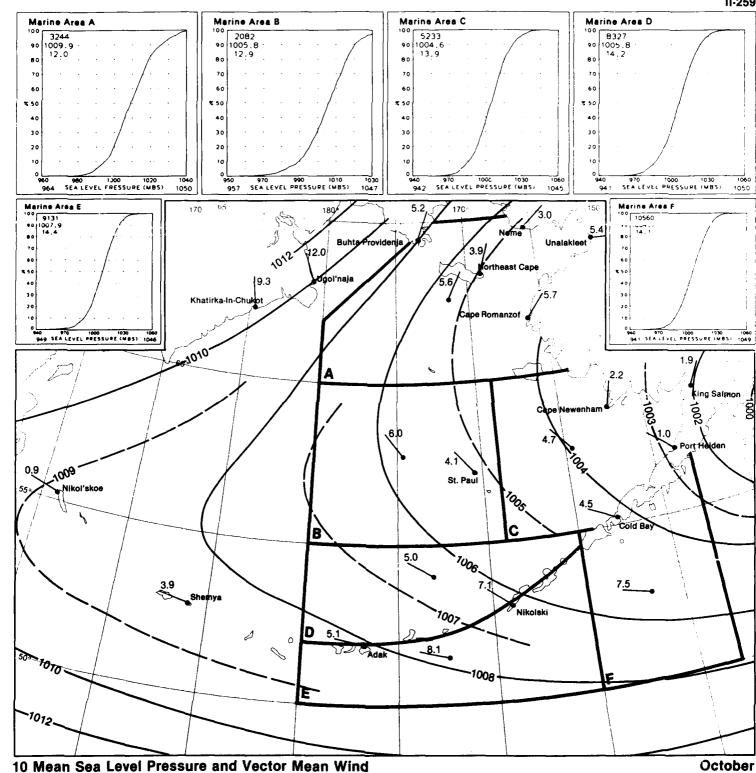
10 Mean Sea Level Pressure and Vector Mean Wind

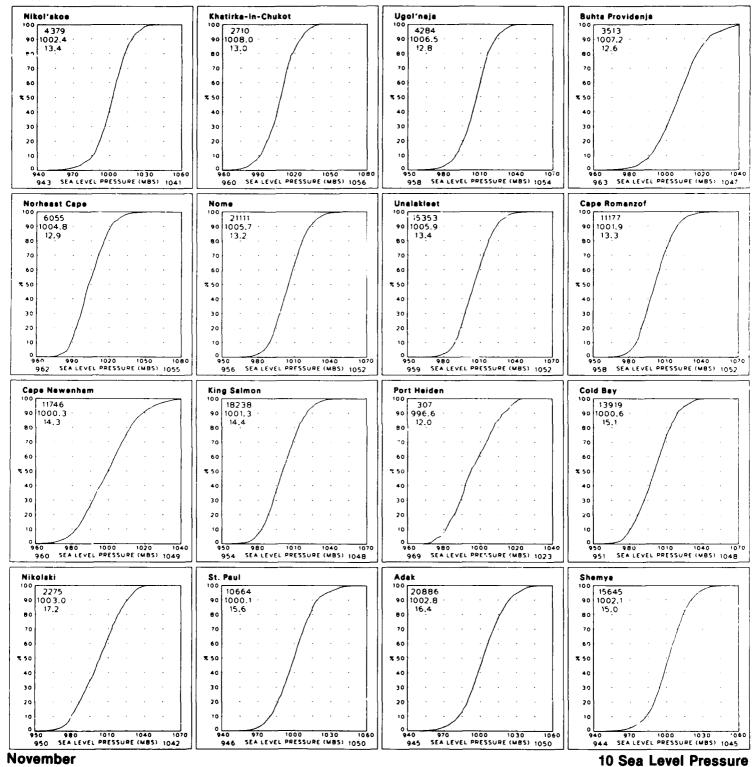
September

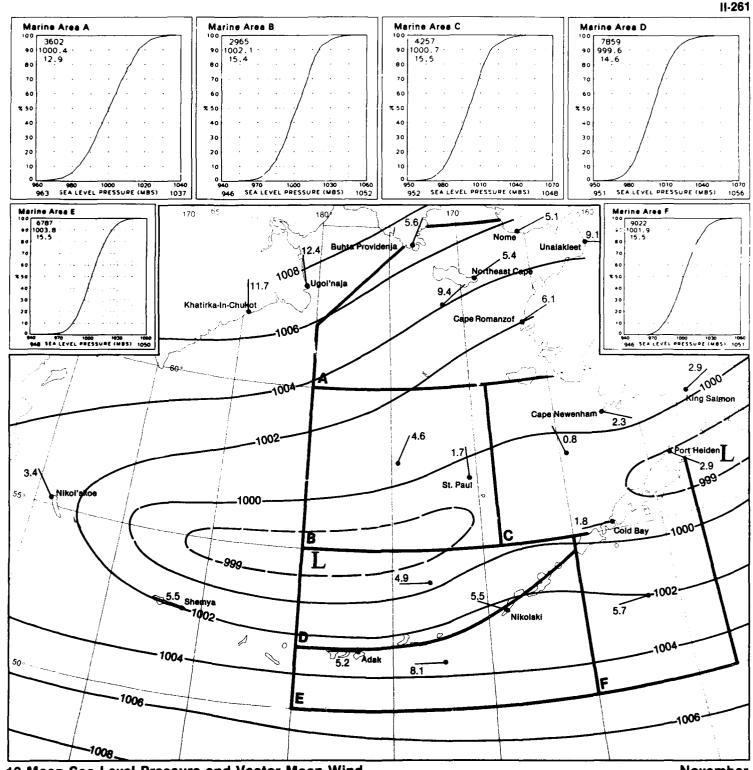


October

10 Sea Level Pressure

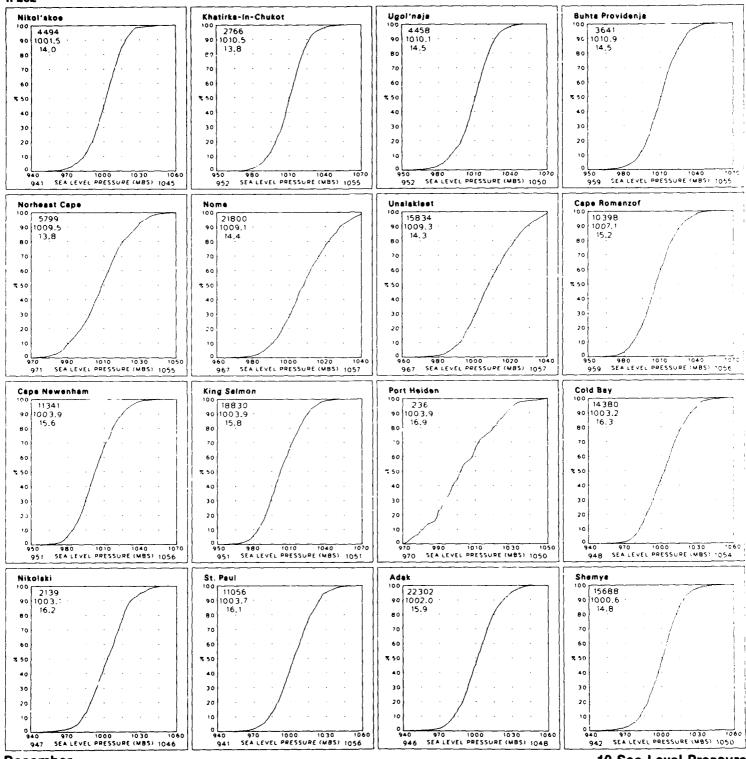






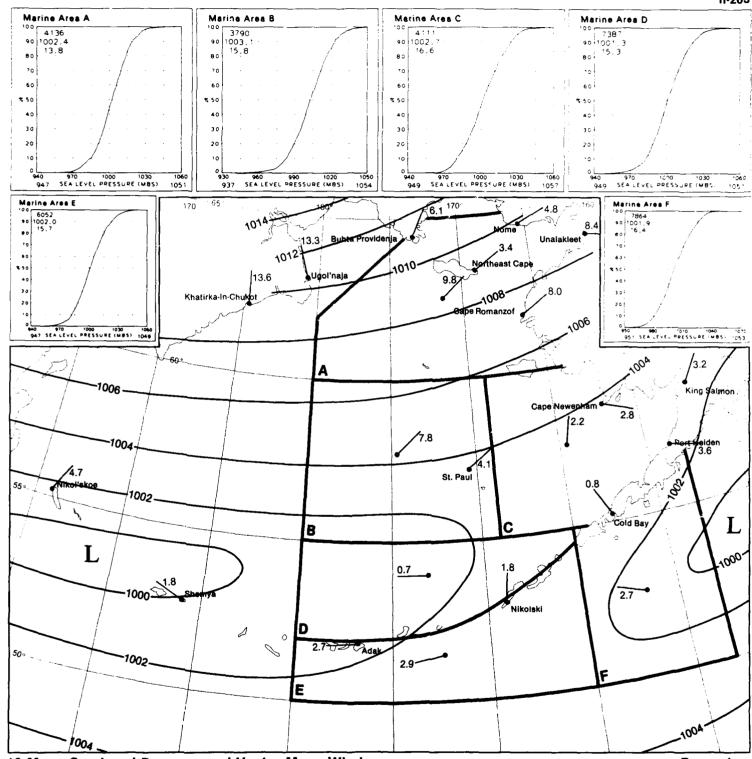
10 Mean Sea Level Pressure and Vector Mean Wind

November



December

10 Sea Level Pressure



10 Mean Sea Level Pressure and Vector Mean Wind

December

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## Map 11. Wind speed ≤10 and ≥34 knots

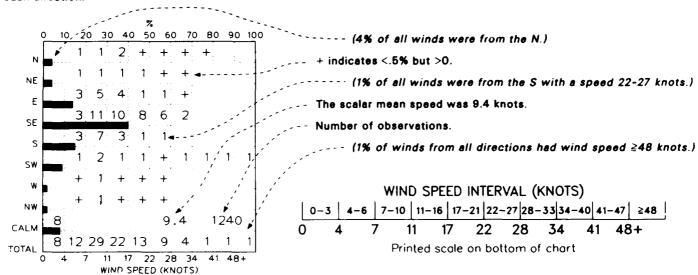
BLACK LINE - Percent frequency of wind speed ≤10 knots (≤12 mph).

BLUE LINE - Percent frequency of wind speed ≥34 knots (≥39 mph).

Albers Equal—Area Conic Projection

### Graphs: Wind speed/direction

Direction frequency (top scale): Bars represent percent frequency of winds observed from each direction. Speed frequency (bottom scale): Printed figures represent percent frequency of wind speeds observed from each direction.

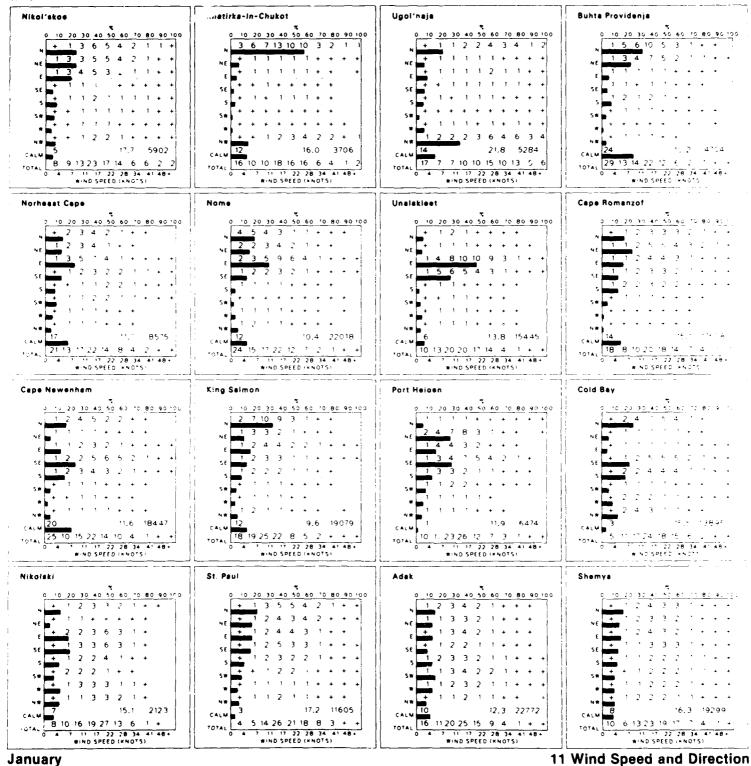


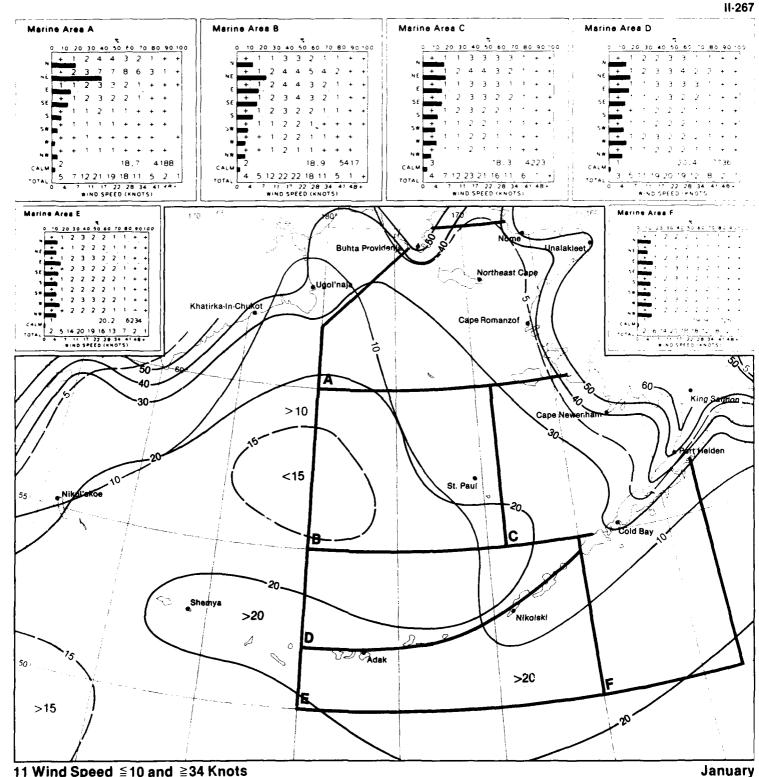
The scalar mean wind speed on the graph is based on the number of observations reporting a wind speed with direction. The sum of the TOTAL line provides the cumulative percent frequency of wind speed below a selected threshold value. In the legend graph, 71% of all winds were less than 17 knots (20 mph). The sum of the percent frequencies of the four wind speed isopleths for a given month and location on Map Sets 11 and 12 should equal 100%.

Surface wind is one of the most commonly observed elements. Many of the observations from the NCDC data base are visual observations based on the roughness of the sea (see table in text of Set 14). In recent years, more ships acquired anemometers and reported measured winds. Prior to 1963, many of the winds were recorded in the Beaufort scale; such estimates have proven to be quite reliable and can be used with a high degree of confidence.

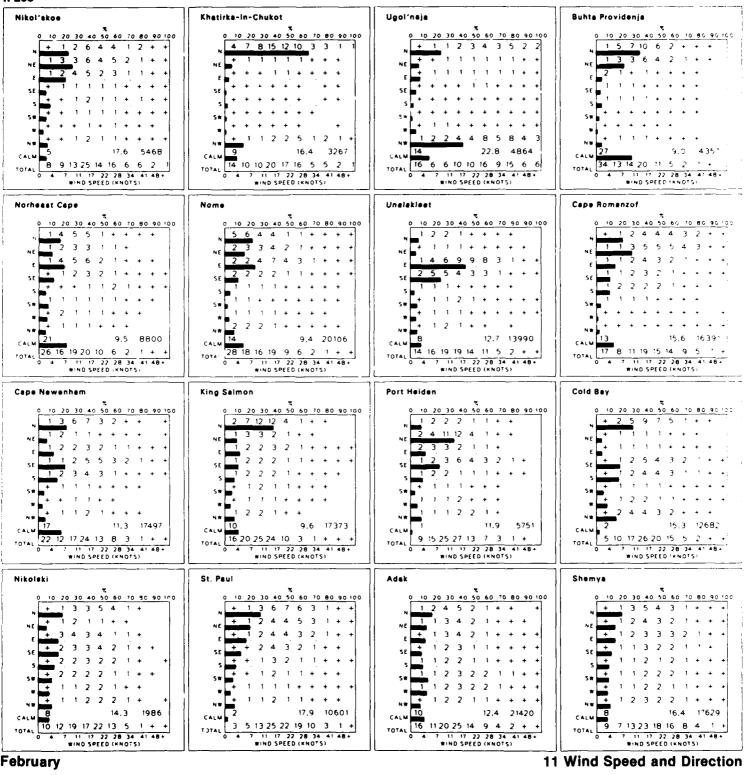
11 Legend

Legend 11



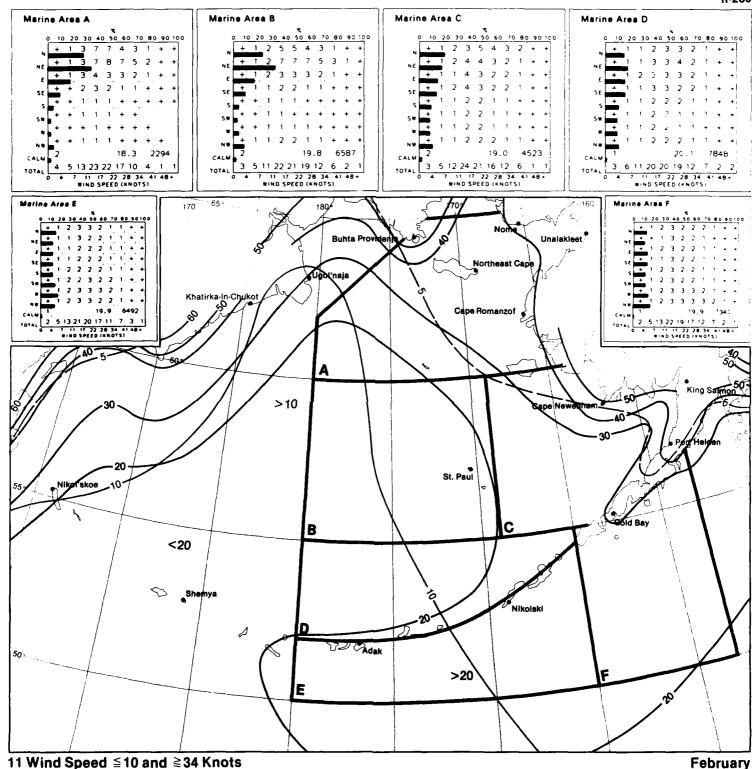


11 Wind Speed ≦10 and ≧34 Knots

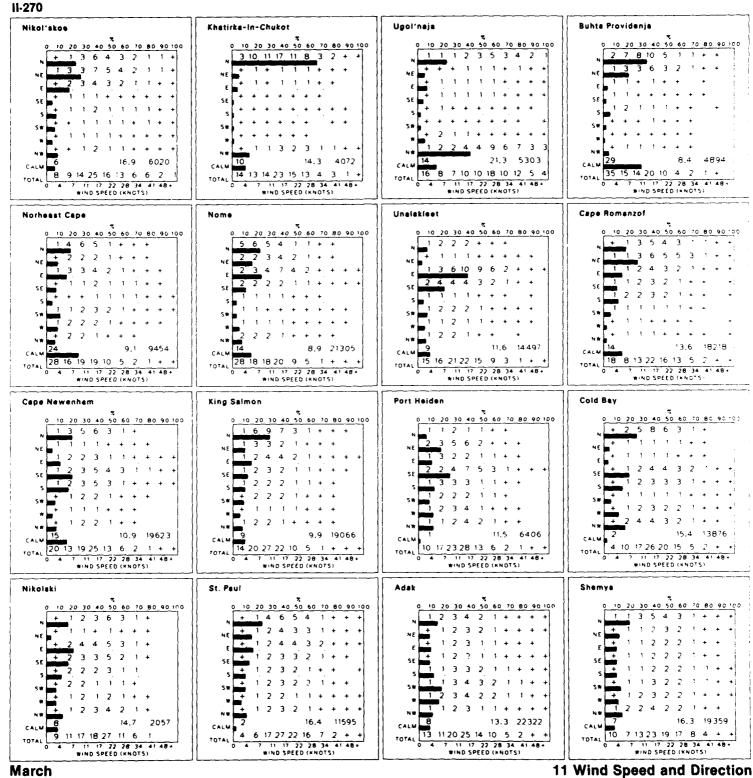


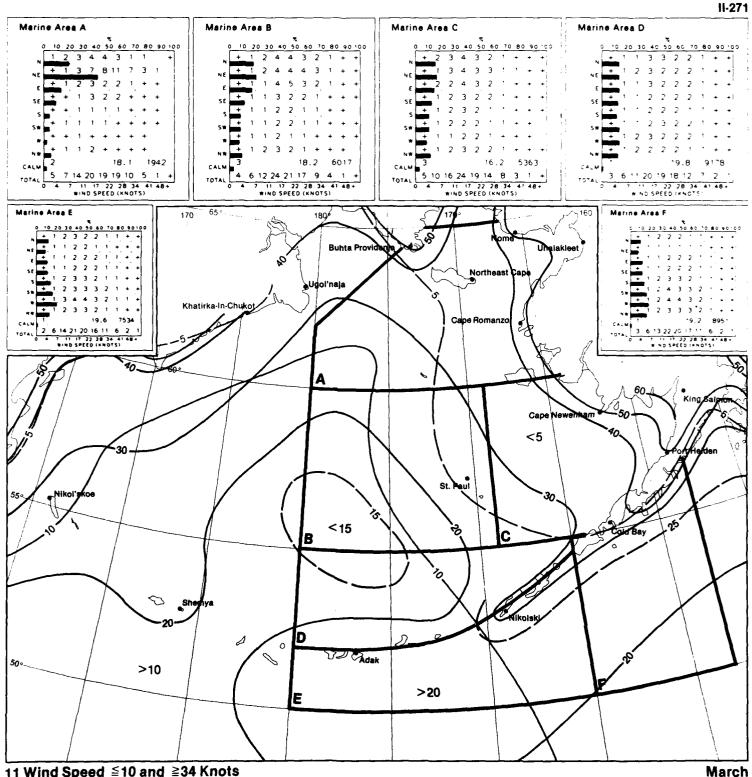
February

11 Wind Speed and Direction

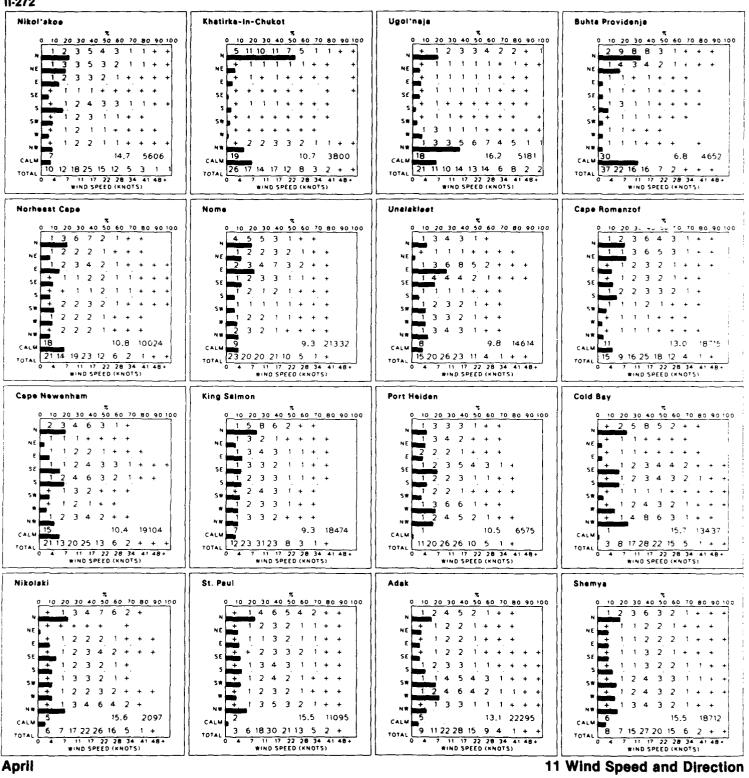


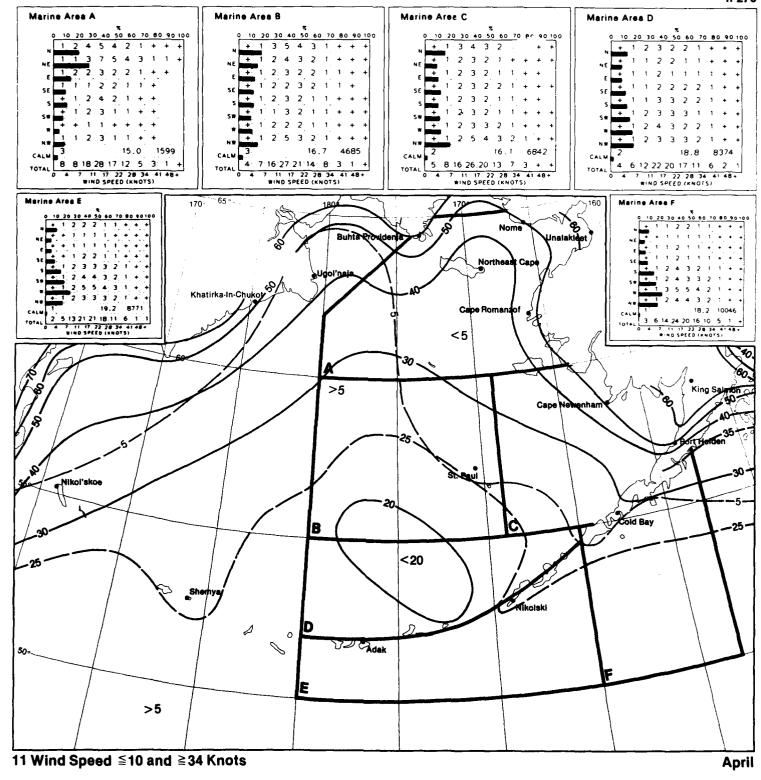
11 Wind Speed ≤ 10 and ≥ 34 Knots

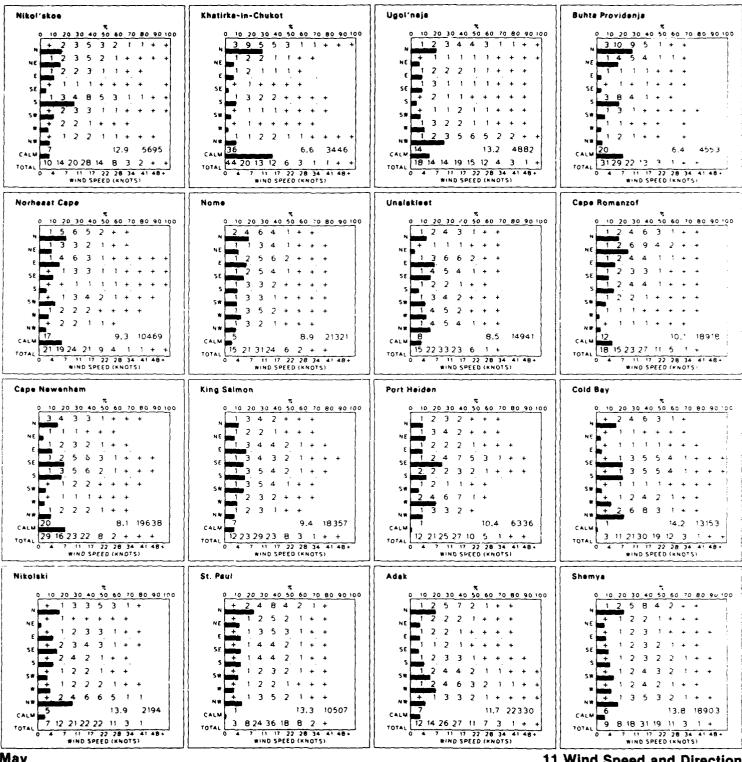




11 Wind Speed ≦10 and ≧34 Knots

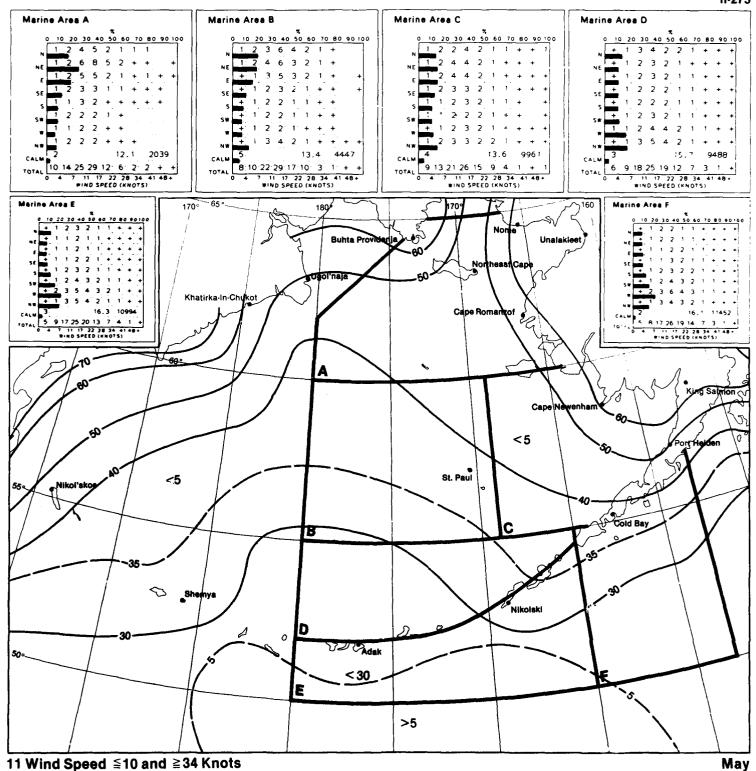


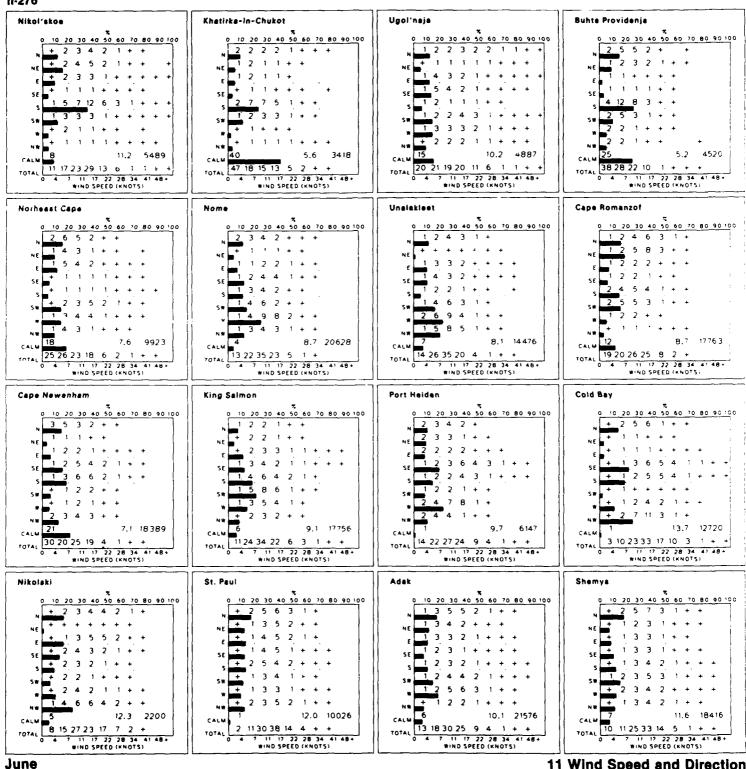




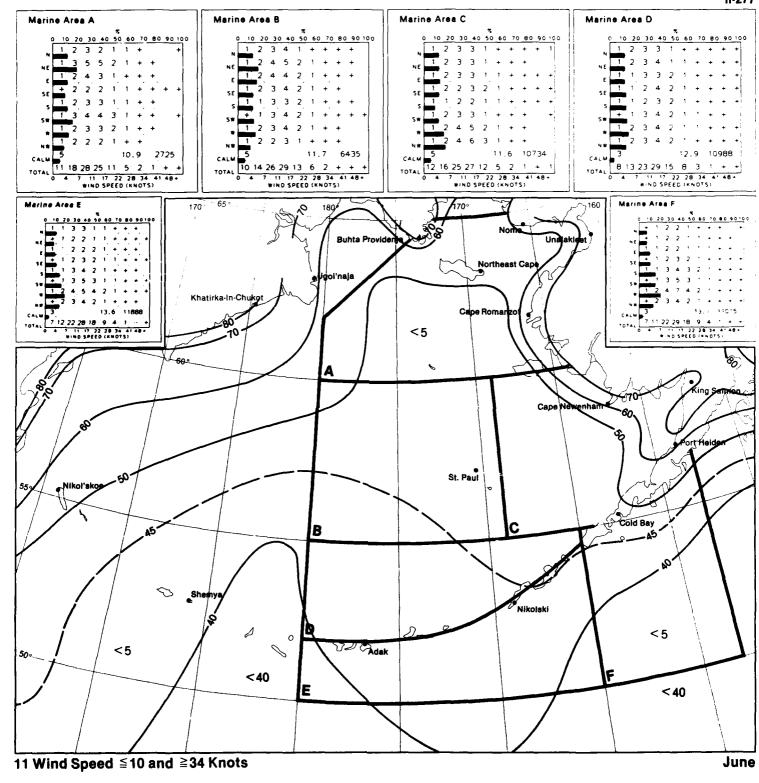
May

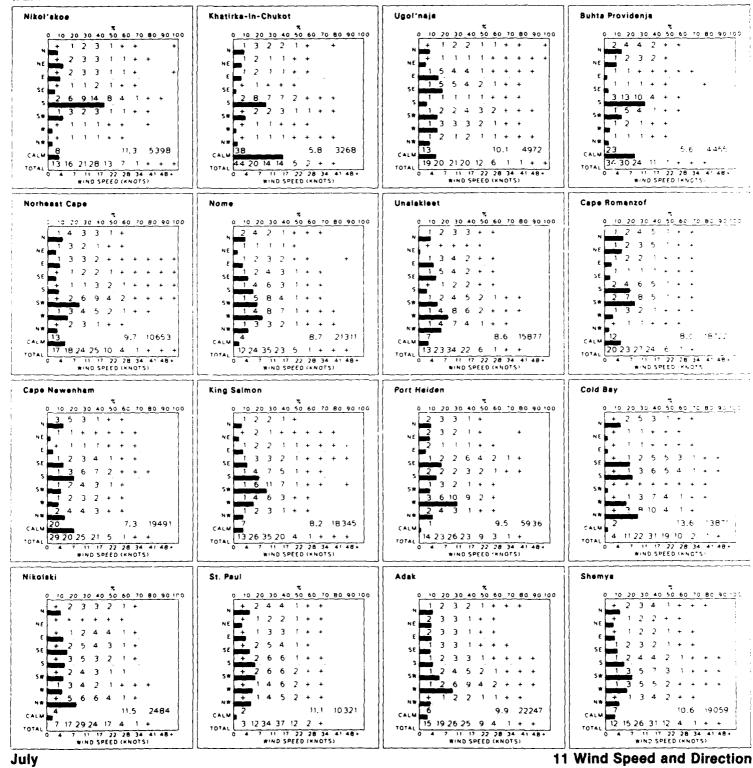
11 Wind Speed and Direction

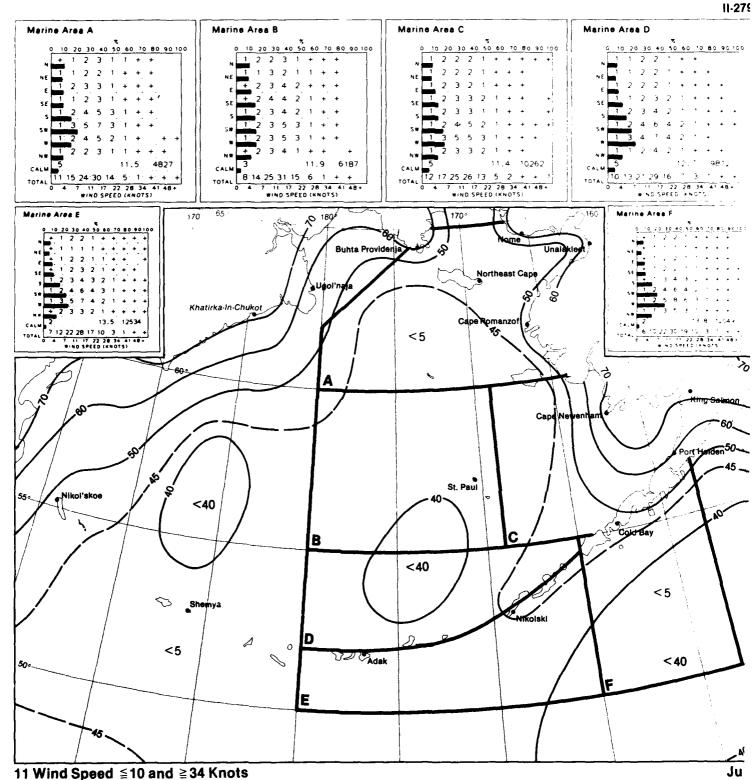


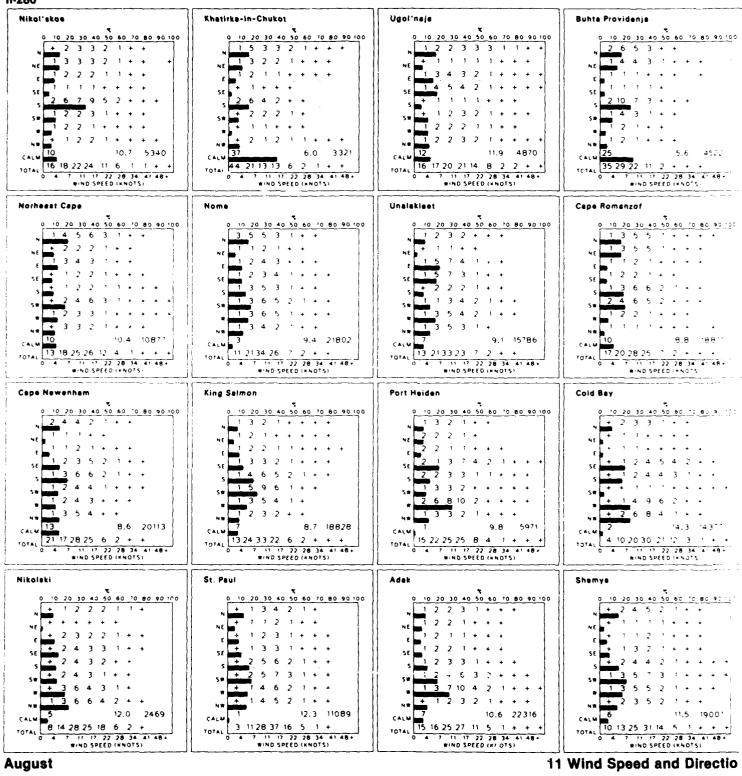


11 Wind Speed and Direction



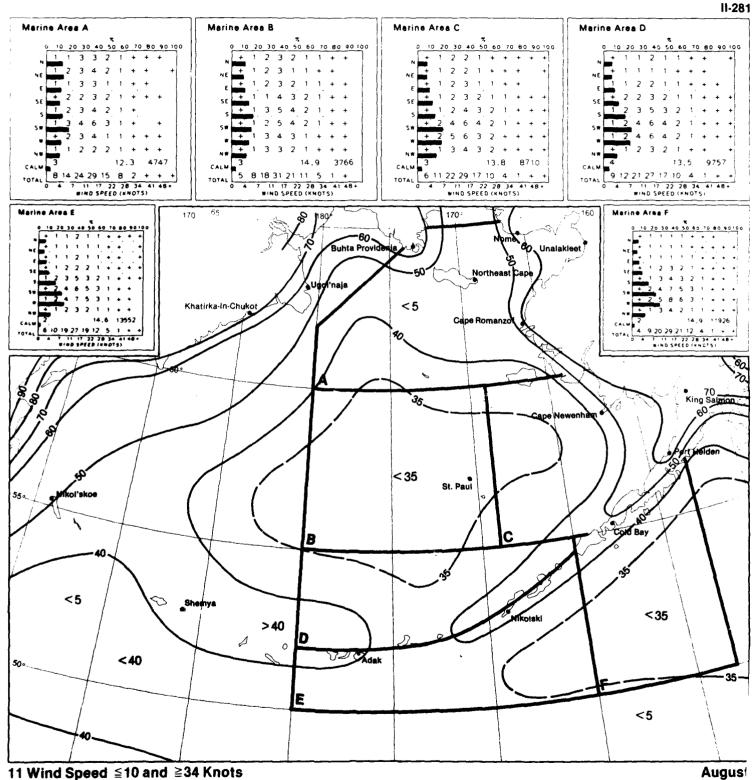


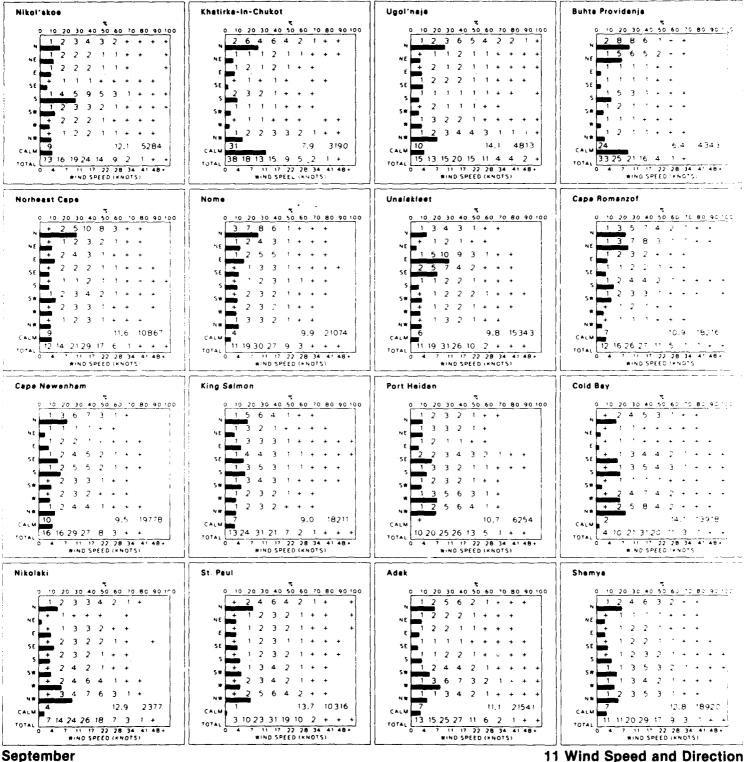


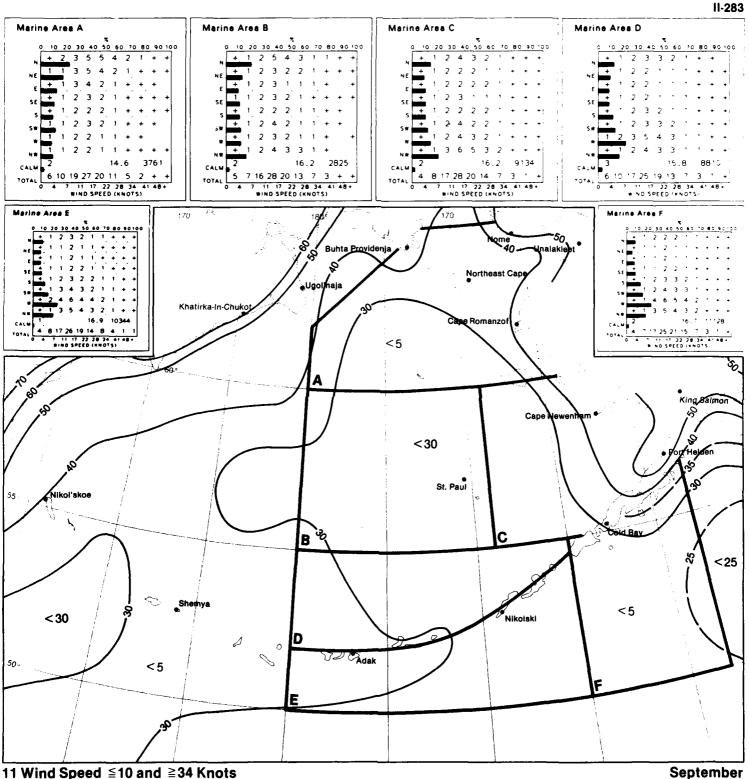


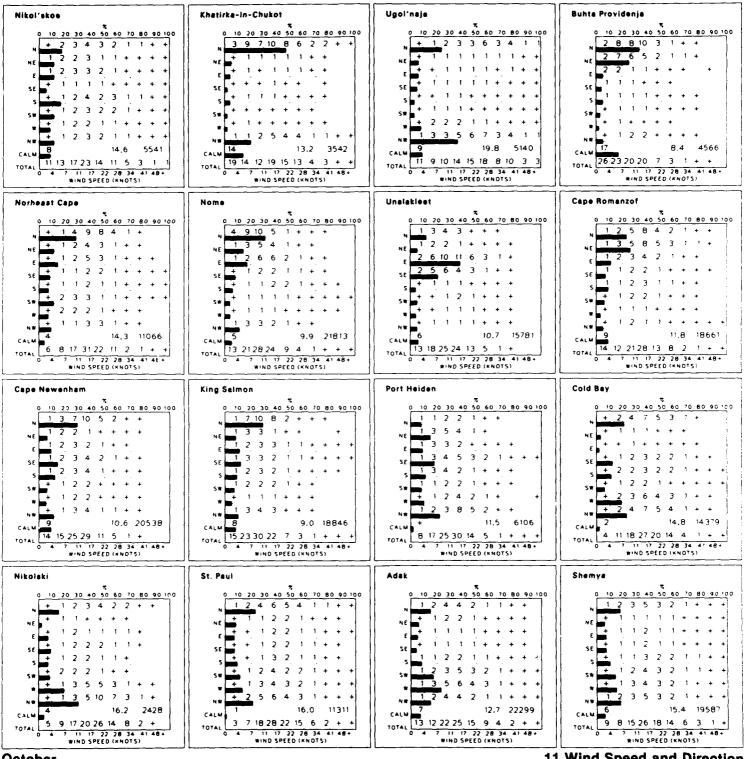
August

11 Wind Speed and Directio



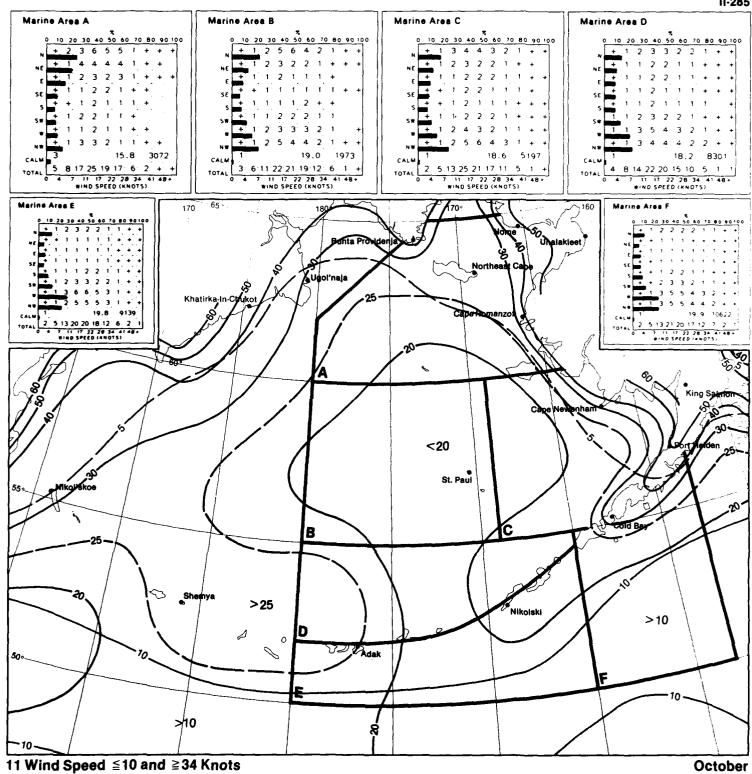




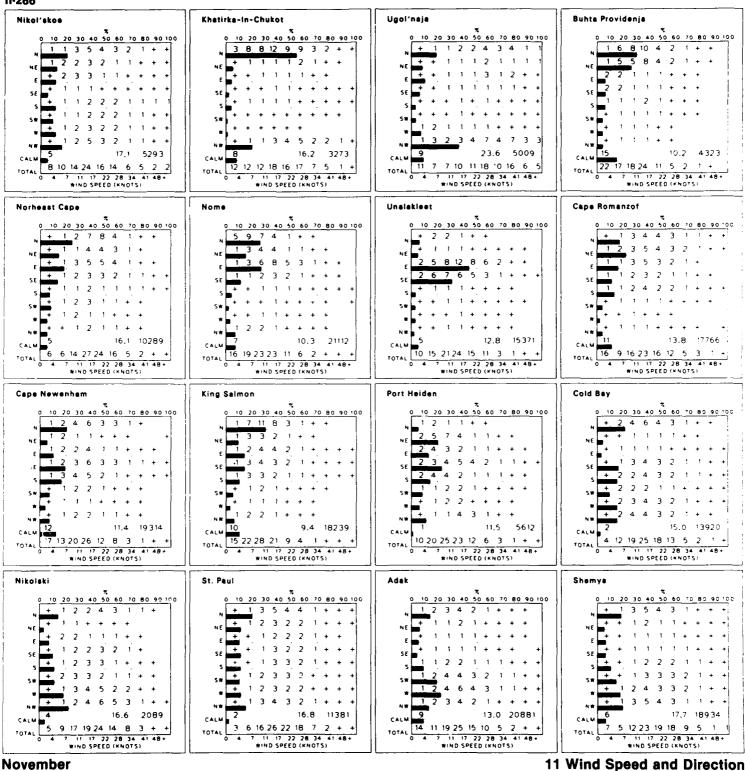


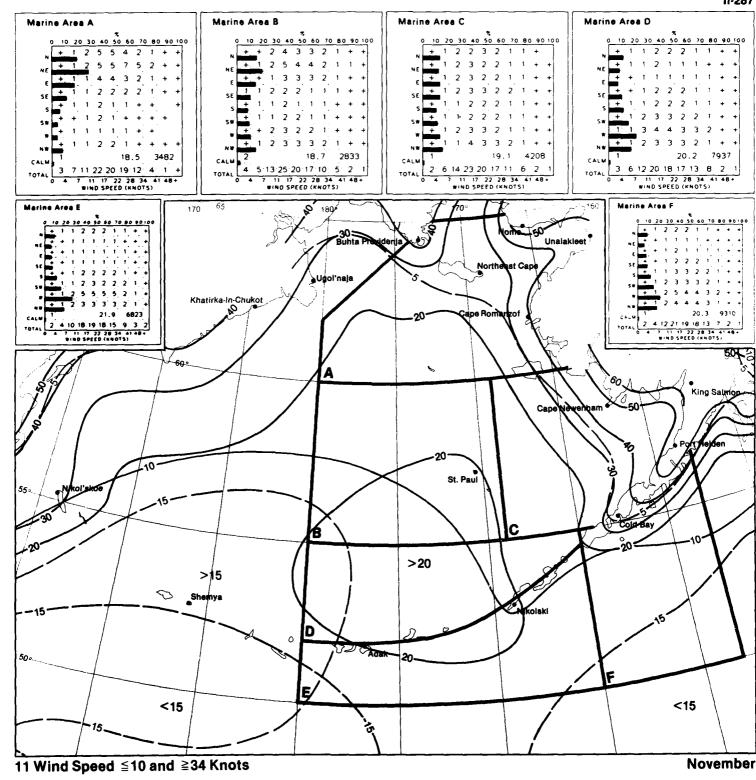
October

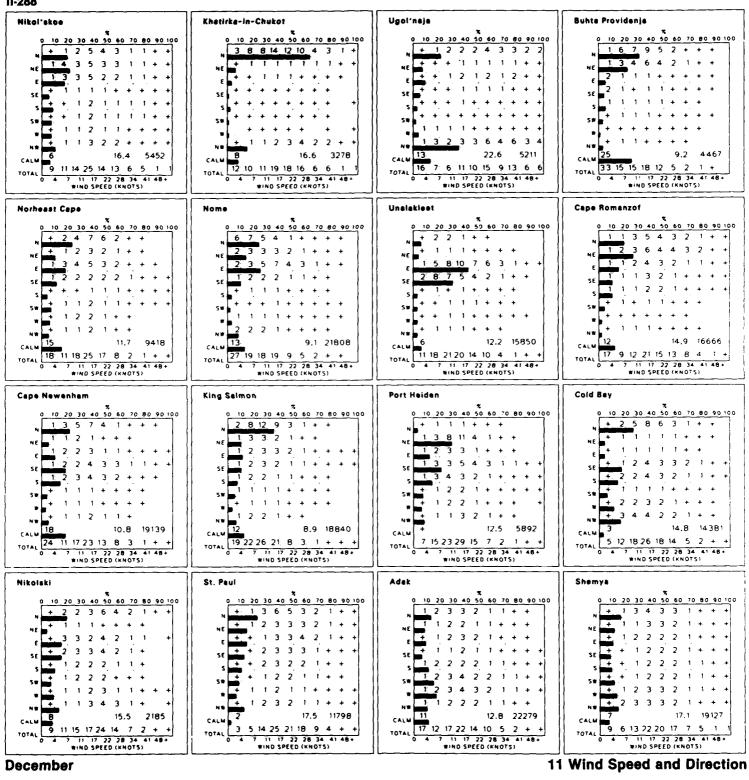
11 Wind Speed and Direction

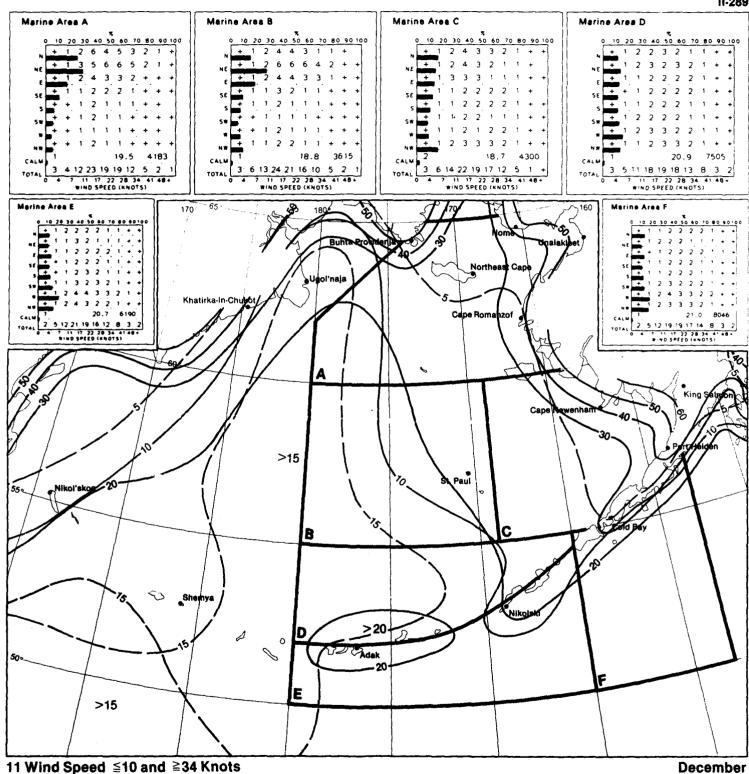


#### 11-286









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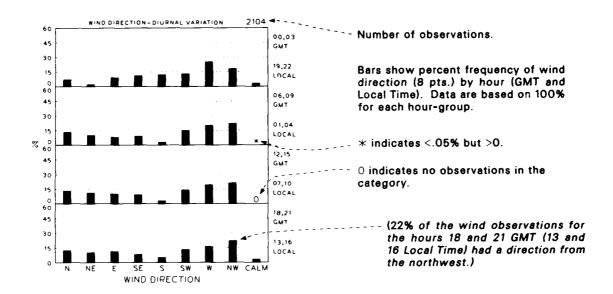
### Map 12. Wind speed 11-21 and 22-33 knots

BLACK LINE - Percent frequency of wind speed 11-21 knots.

BLUE LINE - Percent frequency of wind speed 22-33 knots.

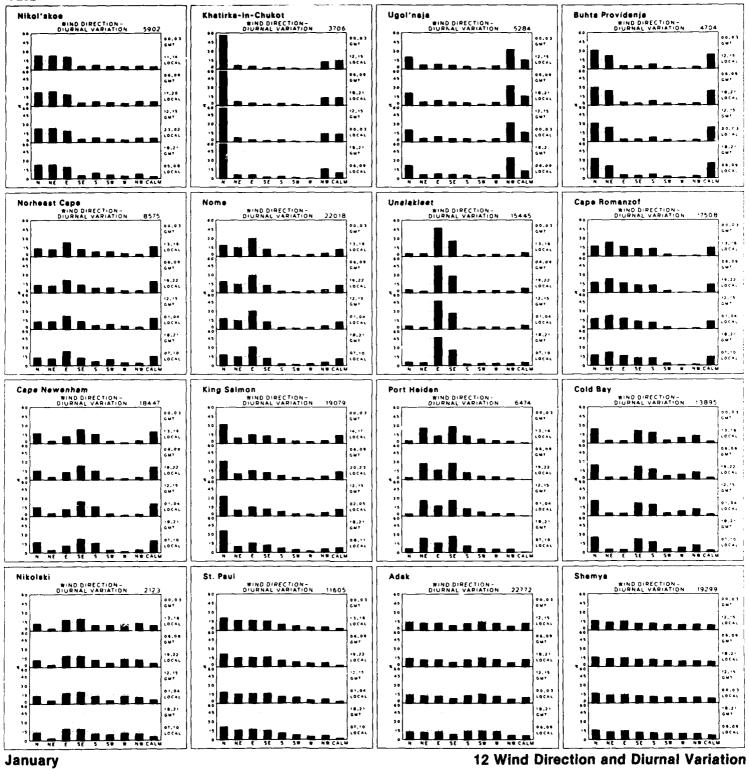
Albers Equal—Area Conic Projection

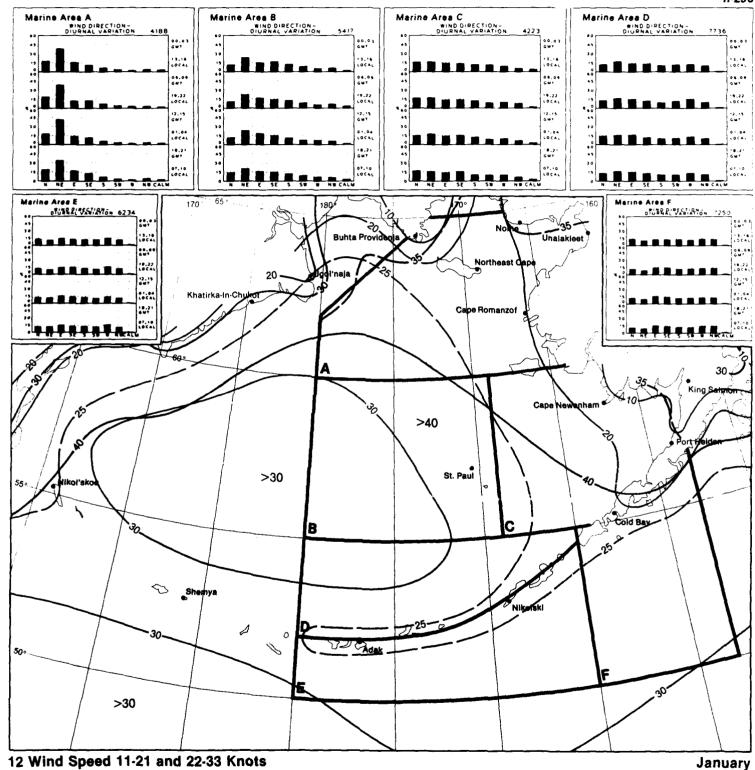
# Graphs: Wind direction/diurnal variation



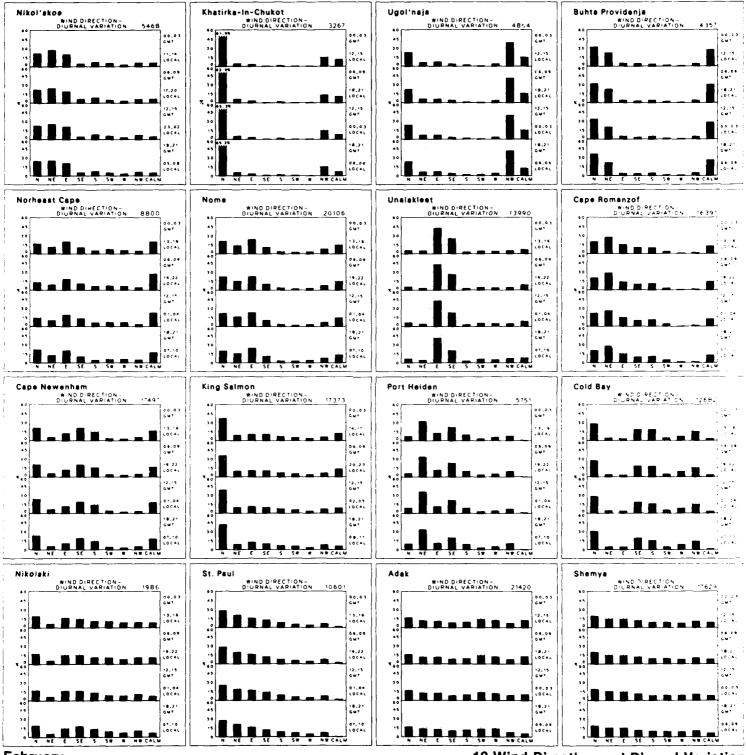
The historical marine data file at the NCDC is made up of data collected and recorded since 1854 in several different units of measurement. Wind direction has been recorded over the years in the 16-, 32-, and 36-point scale. A reduced biasing system was employed in converting wind direction to the 8-point scale used in this atlas. This method attached weighting values to observations which overlap two different 8-point sectors and treats them as "fractional observation counts."

12 Legend Legend 12



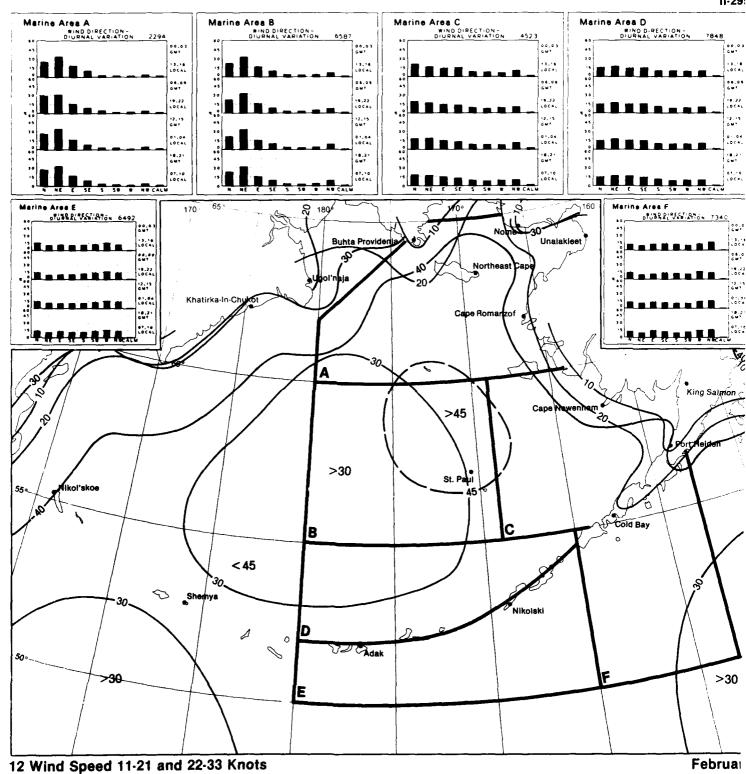


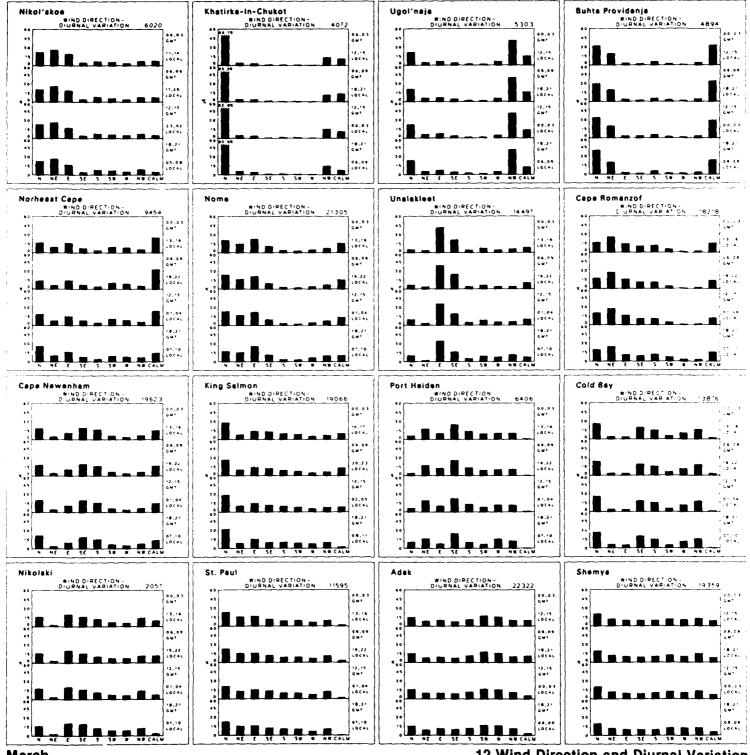
12 Wind Speed 11-21 and 22-33 Knots



**February** 

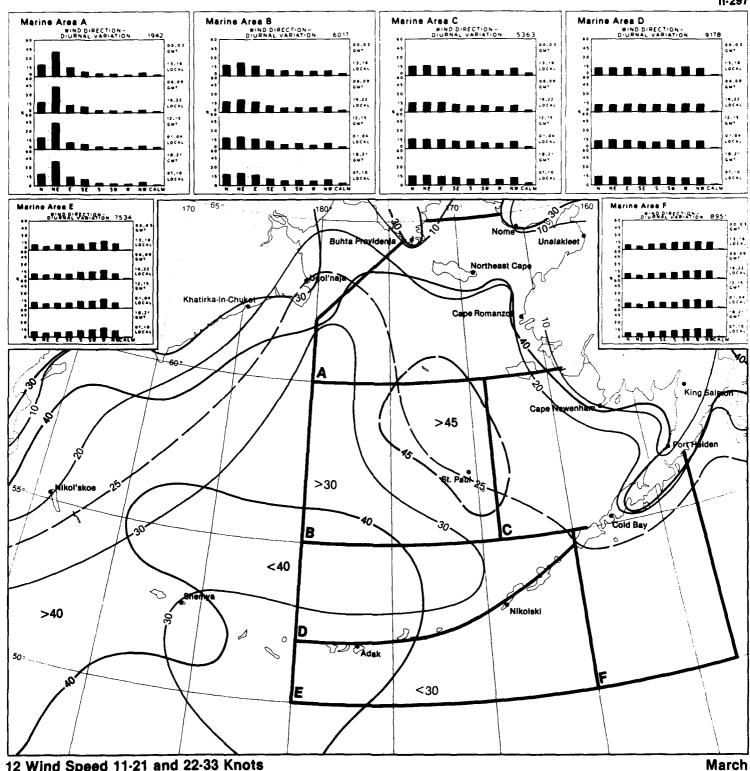
12 Wind Direction and Diurnal Variation



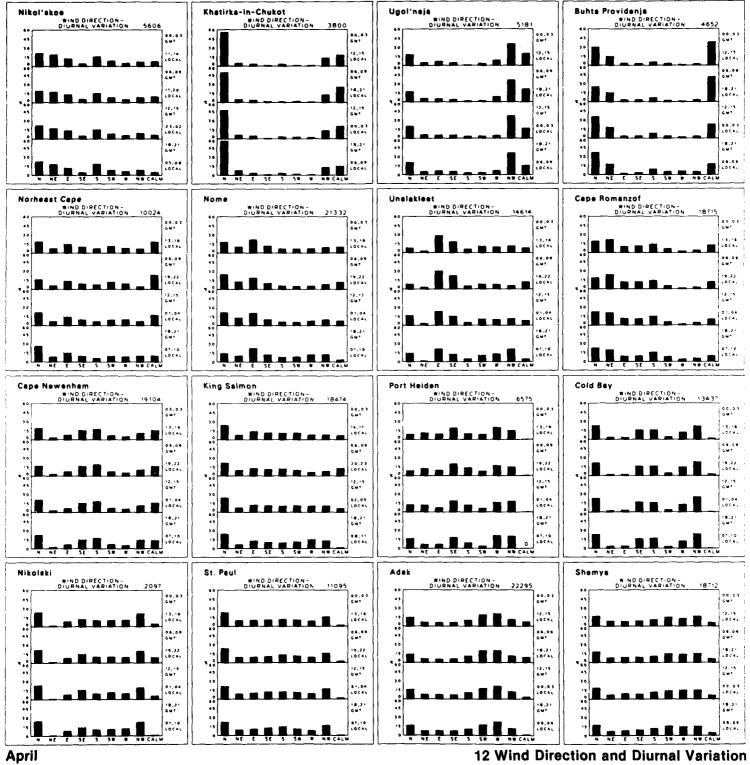


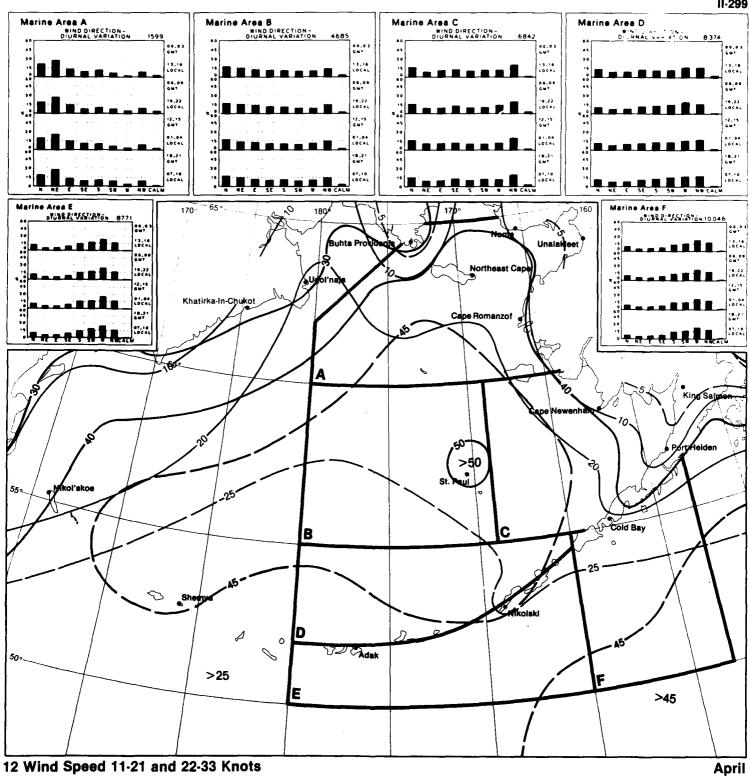
March

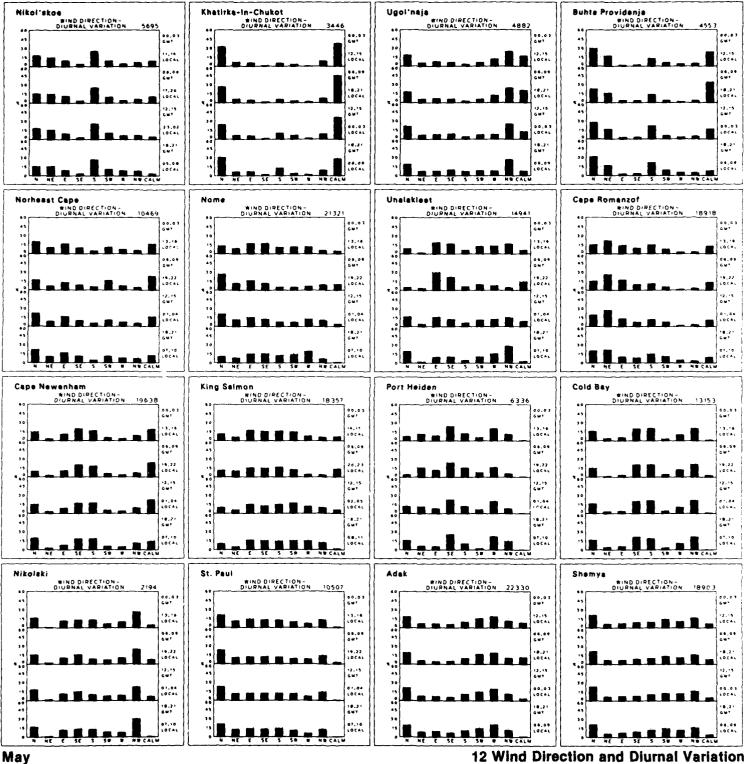
12 Wind Direction and Diurnal Variation

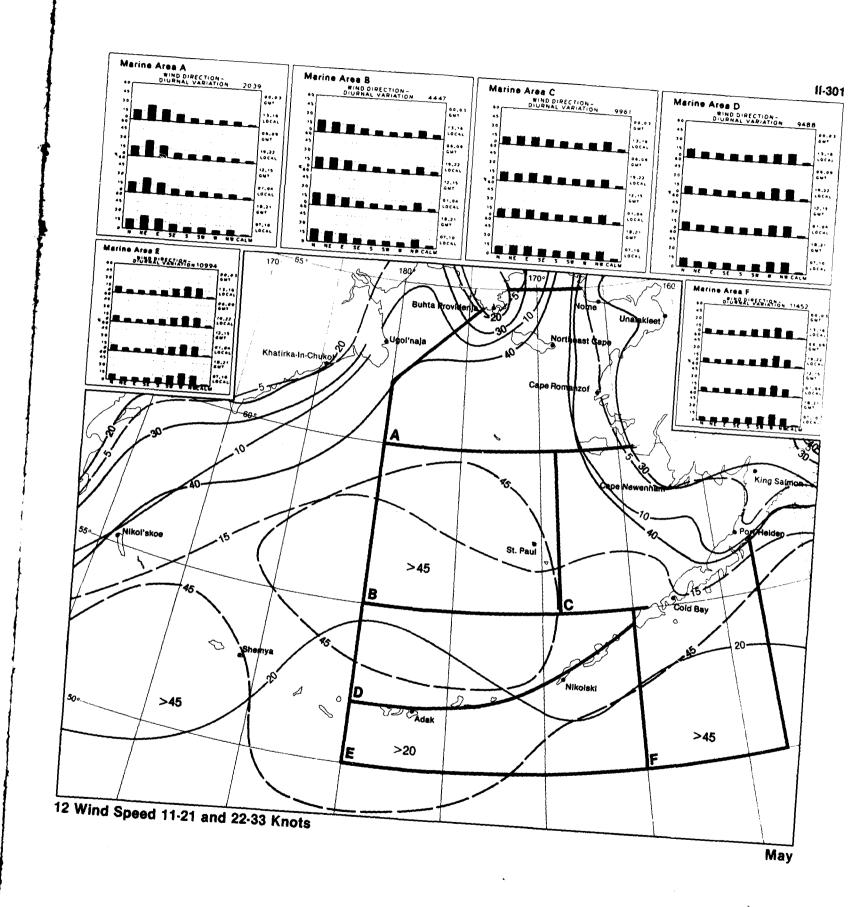


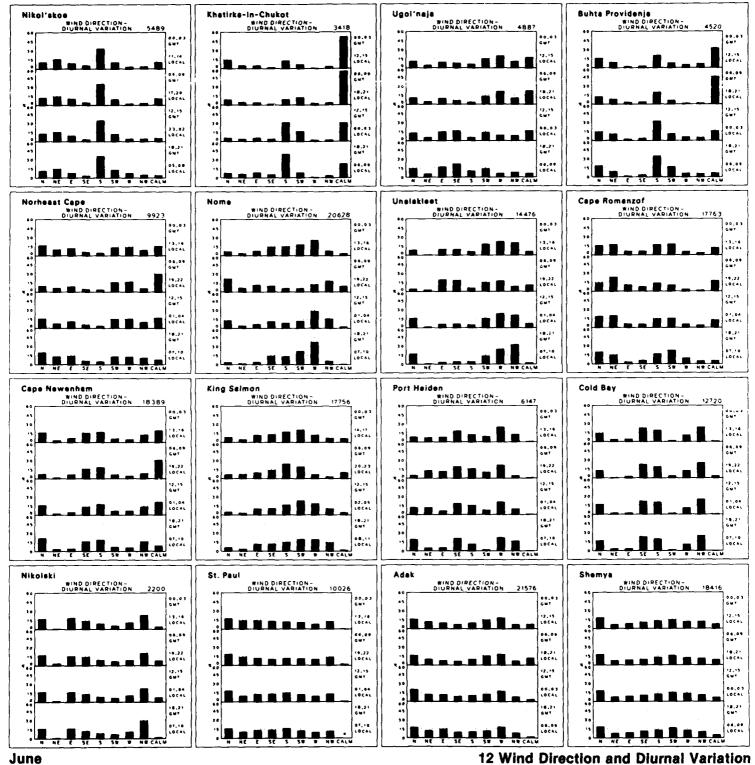
12 Wind Speed 11-21 and 22-33 Knots

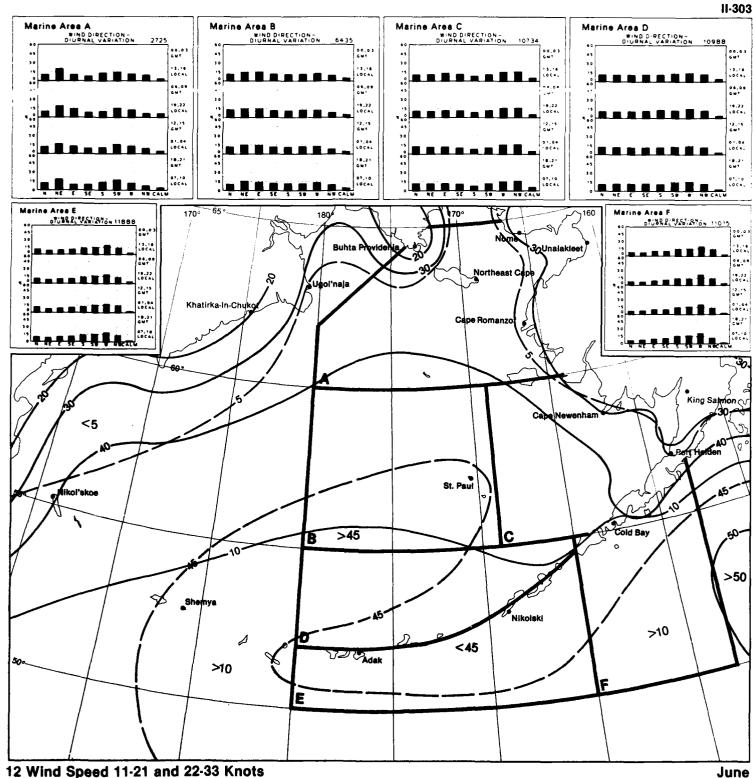




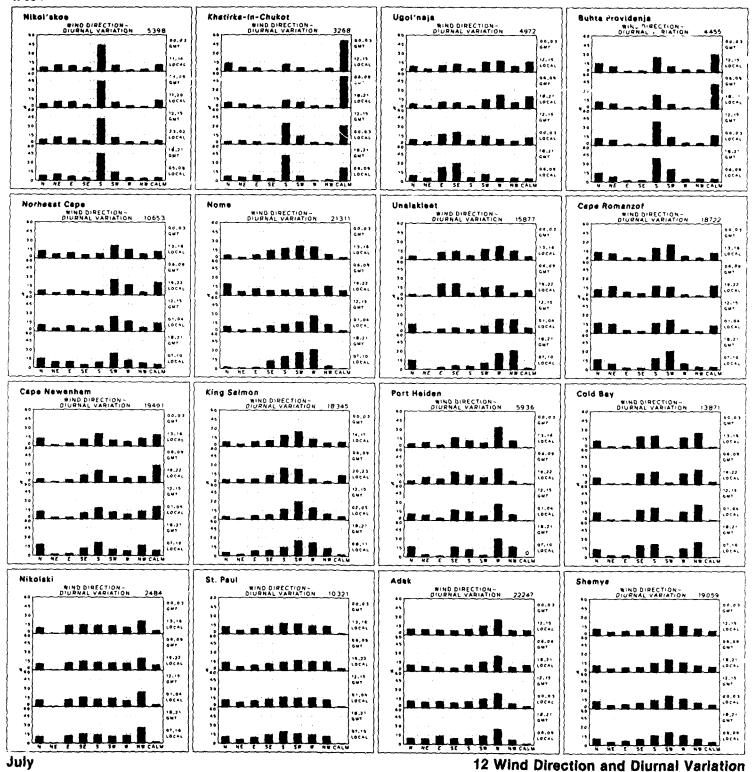


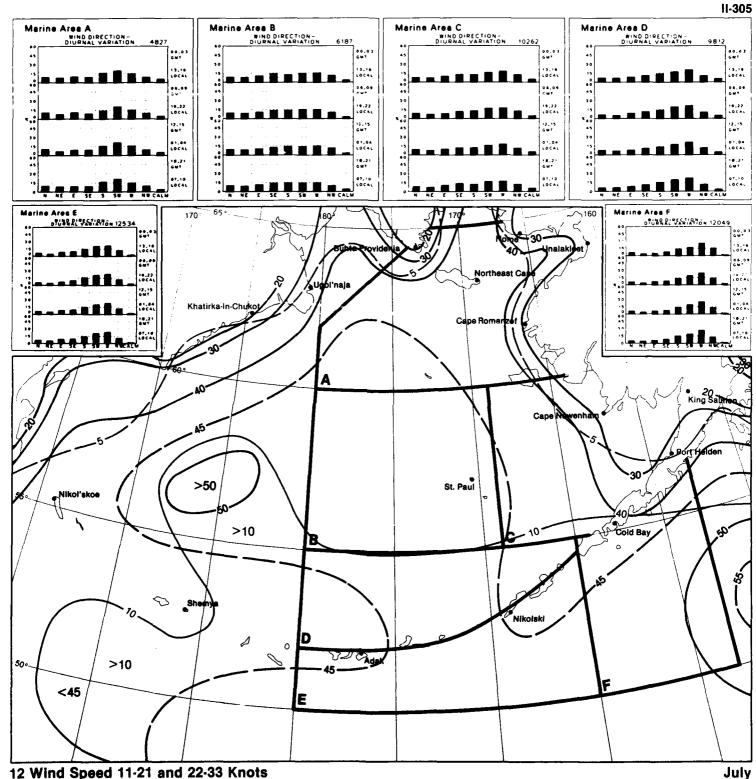


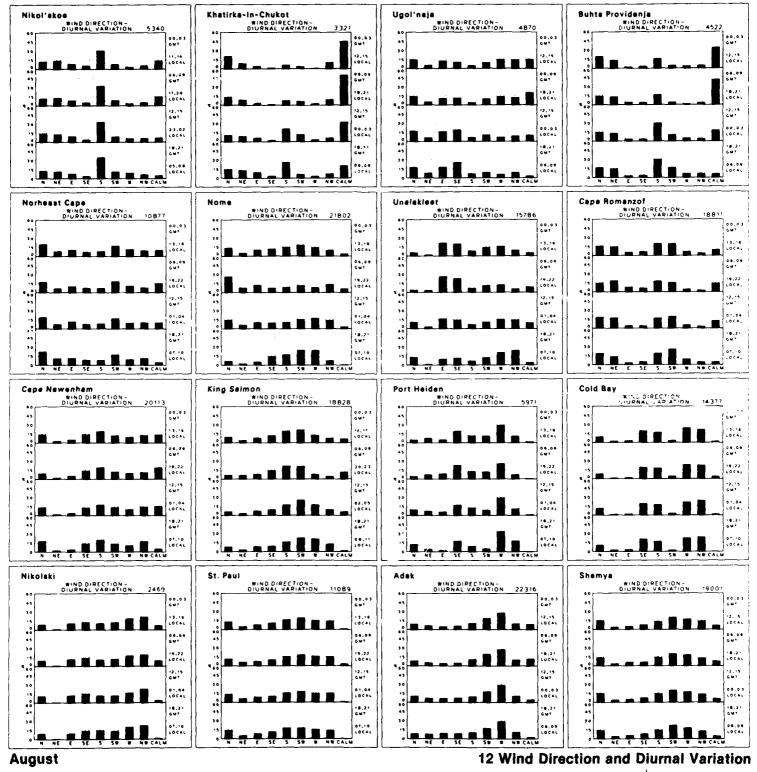




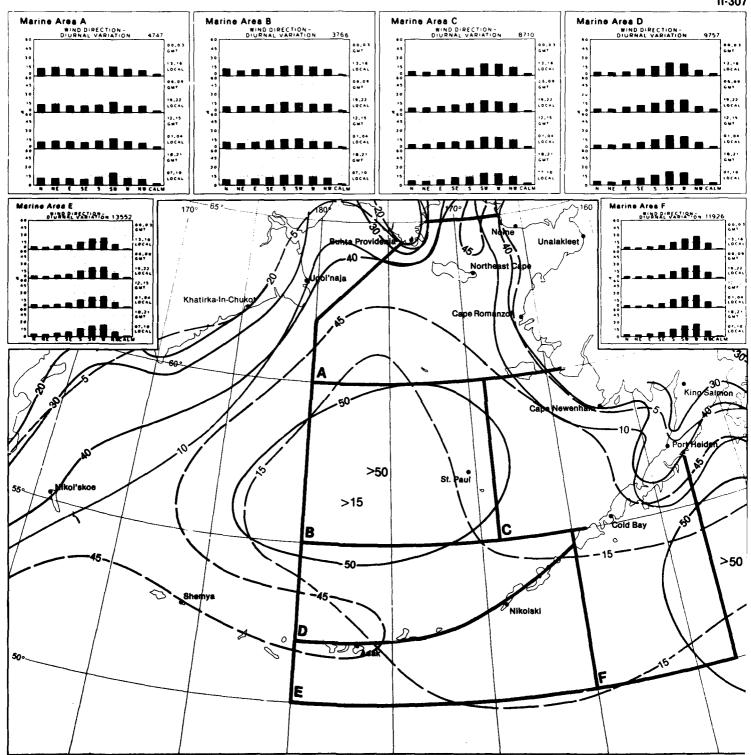




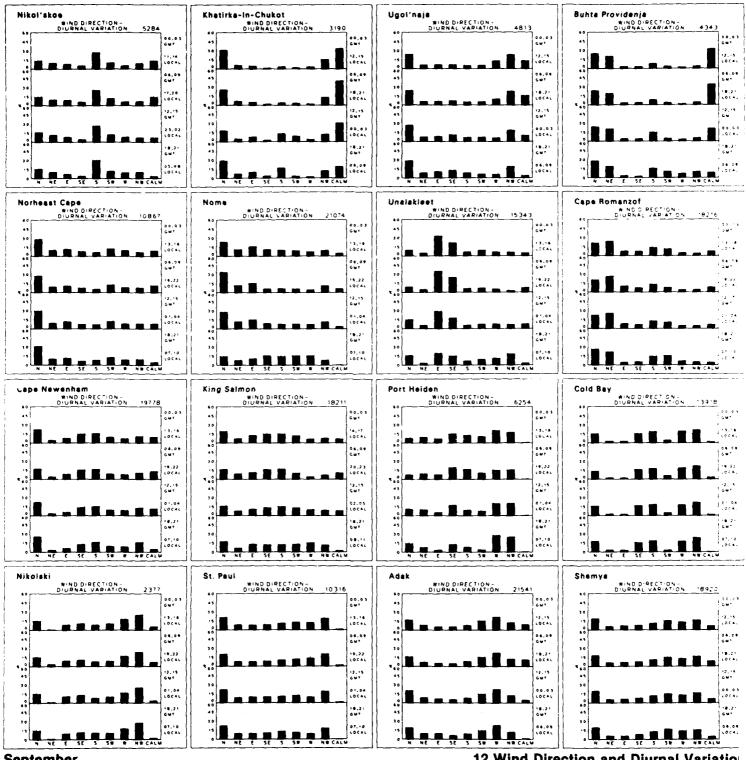




**August** 

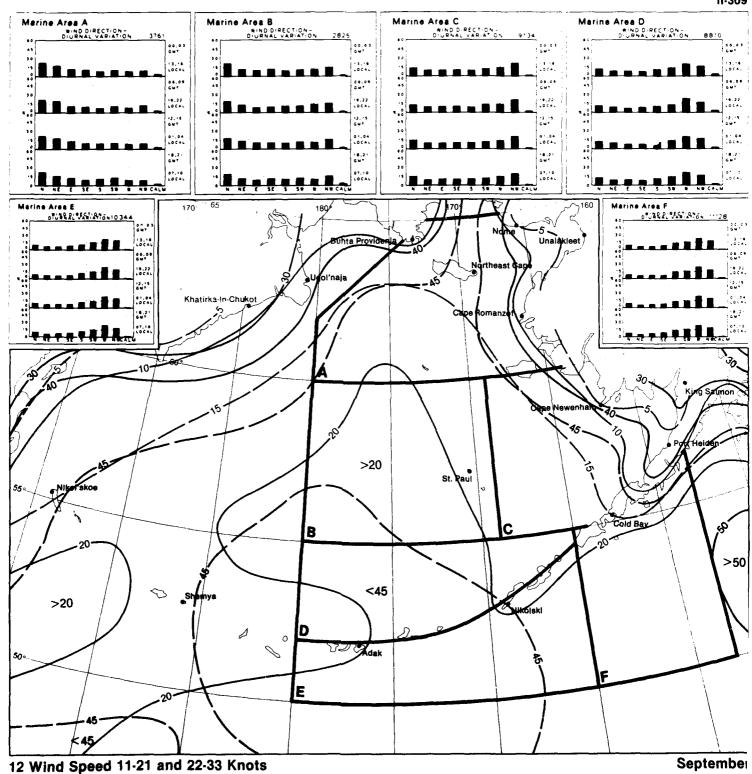


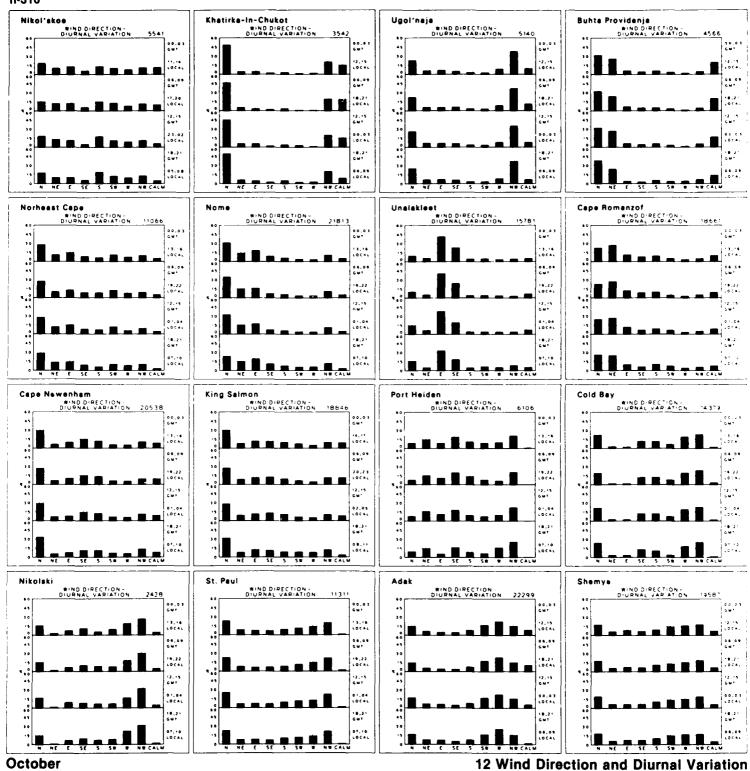
12 Wind Speed 11-21 and 22-33 Knots

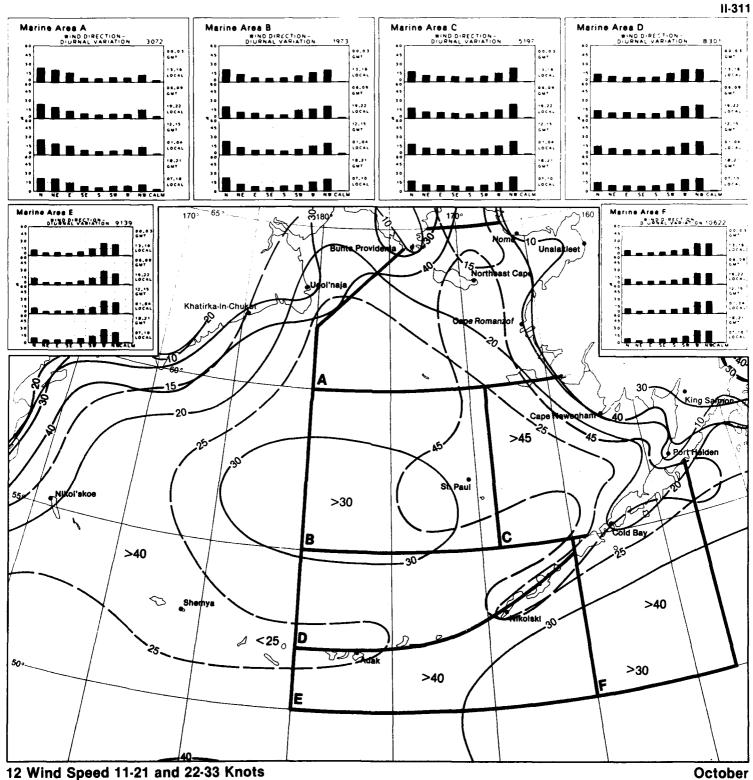


September

12 Wind Direction and Diurnal Variation

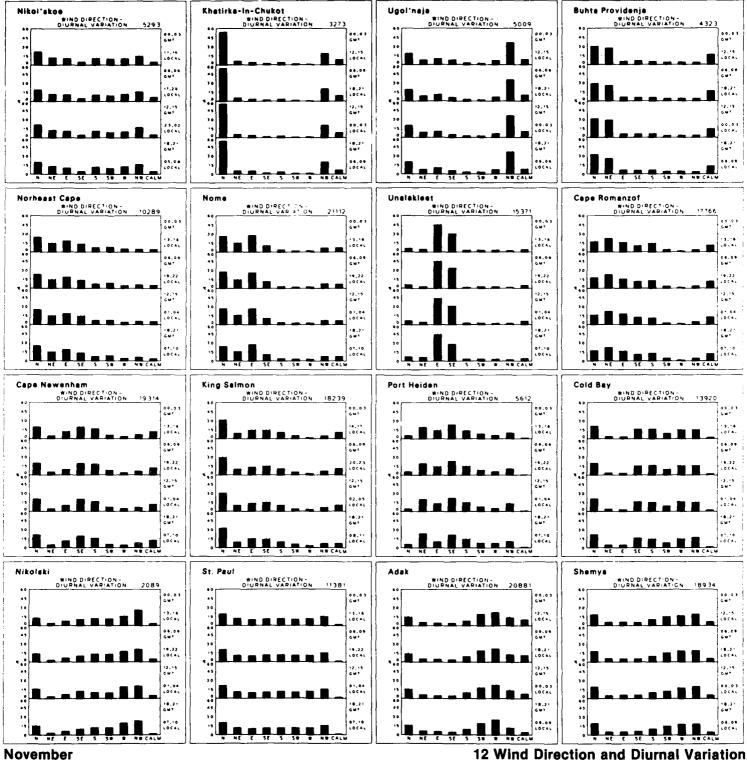


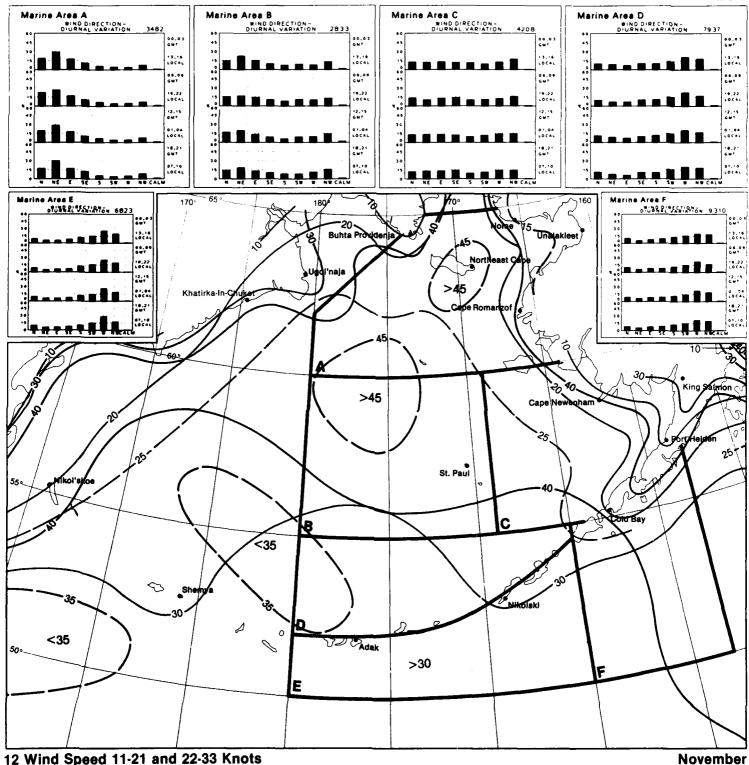




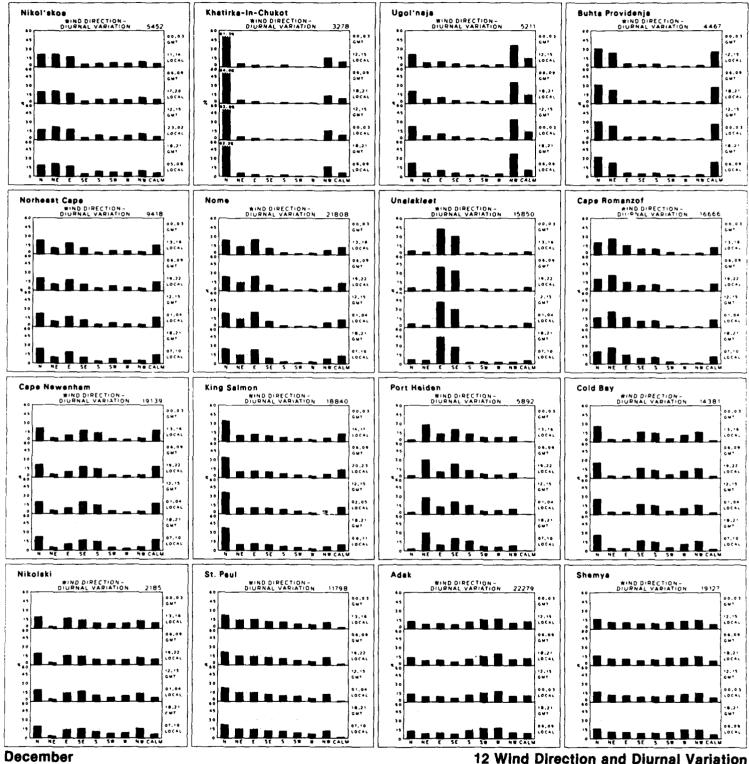
12 Wind Speed 11-21 and 22-33 Knots

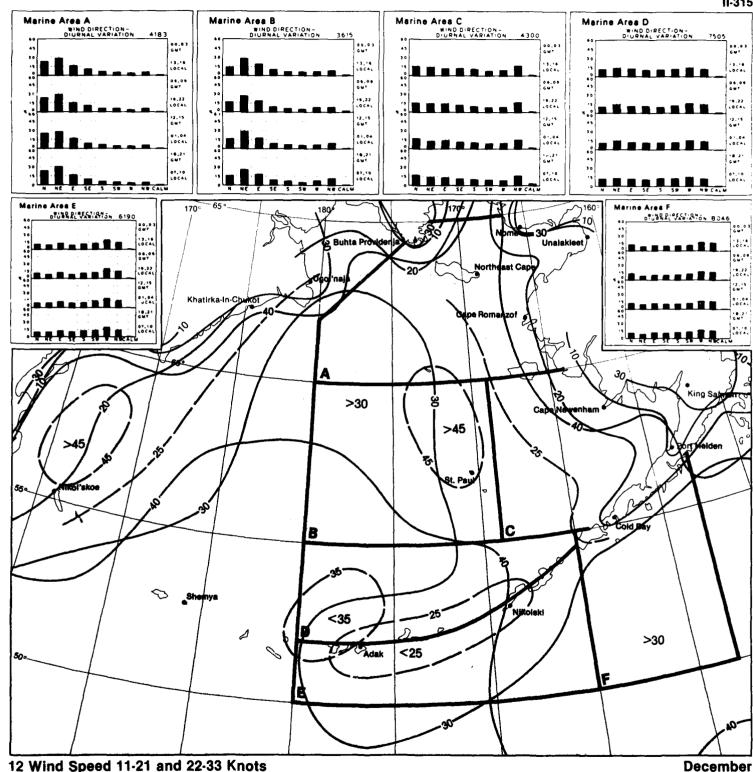
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12 Wind Speed 11-21 and 22-33 Knots





12 Wind Speed 11-21 and 22-33 Knots

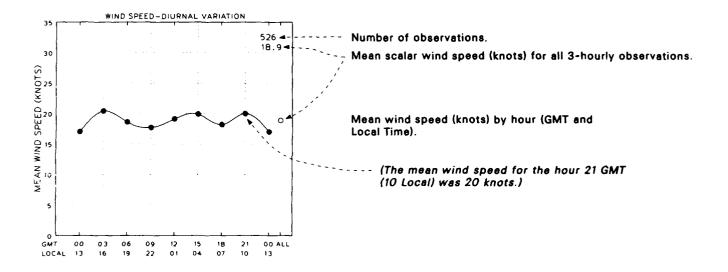
## Map 13. Scalar mean wind speed and wind chill temperature ≤-30°C

BLACK LINE - Mean scalar wind speed (knots).

BLUE LINE – Percent frequency of wind chill temperature  $\leq -30^{\circ}$ C ( $\leq -22^{\circ}$ F).

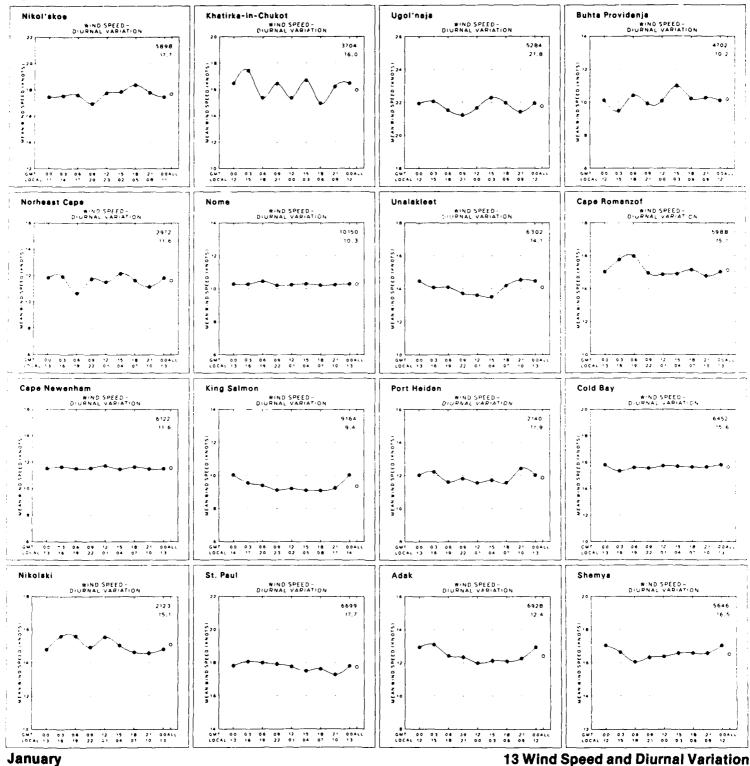
Albers Equal-Area Conic Projection

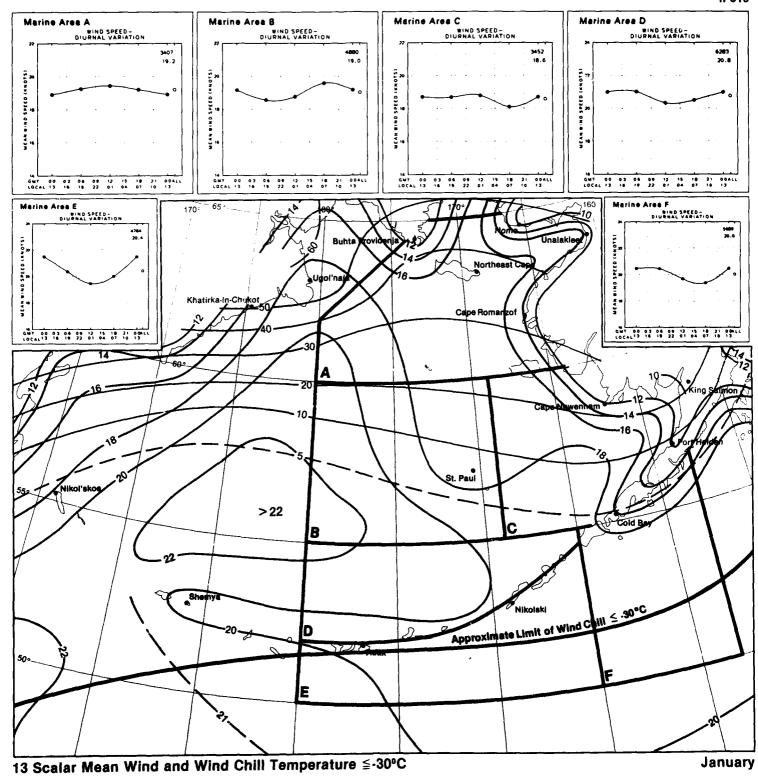
## Graphs: Wind speed/diurnal variation

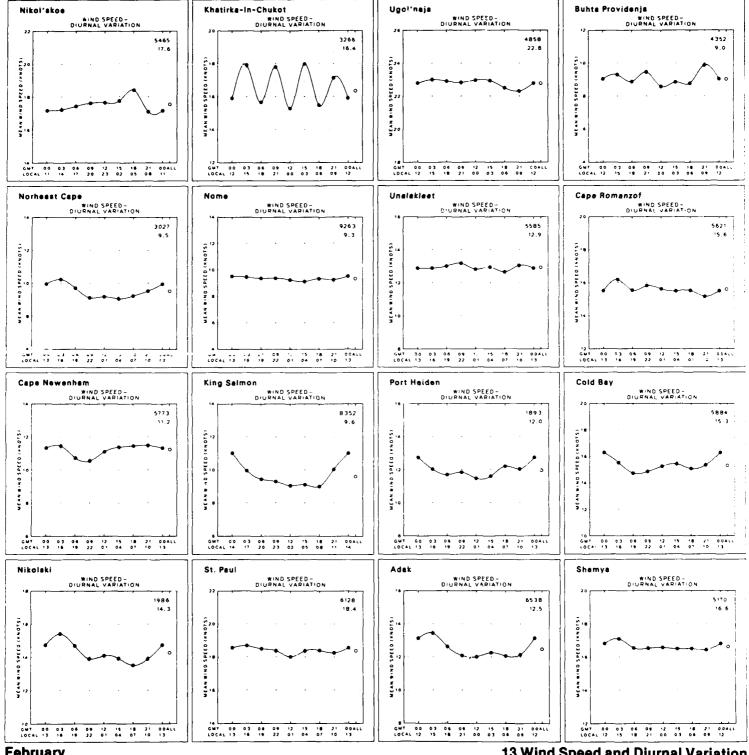


In areas of high persistence (also called constancy, steadiness) of direction, the magnitude of the vector mean wind (Set 10) should closely approach that of the scalar mean wind (set 13). As most of the marine observations are recorded at six-hour intervals (00, 06, 12, 18 GMT), intermediate hours (03, 09, 15, 21 GMT) were not plotted on the graphs for the marine areas. Intermediate hours were plotted for the stations, but users should use caution in interpreting plots for those few stations that reported less than eight observations per day—see the data inventory in the introductory text for Section II.

13 Legend 13

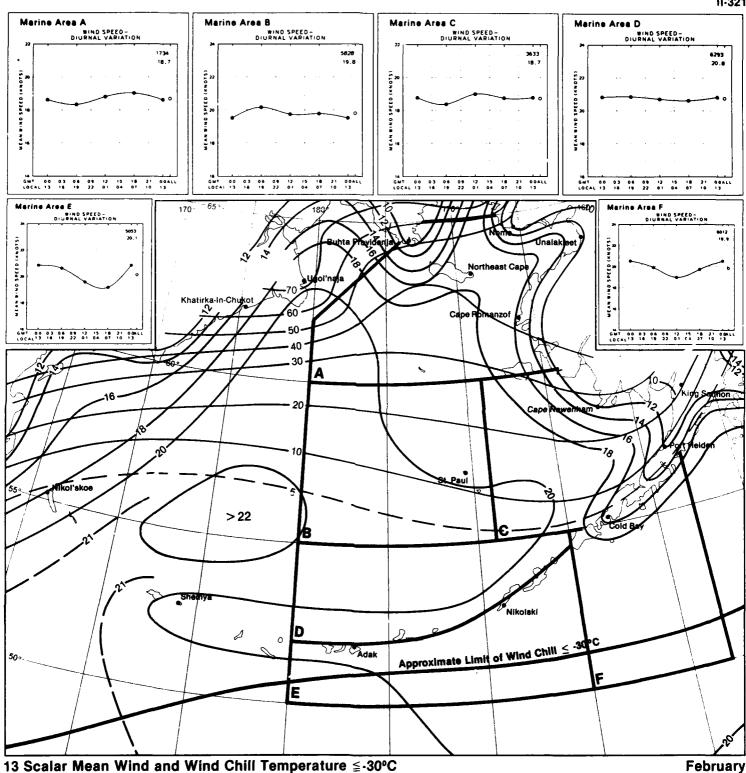




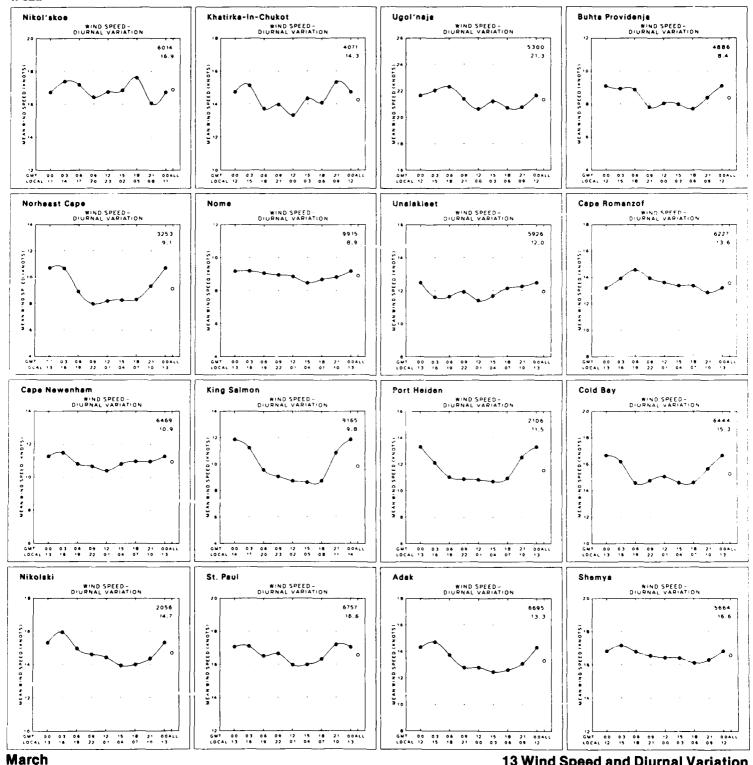


**February** 

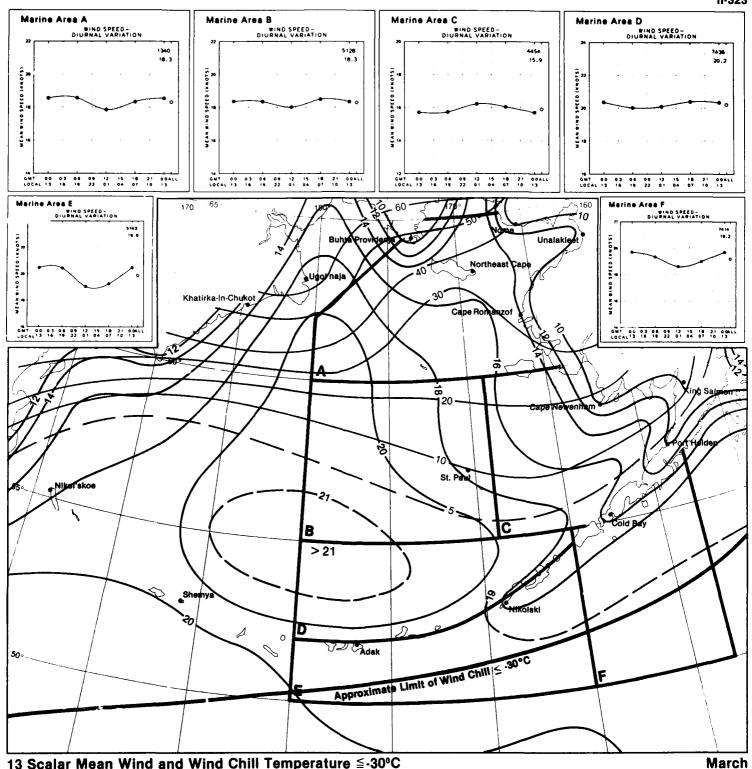
13 Wind Speed and Diurnal Variation



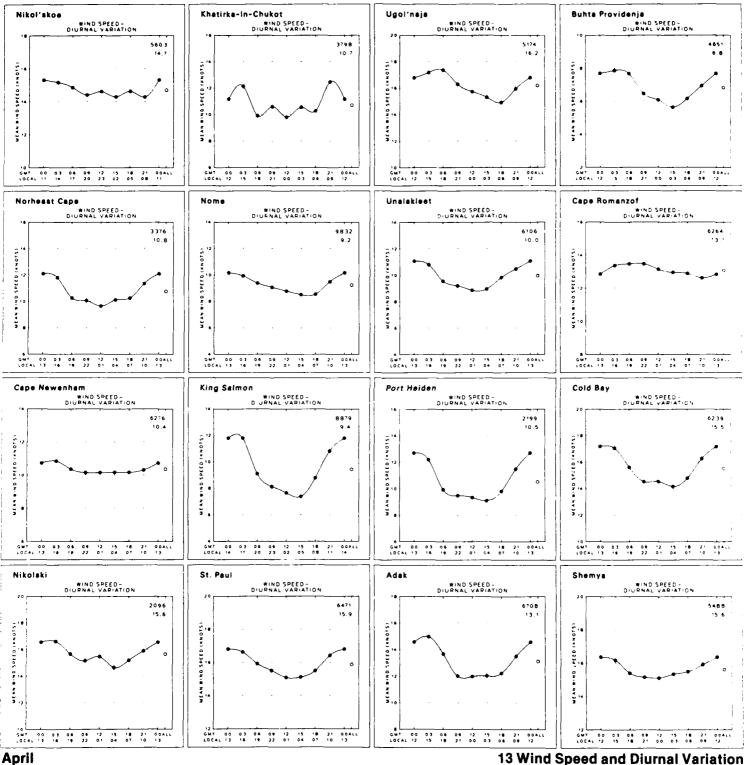
13 Scalar Mean Wind and Wind Chill Temperature ≤ -30°C



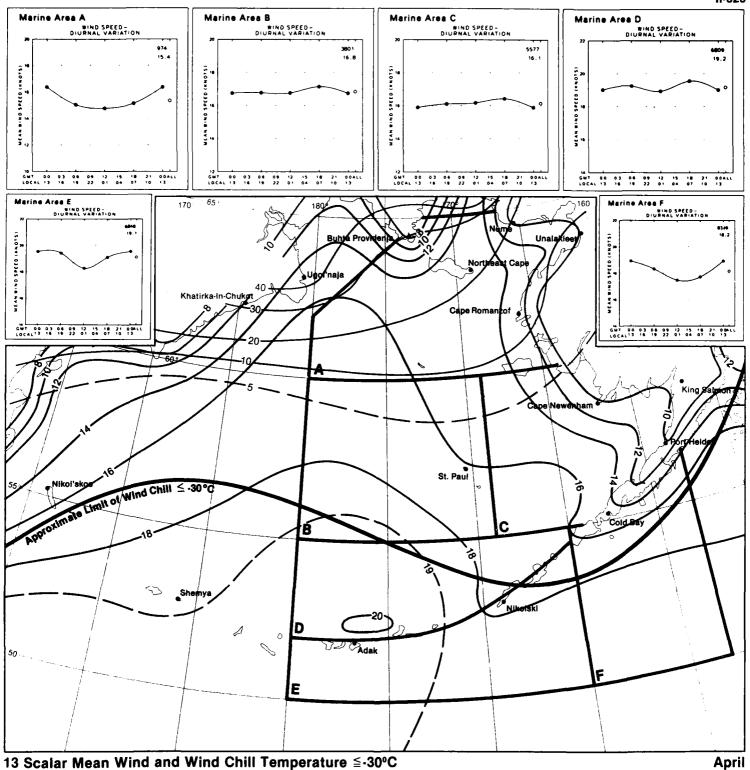
13 Wind Speed and Diurnal Variation



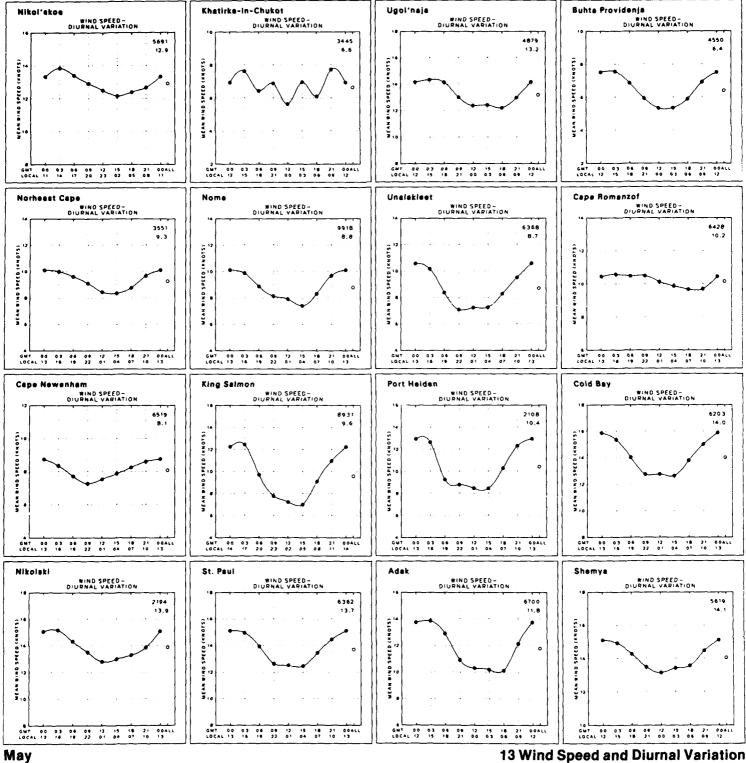
13 Scalar Mean Wind and Wind Chill Temperature ≦-30°C



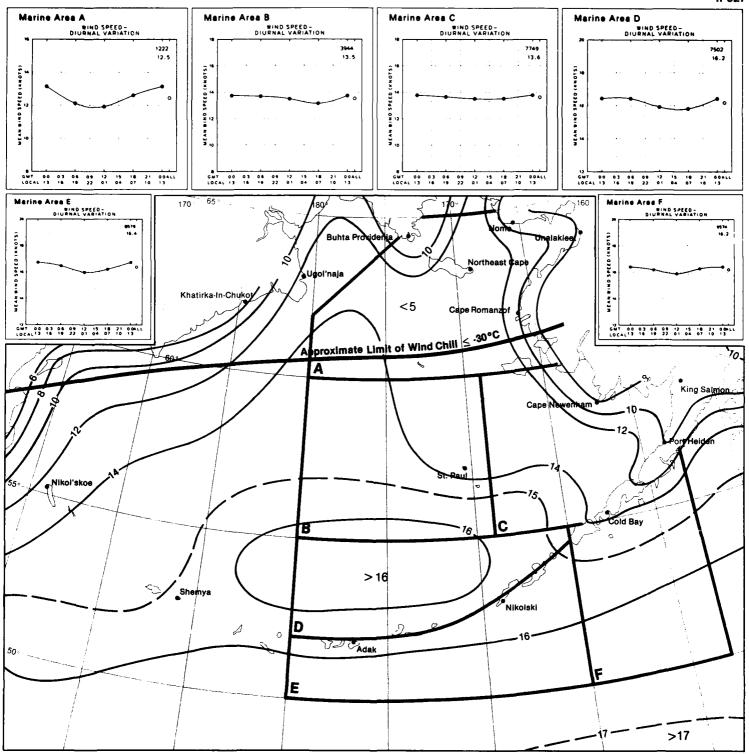
13 Wind Speed and Diurnal Variation



13 Scalar Mean Wind and Wind Chill Temperature ≤-30°C

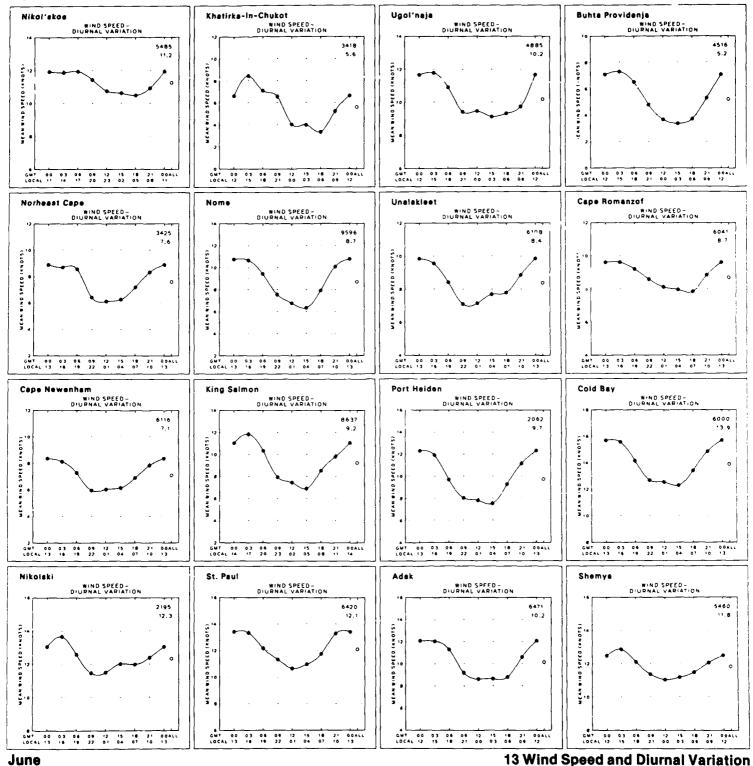


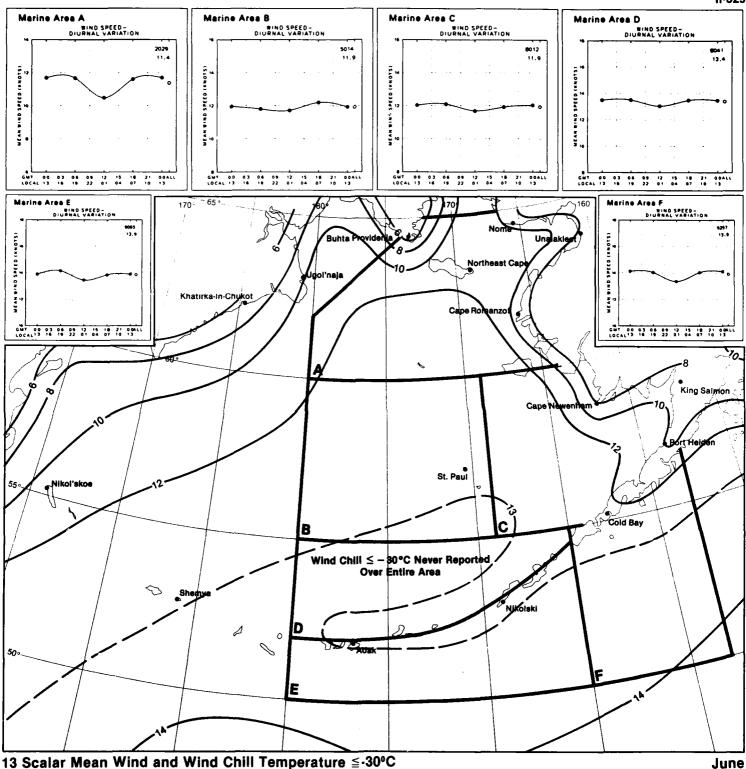
13 Wind Speed and Diurnal Variation



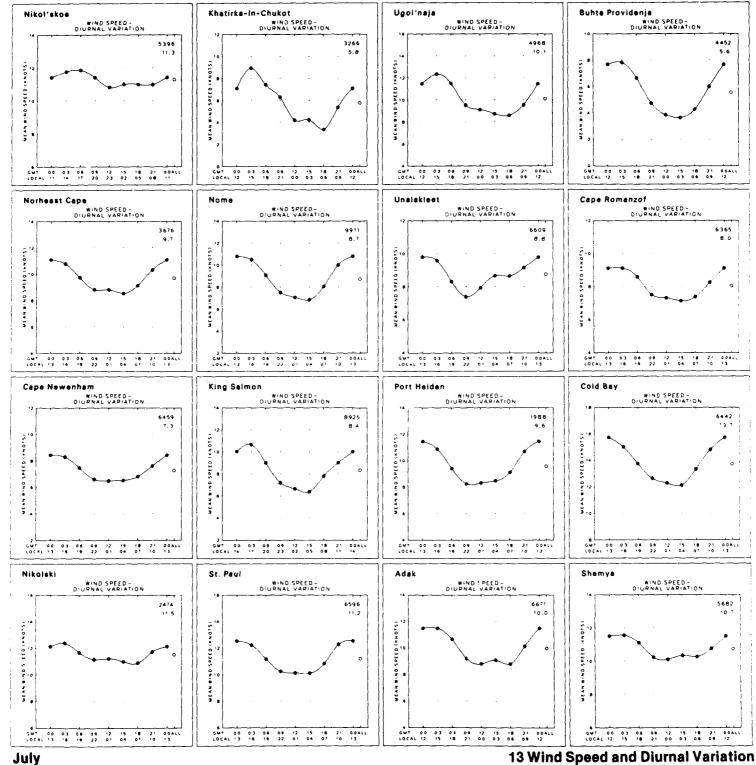
13 Scalar Mean Wind and Wind Chill Temperature ≤-30°C

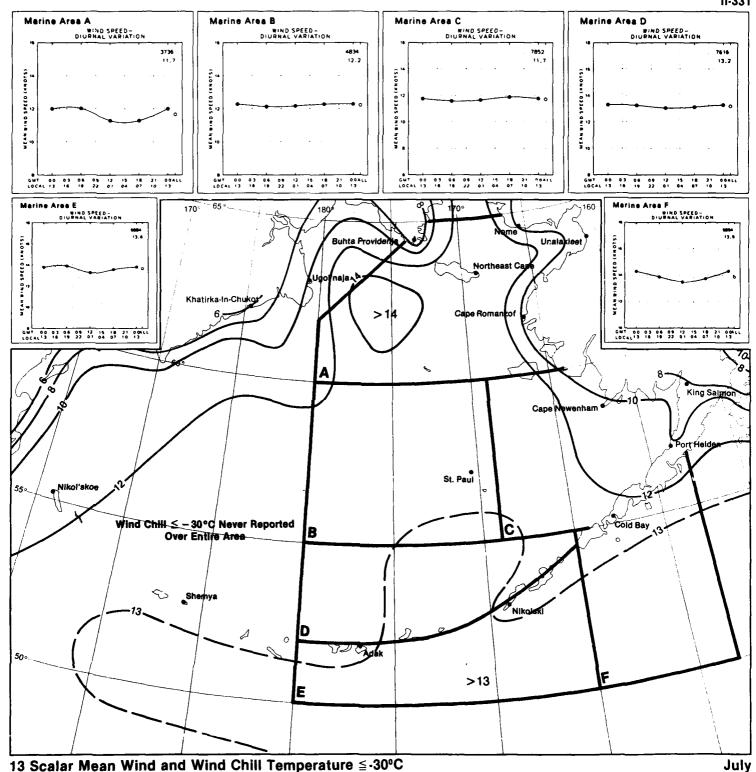
May



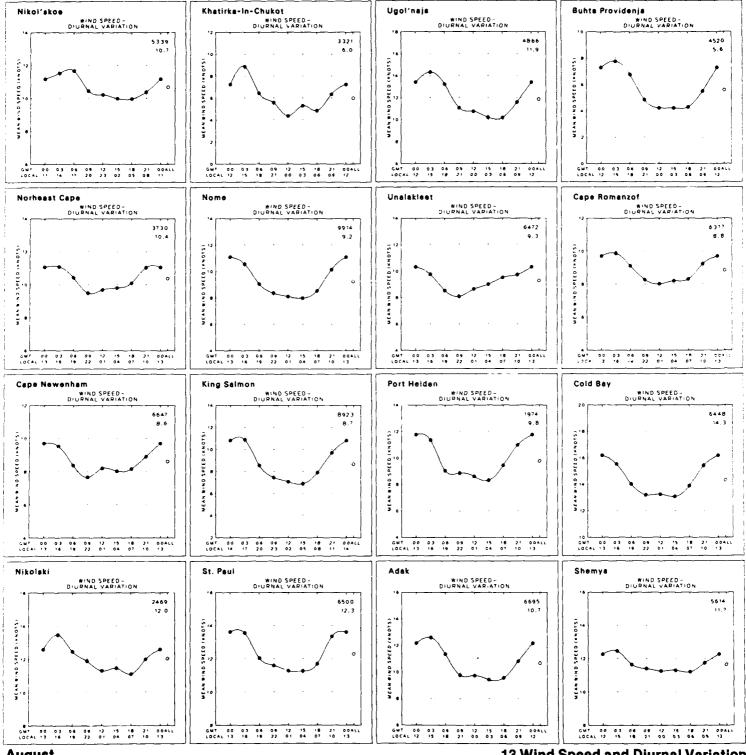


13 Scalar Mean Wind and Wind Chill Temperature ≦-30°C

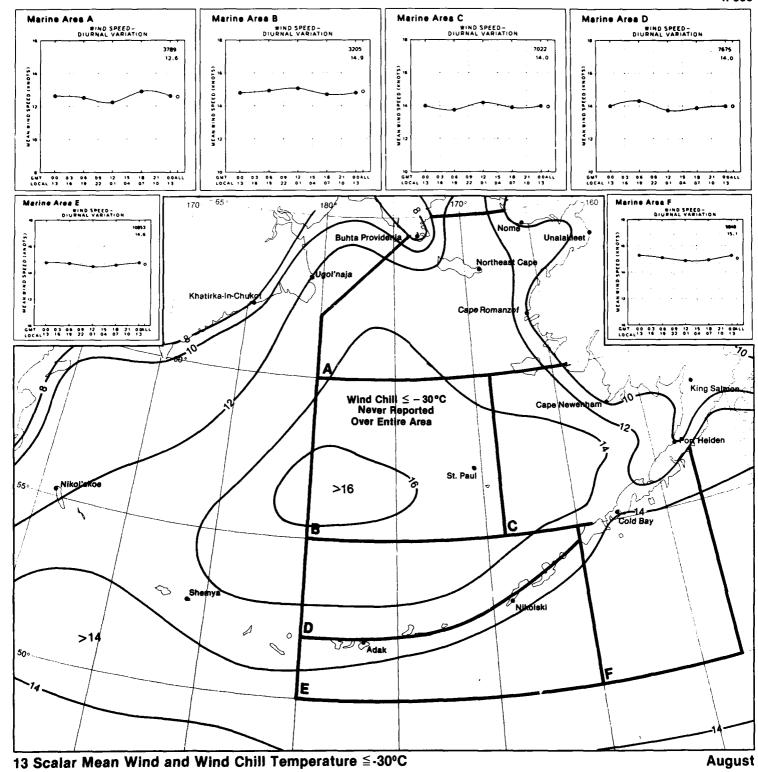


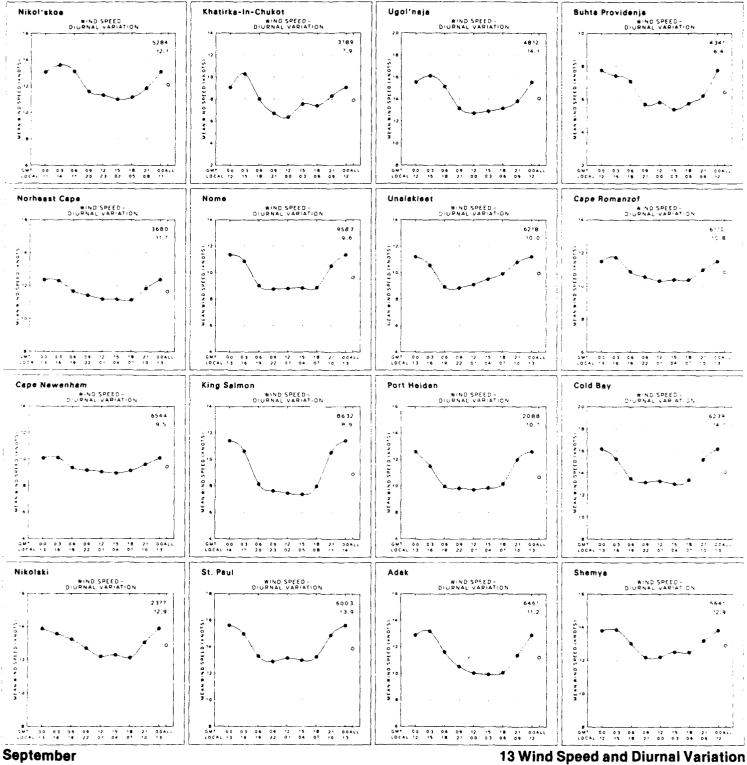


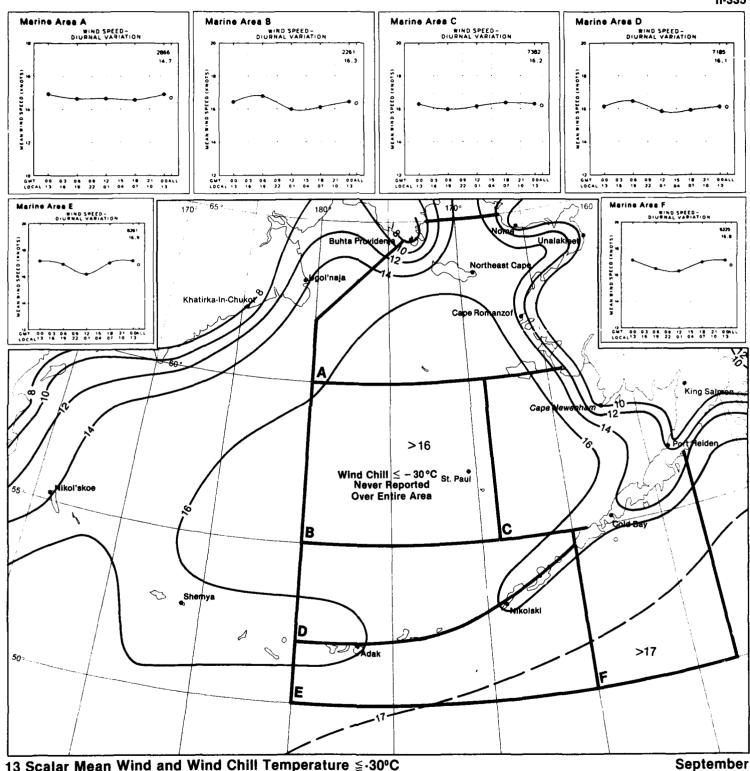
13 Scalar Mean Wind and Wind Chill Temperature ≤ -30°C



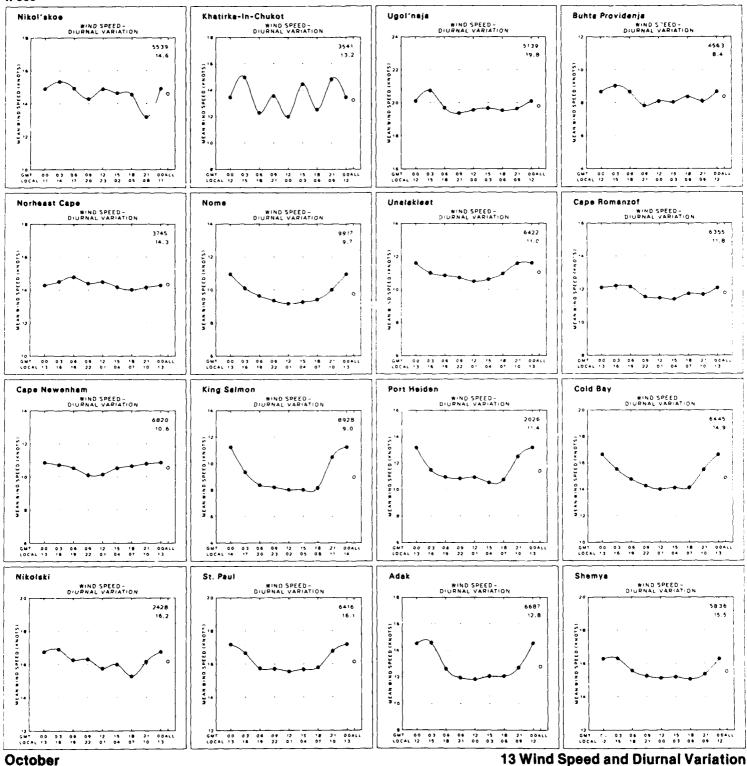
**August** 13 Wind Speed and Diurnal Variation



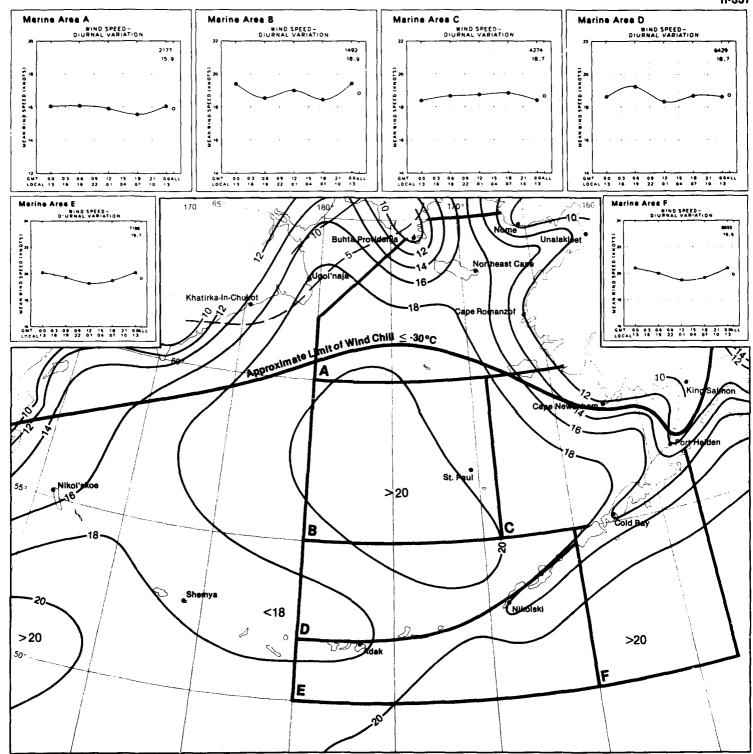




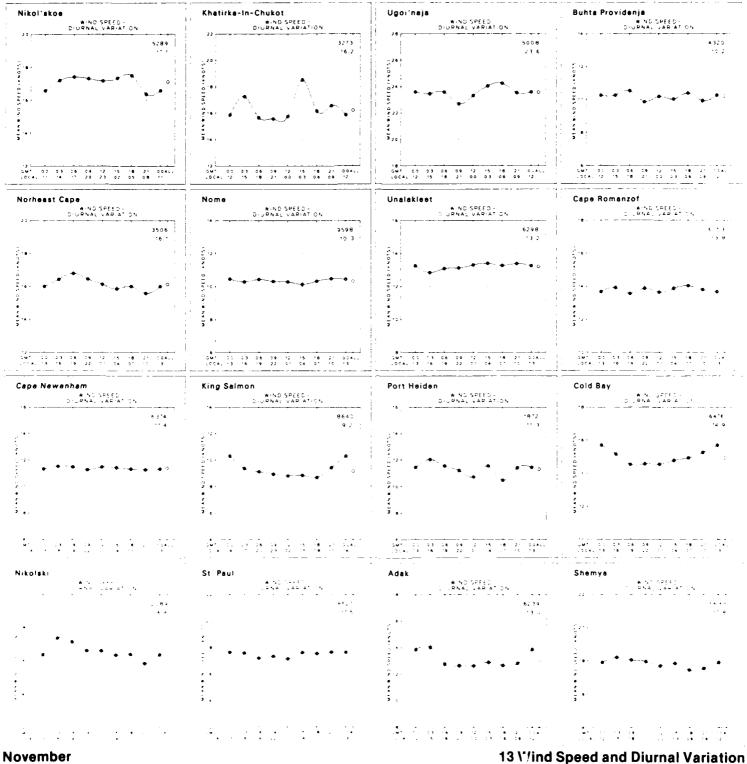
13 Scalar Mean Wind and Wind Chill Temperature ≨-30°C

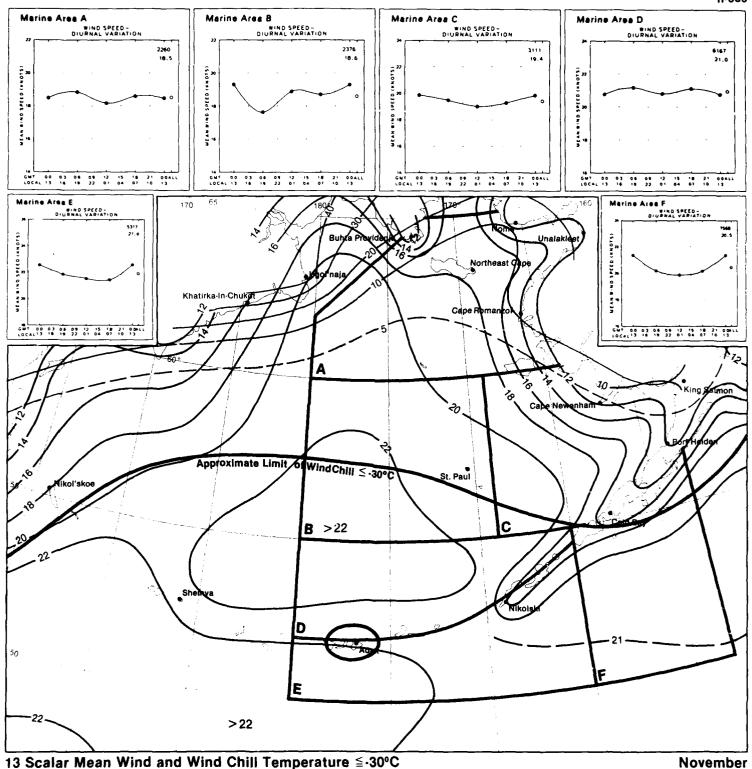


October

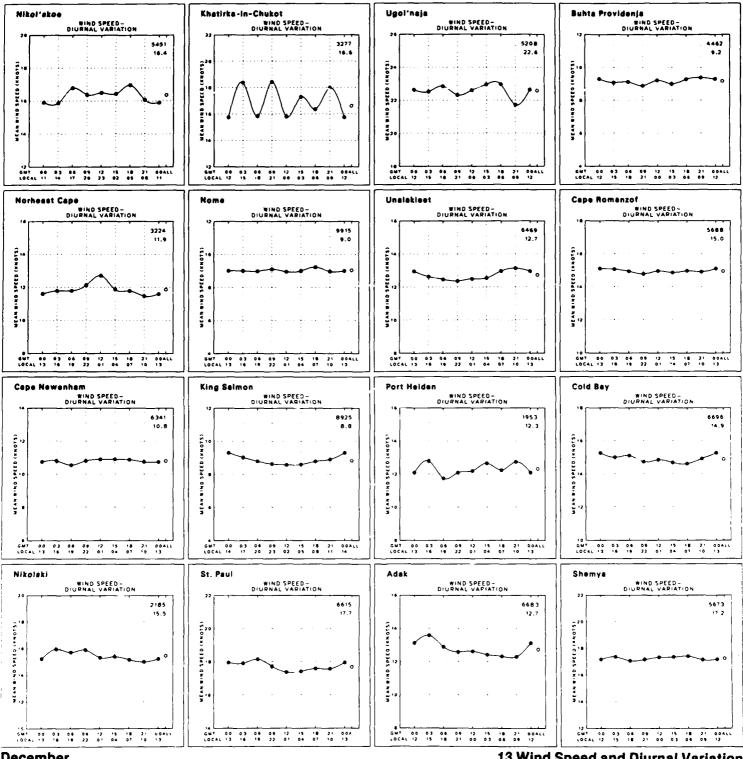


13 Scalar Mean Wind and Wind Chill Temperature ≦ ⋅ 30°C



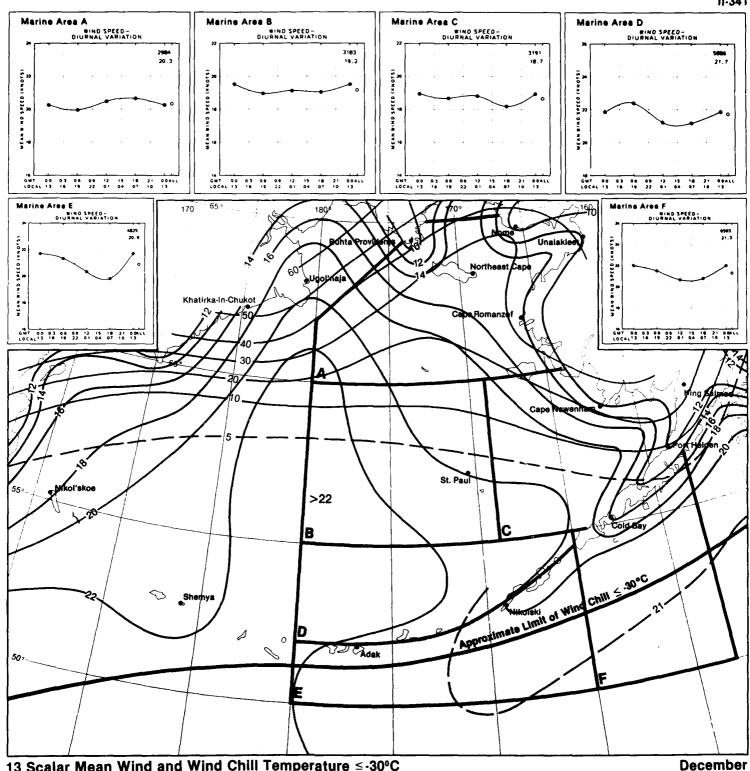


13 Scalar Mean Wind and Wind Chill Temperature ≤ -30°C



December

13 Wind Speed and Diurnal Variation

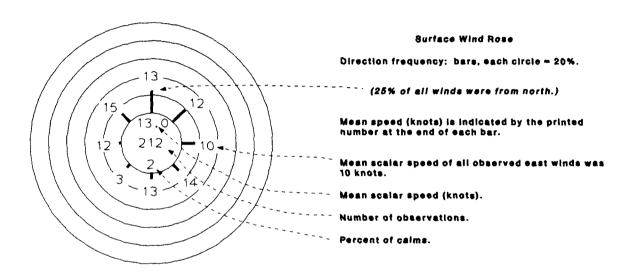


13 Scalar Mean Wind and Wind Chill Temperature ≦-30°C

# Map 14. Wind speed and direction

ROSE - Percent frequency of wind observations by direction (8-points).

Albers Equal-Area Conic Projection



Wind is measured in terms of velocity, a vector that gives both wind speed and direction. *True wind* is the wind that is experienced by an observer standing still. When the ship is moving, an observer experiences what is termed an *apparent wind*. The speed and course of the ship must be eliminated from the apparent wind to obtain the true wind, which is needed for meteorological purposes. Wind estimated from the appearance of the sea surface is a true wind, while wind determined by the appearance of the ship's rigging or by a shipboard anemometer is an apparent wind. True wind direction may be estimated by observing the direction from which ripples, small waves, and sea spray are coming, since they run with the wind. The direction from which the waves are coming is most easily found by sighting along the wave crests and then turning 90° to face the advancing waves. The observer is then facing the direction from which the waves are coming. The direction is determined to the nearest 10° with respect to true north. The true wind speed is the average speed of the wind blowing near the sea surface. Information in the following table is used to estimate the true wind speed based upon the condition of the sea surface. Refer to the text in Set 11 for additional descriptive information on winds.

14 Legend

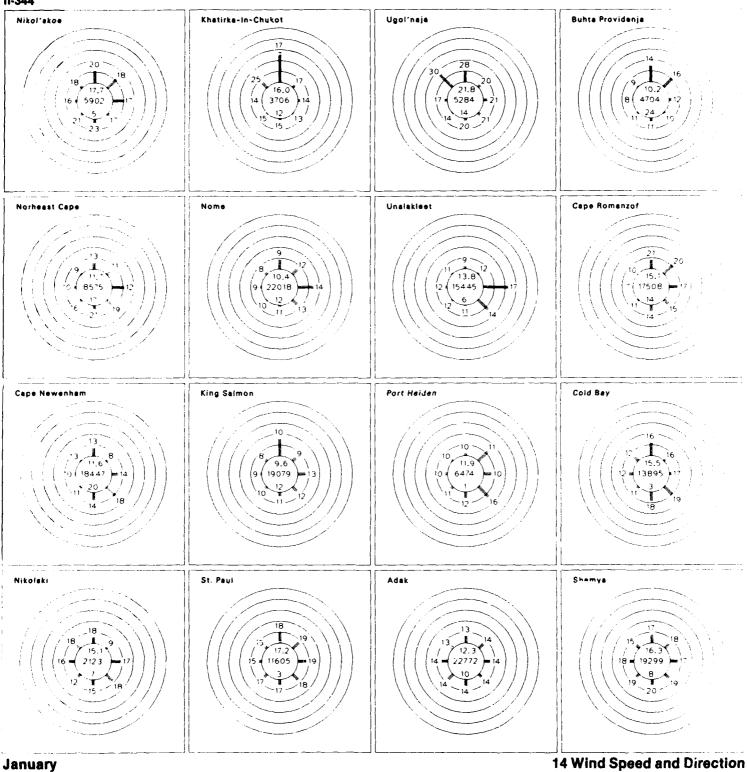
Legend 14

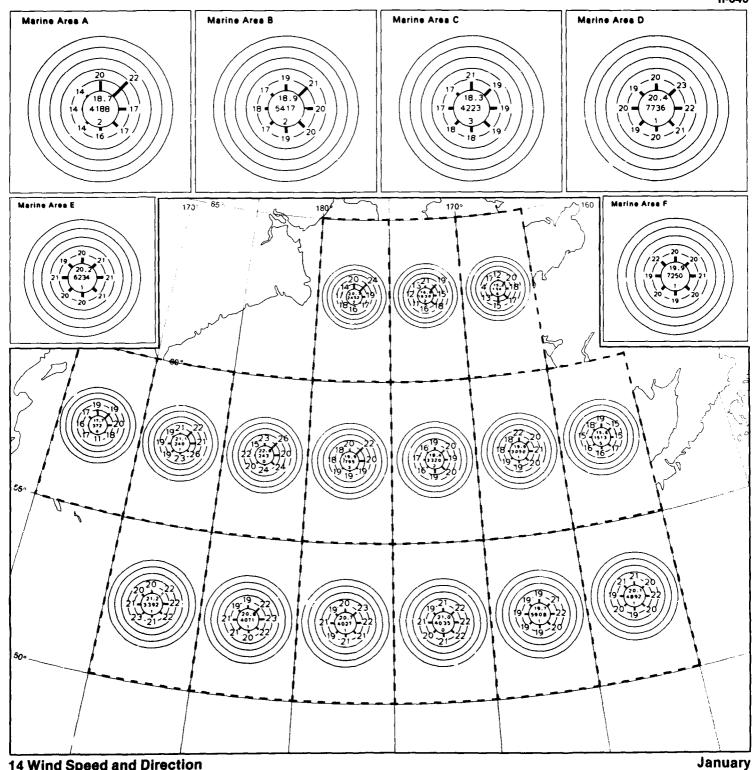
# WIND SPEED IN KNOTS (WMO Code, 1982)

This table is based on sea conditions ov deep water with a fully developed sea. There will be frequent cases where the sea will not be fully developed bacause the wind has not blown long enough over a sufficient distance (fetch). Other factors such as currents and water depth will also affect the look of the sea.

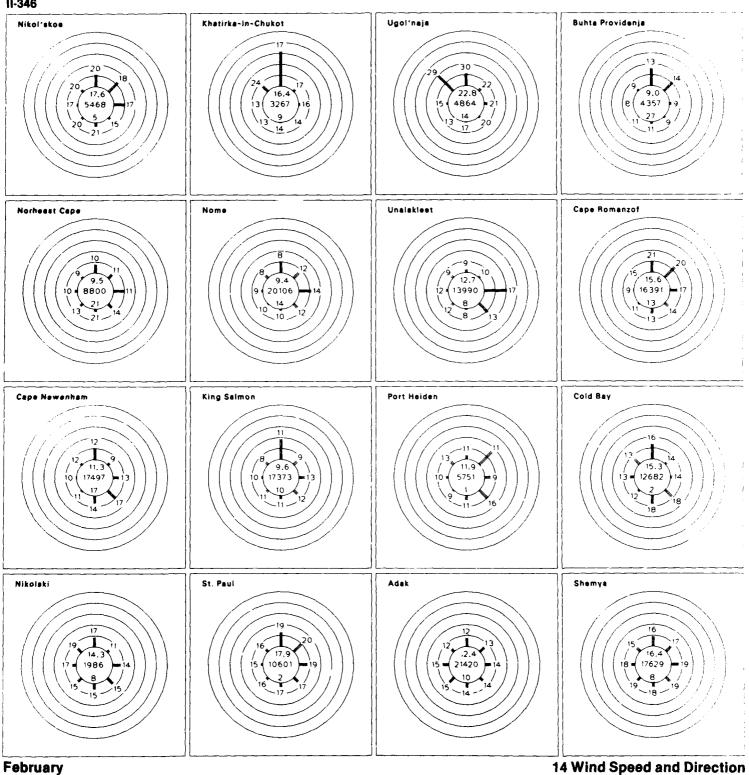
Code figs. (Knots)	Beaufort 0	<b>Description</b> Calm	Sea criterion when sea fully developed  Sea like a mirror	Probable ht. of waves in m (ft)			
				Average		Maximum	
				-			~
01-03	1	Light air	Ripples with the appearance of scales are formed, but without foam crests	0.1	(%)	0.1	('+)
04-06	2	Light breeze	Small wavelets, still short but more pronounced, crests have a glassy appearance and do not break	0.2	(½)	0.3	(1)
07-10	3	Gentle breeze	Large wavelets; crests begin to break: foam of glassy appearance; perhaps scattered white horses	0.6	(2)	1	(3)
11-16	4	Moderate breeze	Small waves, becoming longer; fairly frequent white horses	1	(31/2)	1.5	(5)
17-21	5	Fresh breeze	Moderate waves, taking a more pronounced long form; many white horses are formed (chance of some spray)	2	(6)	2.5	(81/2)
22-27	6	Strong breeze	Large waves begin to form; white foam crests are more extensive everywhere (probably some spray)	3	(9 <sup>1</sup> / <sub>2</sub> )	4	(13)
28-33	7	Near gale	Sea heaps up and white foam from breaking waves begins to be blown in streaks along the direction of the wind	4	(13½)	5.5	(19)
34-40	8	Gale	Moderately high waves of greater length: edges of crests begin to break into the spindrift; the foam is blown in well-marked streaks along the direction of the wind	5.5	(18)	7.5	(25)
41-47	9	Strong gale	High waves; dense streaks of foam along the direction of the wind; crests of waves begin to topple, tumble and roll over; spray may affect visibility	7	(23)	10	(32)
48-55	10	Storm	Very high waves with long overhanging crests: the resulting foam, in great patches, is blown in dense white streaks along the direction of the wind; on the whole, the surface of the sea takes on a white appearance; tumbling of the sea becomes heavy and shock-like; visibility affected.	9	(29)	12.5	(41)
58-63	11	Violent Storm	Exceptionally high waves (small and medium-sized ships might be for a time lost to view behind the waves); the sea is completely covered with long white patches of foam lying along the direction of the wind; everywhere the edges of the wave crests are blown into froth; visibility affected	11.5	(37)	16	(52)
64 and over	12	Hurricane	The air is filled with foam and spray; sea completely white with driving spray; visibility very seriously affected	14	(45)	_	xx

Note: For winds over 99 knots, add 50 to dd (direction) and enter the tens and units digits of the wind speed for ff; e.g. for a wind from 100 $^{\circ}$  true at 125 knc.s, dd = 60, and ff  $\approx$  25.

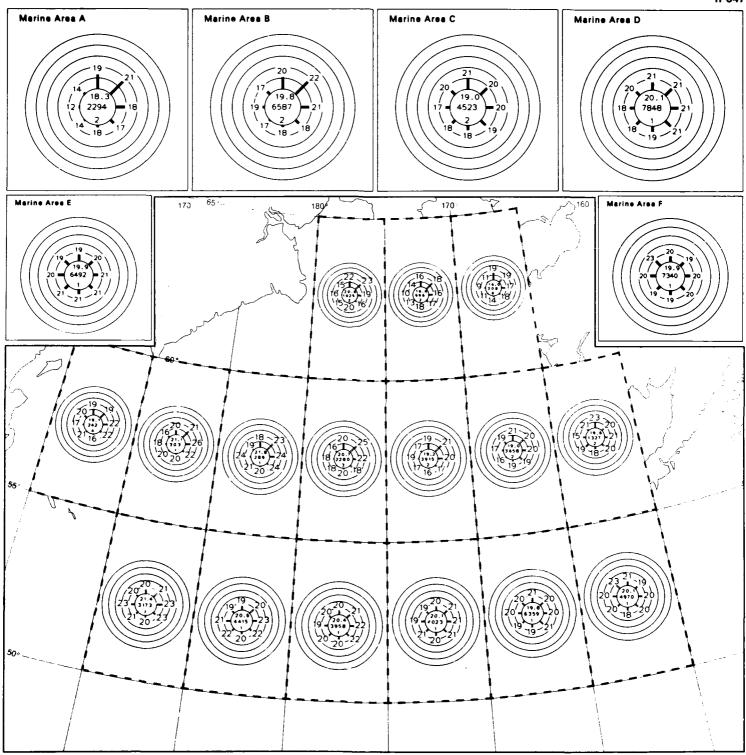




14 Wind Speed and Direction

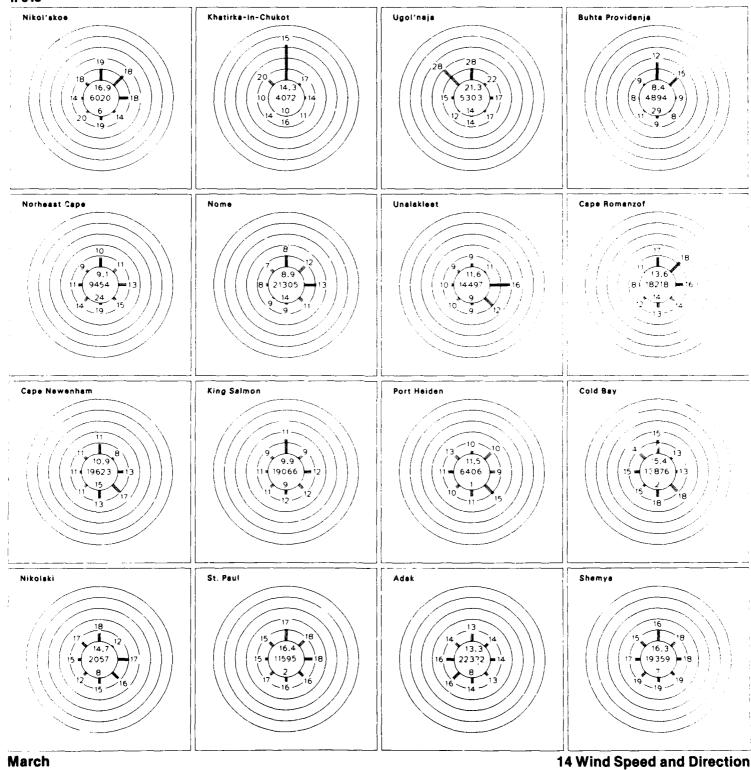


**February** 



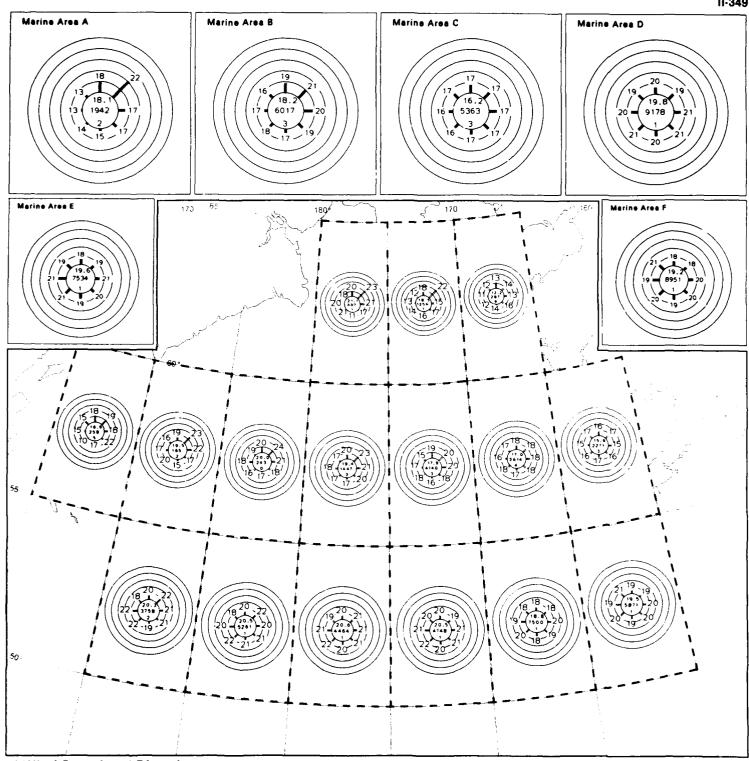
14 Wind Speed and Direction

February



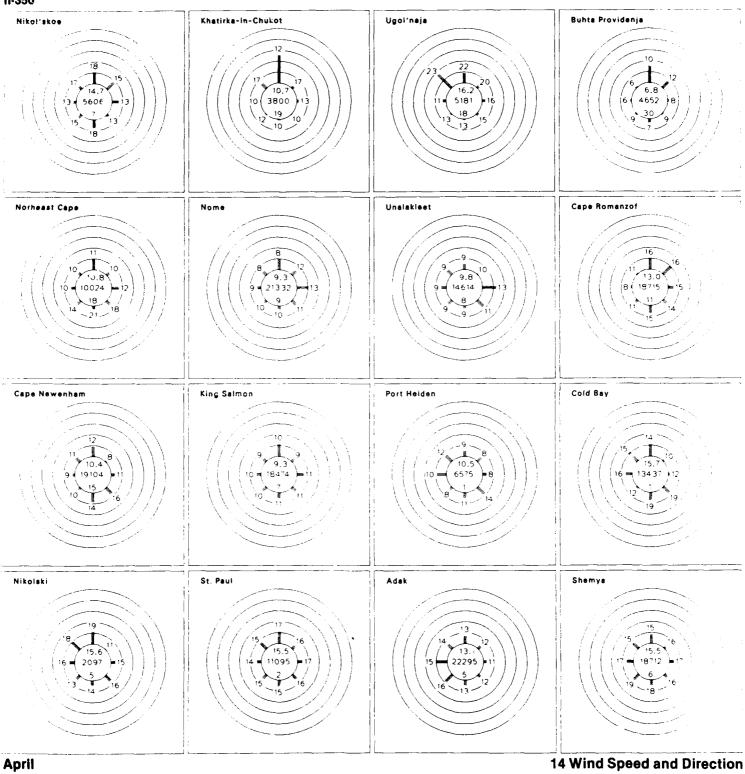
March

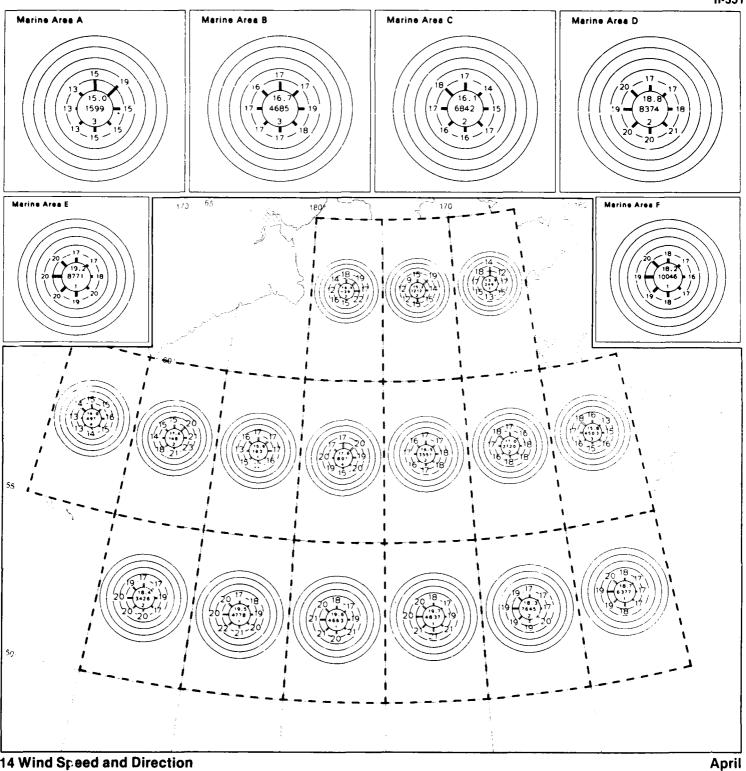
11-349



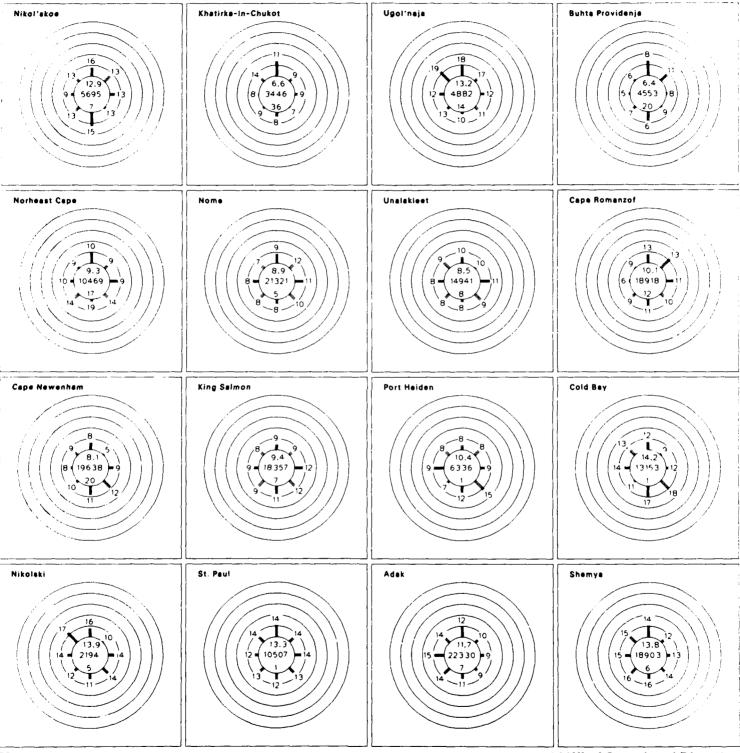
14 Wind Speed and Direction

March



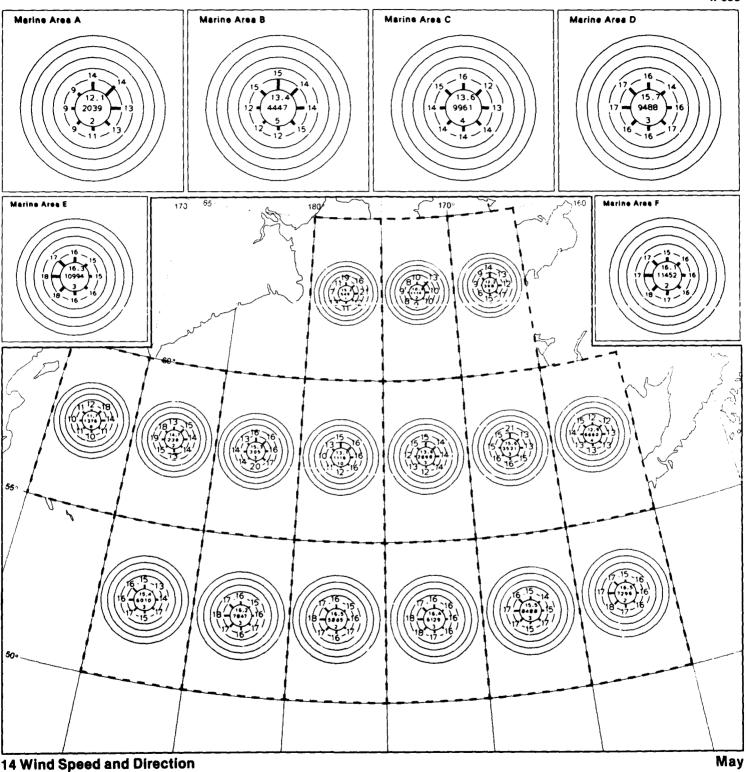


14 Wind Speed and Direction

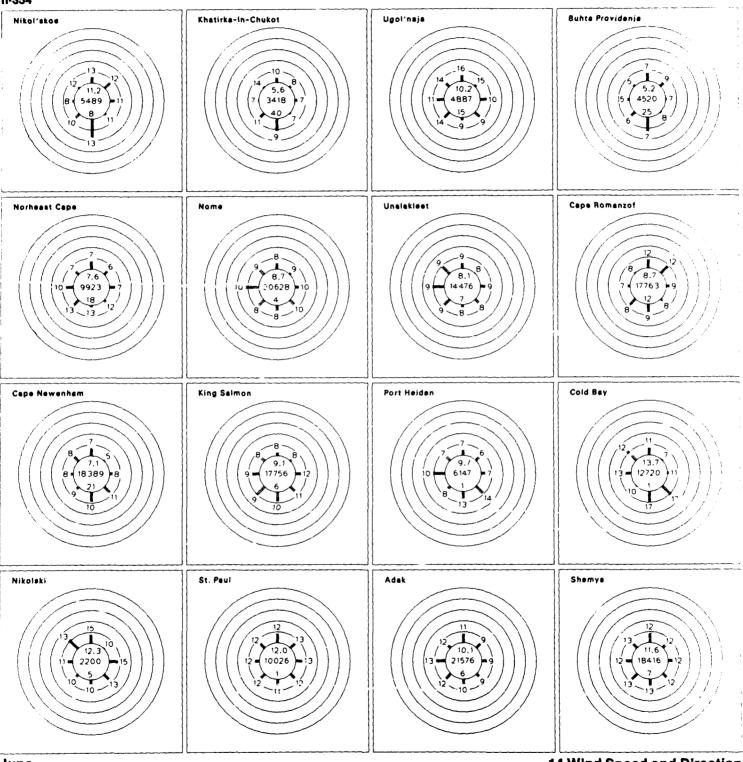


May

14 Wind Speed and Direction

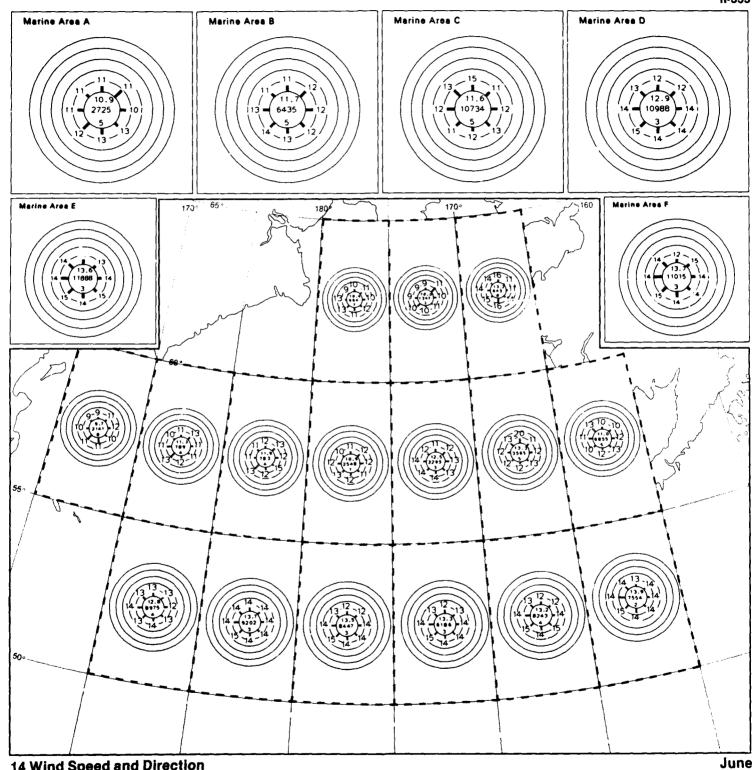


14 Wind Speed and Direction

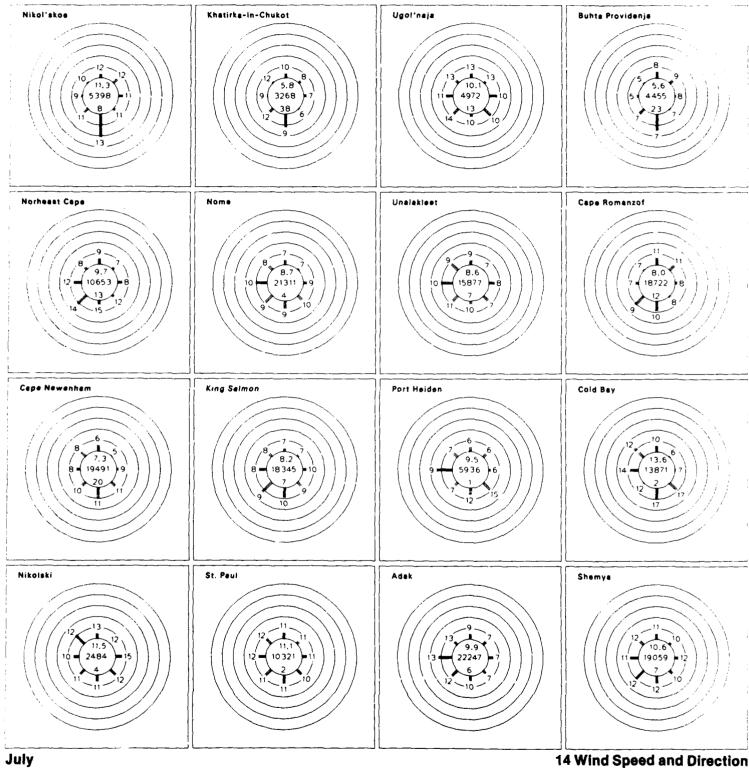


June

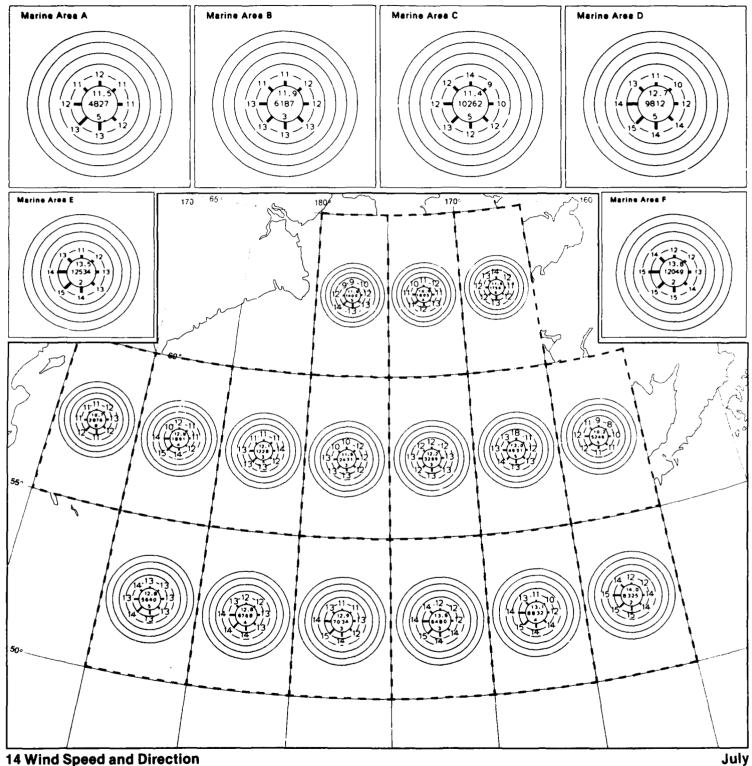
14 Wind Speed and Direction



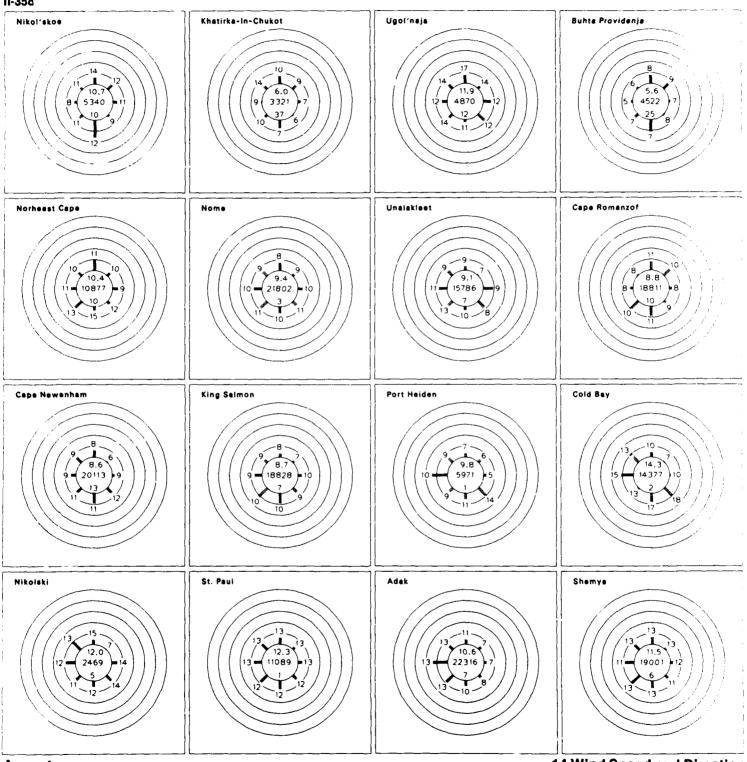
14 Wind Speed and Direction



14 Wind Speed and Direction

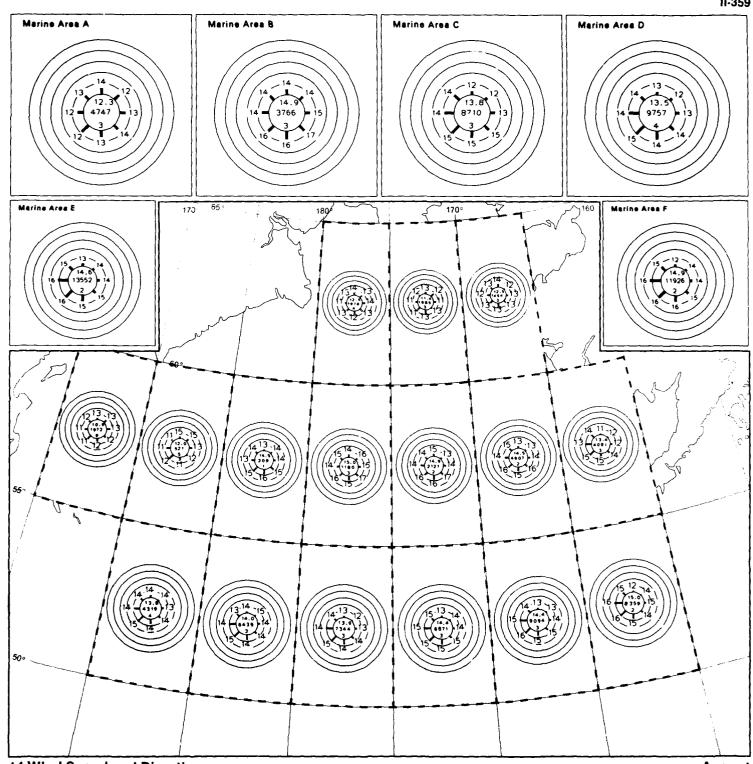


14 Wind Speed and Direction



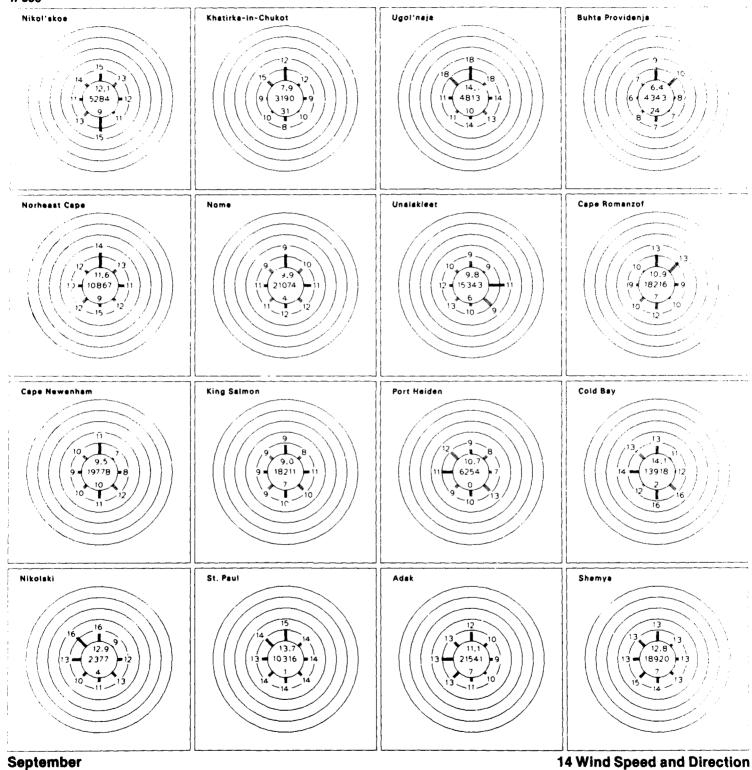
**August** 

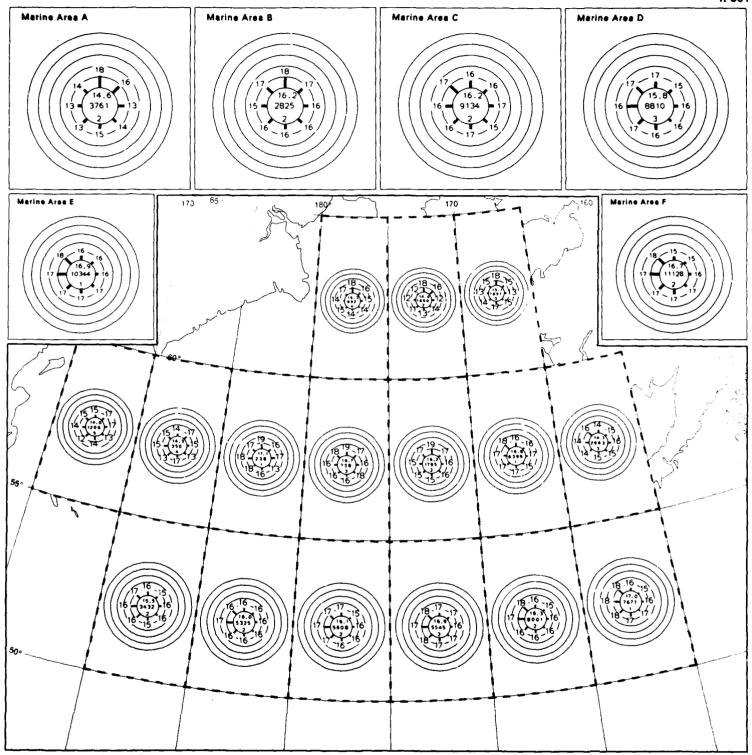
14 Wind Speed and Direction



14 Wind Speed and Direction

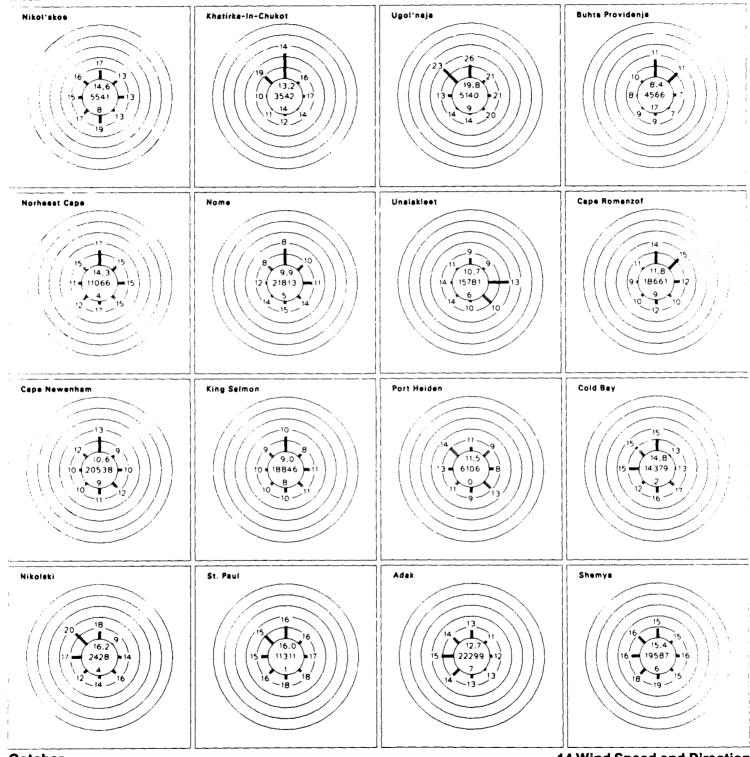
August





14 Wind Speed and Direction

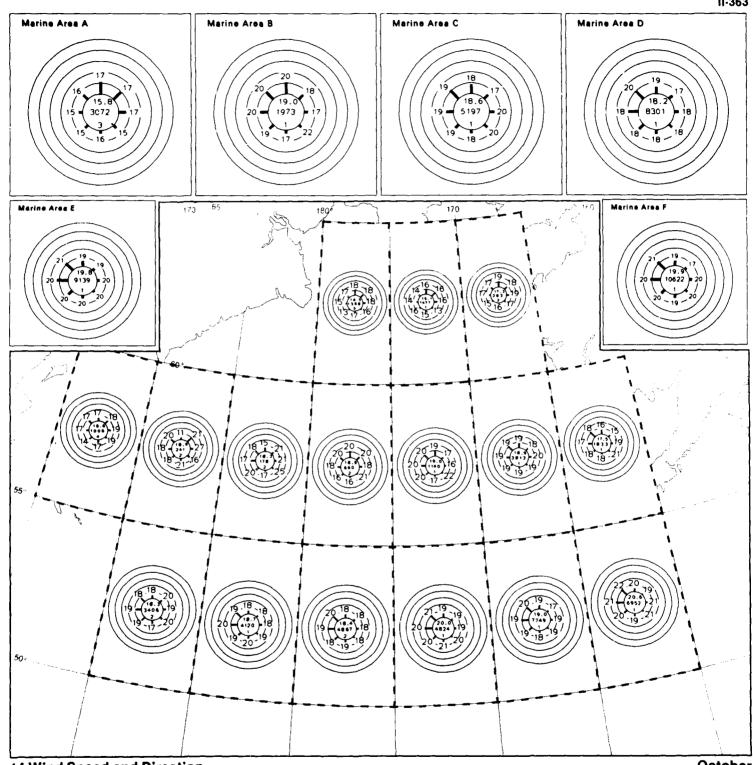
September



October

14 Wind Speed and Direction

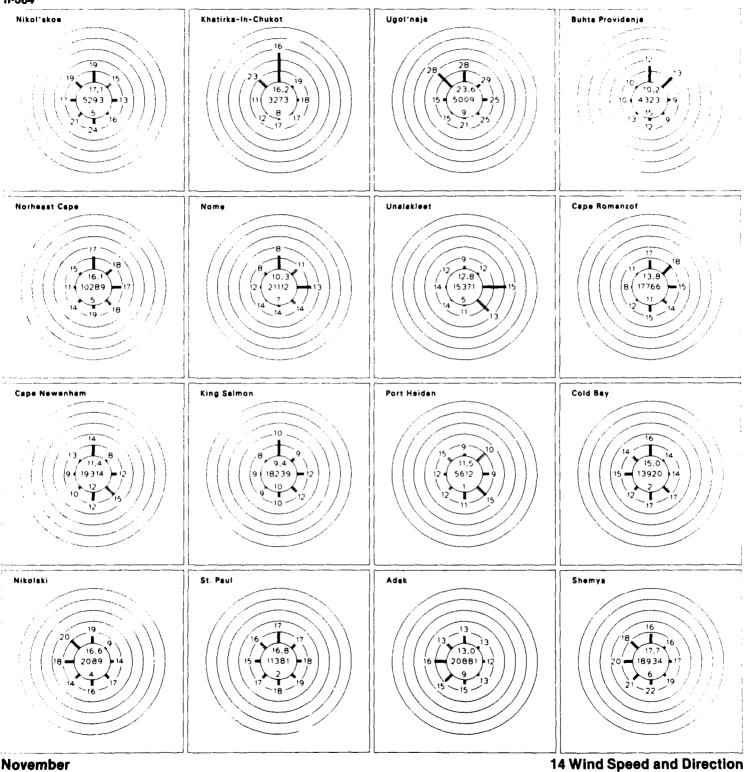
11-363



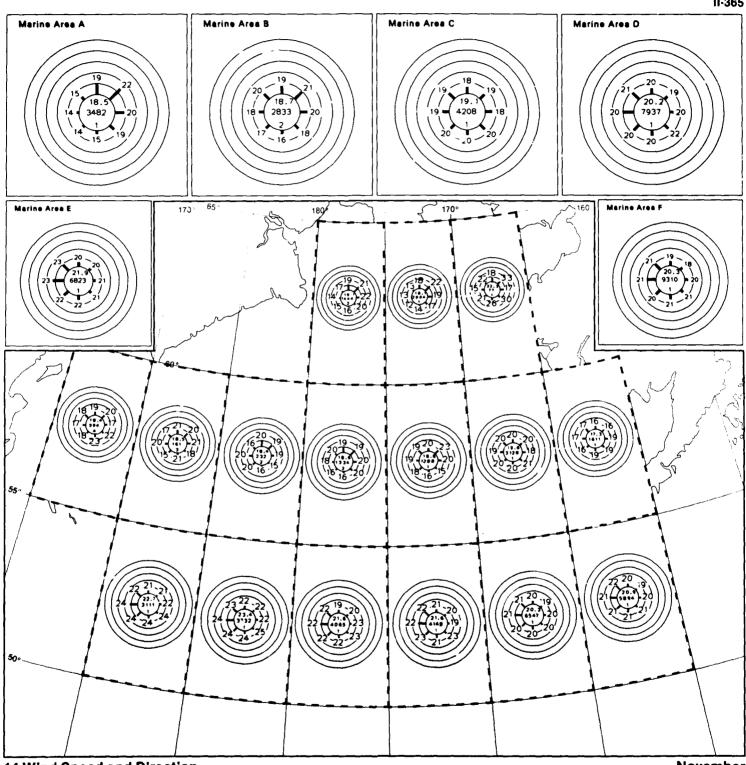
14 Wind Speed and Direction

**October** 

#### 11-364



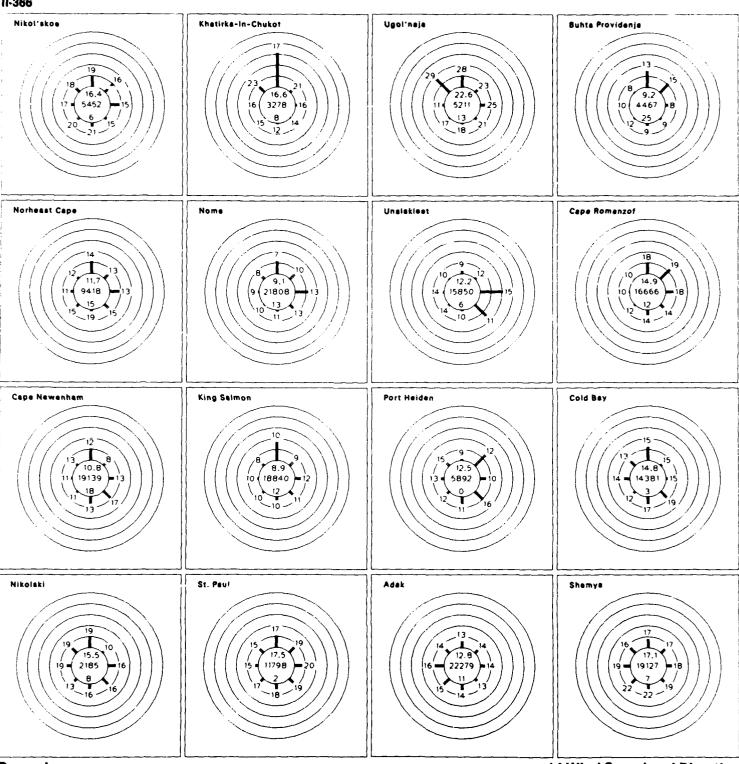
November



14 Wind Speed and Direction

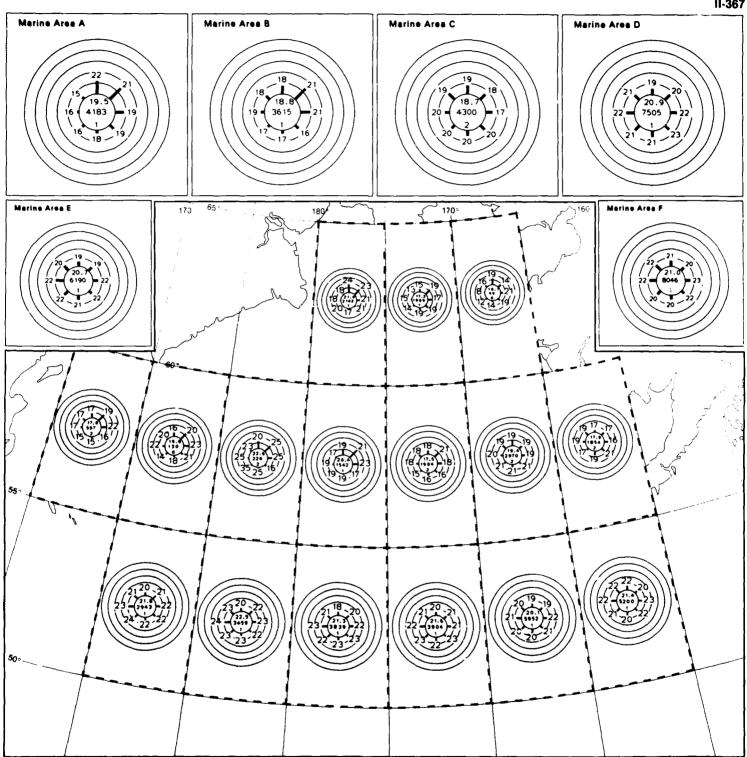
November

#### 11-366



December

14 Wind Speed and Direction



14 Wind Speed and Direction

December

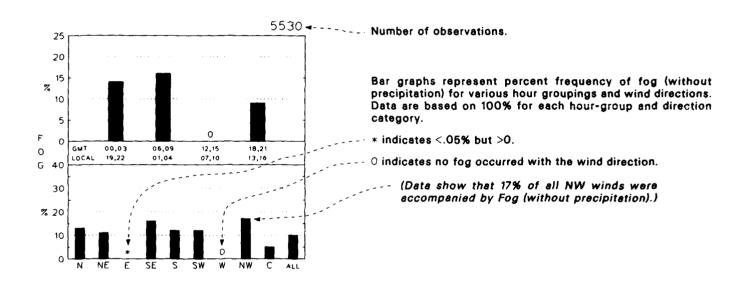
### Map 15. Fog and poor visibility

BLACK LINE - Percent frequency of visibility <1/2 nautical mile.

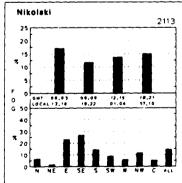
BLUE LINE - Percent frequency of fog occurring without precipitation.

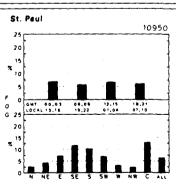
Albers Equal—Area Conic Projection

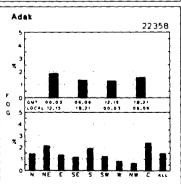
### **Graphs:** Fog/time and fog/wind direction

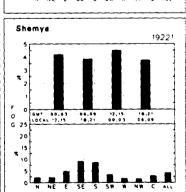


Fog is composed of minute droplets suspended in the atmosphere near the earth's surface which have no visible downward motion (fog is a stratus cloud on the surface). Fog is distinguished from haze (suspended dust or salt particles, yellowish or blue in color) by its dampness and grey color; also its restriction of visibility (less than one-half nautical mile) if deeper than 33 feet, a height considered average for the observer above the sea surface while standing on the bridge of a ship (WMO code). Fog rarely exists when the difference between the air and dew point temperatures is more than 2.5 °C. Present weather coding of fog in the marine observation is restricted to reporting of fog only when no precipitation is occurring at the time of observation (see present weather code table in the text of Set 2). Therefore, determination of occurrences of either fog with precipitation or all fog is not possible. The isopleth presentation (BLACK LINE) of visibility less than one-half nautical mile, includes restrictions to visibility due to any weather phenomena; i.e., fog, precipitation, dust, smoke, etc.









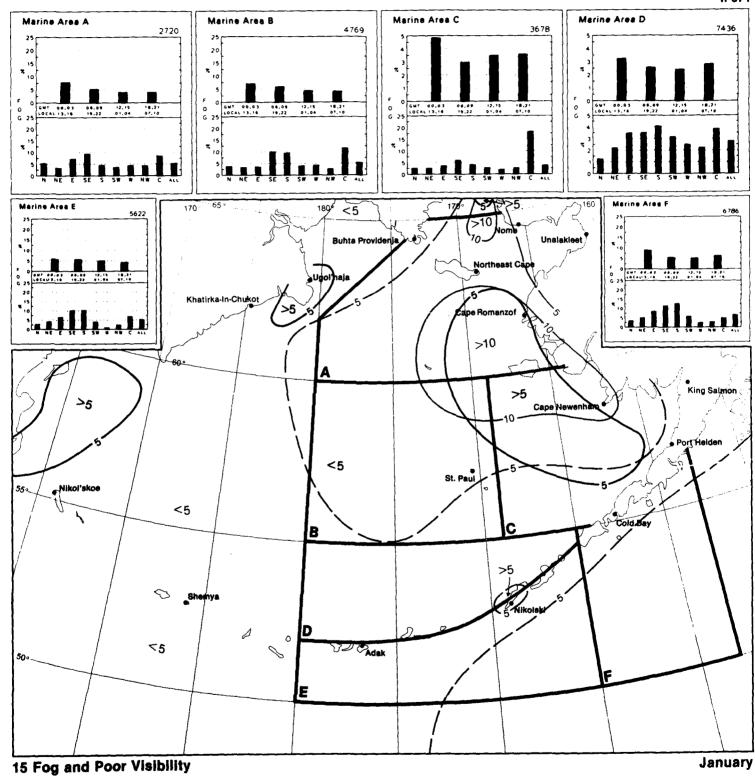
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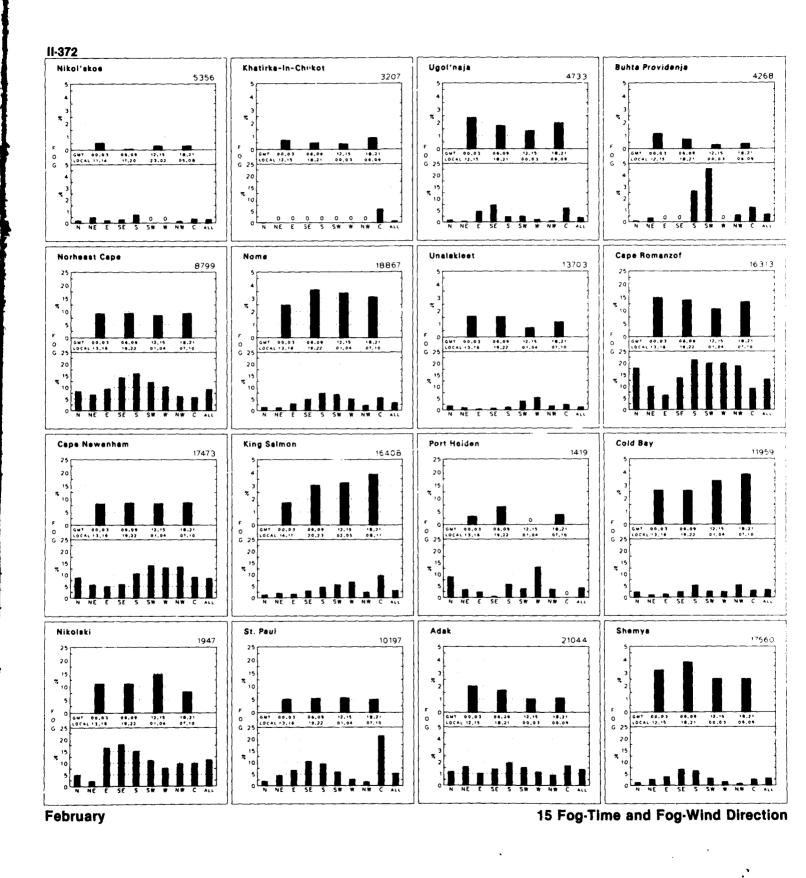
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12954

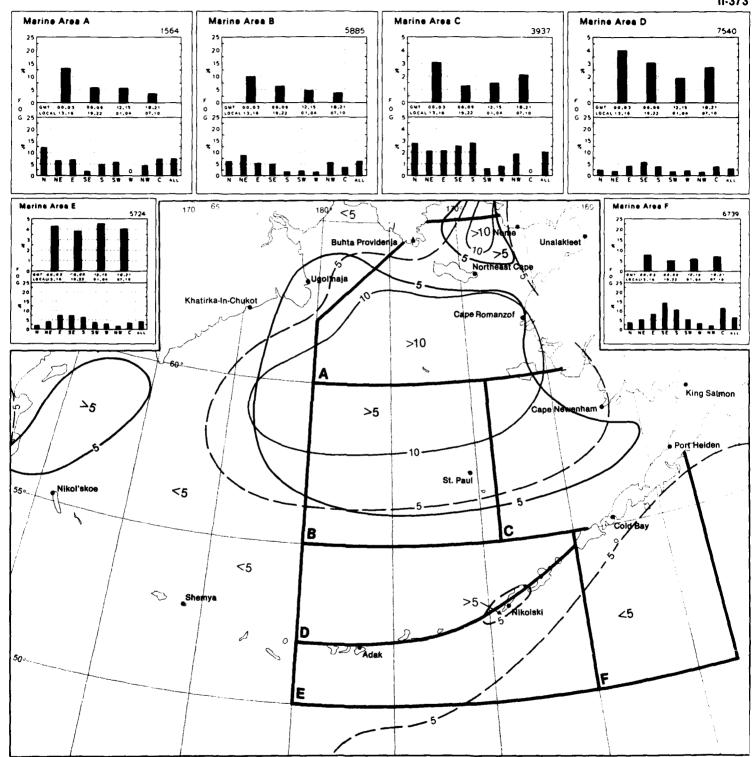
January

15 Fog-Time and Fog-Wind Direction



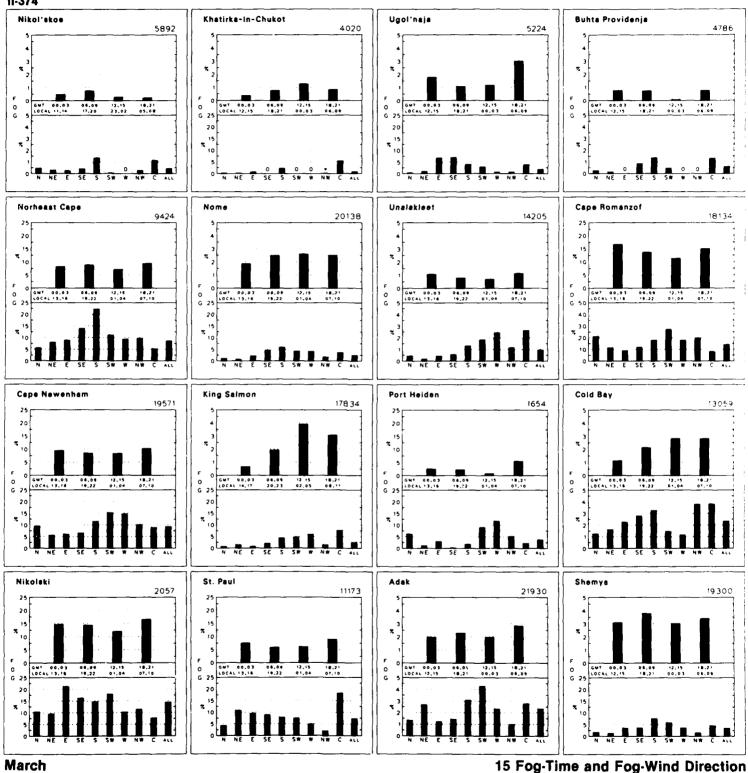


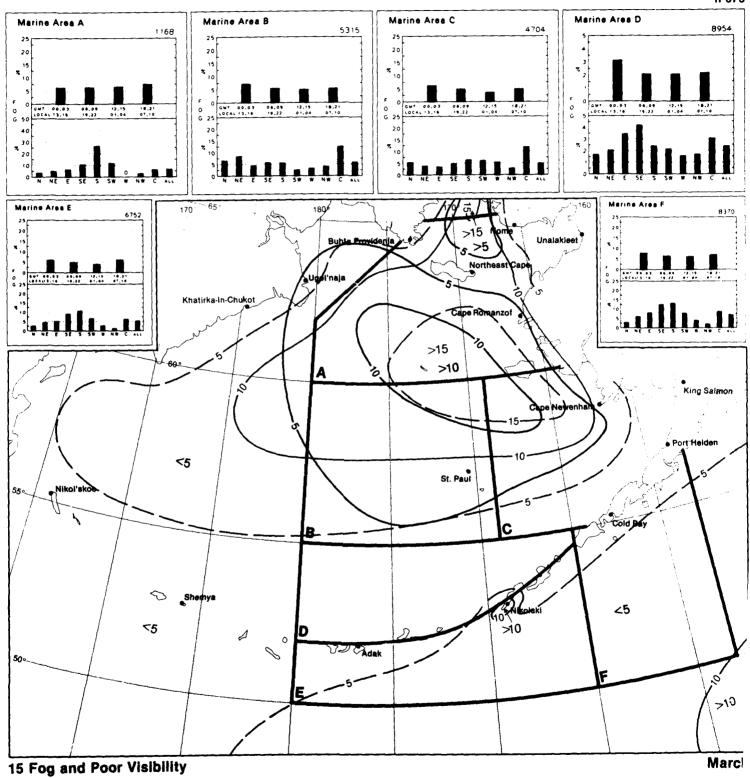
**February** 

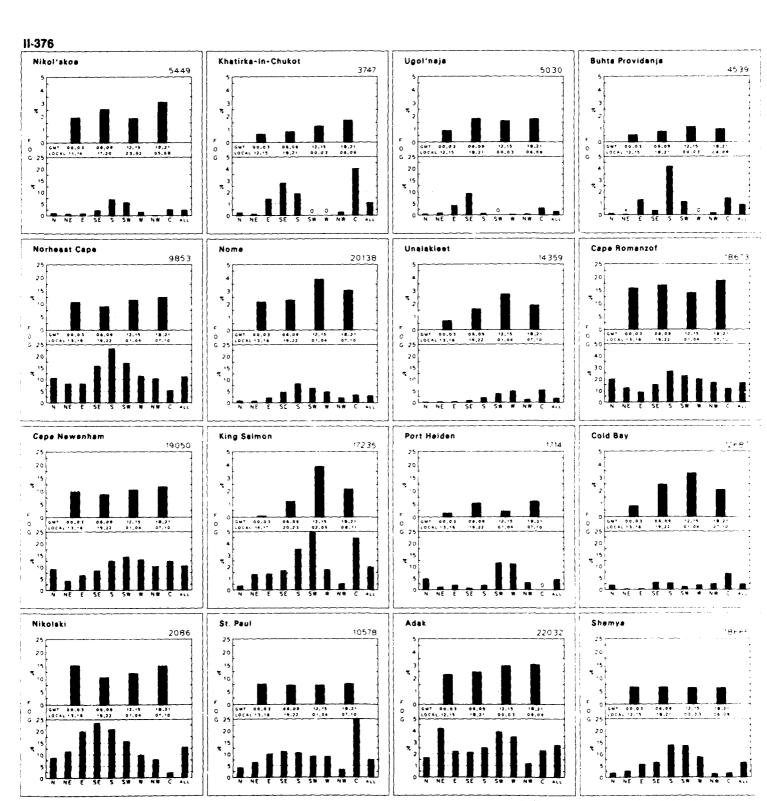


15 Fog and Poor Visibility



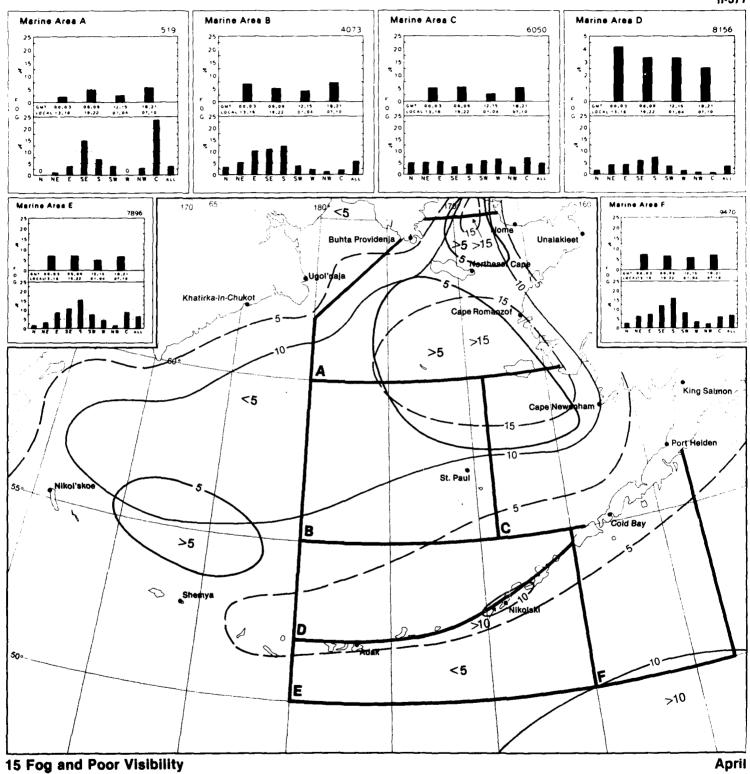


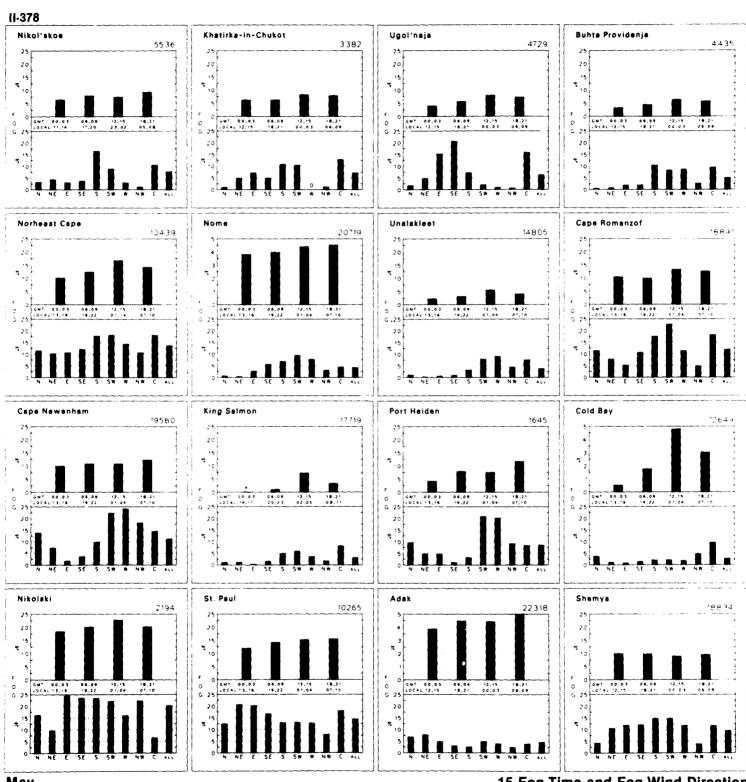




**April** 

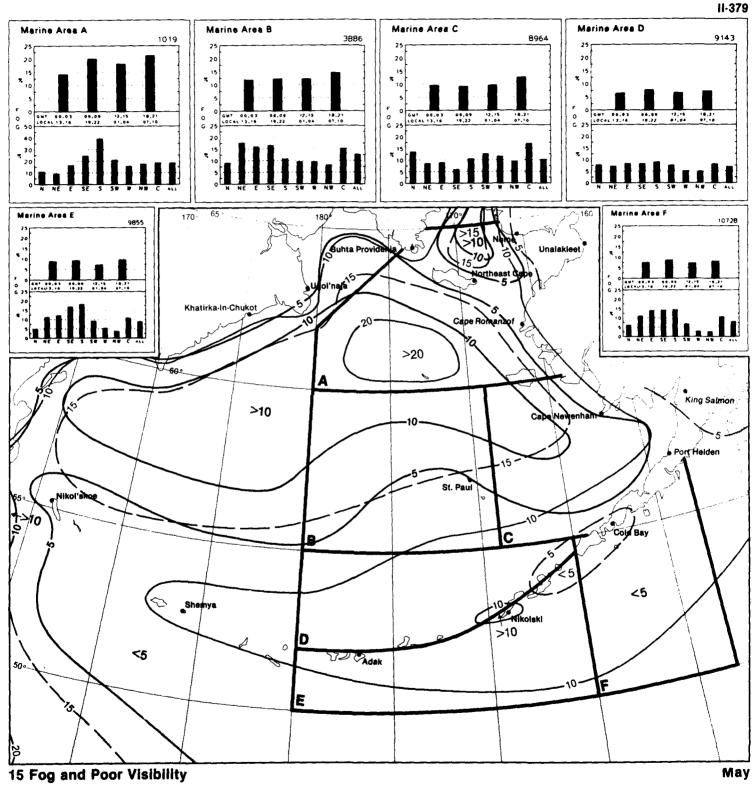
15 Fog-Time and Fog-Wind Direction

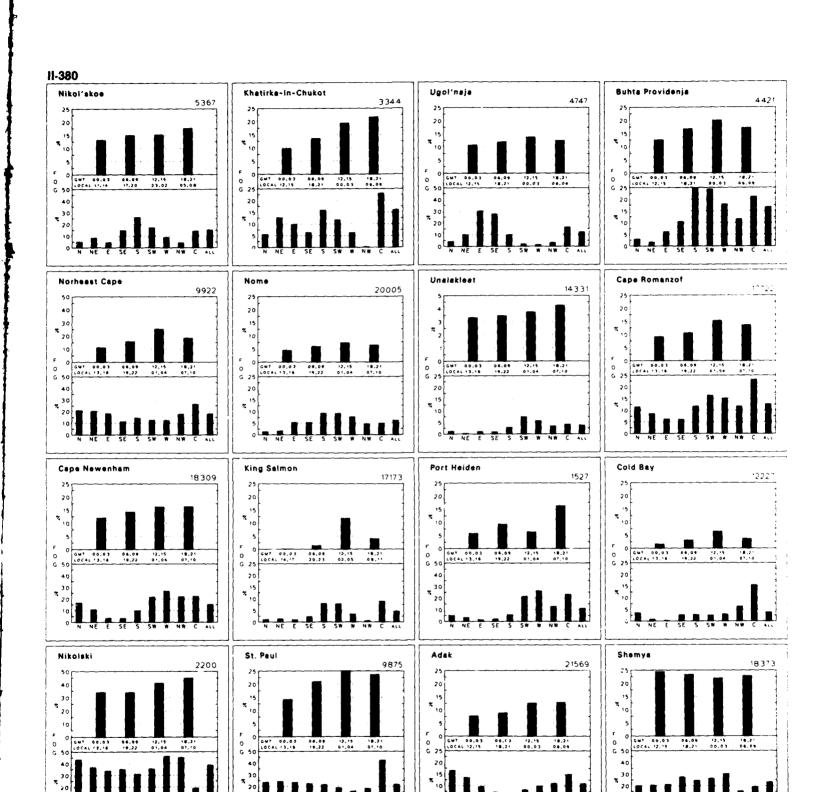




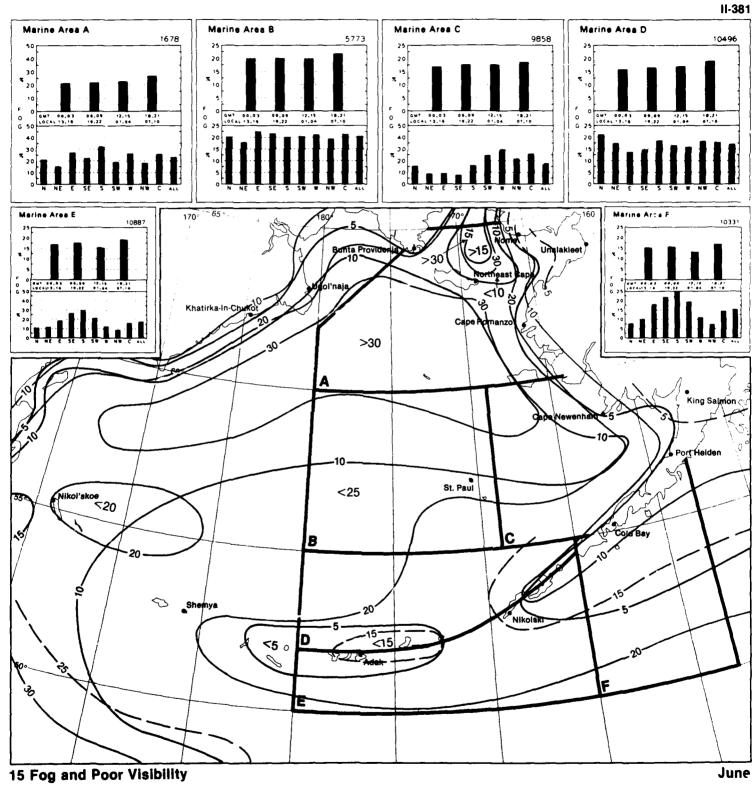
May

15 Fog-Time and Fog-Wind Direction

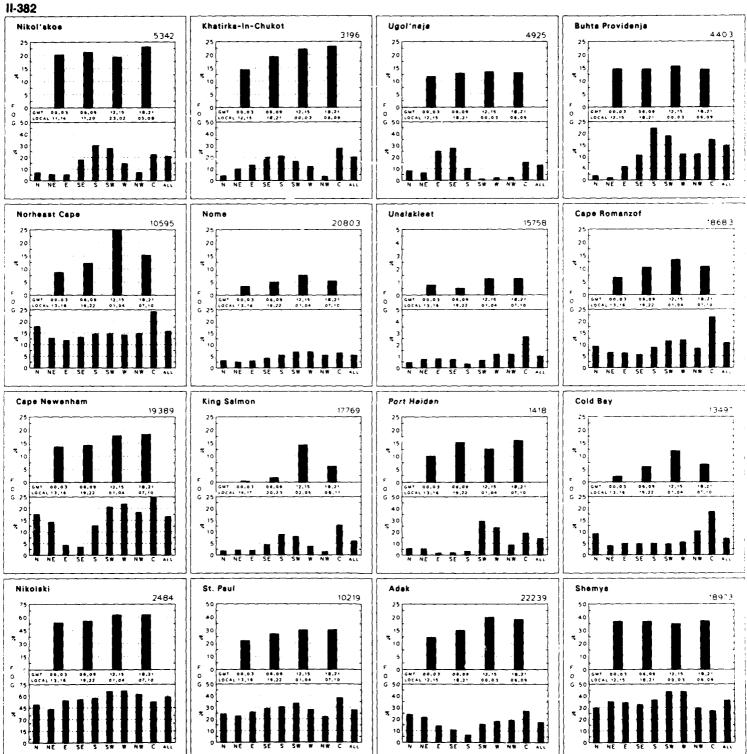




June 15 Fog-Time and Fog-Wind Direction

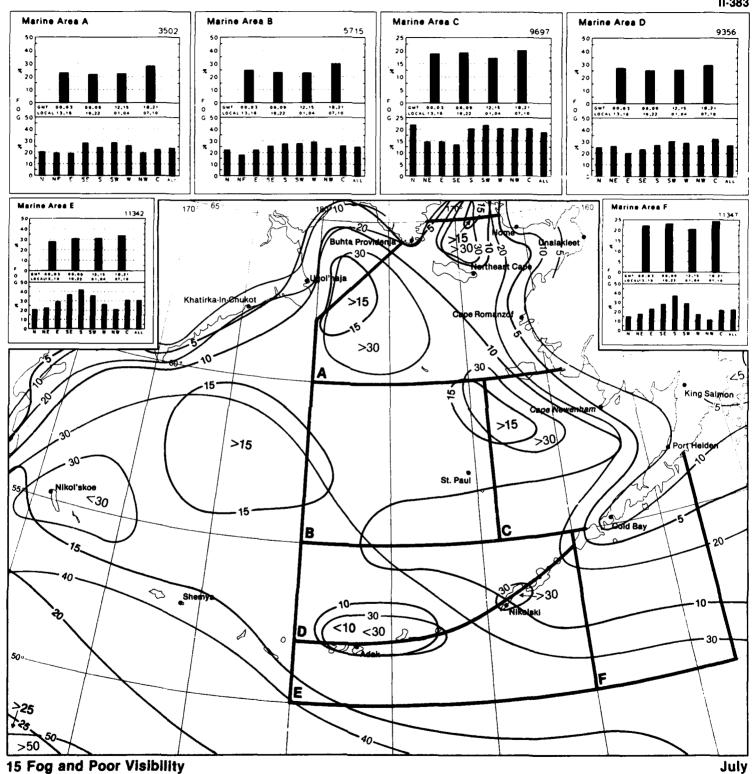


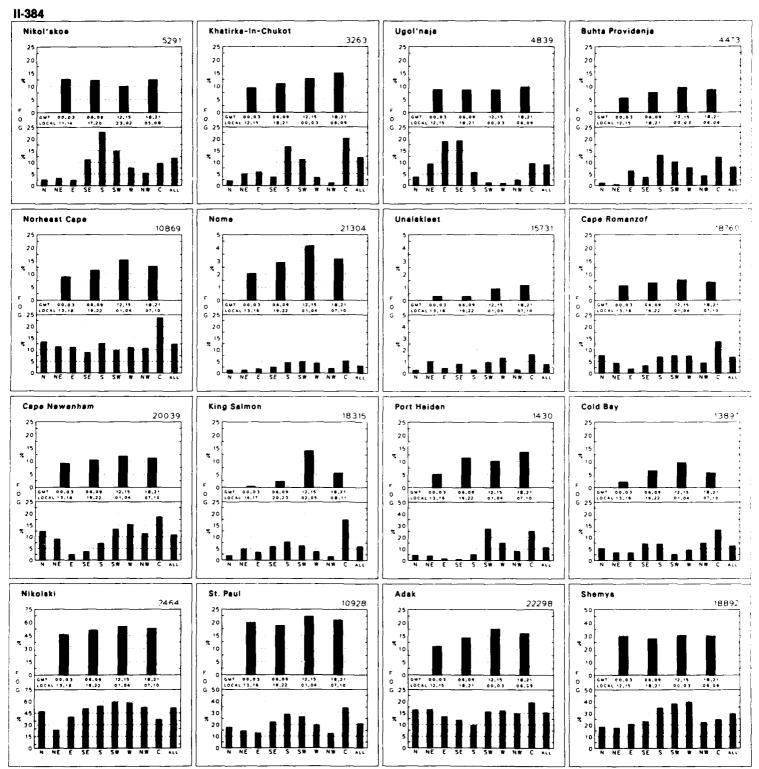




July

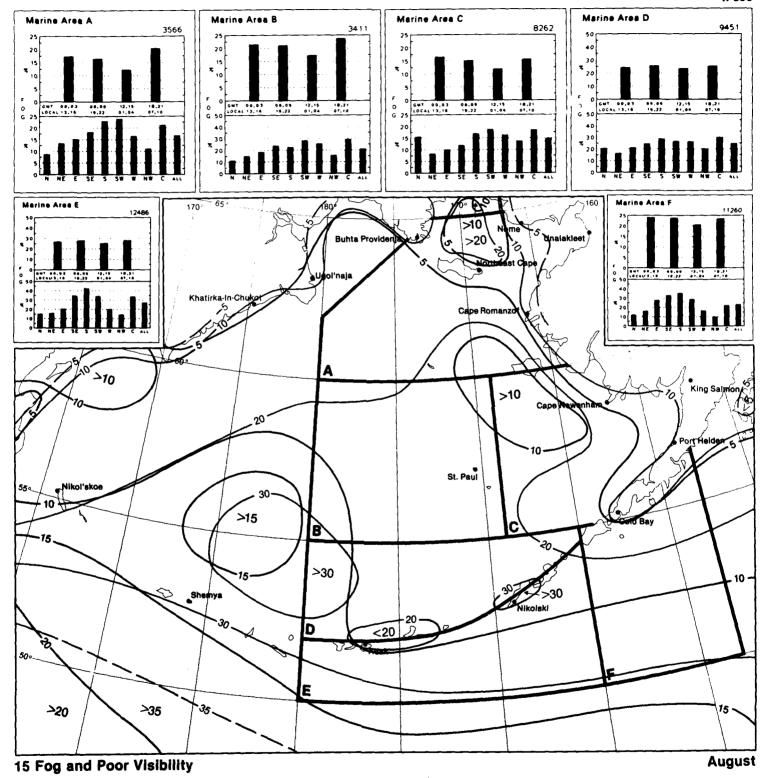
15 Fog-Time and Fog-Wind Direction

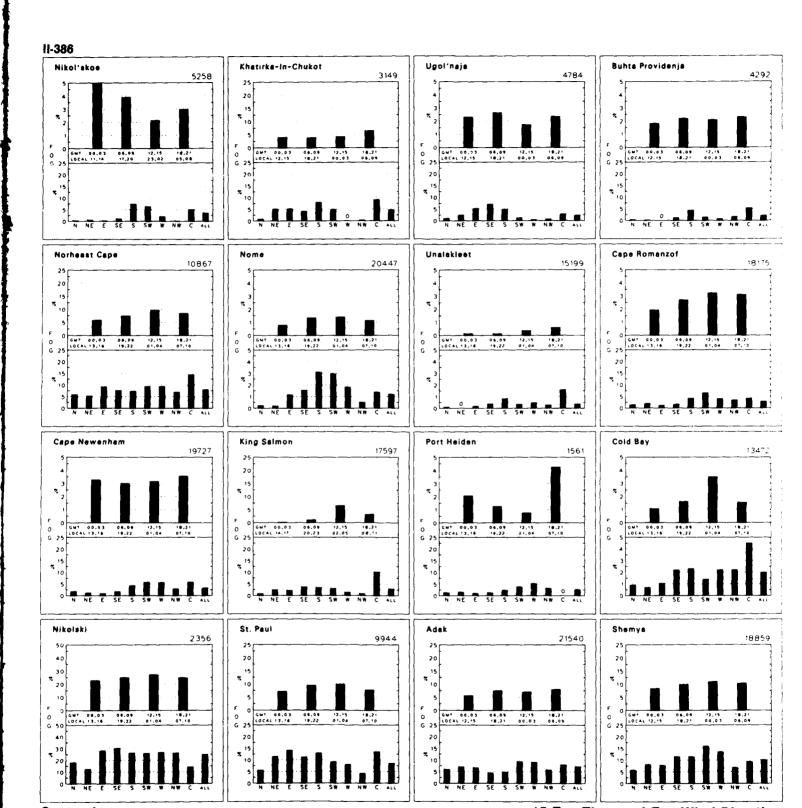




**August** 

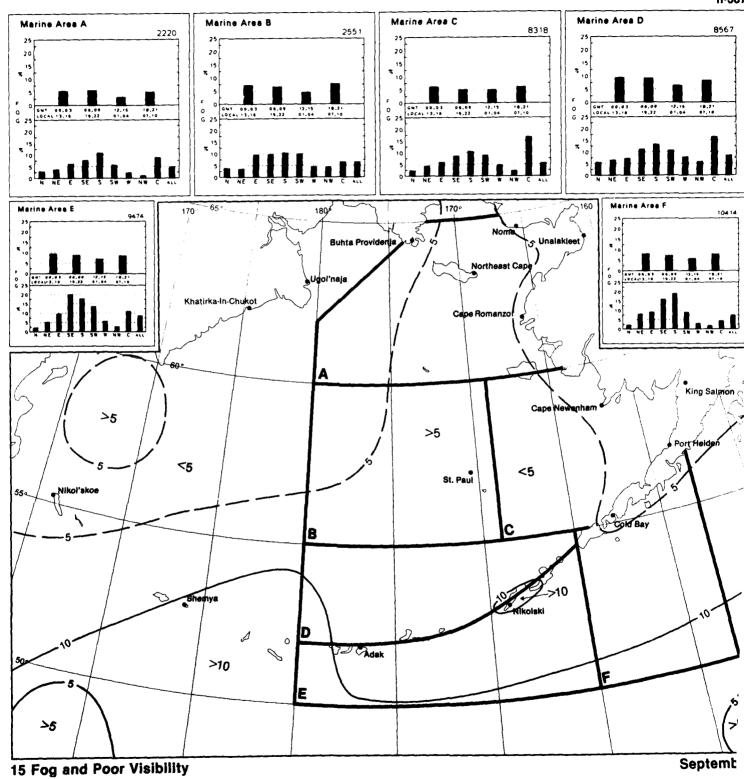
15 Fog-Time and Fog-Wind Direction

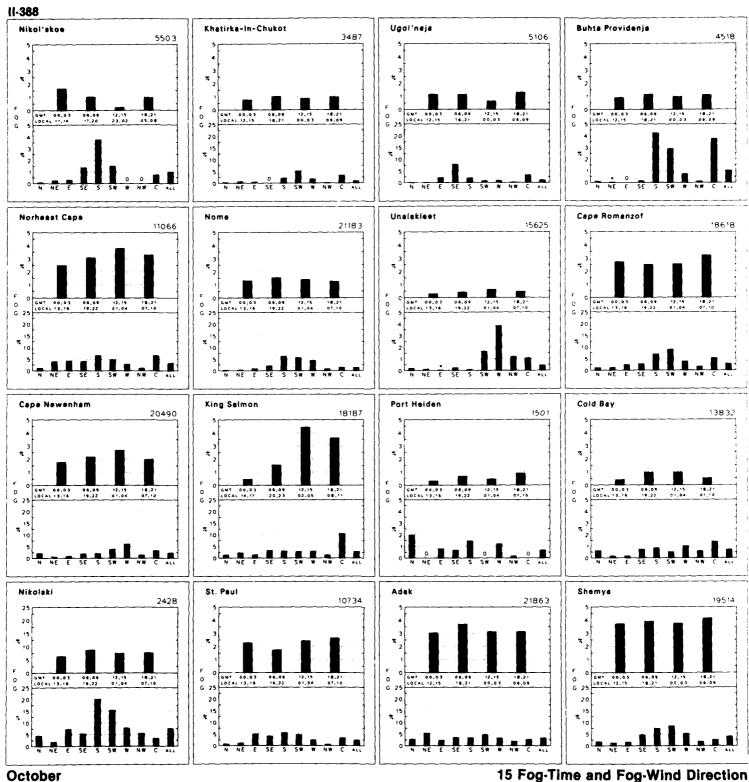


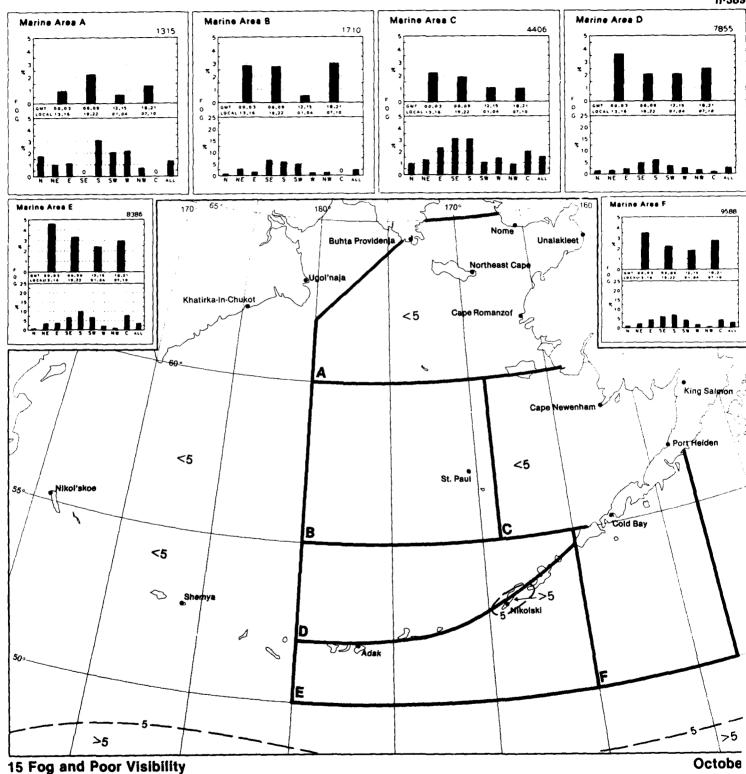


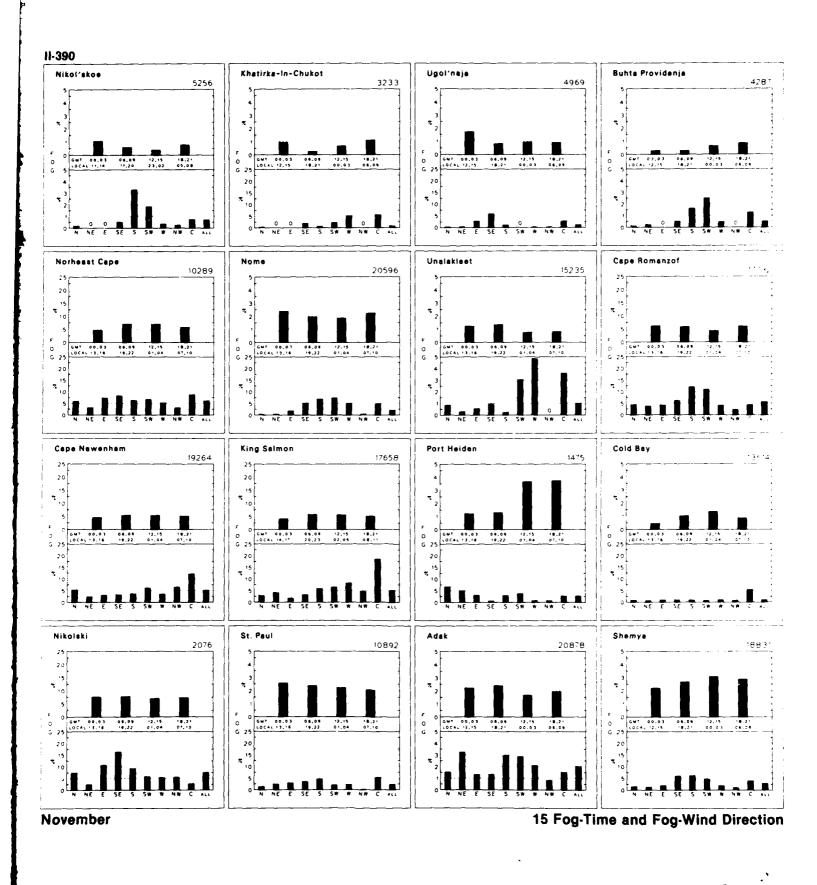
September

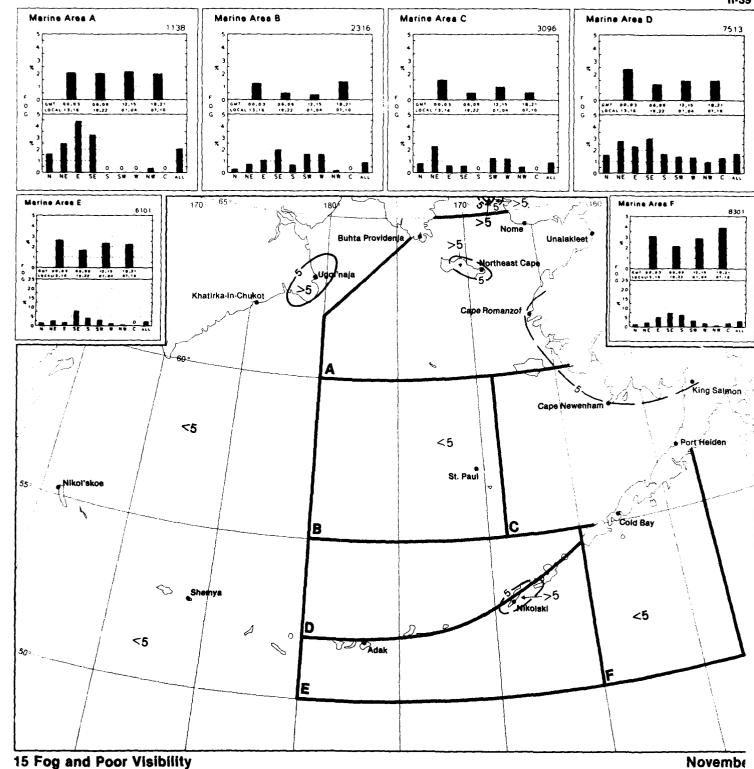
15 Fog-Time and Fog-Wind Direction

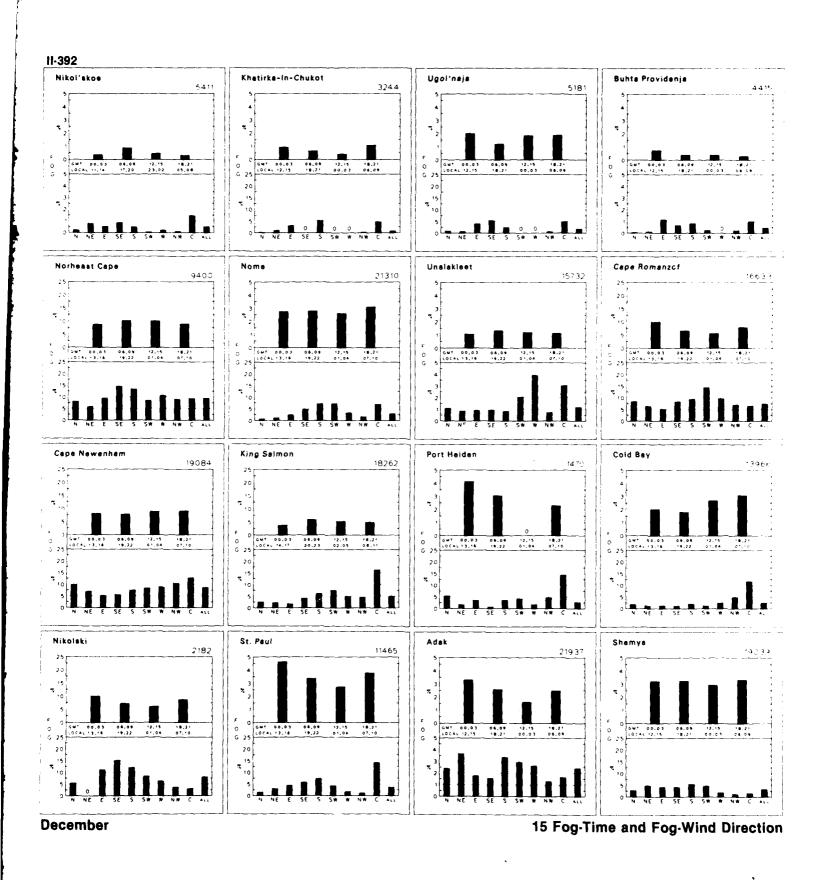


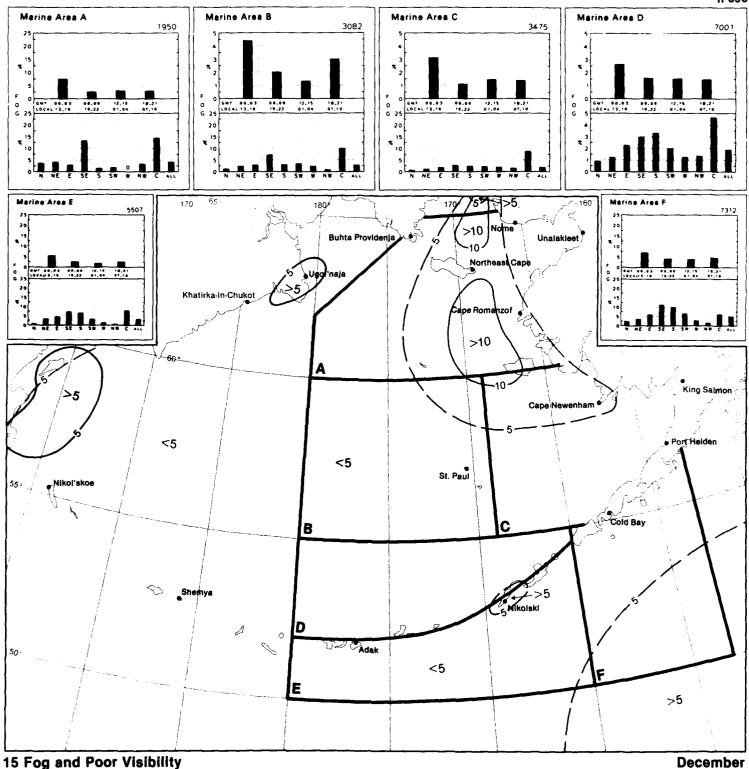












15 Fog and Poor Visibility

# Map 16. Sea surface temperature extremes (°C)

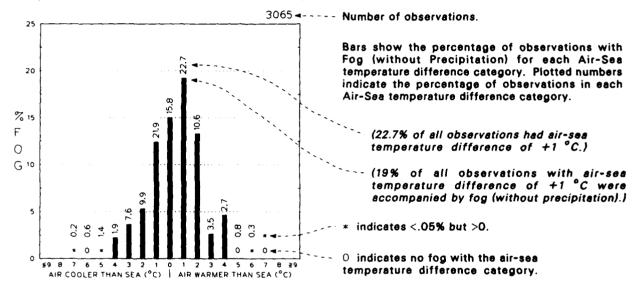
BLACK LINE — Maximum (99%) sea surface temperature (1% of the temperatures were greater than the given value).

BLUE LINE — Minimum (1%) sea surface temperature (1% of the temperatures were equal to or less than the given value).

Albers Equal—Area Conic Projection

## Graphs: Fog/air-sea temperature difference

PERCENT FREQUENCY OF THE OCCURRENCE OF FOG (Without Precipitation) VERSUS AIR-SEA TEMPERATURE DIFFERENCE (°C)

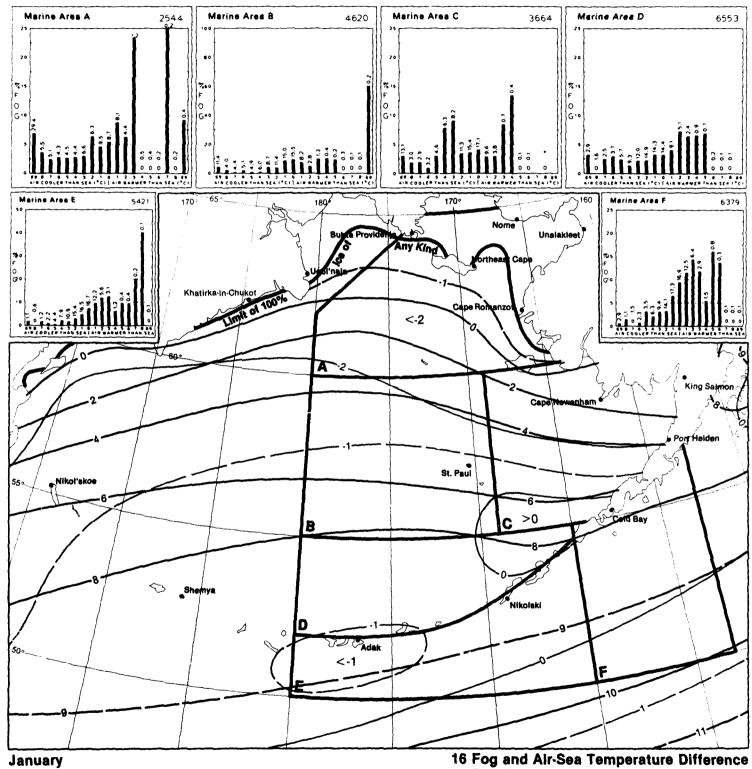


Sea surface temperatures are recorded with a fairly high frequency in marine observations. The principal methods for observing the temperature of the water surface on merchant ships are by either a fluid thermometer located in the condenser intake of the ship or a thermometer immersed in a freshly-drawn bucket of surface water. While the intake method is commonly used on most merchant ships today, the bucket method was the most common a half century ago. Injection temperatures are not considered as representative of the surface temperature as bucket readings because the injectors are commonly located well below the water surface at depths of 5 to 20 meters depending on the size of the ship. Injection temperatures are also subject to varying errors due to heating caused by the ship. Bucket temperatures can also be biased by the air temperature or the bucket itself.

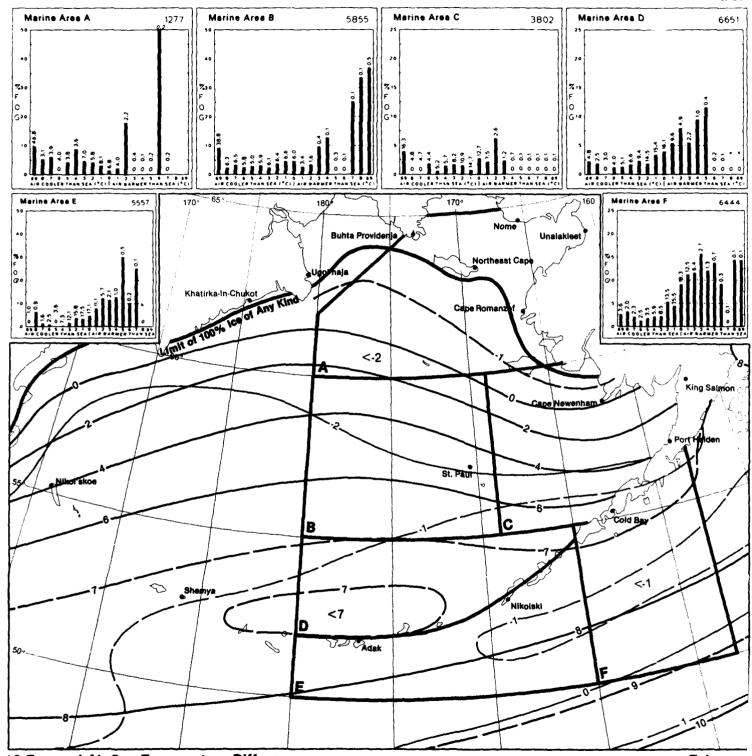
Even though the two methods produce slightly different results, the data can be used with considerable confidence. The isopleths representing extreme conditions show the maximum (99%) and the minimum (1%) levels of sea surface temperature. Gradients and relative values of the isopleths are considered reliable.

16 Legend Legend 16



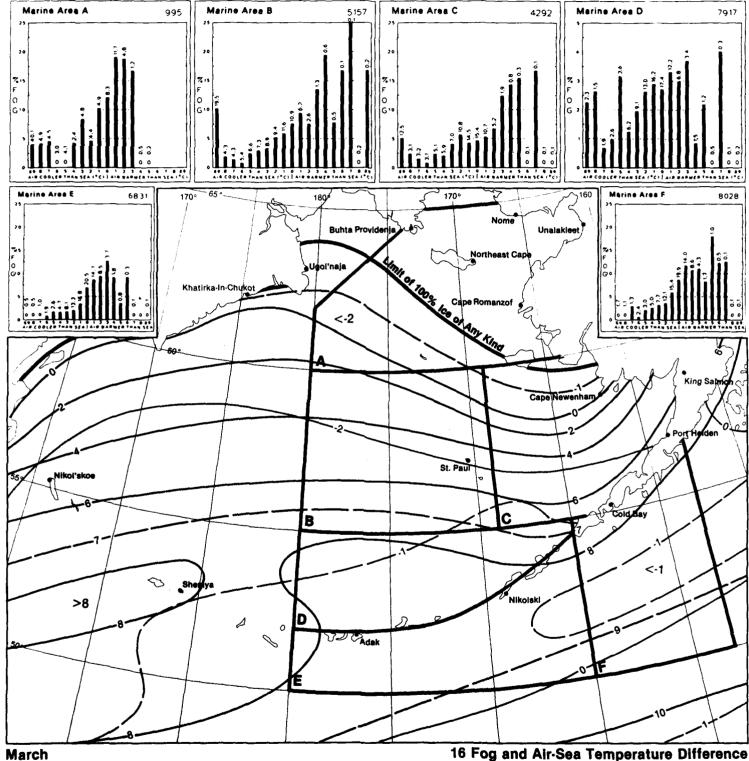


16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes

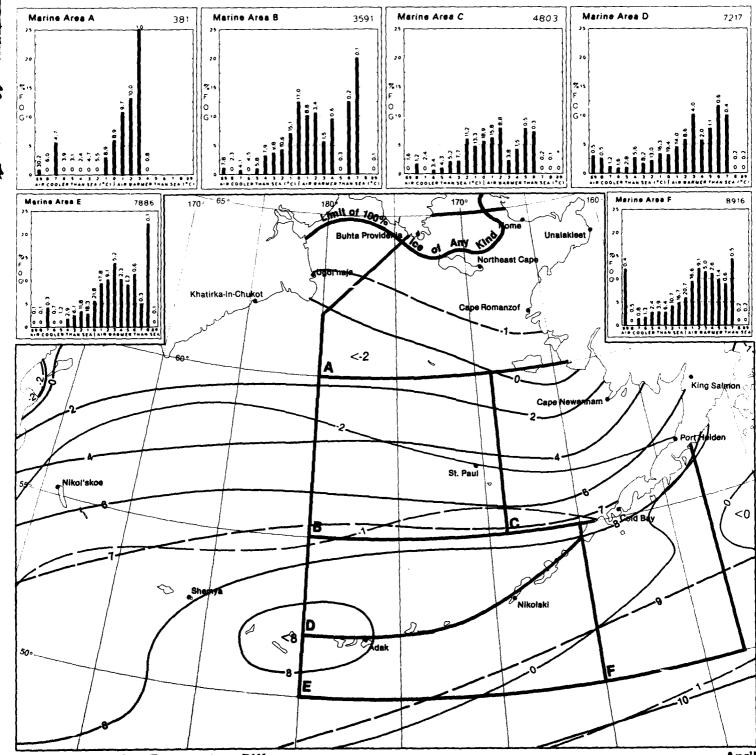


16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes

February

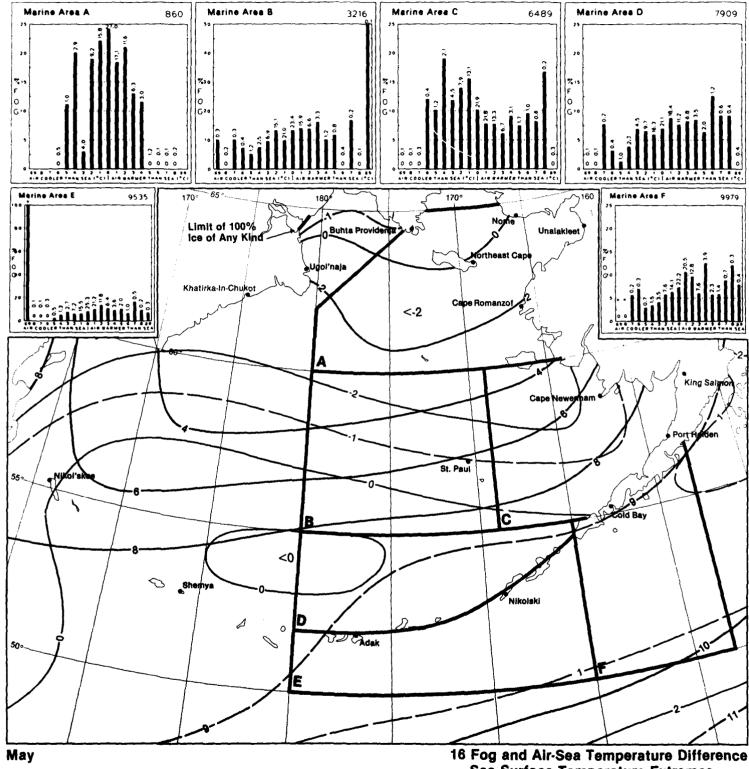


16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes

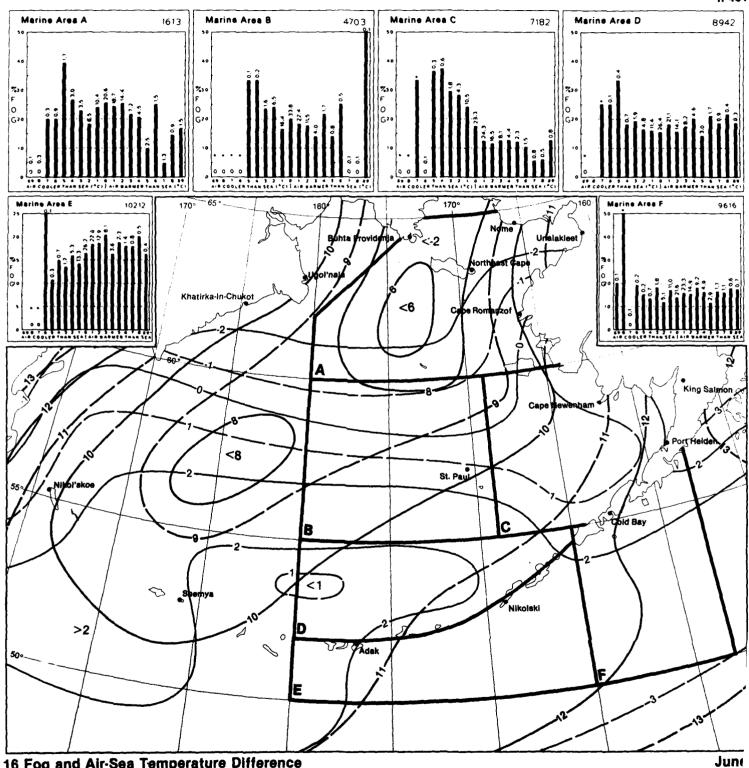


16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes

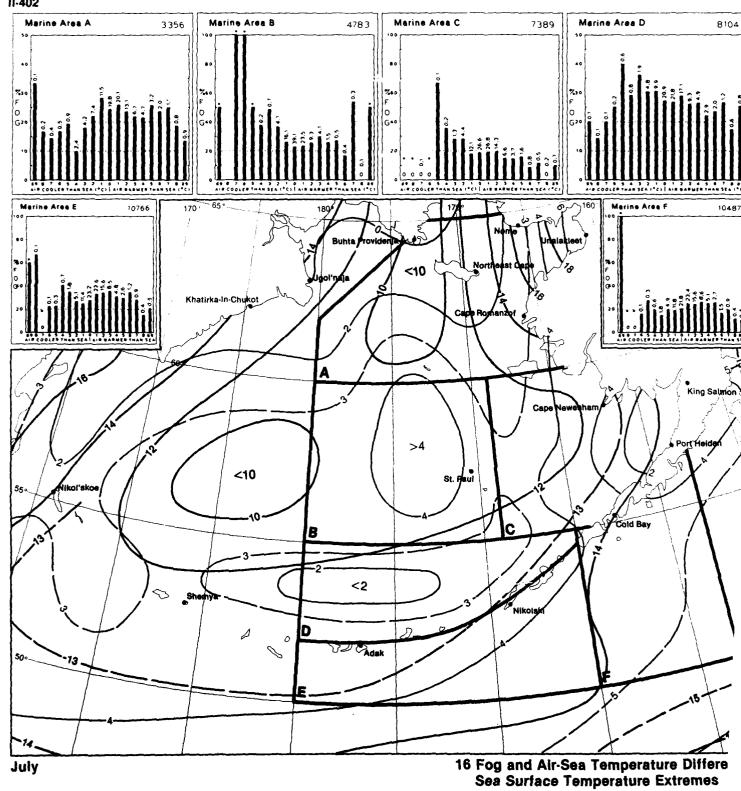
April

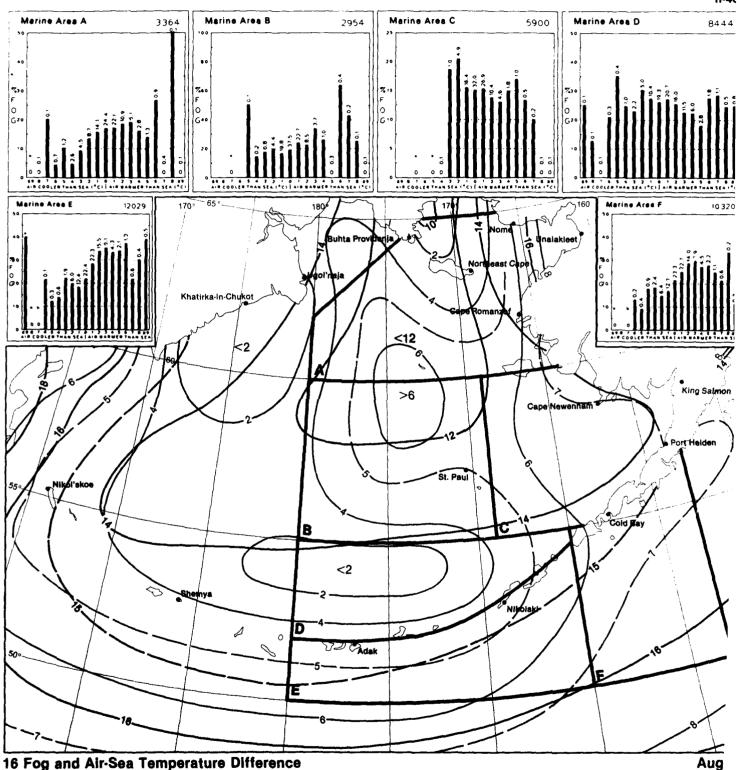


16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes

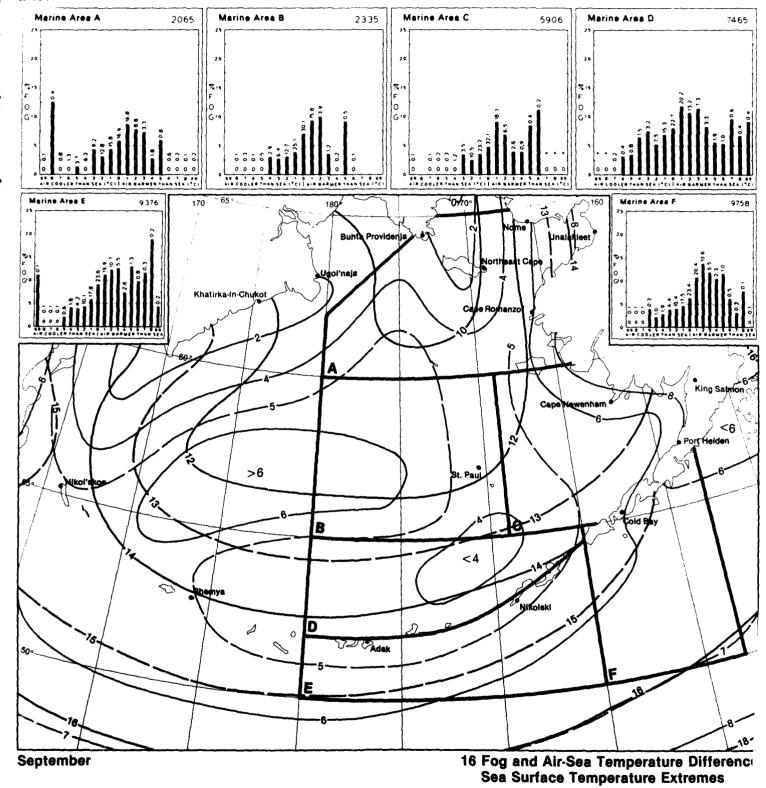


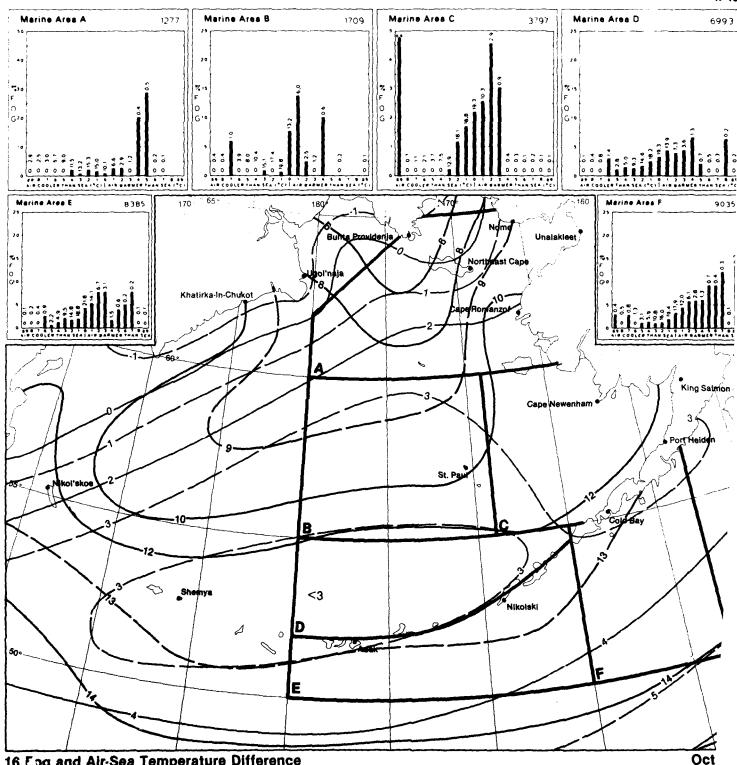
16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes



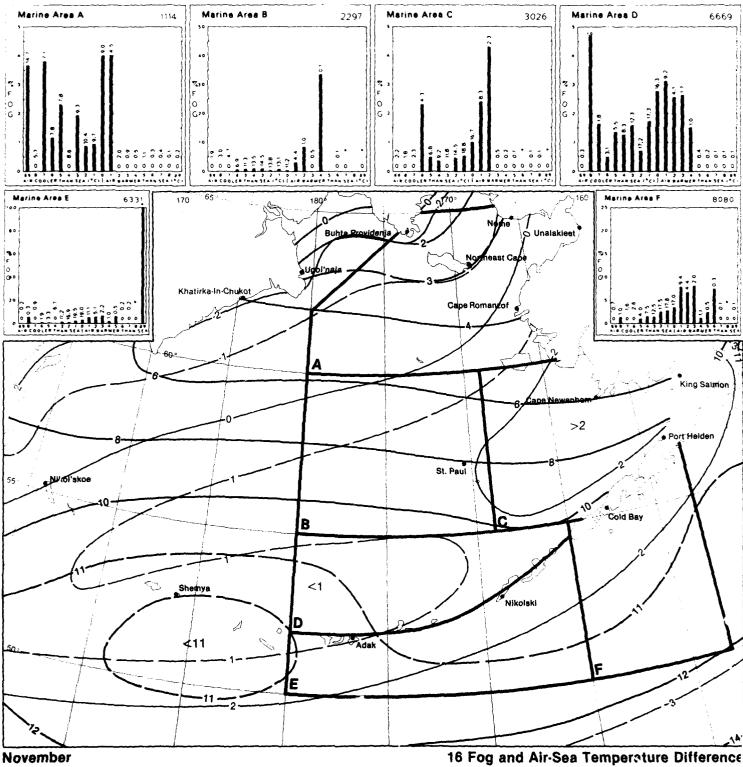


16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes

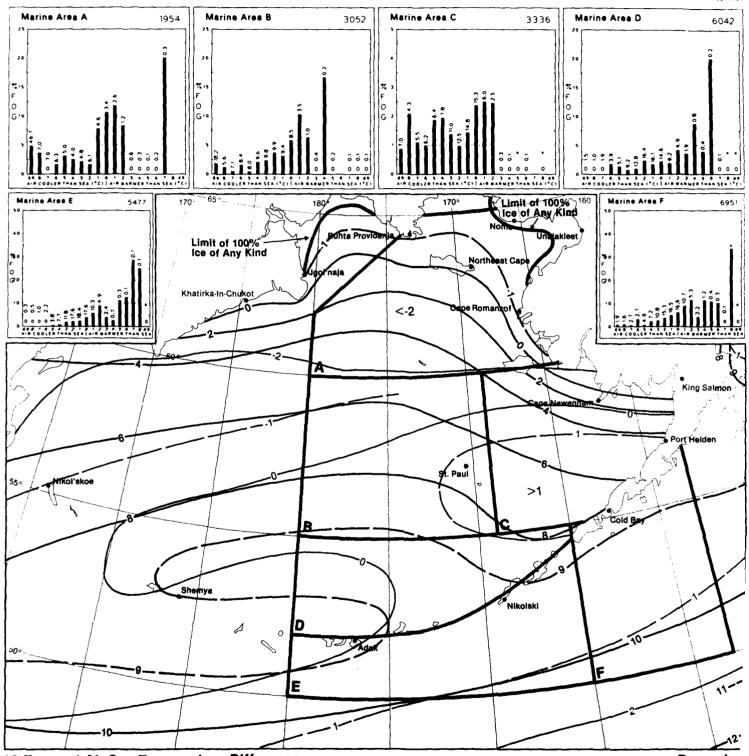




16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes



16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes



16 Fog and Air-Sea Temperature Difference Sea Surface Temperature Extremes

Decembe

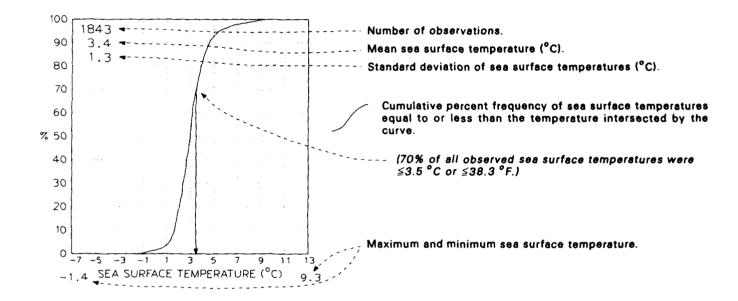
## Map 17. Mean sea surface temperature and ice concentration of any kind.

BLACK LINE - Mean sea surface temperature (°C).

BLUE LINE - Percent frequency of occurrence of ice of any kind.

Albers Equal-Area Conic Projection

## Graphs: Sea surface temperature

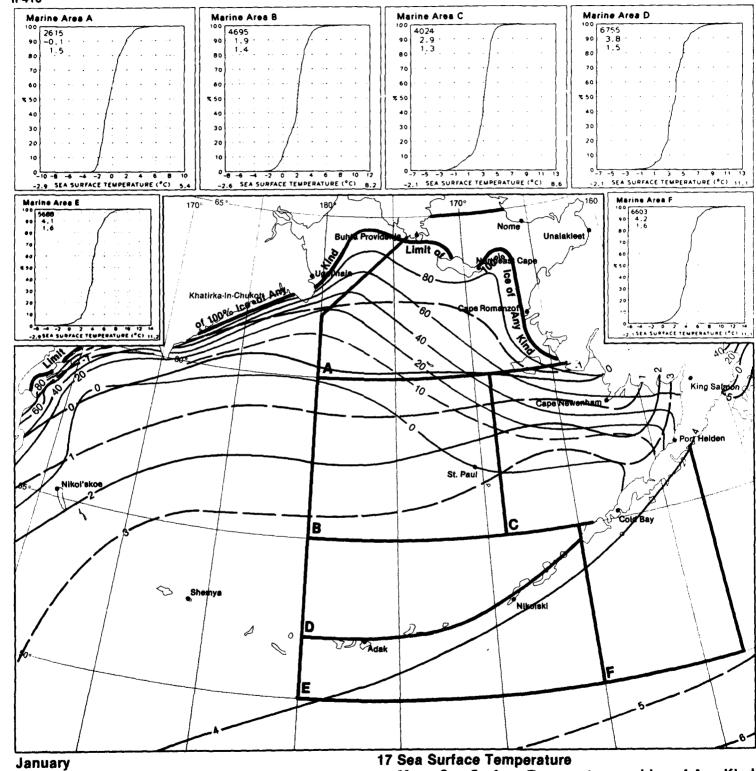


17 Legend 17

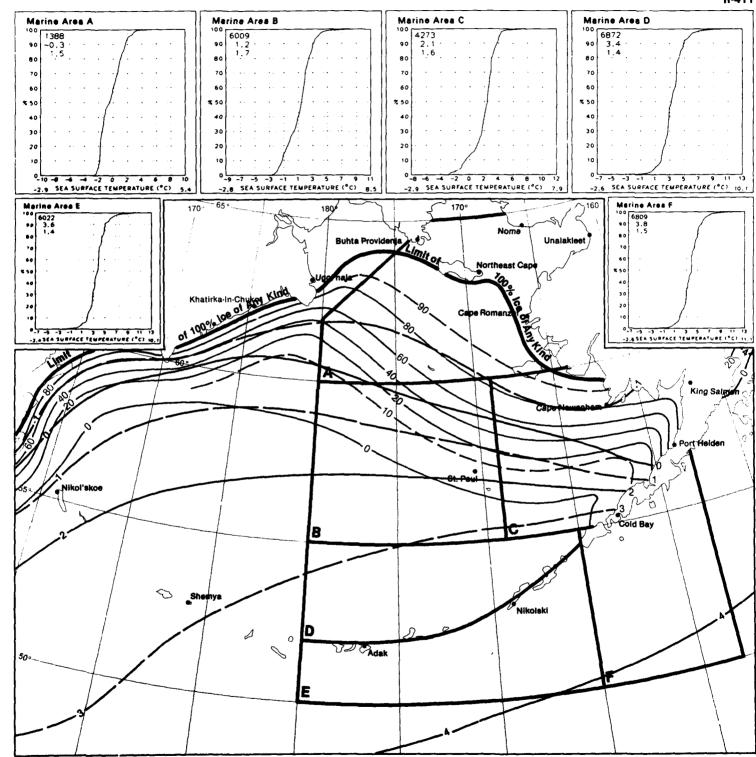
The percentage of temperatures greater than a given value can be obtained from the graph by subtracting the cumulative frequency of that value from 100%. Sea surface temperatures may be used to estimate the length of time a person in ordinary clothes and life preserver may be expected to survive if washed overboard. The approximate survival time as a function of water temperature is shown in the following table (refer to the text in Section I of the atlas for information on immersion hypothermia, and to the introductory text in Section II for sea ice information).

Water Temperature	Exhaustion or Unconsciousness	Expected time of Survival
0°C	15 min	15—45 min
0°—5°C	15—30 min	30—90 min
5°—10°C	30—60 min	1—3 hours
10°—15°C	1—2 hours	1—6 hours
15°—20°C	2—7 hours	2—40 hours
20°—25°C	3—12 hours	3—indefinite hrs
25°C	Indefinite	Indefinite

17 Legend



Mean Sea Surface Temperature and Ice of Any Kind

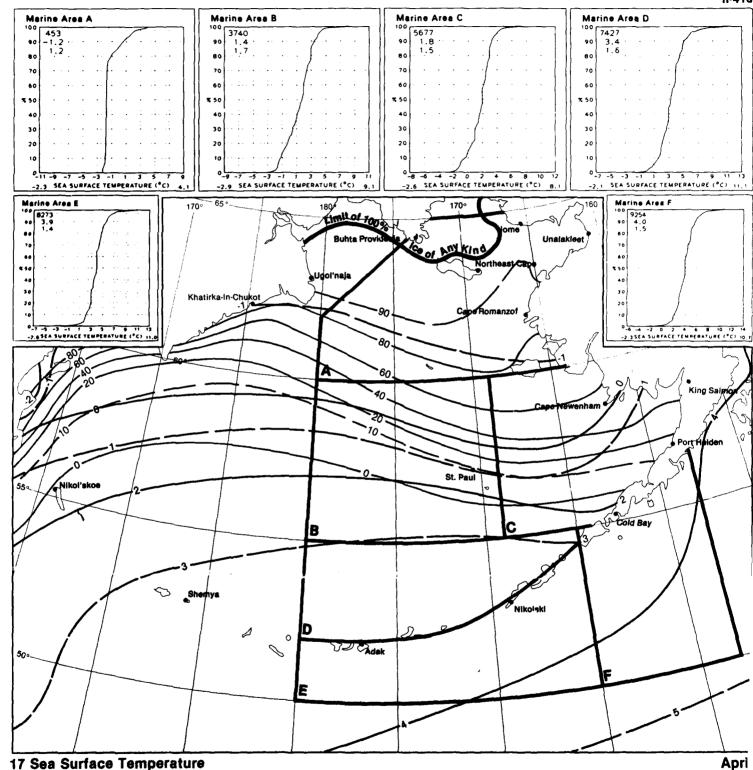


17 Sea Surface Temperature
Mean Sea Surface Temperature and Ice of Any Kind

**February** 

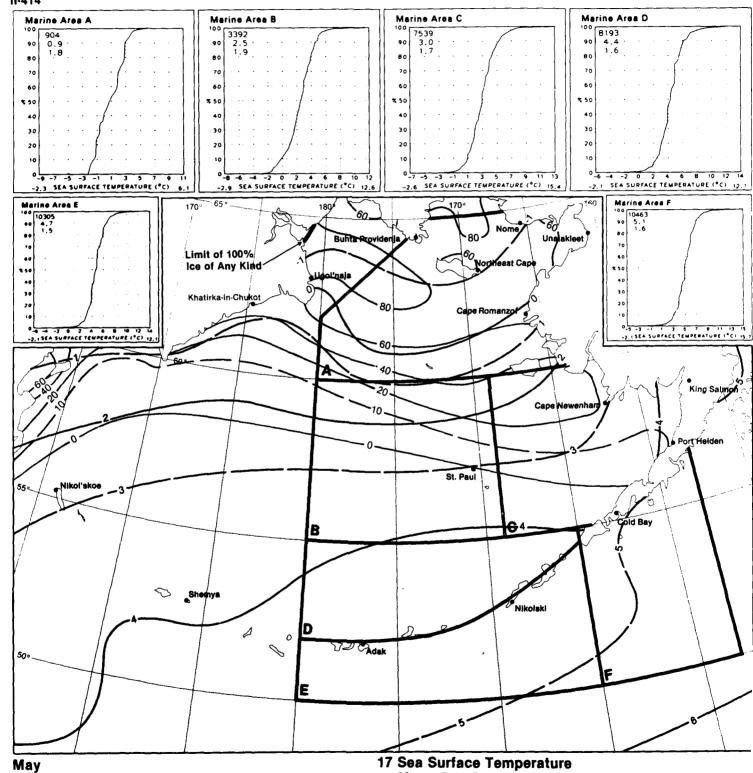
March

17 Sea Surface Temperature
Mean Sea Surface Temperature and ice of Any Kind

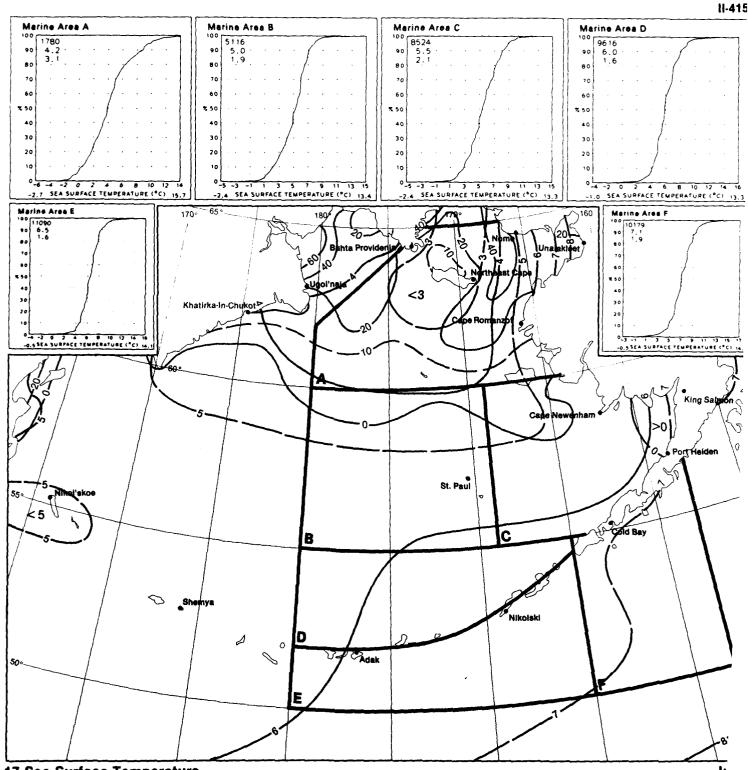


17 Sea Surface Temperature

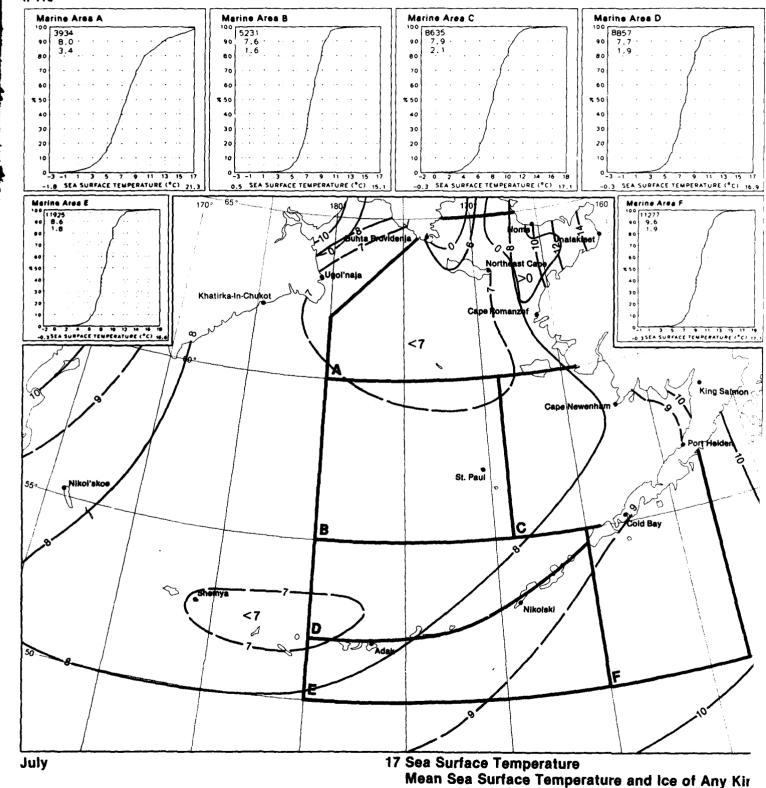
Mean Sea Surface Temperature and Ice of Any Kind

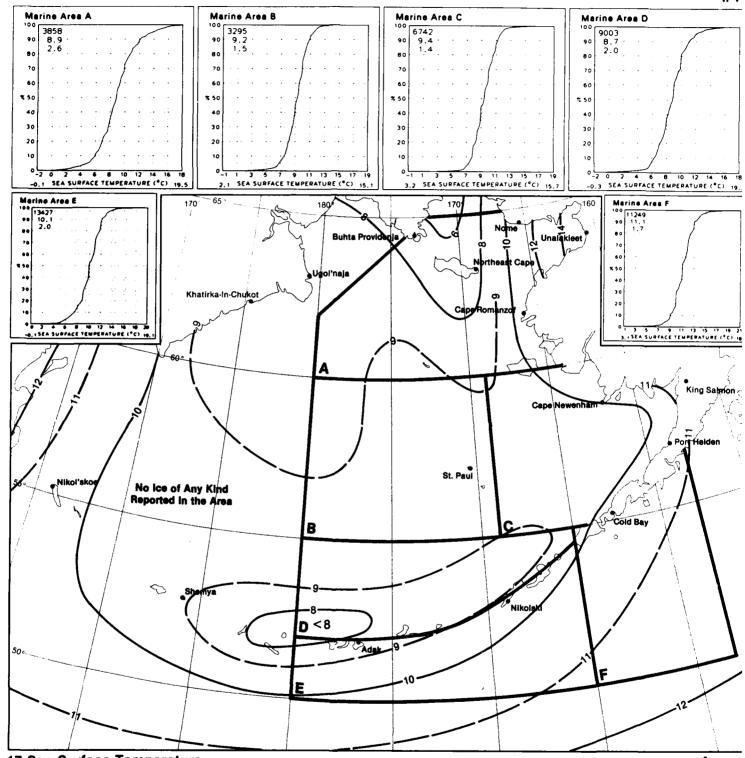


Mean Sea Surface Temperature and Ice of Any Kind



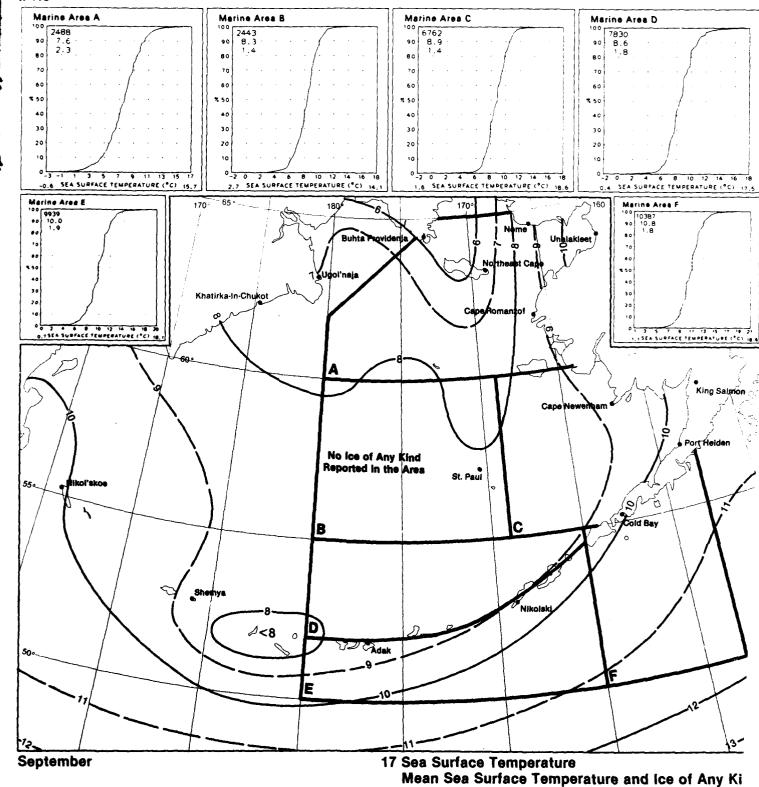
17 Sea Surface Temperature Mean Sea Surface Temperature and Ice of Any Kind

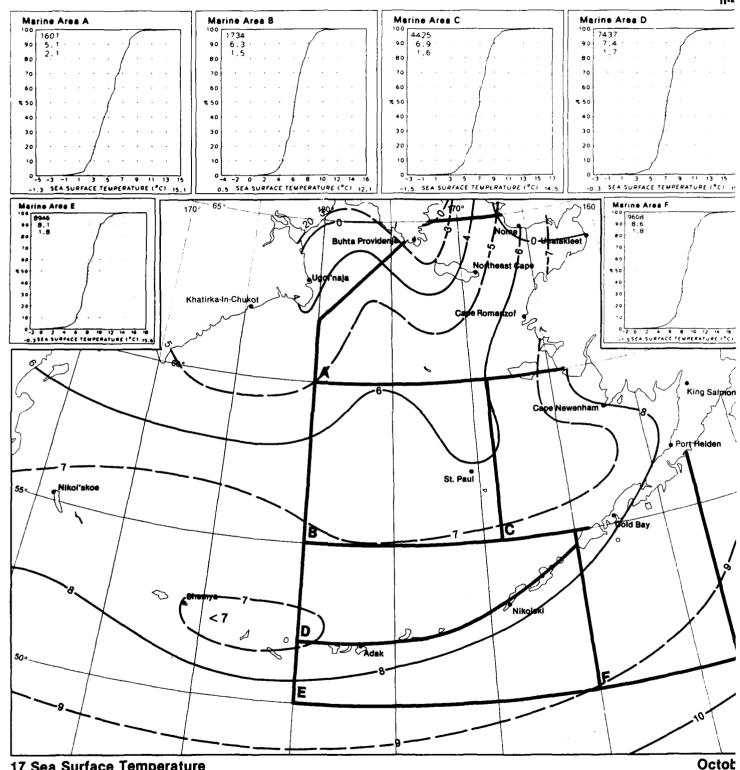




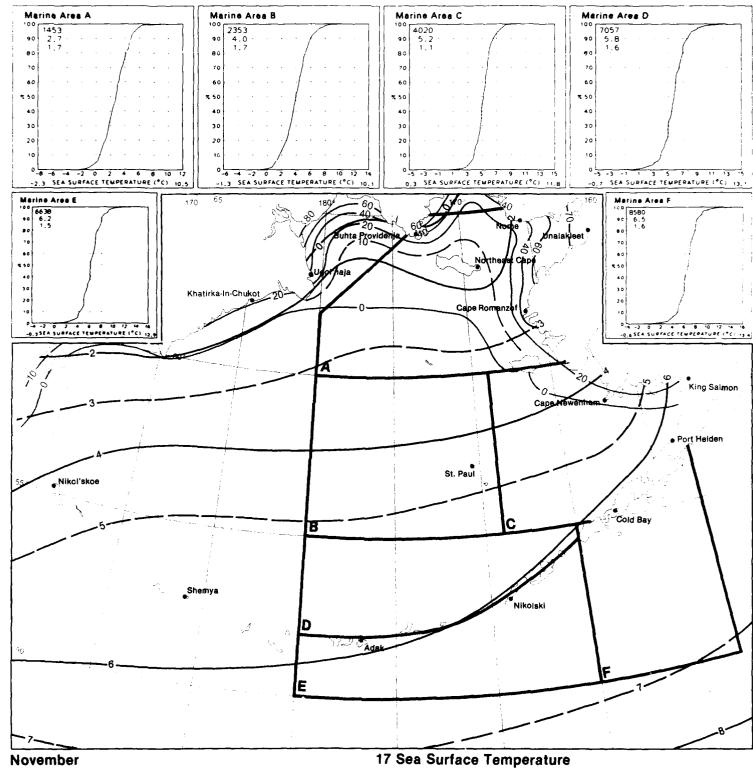
17 Sea Surface Temperature
Mean Sea Surface Temperature and Ice of Any Kind

Augus

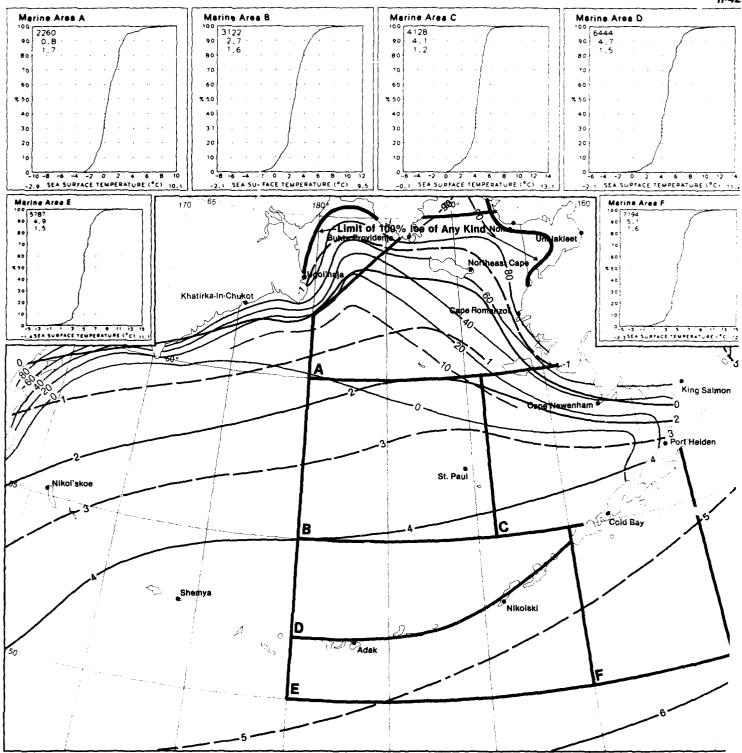




17 Sea Surface Temperature
Mean Sea Surface Temperature and Ice of Any Kind



Mean Sea Surface Temperature and Ice of Any Kind



17 Sea Surface Temperature
Mean Sea Surface Temperature and Ice of Any Kind

Decemi

## Map 18. Wave height ≤3 feet and ice concentration ≥5/10ths

BLACK LINE - Percent frequency of wave height ≤3 feet (1 meter).

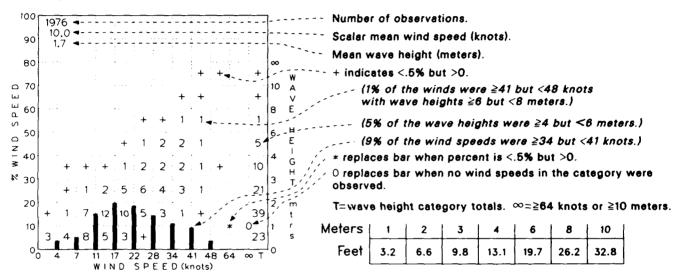
BLUE LINE - Percent frequency of ice concentration ≥5/10ths.

Albers Equal-Area Conic Projection

## Graphs: Wave height/wind speed

Wind speed frequency: Bars are percentages for each wind speed category.

Wave height frequency: Numbers are percentages of wave height for various wind speeds.

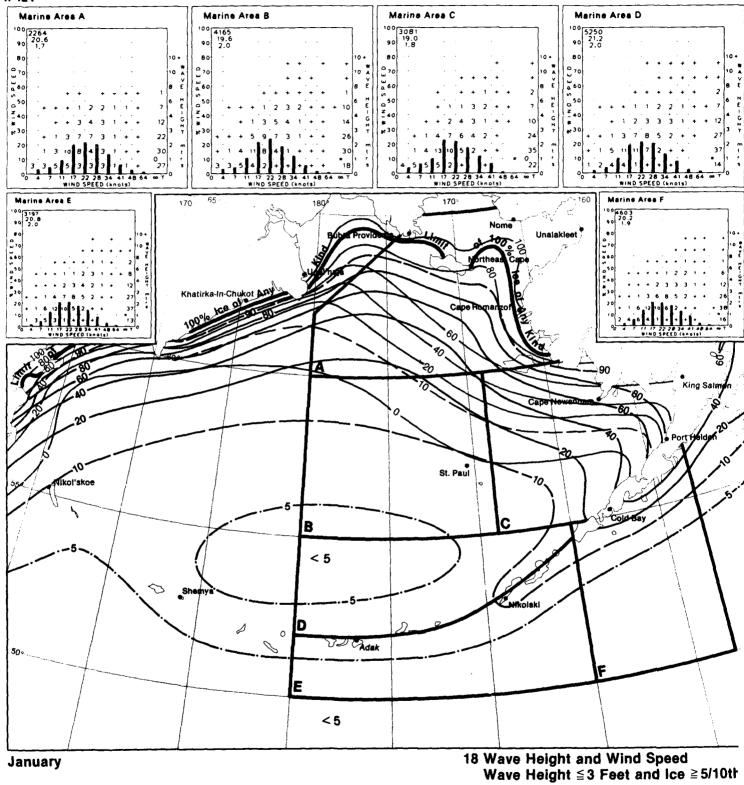


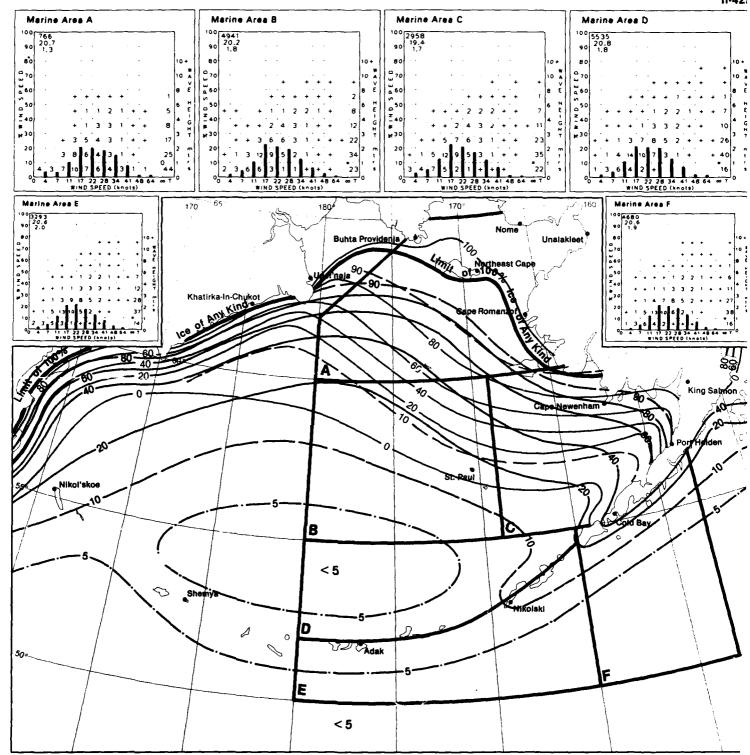
Wave heights have been recorded in a consistent quantitative code only since the late 1940's. The reluctance of many observers to take wave observations in the earlier years and the difficulty in estimating waves, especially in confused seas, make wave observations one of the least commonly observed elements. The observations are also subject to biases in wave characteristics. A correction factor of approximately 10% was suggested by Hogben and Lumb (1967) and has been verified by preliminary work at NCDC where Quayle (1980) found that generally the heights are too low, the periods too short, and sea-swell discrimination poor. The data in this study have not been adjusted for the suspected biases. The marine observations were processed through quality control procedure where an internal check was made between wind speed and sea height. The sea and swell data were then arrayed and suspicious outliers deleted. The higher of the sea wave or swell was selected for summarization. If the heights were equal, the wave with the longer period was selected.

Wave height isopleth presentations in Sets 18 and 19 are for a generally nonhazardous sea condition; i.e., wave heights less than 3 feet and 8 feet, respectively. Isopleth presentations in Set 20 define much more hazardous sea conditions; i.e., wave heights equal to or greater than 12 and 20 feet. Refer to the texts of Sets 14 and 18-21 for complete information on waves, and to the introductory text of Section II for sea ice information.

18 Legend

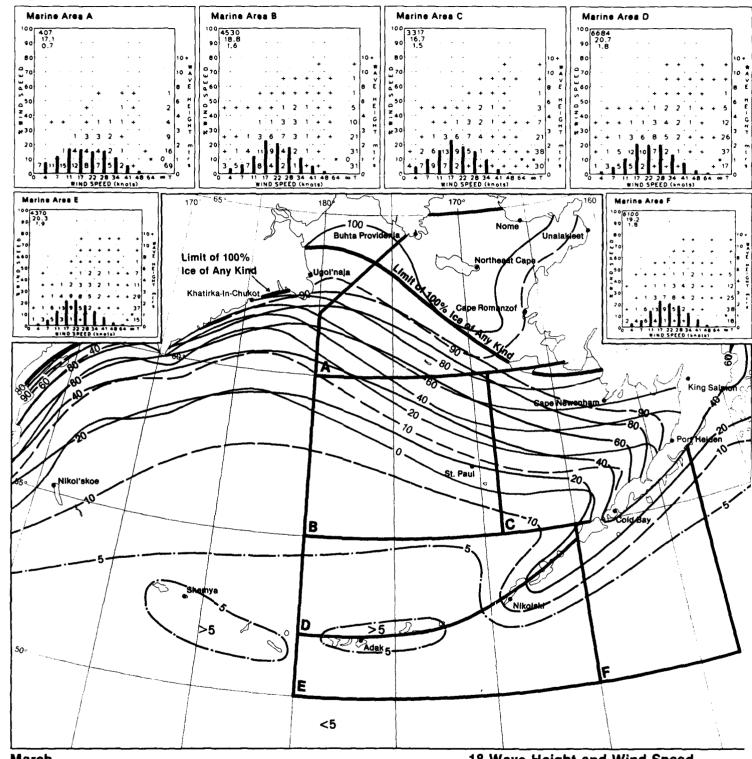
Legend 1





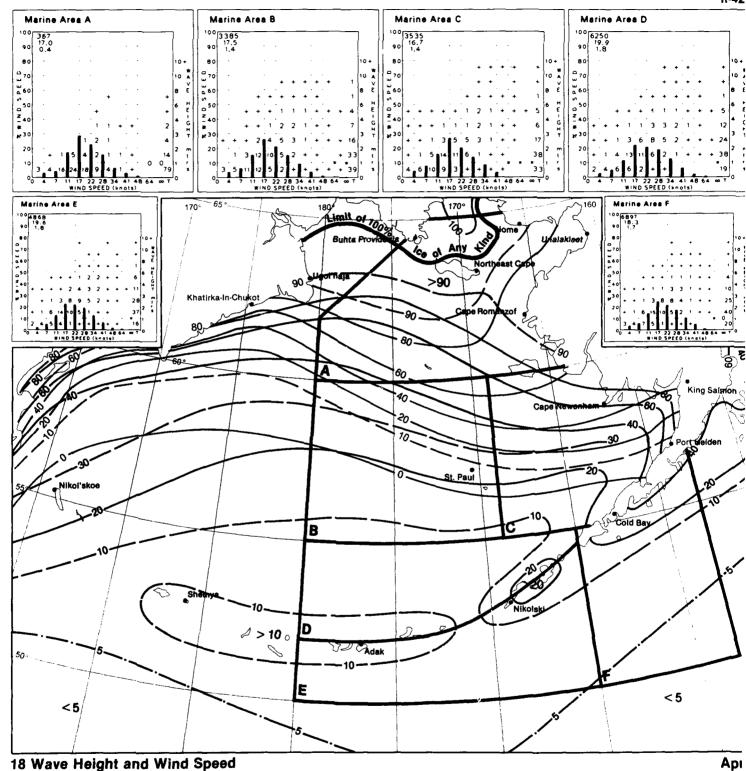
18 Wave Height and Wind Speed
Wave Height ≦3 Feet and Ice ≧5/10ths

Februa

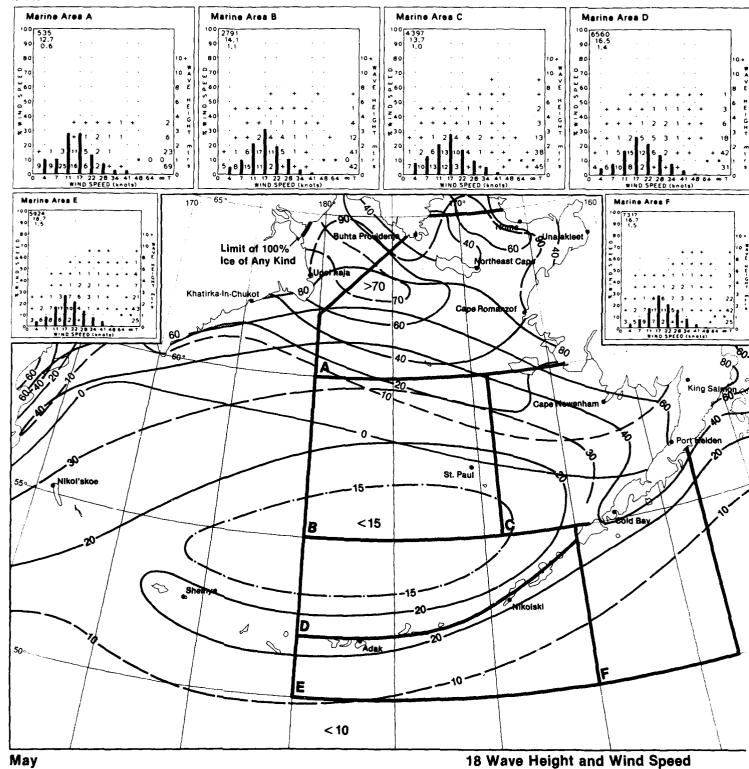


March

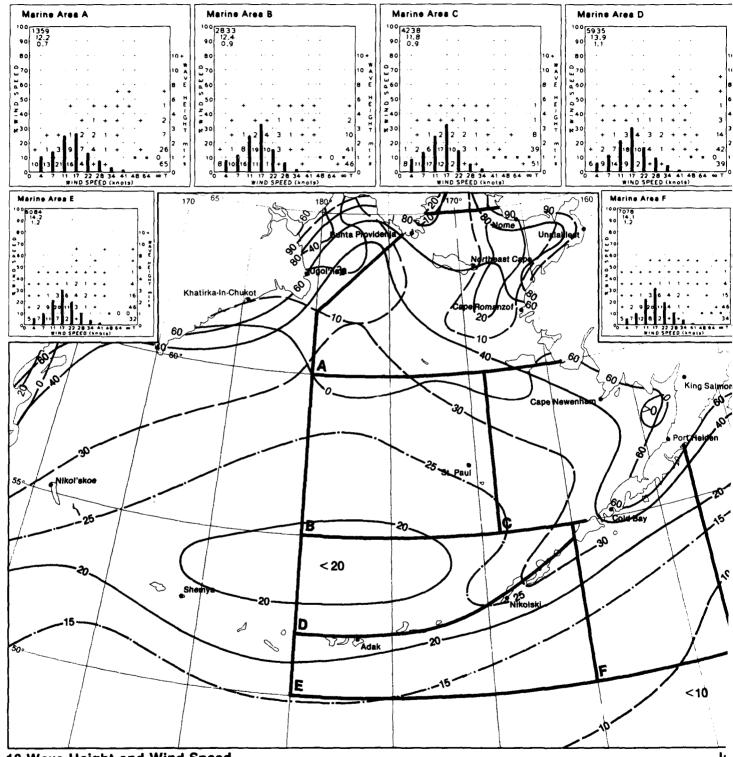
18 Wave Height and Wind Speed Wave Height ≦3 Feet and Ice ≧5/10th



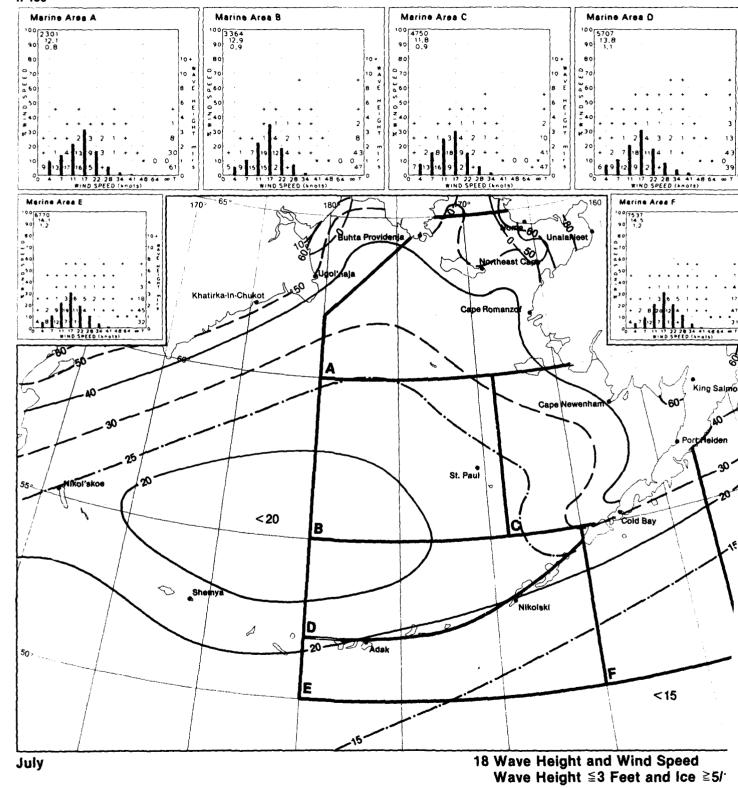
18 Wave Height and Wind Speed Wave Height ≦3 Feet and Ice ≧5/10ths

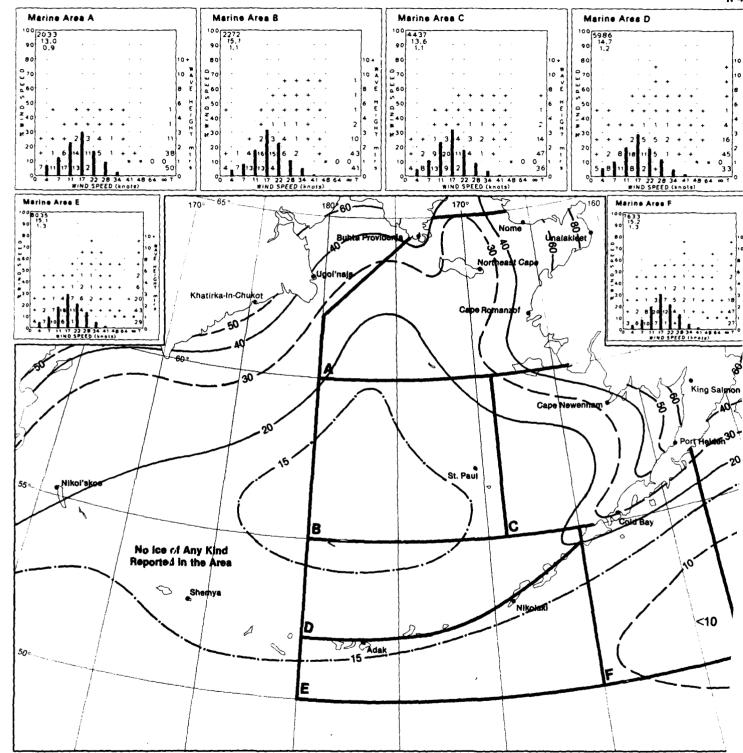


18 Wave Height and Wind Speed Wave Height ≦3 Feet and Ice ≧ 5/10th



18 Wave Height and Wind Speed Wave Height ≦3 Feet and Ice ≩5/10ths

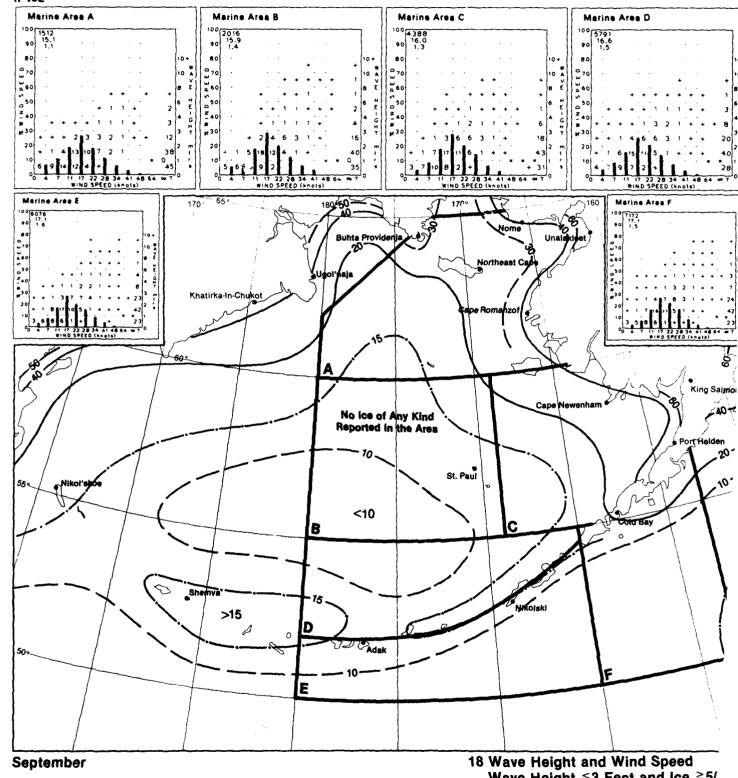




18 Wave Height and Wind Speed
Wave Height ≦3 Feet and Ice ≧5/10ths

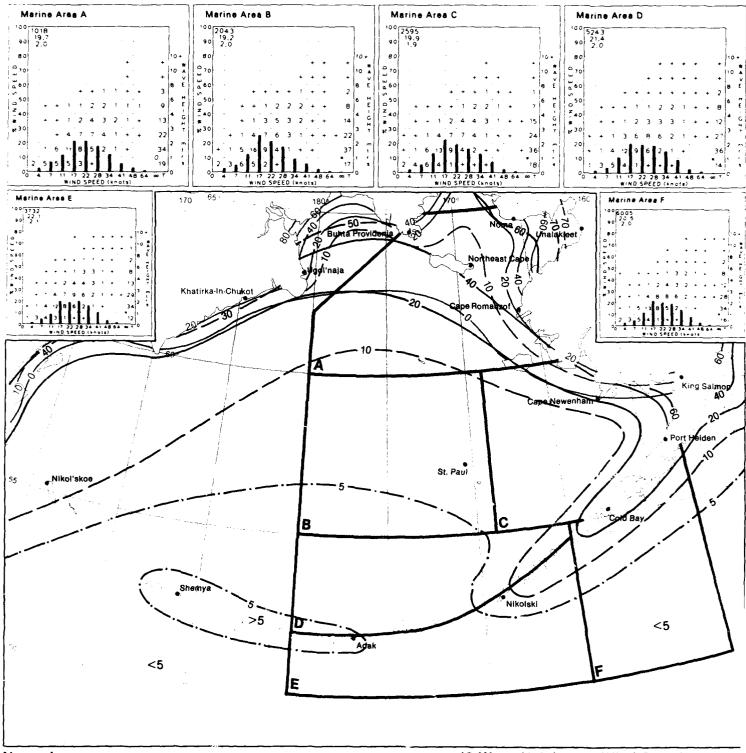
Au





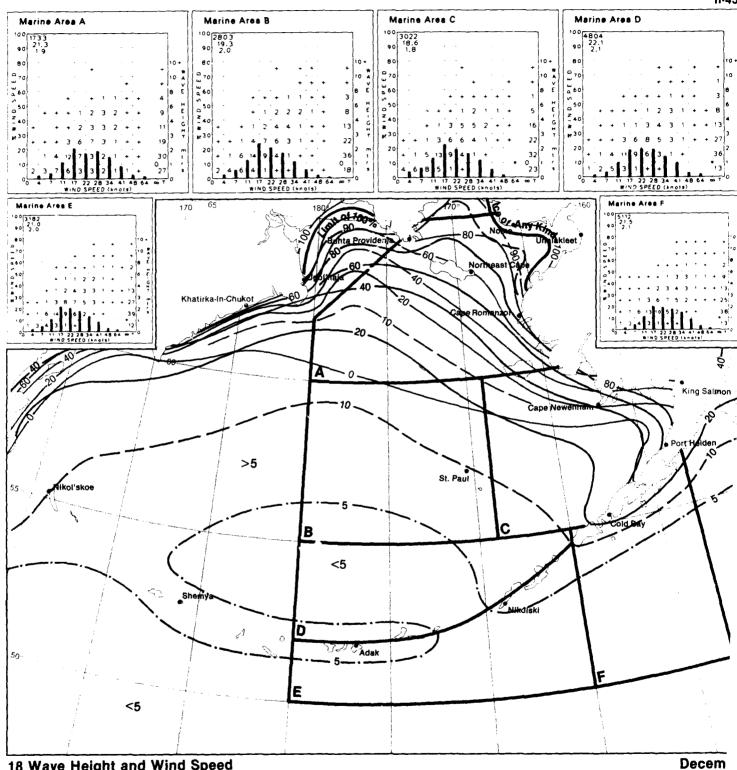
18 Wave Height and Wind Speed
Wave Height ≦3 Feet and Ice ≧5/

18 Wave Height and Wind Speed
Wave Height ≦3 Feet and Ice ≧5/10ths



November

18 Wave Height and Wind Speed
Wave Height ≦3 Feet and Ice ≧5/10th:



18 Wave Height and Wind Speed Wave Height ≦3 Feet and Ice ≧5/10ths

## Map 19. Wave height <8 feet and ice thickness ≥8 feet

BLACK LINE - Percent frequency of wave height <8 feet (2.5 meters).

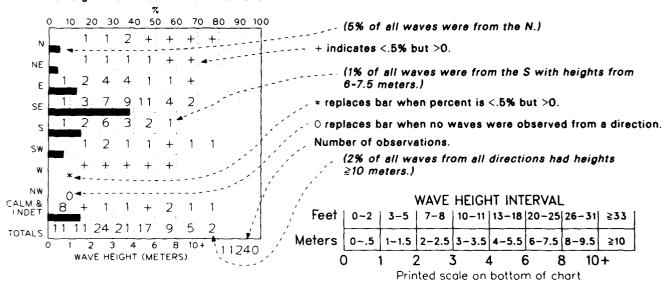
BLUE LINE - Percent frequency of ice thickness ≥8 feet (multi-year ice).

Albers Equal-Area Conic Projection

#### Graphs: Wave height/direction

Direction frequency (top scale): Bars represent percent frequency of waves from each direction.

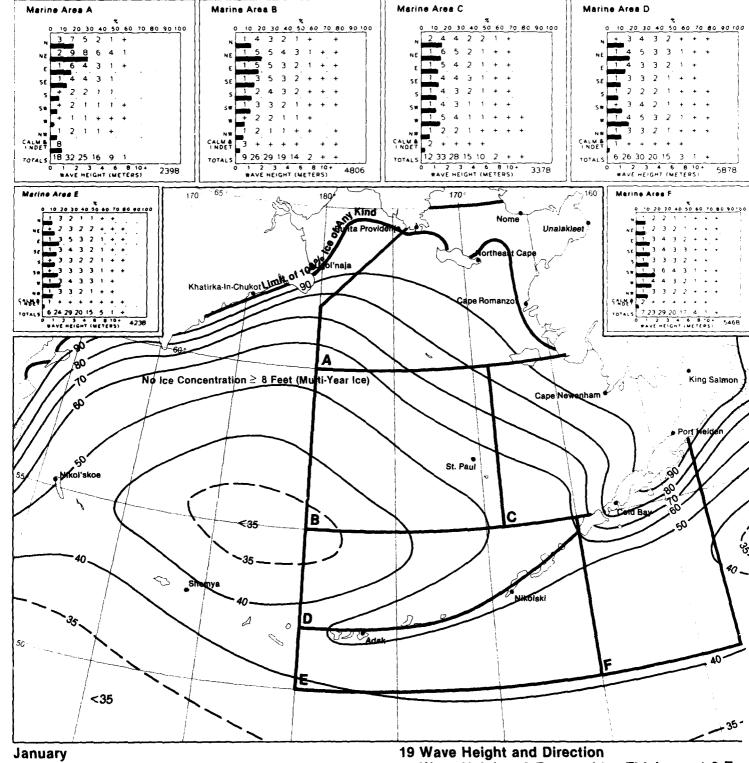
Height frequency (bottom scale): Printed figures represent percent frequency of wave heights observed from each direction.



The observer aboard ship determines and records the period and height of wind waves (sea); and the direction, period, and height of swell waves. Sea waves are waves raised by the local wind and are assumed to have the same direction as the wind Swell waves are waves not raised by the local wind, but rather by distant wind systems or by winds that have sinced ceased to blow. Swell waves characteristically exhibit more regular and longer periods, and have flatter crests than wind waves within their generating area (fetch). Sea and swell waves occur singly or in manifold combination from which they can sometimes be separated only with difficulty.

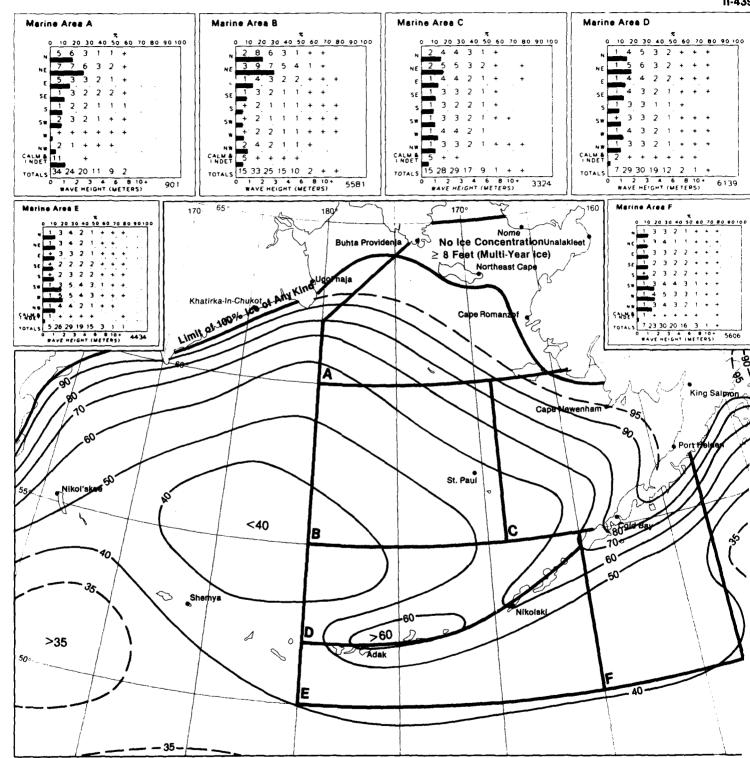
Indeterminate directions are combined with calms in the direction scale of the graph (they can be distinguished by consulting the sea height scale). The number of observations noted on the graphs is from the higher of sea or swell when both arreported; if the heights were equal, then the one with the longer period was selected. If only one wave was reported (sea or swell then that value was used. Refer to the texts of Sets 14 and 18-21 for complete information on waves, and to the introductory tex section of Section II for sea ice information.

19 Legend Legend 1

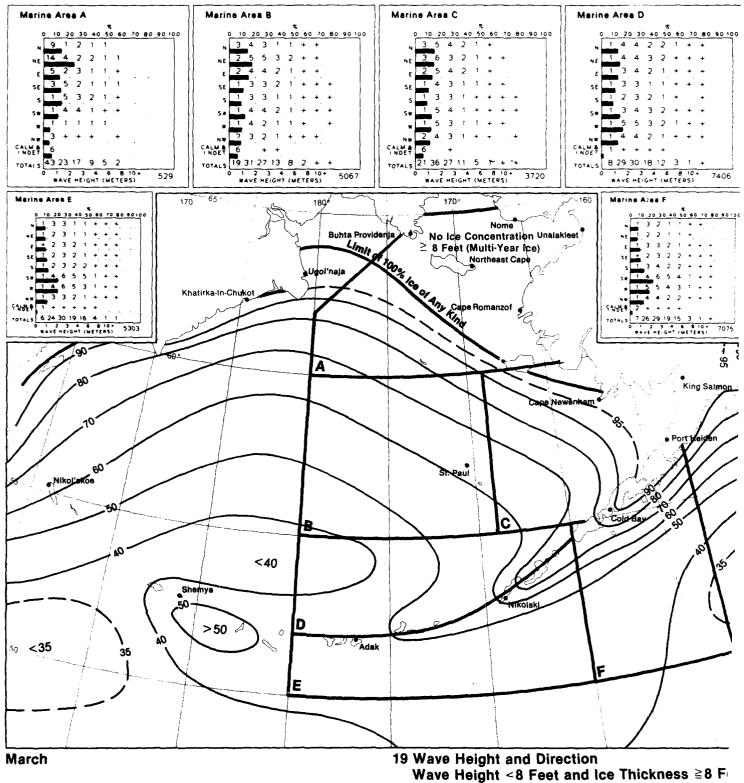


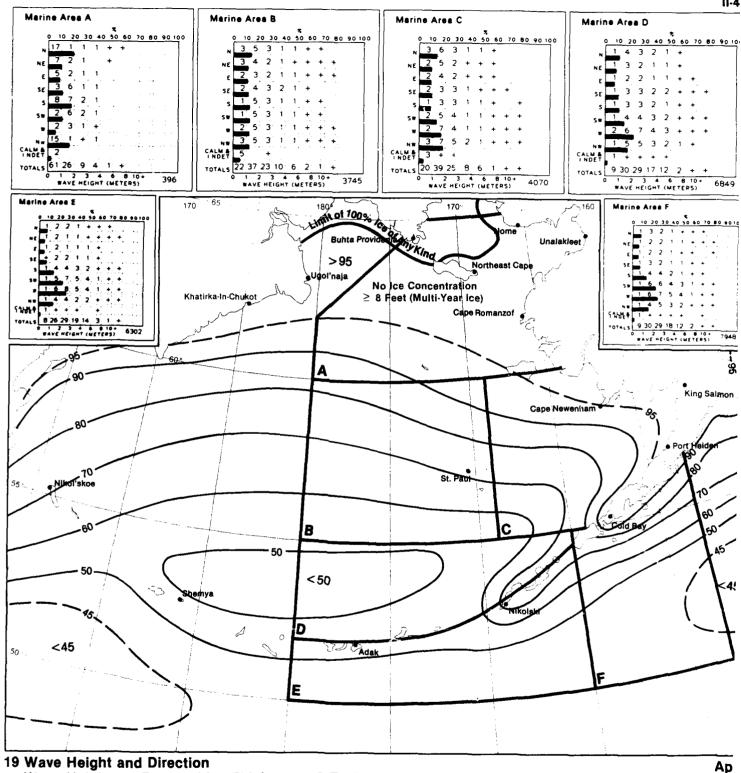
Wave Height <8 Feet and Ice Thickness ≧8 Fe

**Februa** 

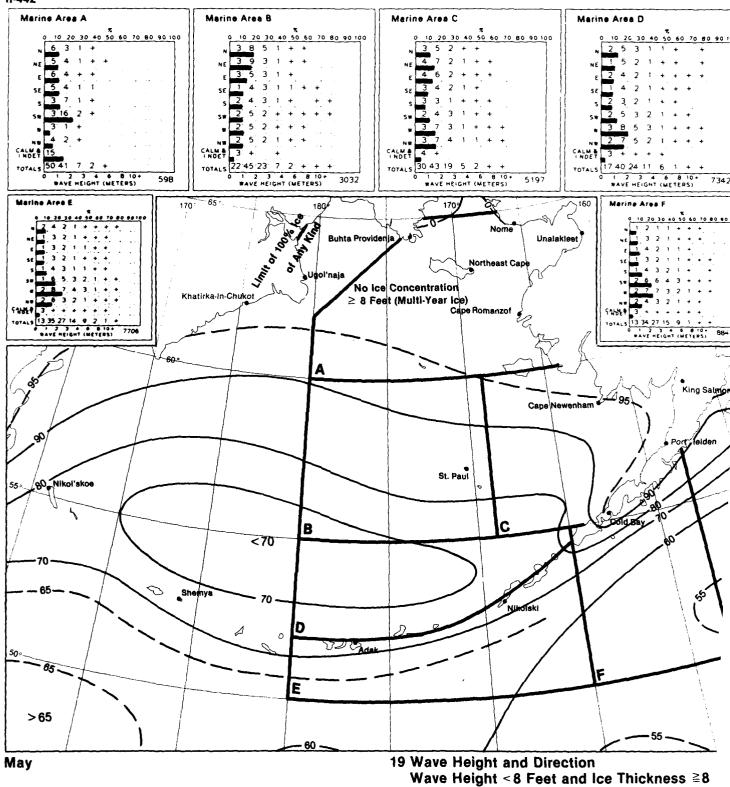


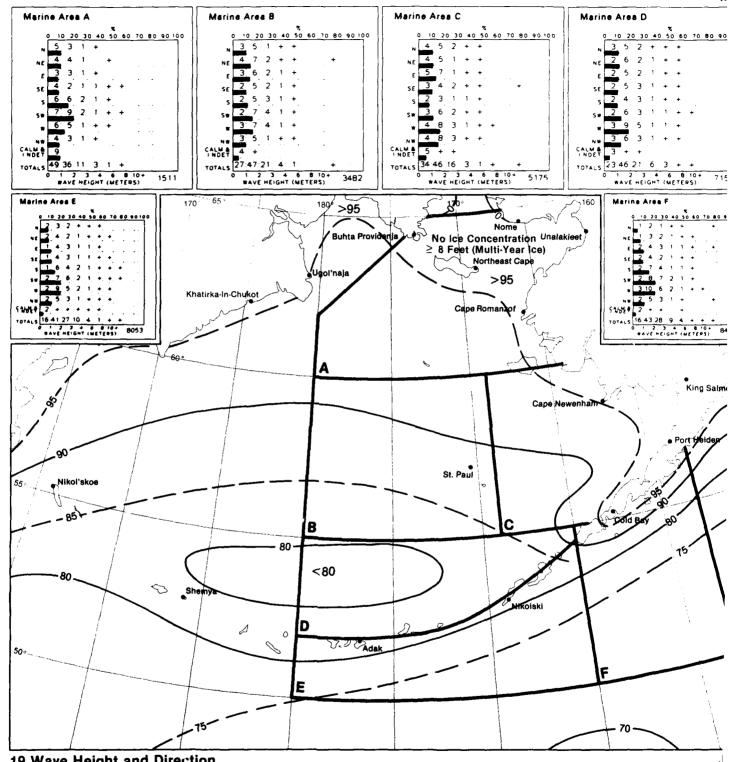
19 Wave Height and Direction Wave Height <8 Feet and Ice Thickness ≧8 Feet



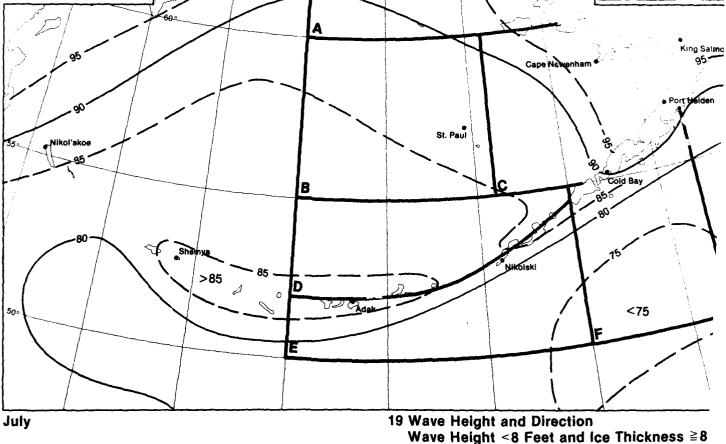


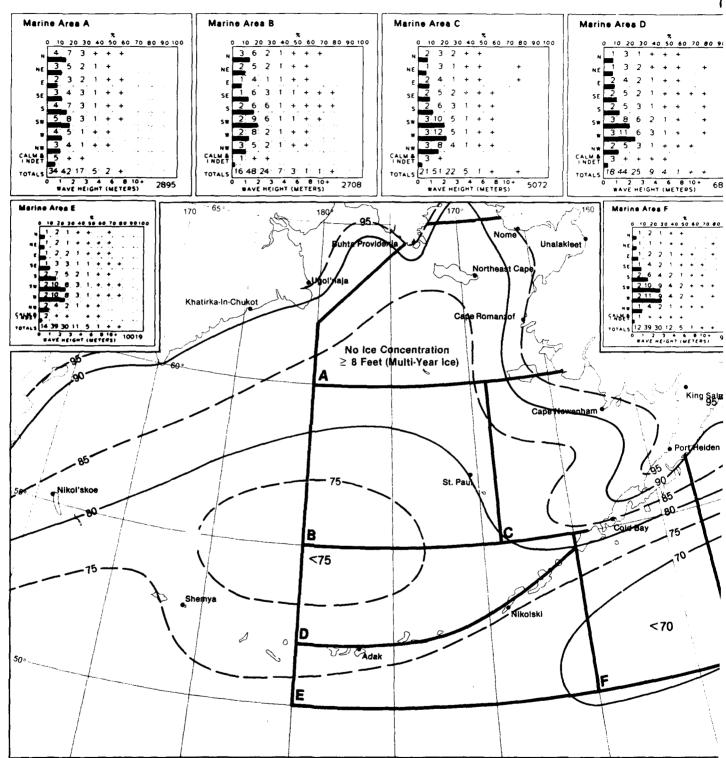
19 Wave Height and Direction Wave Height <8 Feet and Ice Thickness ≧8 Feet





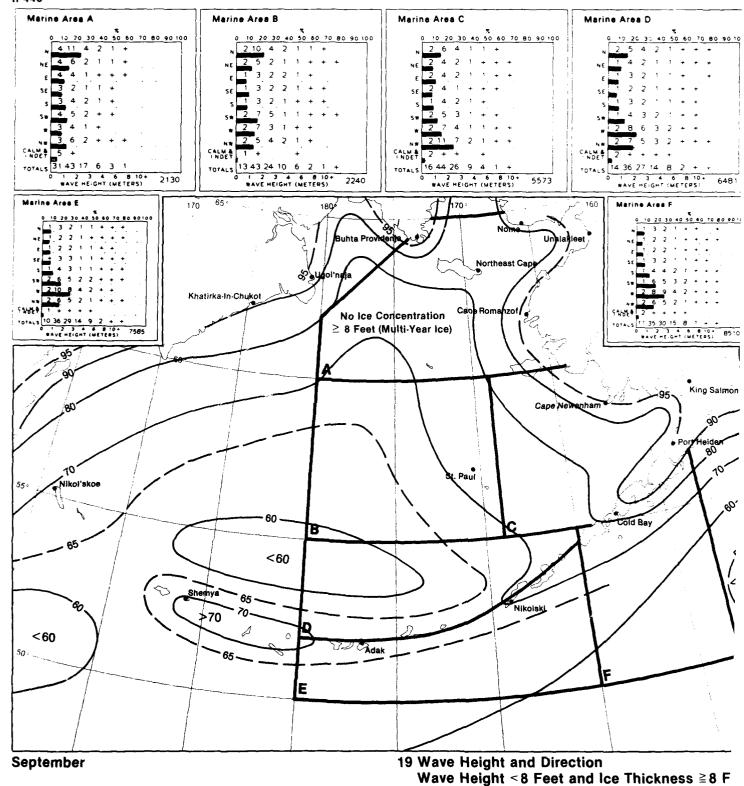
19 Wave Height and Direction
Wave Height <8 Feet and Ice Thickness ≧8 Feet

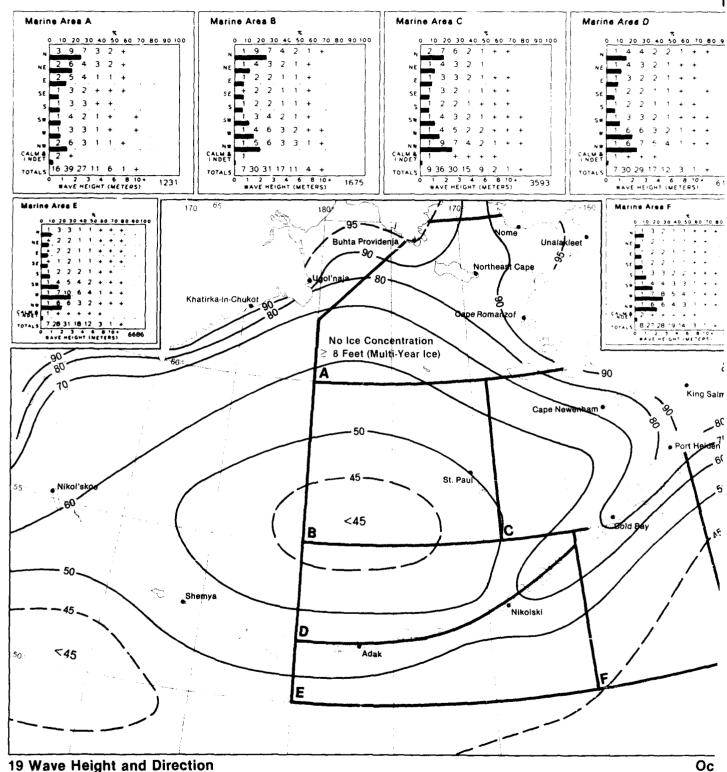




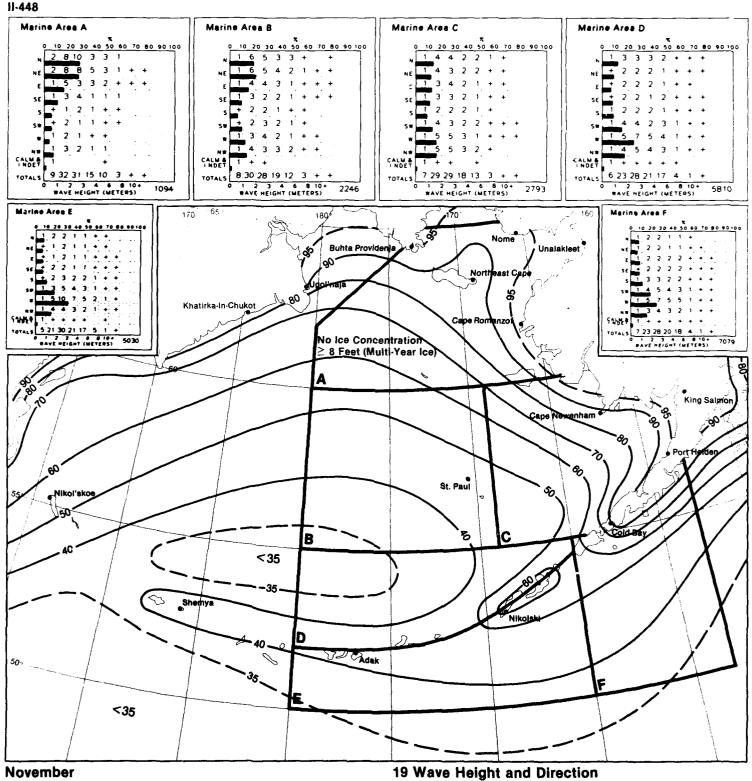
Αu

19 Wave Height and Direction
Wave Height <8 Feet and Ice Thickness ≥8 Feet

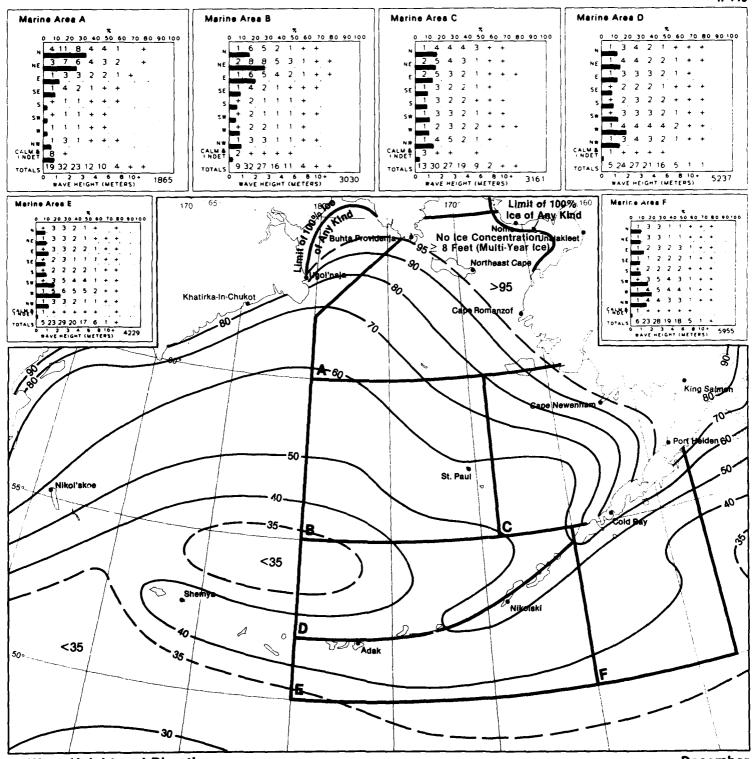




19 Wave Height and Direction
Wave Height <8 Feet and Ice Thickness ≧8 Feet



Wave Height <8 Feet and Ice Thickness ≥8 Feet



19 Wave Height and Direction Wave Height <8 Feet and Ice Thickness ≧8 Feet

December

### Map 20. Wave height $\ge$ 12 and $\ge$ 20 feet

BLACK LINE – Percent frequency of wave height  $\geq 12$  feet ( $\geq 3.5$  meters).

BLUE LINE — Percent frequency of wave height ≥20 feet (≥6 meters).

Albers Equal—Area Conic Projection

### Graphs: Wave height/period

Percent frequency of occurrence of wave period and height.

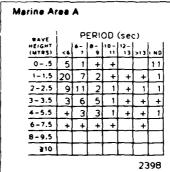
WAVE		Ł	PERI	OD	(sec	)			
HEIGHT (MTRS)	<6	6 - 7	8- 9	10 – 11	12-	>13	IND		
05	21	3	1	+	+	+	6		+ indicates <.5% but >0.
1-1.5	22	16	6	2	1		+		(2% of observed waves had a height of 1-1.5 meters
2-2.5	3	6	4	3	1	+	+		and a period of 10-11 seconds.)
3-3.5	+	1	1	1	1	+	+	,-	Number of observations.
4-5.5	+	+	+	+	+	+	0	,′	
6-7.5	0	+	+	0	0	+	0		Waves are selected on the basis of the higher of sea and swell
8-9.5	0	0	0	+	0	0	0		when both are reported. If both heights are equal, the wave with the longer period is selected.
≥10	0	0	0	0	0	+	0	, '	
						40	10	•	

Wave period is the interval in seconds between the passage of two successive crests or troughs of well-formed waves past a fixed point. Waves in the same system usually occur in a sequence of a few large, well-formed waves followed by an interval in which only small and poorly-formed waves occur, and another series of well-formed waves, etc. Observers aboard ship determine the values of wave height, period, and direction generally using only the well-formed waves and ignoring poorly-formed waves. To describe a similar sea state from a measured wave record, a statistical approach is used to describe the significant wave height ( $\overline{H}$  1/3) which is the average of the highest one-third of the measured waves. This roughly approximates the characteristic height observed visually from aboard ship. To determine the period of wind waves or swell, the observer needs only to select a distinctive patch of foam or a small floating object at some distance from the ship. As the object falls astern, a new one is selected. The elapsed time is determined to the nearest second between the instant when the object is on the crest of the first and of the last well-formed wave in the group. Noting the number of crests that pass under the object during the interval permits computation of the average period. An experienced observer needs only to observe a few representative wave "sets" to derive the average period.

The number of observations noted on the graphs is that of those observations reporting both wave height and period. The wave height isopleth presentations are for a generally hazardous sea condition (wave heights equal to or greater than 12 feet). Refer to the texts of Sets 14 and 18-21 for complete information on waves.

20 Legend

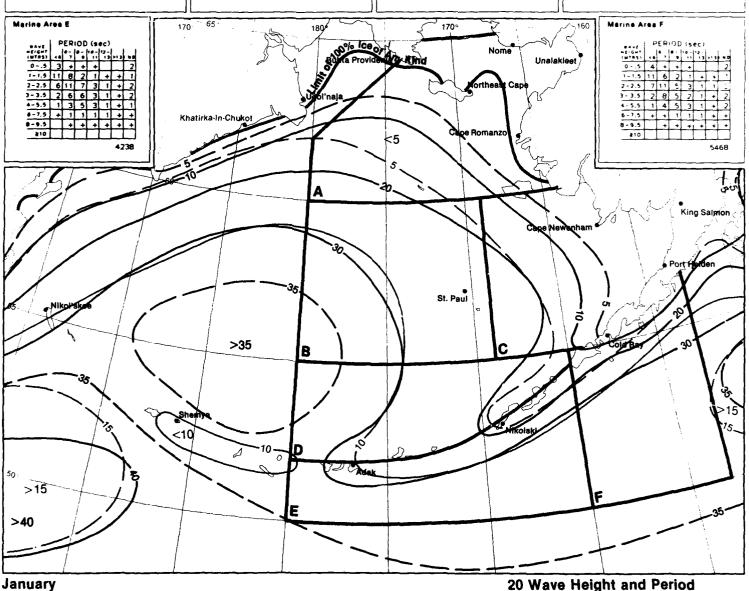
Legend 20



WAVE	i	P	ERI	OD	(se	2)	
HEIGHT (MTRS)	< 6	6 - 7	8 - 9	10 - 11	12 -	>13	. 40
05	4	1	+	+			4
1-1.5	14	5	2	1	+	+	3
2-2.5	9	12	3	2	1	+	_3
3 - 3.5	2	8	6	1	+	+	_2
4-5.5	1	3	5	2	+	+	2
6-7.5	+	+	1	1	+	+	+
8-9.5		+	+	+	+	+	+
≩10							

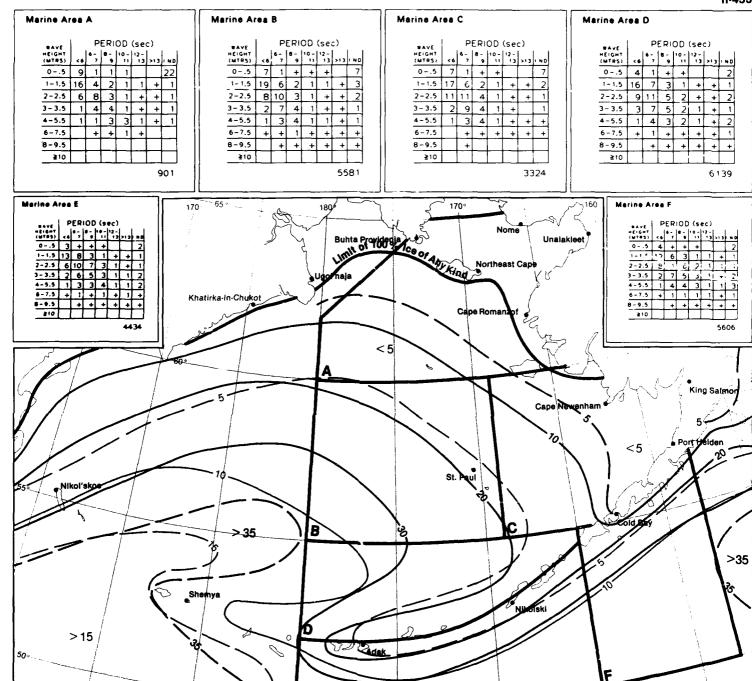
Marine Ar		С					
#AVE	ļ	P	ERI	OD	(se	c)	
HEIGHT (MTRS)	<6	6-7	8-	10 -	12-	>13	. 40
05	7		+	+			3
1-1.5	19	8	2	1	1	+	2
2-2.5	11	11	3	1	+	+	2
3 - 3.5	2	9	3	+	+	+	1
4-5.5	+	4	3	1	+	+	1
6-7.5		+			+	+	+
8-9.5		+	+	+	+		
≩10							
	_					33	378

WAVE		PERIOD (sec)								
HEIGHT (MTRS)	< 6	6-,	8 - 9	10 - 11	12-	>13	: N D			
0~.5	3	+	+	+			2			
1-1.5	14	7	1	1	1	+	2			
2-2.5	10	1 1	4	2	1	+	2			
3 - 3.5	3	8	5	2	+	+	1			
4-5.5	1	4	4	3	1	+	1			
6-7.5	+	1	1	1	+	+	+			
8-9.5		+	+	+	+	+	+			
≩10										

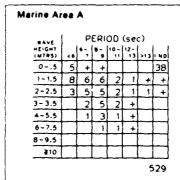


20 Wave Height and Period Wave Height ≧12 and ≥20 Feet

**February** 



20 Wave Height and Period Wave Height ≥12 and ≥20 Feet

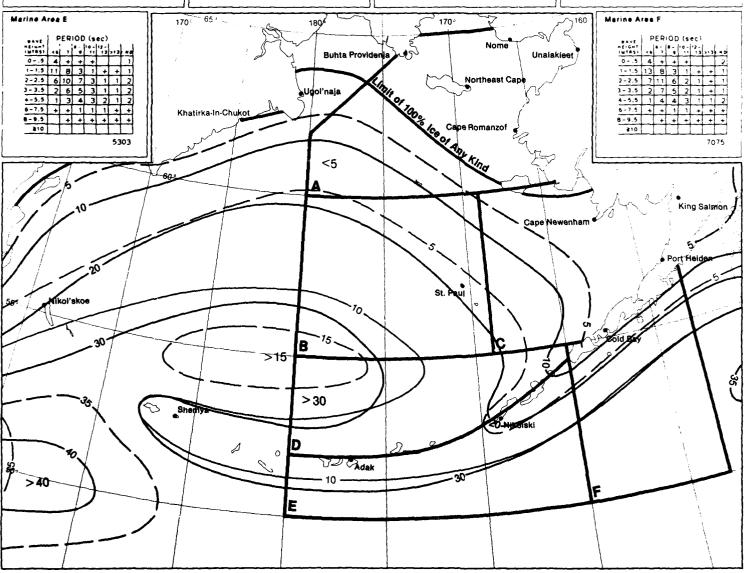


WAVE	1	Р	ERI	OD	(se	c)	
HEIGHT	<6	6-	9-	10 -	12-	>13	NS
05	9	1	+	+			8
1-1.5	16	6	3	2	1	+	2
2~2.5	7	11	4	2	1	+	1
3 - 3.5	2	6	3	1	+	+	1
4~5.5	1	2	3	1	+	+	1
6-7.5	+	+	+	+	+	+	+
8-9.5		+	+	+	+	+	+
≩10							

WAVE	í	ρ	ERO	00	(se	c)	
HEIGHT (MTRS)	< 6	6-,	9 -	10-	12~	>13	
05	11	1	+	+			9
1-1.5	21	s	3	1	+	+	2
2-2.5	7	12	5	1	+	+	1
3-3.5	1	4	3		+	+	+
4-5.5	1	1	2	1	+	+	1
6-7.5		+	+	+	+	+	+
8-9.5		+	+	+		+	
≥10							
						37	20

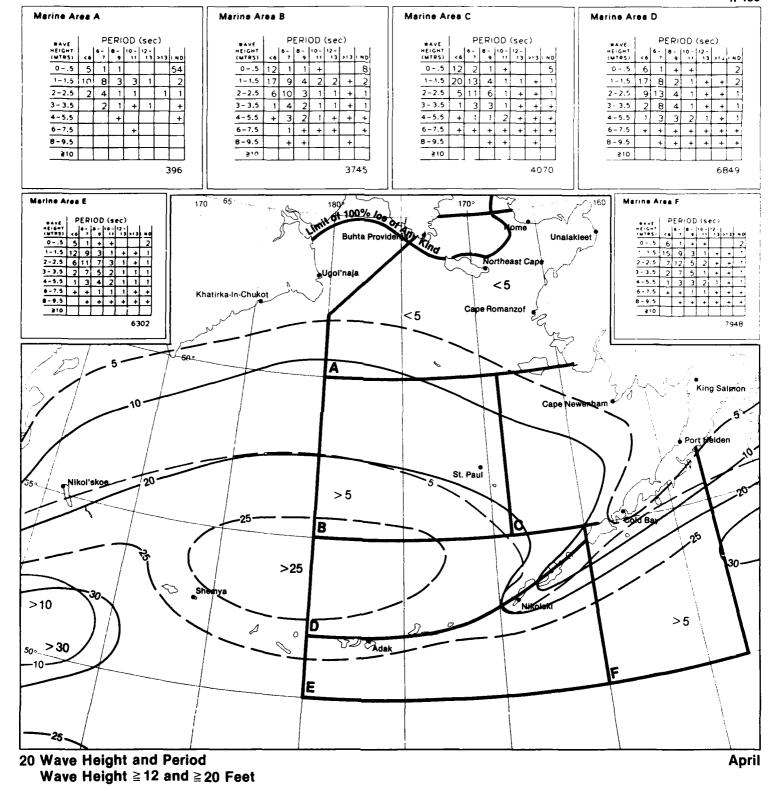
Marine Area C

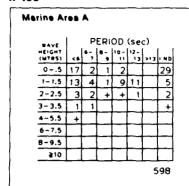
WAVE	į	Р	ERI	OD	(se	PERIOD (sec)								
HEIGHT (MTRS)	<6	6 - 7	8 -	10-	12-	13 د	. 40							
05	5	1	+	+			2							
1-1.5	15	8	3	. 1	+	+	1							
2-2.5	9	13	4	1	+	+	_1							
3 - 3.5	2	8	4	1	1	+	1							
4-5.5	1	4	3	2	1	+	1							
6-7.5	+	1	+	1	+	+	+							
8-9.5		+	+	+	+	+	+							
₹10														



March

20 Wave Height and Period Wave Height ≧12 and ≧20 Feet

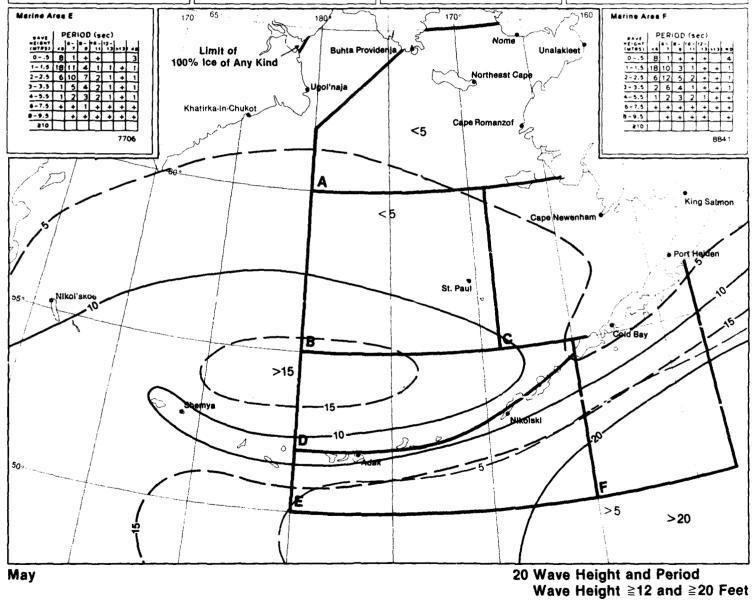


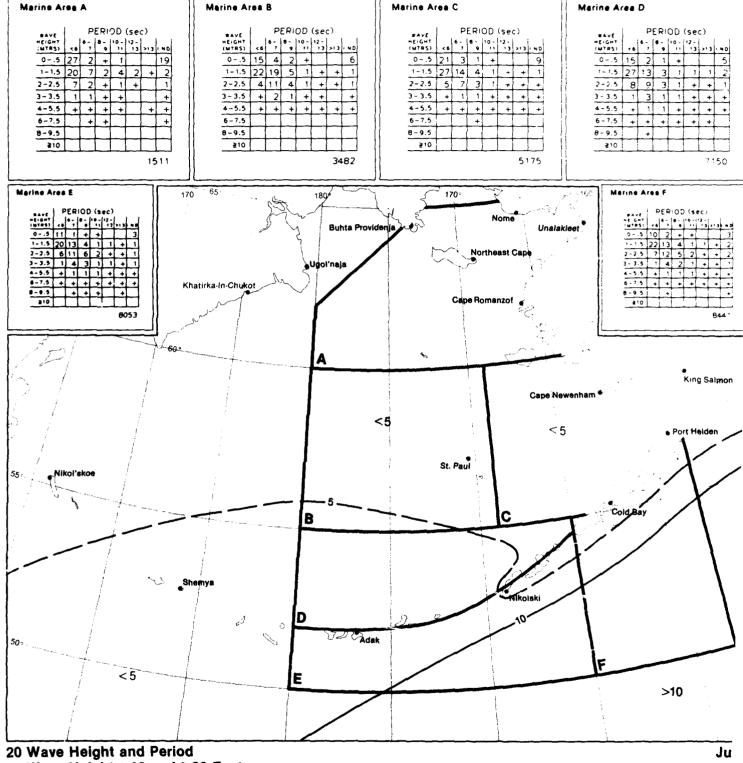


WAVE	1	P	ERI	ac	(se	c)	
HEIGHT (MTRS)	< 6	6-,	8 -	10 -	12-	>13	
05	13	2	1	1			5
1-1.5	23	15	2	2	1	+	2
2-2.5	4	13	_3	1	+	+	_2
3-3.5		4	2	+	+		+
4-5.5	+	1	+	+	+	+	+
6-7.5		+	+	+		+	+
8-9.5			+				
≩10	Γ						

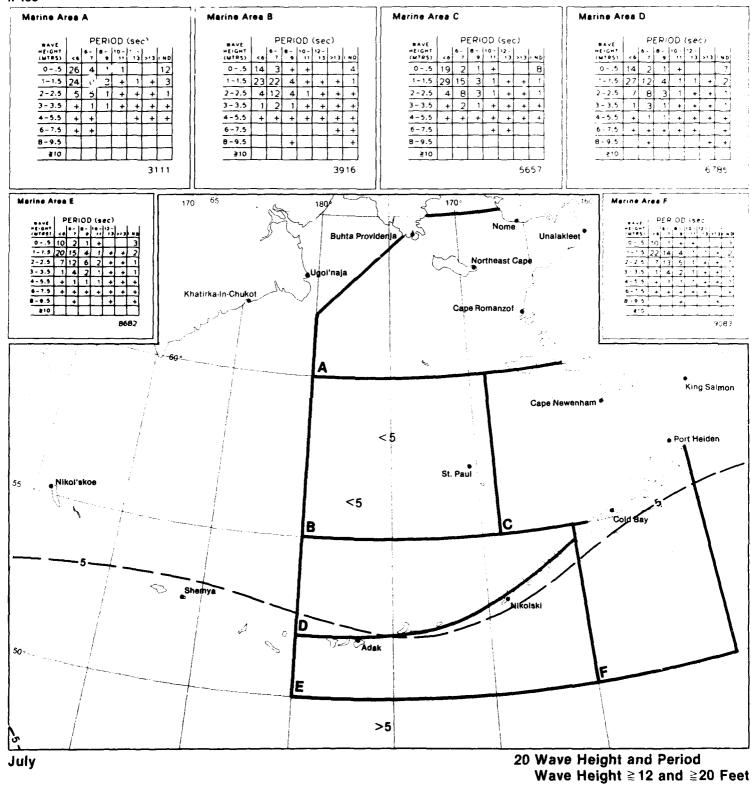
Marine A	0.8	С					
WAVE		P		OD		c)	
HEIGHT (MTRS)	₹6	6 - 7	9	10 -	12 -	>13	I N D
05	20	2	1	+		+	7
1-1.5	25	13	_3	1	+	+	1
2-2.5	4	9	5	1	+	+	+
3-3.5	1	2	1	1	+	+	+
4-5.5	+	1	1	+	+	_+	+
6-7.5		+	+	+		+	+
8-9.5		+		+	+		
≥10							
	_			_		5 1	97

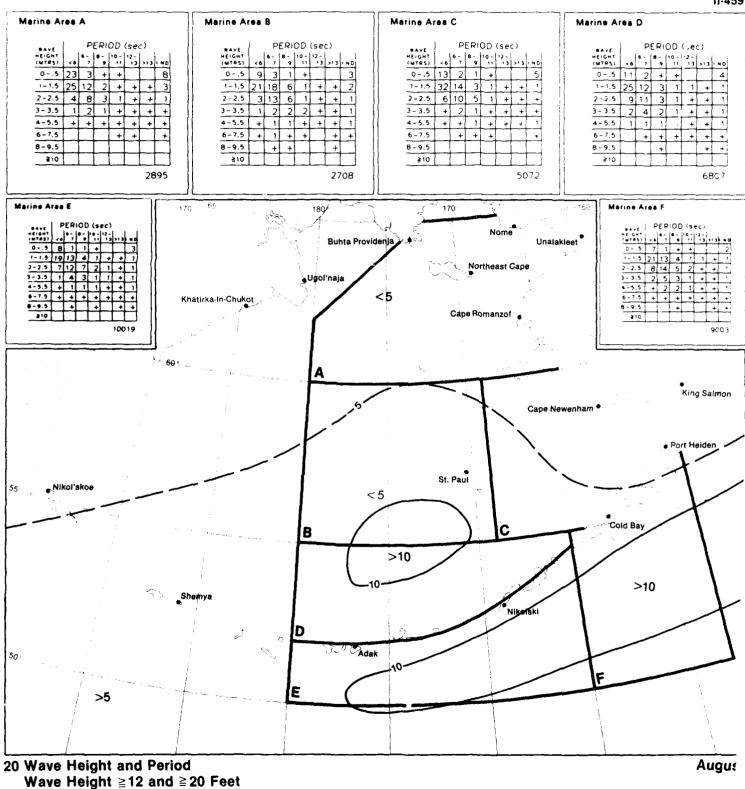
WAVE	l	P	ERI	OD	(se	:)	
HEIGHT	< 6	6-,	8 -	10-	12-	>13	, NO
05	10	2	1	+			4
1-1.5	24	10	3	1	1	+	2
2-2.5	8	10	3	1	+	1	1
3 - 3.5	2	4	2	1	+	+	+
4-5.5	1	1	1	1	+	+	+
6-7.5	+	+	+	+	+	+	+
8-9.5		+	+	+	+		
≥10							

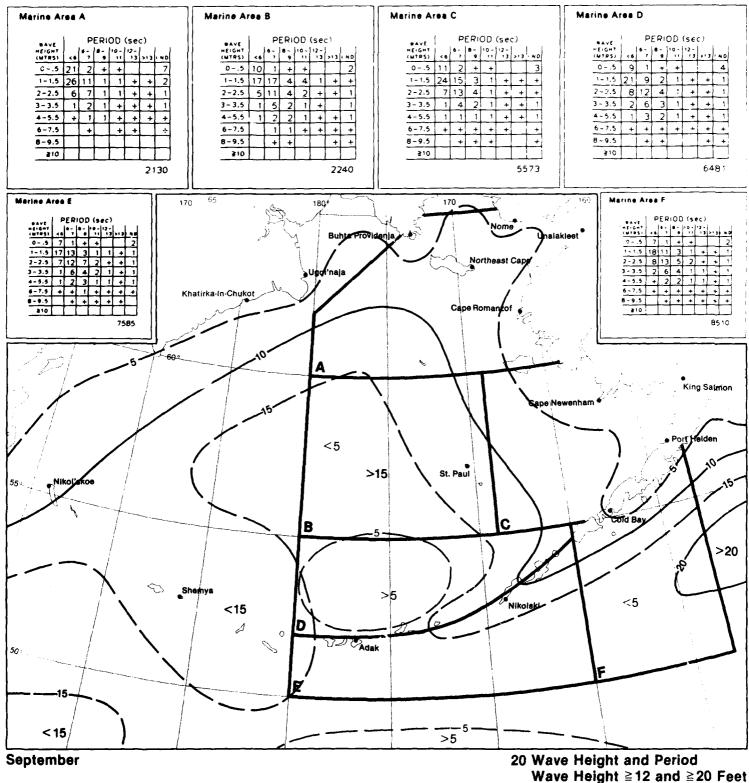


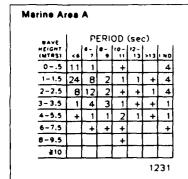


Wave Height ≥12 and ≥20 Feet





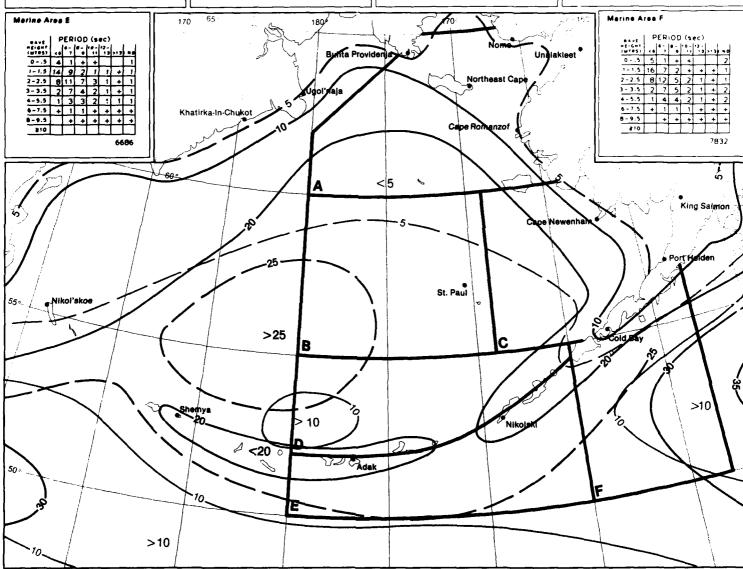




WAVE	1	Ρ	ERI	ΟĐ		c)	
HEIGHT (MTRS)	<6	6-,	8-	10 -	12-	>13	1 40
05	5	1	+	+			1
1-1.5	16	9	3	1	+	+	2
2-2.5	11	11	5	2	+	+	3
3-3.5	2	7	4	2	+	+	3
4-5.5	1	4	3	1	+	+	2
6-7.5	+	1	+	1	+	+	+
8-9.5		+		+	+	+	
≥10						I _	Ī <sup>—</sup>

WAVE	1	Ρ	ERI	GO	(se	c)	
HEIGHT (MTRS)	< 6	6-,	8 - 9	10 - 11	12-	>1 <b>3</b>	
05	6	1	+	+			2
1-1.5	18	13	2	1	+	+	1
2-2.5	8	17	3	1	+	+	3
3 - 3.5	2	7	4	_1	+	+	1
4-5.5	_	2	3	1	+	+	_ 2
6-7.5	+	+	1	+	+	+	+
B-9.5		+	+	+	+	+	
≥10						Γ	

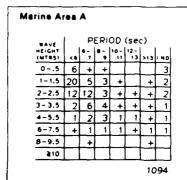
MAYE , PERIOD (sec)											
HEIGHT (MTRS)	<6	6 - 7	8 - 9	٠٥-	17-	>13					
05	4	1	+	+			2				
1-1.5	17	9	2	1	+	+	1				
2-2.5	9	13	4	1	+	+	2				
3 - 3.5	3	7	5	1	+	+	2				
4-5.5	1	3	4	2	+	+	2				
6-7.5	+	1	1	+	+	+	+				
8-9.5		-	+	+	+	+	+				
≩10	$\Box$										



20 Wave Height and Period Wave Height ≧ 12 and ≧ 20 Feet

October

November

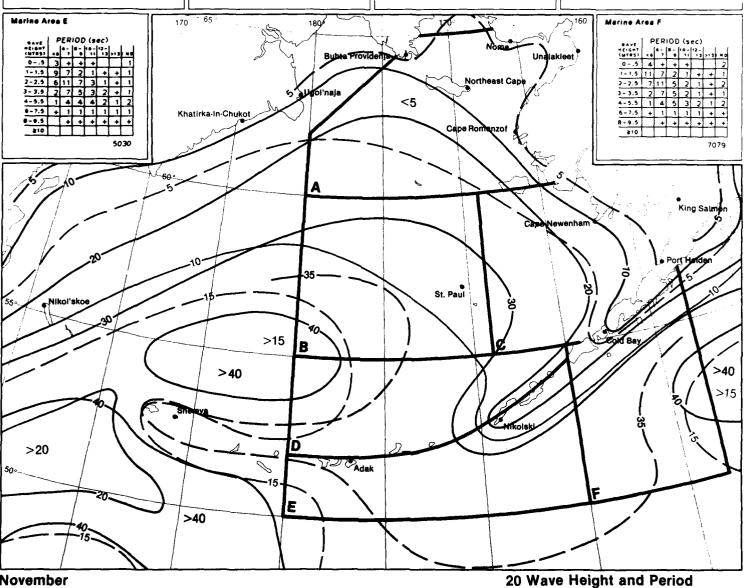


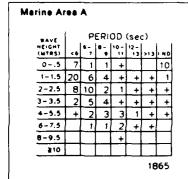
Marine A		8									
MAVE	1	Ρ	ERI	OD	(se	c)					
HEIGHT (MTRS)	<6	<6 7 9 11 13 >13 I ND									
05	5	+	+	+			2				
1-1.5	20	5	2	1	+	+	2				
2-2.5	9	12	3	1.	+	+	2				
3-3.5	2	7	6	1	1	+	2				
4-5.5	2	3	3	2	+	+	2				
6-7.5		1	1	1	+	1	+				
8-9.5		+	+	+	+	+	+				
≩10											
						22	46				

WAVE	ļ	PERIOD (sec)							
HEIGHT (MTRS)	< 6	6-,	8 - 9	10-	12 -	>13	: ND		
05	5	1	+				2		
1~1.5	15	9	_3	1	+	+	2		
2-2.5	9	14	4	1	+	+	1		
3-3.5	2	10	3	1	+	+	1		
4-5.5	1	3	4	2	+	+	1		
6-7.5	+	1	1	1	+	+	+		
8-9.5		+	+	+	+	+	+		
≩10									

BAVE	1	Ρ	ERI	OD	(se	c)	
HEIGHT (MTRS)	< 6	6-,	8 - 9	10 -	12 - 13	>13	0
05	_ 3	1	+	+			2
1-1.5	12	6	1	1	+	+	1
2-2.5	9	11	4	2	+	+	2
3 - 3.5	3	8	5	2	+	+	1
4-5.5	1	5	5	2		+	2
6-7.5	+	1	1	1	1	+	1
8-9.5		+	+	+	+	+	+
≩10							

Wave Height ≥12 and ≥20 Feet

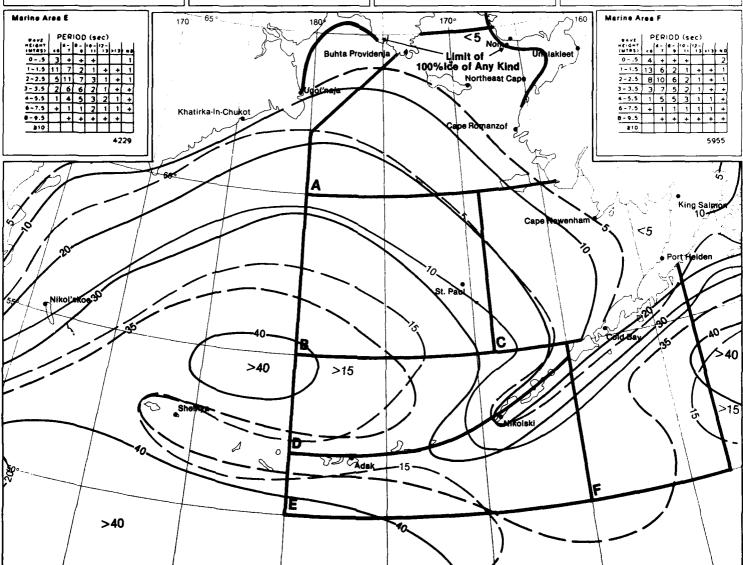




WAVE	ĺ	Ρ	ERI	OD	(se	c)	
NEIGHT (MTRS)	< 6	6-,	8-	10 -	12 - 13	>13	0
05	4	+	+	+			3
1-1.5	22	5	1	1	+	+	2
2-2.5	9	12	2	1	1	+	1
3-3.5	2	7	5	+	+	+	1
4-5.5	1	2	4	2	+	+	1
6-7.5	+	+	1	1	+	+	
8-9.5		+	+	+		+	
≩10							

WAVE	1	PERIOD (sec)						
HEIGHT (MTRS)	< 6	6 - 7	8 - 9	10-	12-	>13		
05	8	2	+	+			3	
1-1.5	18	R	1	1	_+	+	1	
2-2.5	9	13	3	-	_+	+	1	
3-3.5	1	10	3	1	_+		1	
4-5.5	+	2	3	2	_+		+	
6-7.5	+	+	+	1	_+	+	+	
8-9.5		+	+	+	+			
≩10								

Marine A	• •	D						
WAVE		P	ERI			c)		
MEIGHT (MTRS)	<6	6-,	8 -	10-	12-	>13	I N D	
05	3	+	+	+			1	
1-1.5	13	6	2	1	+	+	1	
2-2.5	8	10	5	2	+	+		
3 - 3.5	3	9	5	2	1	+	1	
4-5.5	1	4	5	2	1	+	+	
6-7.5	+	1	- 1	1	1	+	+	
8-9.5		_+	+	+	+	+	+	
≥10								
						52	37	



20 Wave Height and Poriod Wave Height ≧12 and ≥20 Feet

December

# Map 21. Wave height thresholds

TABLE - Wave height frequencies.

Albers Equal—Area Conic Projection

# Graphs: Wave height thresholds

Wave height frequencies.

	%	WAVE HEIGHT (M)
Percent frequency of various ranges within the area.	10.0 F	0-0.5
(30.0% of all observed wave heights were in the range 2 to 2.5 meters.)	20.0	1-1.5
(ne range 2 to 2.5 meters.)	30.0	2-2.5
N = Observation count.	20.0	3-3.5
	10.0	4-5.5
Wave data for these tables were selected from the higher of sea or swell when both were reported.	10.0	≥6.0
•	1363	N=

The wave height should be estimated from the best available point on the ship that permits the height of the waves to a compared to the height of the ship. The point of observation should be chosen amidships where the pitching of the vessel is a minimum, and the wave height should be estimated when the ship is on an even keel. In general, it has been found by comparing instrument measurements to "eyeball" estimates that small wave heights are underestimated while large wave heights a overestimated. Theoretically, the wave height cannot exceed 1/13 of the wave length, measured from trough to trough. Whooth sea and swell, or two systems of swell, are present at the same time, the observer first estimates the higher system waves and then repeats the process for the lower system.

Swell direction may be determined by "eyeball" or by sighting from a compass along wave crests and adding or subtracti 90°. Ship's true heading can also be used to determine the direction from which swells are approaching. The higher the obsertion point, the easier it is to determine swell direction. The average of several observations, rounded to the nearest 10°, show be used as the observed swell direction. Refer to the texts for Sets 14 and 18-21 for complete information on waves.

21 Legend Legend

January

Marine Area A

WAVE HEIGHT (M)

0-0.5

17.5

Marine Area B

WAVE HEIGHT (M)

0-0.5

	0.5	''''	0 0.5	9.0	0.5	, , , , ,	0-0.5	٦.٥
	1-1.5	32.1	1-1.5	26.2	1-1.5	33.1	1-1.5	25.6
	2-2.5	25.1	2-2.5	29.4	2-2.5	28.2	2-2.5	29.6
	3-3.5	15.6	3-3.5	19.0	3-3.5	14.9	3-3.5	20.0
	4-5.5	8.8	4-5.5	13.6	4-5.5	9.6	4-5.5	14.7
	≧6.0	0.9	≧6.0	2.9	≥6.0	2.4	≧6.0	4.4
	N=	2398	N=	4806	N=	3378	N=	5878
	L							
	Marine Area E	170	0 65	180	170-	7	160 Marine Area F	
	BAVE HEIGHT (M)	s    /	12		47-+-	- SV	WAVE HEIGHT (	<u>w)</u> \$
	0-0.5	5.8		WV HGT (M) %	WV HGT (M) & WV H	ST (M) 2	0-0.5	6.7
	1-1.5	23.9	<i>j.</i> 7	9 0.05 15	0 05 17 50-0	.5 51.4	1-1.5	22.6
	2~2.5	28.7	1				2-2.5	29.5
Į	3-3.5	19.7	: 0	> 17-75-35	2-2.5 24.2 2-2	2.5 15.9	3-3.5	19.6
	4-5.5	15.3	1 Ma	2-2.5 25.9	3-3.5 10.3 3-	3.5 5.6	4-5.5	16.6
	≩6.0	6.7	N	3-3.5 16.9	4-5.5 4.5 4-	5.5 6.5 1	≧6.0	5.1
	N=	4238		4-5.5 9.7	4-5.5 4.5		N=	5468
Į		~	]	1	=0.0 0.5	V= 107 12	/	
- {		60:		N= 1977	N= 331 1	· K	\$	- C
ı	NV MC	ST (M) Z WY HCT					'	$_{A}$ $\subset$ $\Box$
	( O-0.	5 1 WV HGT	7.3 0-0.5 4. 19.7 1-1.5 18.		+	7 W	VHGT (M)	7 23
ł	/_ /_1-1.5	31.5/0-0.5	WV HGT (M) 7	WV HGT (M) Z	WY HGT (M) 2	V HGT CHI	λ ξ 20·31 V	1 1.2
- [	/ 2-2.5	31.8/1-15	10-0.5 4.	8 0-05 7 6	0-0.5 9.7 0	-0.5 / . /	1-1.5 37.2	1 / 50
Į	$\sqrt{3-3.5}$	15.3/2-25	19.7 1-1.5 18.	4 1-15 22 6	1-15 27.0	7.7 0 1-1.5 32.1 2.5 28.9	2-2.5  26.3	/ ) \i
ı	/ 14-5.5	$\frac{13.6}{11} \cdot \frac{3}{11}  $\frac{M}{2}$ $\frac{2}{3}$ $\frac{M}{3}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $\frac{N}{4}$ $N$	212-25 20 0	7-25 29.5	2-2.5 28.9	$\frac{2-2.5}{3-3.5}$ 9.9	١ ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' '	
- 1	/ ≧6.0	2 4-5.5	4.8 3-3.5 20	613-35 10	3-35 19.31	3-3.5 16.01	3-3.5 4.9	
- 1	N= .	2.5 ≥6.0	9.3 4-5.5 23	7 4-55 17 1	4-55 12 0	4-5.5 11.9	4-5.5 1.71 ≥6.0	) <b>v</b>
J	55	03g / N- 0	1.31 260 c.	7 4-3.5 17.1	75.0 2.5	>60 2.0.	1 125 18	
ı		2	18 N= 228			N = 24.18		
		7	220	N= 1717	N=2822			
	/	<i></i>	-	<b></b>			WV HGT (M) Z	
	/	WV HGT (M) Z	No			HGT (M) %		
1	i	0-0.5 4.9	WV HGT (M) %	WV HGT (M) %	WV HGT (M) %	WV NO	8 0-0.5 22.6	1
		1-15 20	1 0.5 4 1	0 05 5 6	1005 14			31
- (		$\sqrt{\frac{2-2.5}{3-3.5}}$ 28.0	1-1.5 19.7	1 15 00 0	1 15 71 4	1-1.0	2 2-2.5	91
1	į	3-3.5	1 - E.J JA ()	7-25 20 1	2-2.5 30.8	11 )-2.5	12/3-3.5	3
ı	· /	4-5.5		3-3.5 22.0	3-3.5 19.8	11 3-3-3		4
- {	1	>60.0	1 TTO.O 17 71	4-5.5 18.0		4-5.5	1.01 ~60 3.	66
- {	500	A, U. 1	≧6.0 6.9			1 >60 A	F. O 1 N 30	· \
- [	1	N= 2861	N= 3181			A.	216 N-	_
- 1	/			N= 2803	N = 3100	1		\
	/	Γ				4		\
- 1	/	[		_		1	1	\
	/	1	1			1		\
- 1	1	1				1		\

Marine Area C

<u>z</u>

9.0

WAVE HEIGHT (M)

0-0.5 11.8

<u>z</u>

Marine Area D

WAVE HEIGHT (M)

0-0.5

21 Wave Height Thresholds

3

5.8

Marine Area D

WAVE HEIGHT (M)	<u>z</u>	WAVE HEIGHT (M)	<u>3</u>	WAVE HEIGHT (M)	<u>z</u>	WAVE HEIGHT (M)	2
0-0.5	34.0	0-0.5	14.7	0~0.5	14.9	0-0.5	7.2
1-1.5	24.4	1-1.5	32.8	1-1.5	28.4	1-1.5	29.3
2-2.5	20.2	2-2.5	24.7	2-2.5	28.9	2-2.5	29.6
3-3.5	10.9	3-3.5	15.1	3-3.5	17.2	3-3.5	18.5
4-5.5	8.8	4-5.5	10.1	4-5.5	9.3	4-5.5	12.3
<del>-</del> 4-3.3	1.8	¥-3.3 ≧6.0	2.6	4-5.5 ≥6.0		l .	3.1
N=	901			≥6.0 N=	1.3	≥6.0	
N-	901	N=	5581	N-	3324	N=	6139
Merine Ares E	173	65	180	170°	Z	160 Merine Area F	
BAVE HEIGHT (M)	ž		<del></del>		V-SV	WAVE HEIGHT (N	<u>.</u>
0-0.5	5.3		WV HGT (M) %	WV HGT (M) 7 WV HGT	(M) 2	) 0-0.5	6.7
1-1.5	26.3	;	0 05 00	0 05 13 80-0.	5 81.7	1-1.5	23.1
2-2.5	29.4		1-15 26	7 1-1.5 23.6 1-1.		2-2.5	29.7
3-3.5	19.4	1	5 12-26 24	0 2-2.5 15.3 2-2.		3-3.5	19.9
4-5.5 ≩6.0	14.5		$\sqrt{\frac{12-2.5}{3-35}}$ 24.	3 3-3.5 11.8 3-3		4-5.5 ≥6.0	15.6 5.0
N=	4434		4-5.5 11.	2 4-5.5 5.6 4-2	.5	≥0.0   N=	5606
		~	≥6.0 2.5	≥6.0 0.0 ≥6	.0 0.0		
J- 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Too.		N= 64	1 N	= 120	\$	47.1
J. O. A.	ST (M) Z WY HGT (					7	n / [
0-0.5	5 17 O WY HGT (	M) Z WV HGT (M) Z 10.1 0-0.5 7.( 23.3 1-1.5 17.:			HGT (M) Z	1 HGT (N) 3 4	
12-25	30.5/0-0.5	10 1 0 05	WV HGT (M) %	WV HGT (M) 3	HGT (M) 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0.5 29.5	7 / (31)
/3-35	23.8/2 1-1.5	23.3 1.15 7.0	0 0-0.5 14.	0 0-0.5 15.5 0	-1.5 29.8	1-1.5 23.1\ 2-2.5 23.1\ 2-8.3\	
14-55	12.6 2-2.5 2	9.4.7-25	7 1-1.5 28.	7 1-1.5 34.5	-2.5 30.9	2-2.5 18.31 /	'
/ ≥6.0 f	$13.0^{13-3.5}$	M) 2 WV HGT (M) 2 10.1 0-0.5 7.0 23.3 1-1.5 17.3 19.4 2-2.5 27.3 6.9 3-3.5	2-2.5 22.	4 2-2.5 25.6 2	7	3-3.5 9.21	ا ا
N=	$3.1 \stackrel{4-5.5}{>} 14$	10. $10 - 0.5$ 7. $00 - 0.5$ 7. $00 - 0.5$ 7. $00 - 0.5$ 17. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 26. $00 - 0.5$ 27. $00 - 0.5$ 26. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 - 0.5$ 27. $00 $	3-3.5 18.	8   3 - 3.5   13.4   3	-5.5 8.5	4-5.5	9
55.	$\frac{2}{23} = \frac{60.0}{N} = \frac{6}{3}$	.1 >6.0	4-5.5 13.	7 4-5.5 8.3	260 1.61	922 7	
The	/ N= 29	96 1 1		20.0 2.0	N= 2843	N-	
1		N= 271	N= 204	N= 3158			,
1/	1				-	TT (M) Z	ł
1/	WV HGT (M) Z	WV HCT			WV HGT (M) %	WV HOT 6 41	l
V	1 0.5 4	2 0 0 5	WV HGT (M) %	WV HGT (M) %	M A 11.	$610^{-0.5}$ 22.91	\
Ì	12. 2.3 19.5	1 15	0-0.5 4.		0-0.5	01 "- 29.3	
	2-2.5 25.1 3-3.5 21.1	72-25 19.1	1-1.5 24.	0 1-1.5 26.8	25 29		1
J /	4-5.5 21.4	2-2.5 28.3	2-2.5 28.	6 2-2.5 31.11	2-2.5 29	.113-55 16.	11
1	≥6.0 21.7	14-55	3-3.5 20.	6   3-3.5 18.9	4-5.5 11	014-3.5	5
1	8.01	>60	4-5.5 17.	0 4-5.5 13.3	≥6.0 3	.3 ≥6.0 N= 375	5 \
500	N= 2590	· · · · · · · · · · · · · · · · · · ·	<b>≧6.0</b> 5.		N= 46	19	
1		N= 3502	N= 2800	N = 3155	, , , , ,	1	- \
/			<del></del>	1	1		\
/					1		\
/	1						\
_ /	/						_ \
21 Wave Heig	ht Thresholds						February

Marine Area C

Marine Area A

Marine Area B

Marine Area A		Marina Area 8		Marine Area C		Marine Area D	
WAVE HEIGHT (M)	2	WAVE HEIGHT (M)	<u> </u>	))			
0-0.5	42.9	0-0.5	18.8	WAVE HEIGHT (M)	3	WAVE HEIGHT (M)	5
1-1.5	22.9	1-1.5	31.1	0-0.5	20.7	0-0.5	7.7
2-2.5	17.4	2-2.5	26.6	1-1.5	35.9	1-1.5	28.7
3-3.5	9.5	3-3.5	13.4	2-2.5	26.7	2-2.5	30.0
4-5.5	5.5	4-5.5	7.9	3-3.5	10.7	3-3.5	17.5
≧6.0	1.9	≥6.0	2.2	4-5.5	4.7	4-5.5	12.2
N=	529	N=	5067	≥6.0	1.3	≧6.0	3.8
			3007	N=	3720	N≡	7406
Marine Area E	170	65.	180		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
MAVE HEIGHT (M)	s	200	7	170°	-K-4-7	2160 Merine Area F	
	5		WV HGT (M) %	WV HGT (M) % WV HG	T(M) Z	MAYE HEIGHT (M)	3
	.0	4	0-05 21	10-0.5 48.7 0-0.		0-0.5	7.2
	.5	/	1-1.5 29	9 1-1.5 21.7 1-1.	5 9.8	1-1.5	25.6
	.8		2-2.5 22	7 2-2.5 16.2 2-2.	5 4.9	2-2.5 3-3.5	28.8
	.4	Jan Jan Jan Jan Jan Jan Jan Jan Jan Jan	3-3.5 12.9	3-3.5 8.7 3-3	.5 1.6	4-5.5	19.3 15.1
N= 53			4-5.5 11.3	4-5.5 2.5 4-5	5 0.01	≥6.0	4.0
	هر السي		≧6.0 2.1	1 .	0.01	N=	7075
J- 2/-		1	N= 194	1 -	= 61 12		
0-0.5 -					K		ξ.,
0-0.5	3. 1 0-0.5 . 3 1-1.5 1						/
) / 1-1.5 35	. 1/0-05	7.6 WY HGT (M) %			HGT (M) Z WV	HGT (M)	کی
2-2.5	3/1-15	7.6 0-0.5	WV HGT (M) %	WV HGT (M) 2 WV 3 0-0.5 21.6 0-	FOT 10 5 0-	$-0.5 \ ^{24} \cdot 4 \ $	4
3-3.5 13.	5/2-25	9.7 1-15 25 6	10-0.5 12.3	0-0.5 21.6 0-	0.5 10.5	-1.5 41.0	~ \/
5.5	3-3.5	3.1/2-2.5 30.0	1-1.5 28.6	1-1.5 31.6	7.5 30 11 2	-2.5  23.	) \
\$6.0	14-5.5	.8/3-3.5 21 5	2-2.5 28.3	2-2.5 26.5 2	25 13 0 3	-3.5	/ مرح
V= 221	≥6.0	7.6 0-0.5 7.7 9.7 1-1.5 25.5 3.1 2-2.5 30.8 3-3.5 21.5 4-5.5 11.3 3 ≥6.0 3 3	3-3.5 16.3	3-3.5 12.113		-5.5 2.7	
-21 h	' N= '·	3 ≥6.0	4-5.5 10.6	4-5.5 6.8 4	-5.5	≥6.0 0.7 ≥6.0 1643 W	
O To	15	7 = 0.0 = 3.2 $N = 247$	€0.0 3.9	≥6.0 1.4	25.63	N = 1643 V	سسسد
·	-	24/	N= 1295	N= 3381	N= 2552	and the second	
/ w	V #c-	-	_	1			
10-	V HGT (M) Z	WYWOT	-			WV HGT (M) 2	
1 1-	15 5.2	0-0.5 4.9 0	V HGT (M) %	WV HGT (M) %	NV HGT (M) %	1 ~ 6 ()	
12-	2.5	0-0.5 4.9 0 1-1.5 21.5 1 2-2.5 38 3	~0.5 3 a	0-0.5 4.4	^ 0	0-0.5 24.8	
3-3	2.5 29.8 1.5 22.1	2-25 21.5 1	1-1.5 20.9		1-15 31.0	25 28.9	
4-5	~ <<.11	2 2 40.012	-2.5 29.9	2-2.5 31.4	D-2.5 29 · 3	25 19.9	
<b>∫</b> ≥6.0	11.91	1 5 21.7 3-	-3.5  21.2	3-3.5 19.2	3-3.5 16.4	15.6	
N=	0.51	773.5 16 7	-5.5 18.2	4-5.5 14.9	4-5.5 10.4	414-5.5 4.3	1
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	3095	=0.0 6.3   ≥	6.0 5.8	£6.0 5.6	≥6.0 3.3	2 4588	1
7		N= 40c-1 =	V= 3264		N= 572	7 N= 4500	
}	-		2204	N= 3721	• •	Luna	
/	1						
/	}		}				
1	1	1	}			}	1
rch							1
							1

Marine Area A	}	Marine Area B	<del></del>	Marino Area C	<del></del>	Addison Associated	11-46
				Marille Area C		Marine Area D	
WAVE HEIGHT (M)	3	WAVE HEIGHT (M)	3	WAVE HEIGHT (M)	7	WAVE HEIGHT (M)	7.
0-0.5	60.6	0-0.5	22.0	0-0.5	19.8	0-0.5	9.1
1-1.5	26.0	1-1.5	36.6	1-1.5	39.2	1-1.5	29.6
2-2.5	8.6	2-2.5	23.0	2-2.5	25.5	2-2.5	29.5
3-3.5	4.0	3-3.5	9.7	3~3.5	8.5	3-3.5	17.3
4-5.5	0.5	4~5.5	6.3	4-5.5	5.6	4-5.5	12.2
≧6.0	0.3	≧6.0	2.3	≧6.0	1.4	≧6.0	2.4
N=	396	N=	3745	N=	4070	N≈	6849
Marine Area E		65.					
MAVE HEIGHT (M)	170	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	1806	170°	Z7	160 Marine Area F	
0-0.5	7.9					WAVE HEIGHT (M)	*
	25.8	, C	WV HGT (M) %	WV HGT (M) & WV HGT	(M) 3	0-0.5	9.0
2-2.5	29.1	į	0-0.5 60.	70-0.5 42.20-0.5	5 13.5	1-1.5	29.5 28.7
	19.4	,	<b>)   1~1.5</b> 18	ni 1-1.5 41.01 1-1	. J. J. J. J. J. J. J. J. J. J. J. J. J.	3-3.5	17.8
	13.7	la sh		1 2-2.5 13.3 2-2.		4-5.5	11.8
≧6.0 N= €	302	~ 1	<b>.</b>	3-3.5 3.0 3-3 4-55 0.6 4-5		≥6.0	3.1
14 (	ر ∰ 200		4-5.5 1.1	76		N=	7948
7 7			≧6.0 1.1	=0.0			
/ D/W	60:-		N= 89	N= 166 N	<u> </u>		الم
WV MGT (	W z		-			27 (W) 21 A	<i></i>
$\langle \rangle$ $1 = 1.5$	34 BY HGT (A	W) 3	•		- W		, (
$\int_{2-2.5}^{2-1.5}$	34.80-0.5 37.4 1-1.5 5.5 2-2.5	12.70 0.05	WV HGT (M) %	WV HGT (M) 3 WV	HO1	- = / )	- 54 / A
$\begin{cases} 3-3.5 & 16 \\ 3-3.5 & 5 \end{cases}$	$5.5\sqrt{3}^{-1.5}$	28.2 1 15 19.1	0-0.5 19.	0-0.5 22.2	-0.5 10.01	1-1.5 39.1	1 1/2
	.9/3 2.5 2	5.5 7-25 34.8	1-1.5 36.8	ol 1-15 36 1 1	-1.5 39.0	7-2.5 24.	10
≥6.0 4.	3 4 5 10	28, 2 1-1.5 34.8 5.5 2-2.5 27.0 3-3.5 12.2 4-5.5 4 3	2-2.5 24.3	2-2.5 23.0 2	-2.5 25.6	3-3.5	/ کې
N	21 \~ <1	814 55	3~3.5 9.8	3-3.5 10.0 3	-3.5	4-5.5	/
49	)	.91 >6 - 1.31	4-5.5 6.9			≥6.0 0.1 N= 2486 W	
/ V	N= 1	10 2.6	≧6.0 3.1	≥6.0 2.4	1004	N= 2400	
		115	N= 655	N= 2819	N= 1804	I amount	
/		-	·				
( I	WV HGT (M) 3					WY HGT (M)	
<i>[</i>	0-0.5	WV HGT (M) 3	WV HGT (M) %	WV HGT (M) %	WV HGT (M)	1 25 / 1	
1-	1-1.5 26.6	/ 11=11 E = 1		<u> </u>	205 9.		
12	7-2.5 26.1 -3.5 27.2	1-1.5 23 7		100.0	1-1.5 30.	Y 1 0 6 / 2 1 1	
		~ /~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		1 ,	2-25 30.	4 2 35 18.01	
14-	-5.5	3-3.5 10 7			2-35 10	- 1 . Eh 14	1
	··· / ~ /	4-5.5 15 1		) -	1-55 10		1
/ N	2866	≤0.0 5 1		•	>60 2	.3 \ = 4939	1
	-500	N= 3969	• •	1	N=60	13 N-	
/	-	-	N= 3326	11- 3012		-	/
/	1		-				
/	1						\
/	1			-			\
Waya Halahi	Throob-1-1-		<del></del>	<u> </u>	1		
Wave Height	INFESTOIGS						Apri
							-

Marine Area A		Marine Area B		Merine Area C		Marine Area D	
WAVE HEIGHT (M)	<u>z</u>	WAVE HEIGHT (M)	3	WAVE HEIGHT (M)	<u>%</u>	WAVE HEIGHT (M)	3
0-0.5	49.7	0-0.5	22.0	0-0.5	30.1	0-0.5	17.2
1-1.5	41.0	1-1.5	45.3	1-1.5	42.7	1-1.5	40.5
2-2.5	7.2	2-2.5	22.9	2-2.5	19.3	2-2.5	24.3
3-3.5	2.0	3-3.5	7.3	3-3.5	5.1	3-3.5	10.7
4-5.5	0.2	4-5.5	2.1	4-5.5	2.4	4-5.5	5.8
≥6.0	0.0	≥6.0	0.4	≧6.0	0.4	≧6.0	1.5
N=	598	N=	3032	N=	5197	N=	7342
Marine Area E	17.	) 65 · nim	189	170	Pa /	160 Marine Area F	
WAVE HEIGHT (M)	3				m & 1 -3V	WAVE HEIGHT (M)	3
0-0.5	12.7		WV HGT (M) %	WV HGT (M) X WV HGT	68 7	0-0.5	13.3
1-1.5	35.4	`	0-0.5 29.	0 0 - 0.5 76.0 0 - 0.5	: 22.71	1-1.5	33.7
2~2.5 3~3.5	26.7		\$ 1-1.5 59.	0 0 - 0.5 76.00	5 2 ( )	2-2.5	27.2
4-5.5	13.8	_lh	147-76 4	7 17 - 7 5 1 1 6 -		3-3.5 4-5.5	14.7 9.2
≥6.0	2.7		√ <b>3</b> -3.5 1.9	3-3.5 0.0 3-3.	_	≥6.0	1.9
N=	7706		4-5.5 0.0	0.0 4-5.5		N=	884 1
L		37	≥6.0 0.0	0 ≥6.0 0.0 ≥6. N= 96 N=	2111/	/ L	
1-1.5 2-2.5 3-3.5 4-5.5 ≥6.0 N= 13	5. 3 2. 6 4-5.5 2. 0 ≥6.0 N=	19.1 2-2.5 18.2 10.3 3-3.5 12.3 5.9 4-5.5 5.2 20.0 ≥6.0 0.5 N= 212 10-0.5 19.2 1-1.5 35.7 2-2.5 23.6 3-3.5 12.0 4-5.5 7.6 ≥6.0 1.9	4 2-2.5 23. 3 3-3.5 7. 4-5.5 1. ≥6.0 0. N= 82	7 0-0.5 19.9 0-1 1-1.5 47.8 16 2-2.5 22.7 2 3-3.5 6.9 3 4-5.5 2.2 5 ≥6.0 0.4 N= 1957 $\frac{1}{2}$ 5 0-0.5 15.2 1-1.5 36.9 5 2-2.5 25.5 9 3-3.5 12.6 0 4-5.5 7.3 9 ≥6.0 2.4	-2.5 25.6 -3.5 7.8 -5.5 3.1 ≥6.0 0.4 N= 2211 WV HGT (M) 3 0-0.5 15 1-1.5 38 2-2.5 25 3-3.5 12 4-5.5 ≥6.0	1-1.5 $2-2.5$ $15.11$ $2-2.5$ $3.51$ $3-3.5$ $3.51$ $4-5.5$ $0.41$ $10-0.5$ $10.41$ $10-0.5$ $10.41$ $10-0.5$ $10.41$	
		N= 5781	N= 427		N= 5		
May						21 Wave Height T	hresho

Marine Area A		Marine Area B		Marine Area C		Marine Area D	
			.		_		_
<u>WAVE HEIGHT (M)</u> 0-0.5	<u>*</u> 48.8	<u>WAVE HEIGHT (M)</u> 0-0.5	<sup>3</sup> 26.9	<u>₩AVE HEIGHT (M)</u> 0-0.5	33.8	<u>₩AVE HEIGHT (M)</u> 0-0.5	<u>₹</u> 22.6
1-1.5	36.2	1-1.5	47.1	1-1.5	46.3	1-1.5	46.5
2-2.5	11.1	2-2.5	20.5	2-2.5	15.9	2-2.5	21.2
2-2.5 3-3.5	2.8	3-3.5		3-3.5		3-3.5	
3-3.5 4-5.5	0.8	3-3.5 4-5.5	4.1	3-3.5 4-5.5	2.6	3-3.5 4-5.5	6.4 3.0
4-5.5 ≧6.0	0.8		1.3		1.3		0.3
≥6.U N=	1511	≥6.0 N=	0.0	≧6.0	0.0 5175	≥6.0 N=	7150
IV	١١١١	IN-	3482	N=	51/5	N-	7150
Marine Area E	173	0 66	180	170	7	Marine Area F	
WAVE HEIGHT (M)	3	1620	<del></del>	<del></del>		MAVE HE GHT (M)	ž
	16.4		WV HGT (M) =	WV HGT (M) 3 WV HGT	(M) 3	0-0.5	15.8
	40.9					!= 1.5	42.~
	27.5	,	1-1.5 45	1 0 - 0.5 62.0 0 - 0.3 3 1 - 1.5 30.2 1 - 1.6 6 2 - 2.5 6.4 2 - 2.6 2 3.5 1 1 1 3 - 3	5 30.8	2-2.5	27.7
3-3.5 4-5.5	10.2	ية أكر	5 2-2.5 13.	6 2-2.5 6.4 2-2.	5 13.0 <b>↓</b>	3 – 3.5 4 – 5.5	9.3 4.1
4-5.5 ≩6.0	0.8	1	/ 3-3.5 2.2	$6 \mid 2-2.5  6.4 \mid 2  3-3.5  1.1 \mid 3-3  4-5  3.4 \mid 4-5  3.5  3.1 \mid 3-3 \mid 4-5  3.1 \mid 4-5 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 \mid 3.1 $	5 1.41	4-5.5 ≥6.0	4. 0.4
	8053		14-5.5 0.5	$\frac{2}{3} = \frac{3.5}{3.5} = \frac{1.13}{3.5} = \frac{3.5}{3.5} = 3$	.0 0.21	N=	844
		<i>p</i>	1 ≧6.0 0.2	≥6.0 0.0   =0		<u> </u>	
	- Fee - L		N= 806		į.		
WV HGT	(M) Z	28.810-0.5 26.6	·	· · · · · · · · · · · · · · · · · · ·		·	
10-0.5	33 WV HGT (	M) Z WV HGT (M) Z 28.810-0.5 26.6 54.81 1-1.5 46.3	1	1	HCT (M) 7 W	VHGT (M	
12 -1.5	48 3 0-0.5	28 810 05	WV HGT (M) %	WV HGT (M) Z	05 26.50	-0.5 36.31	
$l_{3-2.5}$	14.917-1.5	54.81 1.15	610-0.5 29.	9,0-0.5 24.0,0	15 47.71	1-1.5 13.31	
4-5.5	2.6	M) 3 WV HGT (M) 3 28.810-0.5 26.6 54.81 1-1.5 46.2 11.212-2.5 19.1	21 1-1.5 46.	21 1-1.5 48.51	-25 20.51	2-2.5 2.01	
≥6.0 1	.3 14-55	28.810-0.5 26.6 54.81 1-1.5 46.2 11.212-2.5 19.1 4.613-3.5 7.6	12-2.5 19.	0 2-2.5 22.0 2	-3.5 4.01	3-3.5	
N= 0	.0	1.4 14 55	3-3.5 3.5	513-3.5 4.41	-5.5 1.2	4-5.5 >6.0 0.1	
ss N= 0			4-5.5 1.4 ≥6.0 0.0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	≥6.0 0.0	≥6.0 235.	
7	5	(I() <b>I</b>	≥0.0 0.0 N= 131:	J • =0.0		i1	
	T	#	1	· 1		-1	
i	WV HGT (1.	9 0-0.5 22 4	<u>-</u>	+		WY HGT (M) 3	
i.	10-05 3	WV HGT (M) Z	W// HCT (15) ==	WAY HOT (M) Z	WV HGT (M) 3	710-0.5 14.11 710-0.5 42.61 41 1-1.5 42.61	
1	1-1.5	9 0-0.5 22 1	0-05 17	2 0 05 10 8	0-0.5 19.	71 0-0.5 42.61 41 1-1.5 42.61 91 2-2.5 29.2 91 3-3.5 9.4	
<i></i>	2-2.5	1-1.5 42 51	1-15 44	1 1-15 44 7	1-1.5 42	41 1-1.5 42.0 41 1-1.5 29.2 91 2-2.5 9.4 61 3-3.5 9.4	
/.	$3-3.5 \stackrel{2}{\sim} 1.8$	2-2.5 23 1	2-2.5 25.	4 1-1.5 77.2	17-7.5 24	9.2-3.5	1
	1-5.5	3-3.5 8 7	2-2.5 25. 3-3.5 8.1	8 3-3.5 7.9	3-3.5	.714-5.5	1
	7 0	14-5.5 301	4-5.5 3.1			7 5 579	, \ }
500	N= 5168	≤6.0 0.5	≥6.0 O.	4 ≥6.0 0.6	≥6.0	521 N= 5/3	٠
<b>*</b>		N= 6335	N= 504	1	N= 50	1 1	•
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						· · · · · · · · · · · · · · · · · · ·	
21 Wave Heigh	t Thresholds						Jur

July

Marine Area A		Marine Area B		Marina Area C		Marine Area D	
WAVE HEIGHT (M)	ž	WAVE HEIGHT (M)	<u>z</u>	WAVE HEIGHT (M)	<u> 3</u>	WAVE HEIGHT (M)	3
0-0.5	43.3	0-0.5	22.0	0-0.5	30.6	0-0.5	24.1
1-1,5	41.2	1-1.5	51.4	1-1.5	48.6	1-1.5	46.1
2-2.5	12.4	2-2.5	21.9	2-2.5	15.7	2-2.5	21.1
3-3.5	2.3	3-3.5	4.0	3-3.5	4.3	3-3.5	6.1
4-5.5	0.6	4-5.5	0.7	4-5.5	0.7	4-5.5	2.2
≧6.0	0.1	<b></b>	0.1	≧6.0	0.1	≧6.0	0.4
N=	3111	N=	3916	N=	5657	N=	6785
		<u></u>					
Marine Area E	1	73 65	189/	170	27	Marine Area F	
BAVE HEIGHT (M)	*				(M) & 1	WAVE HEIGHT (M	-
0-0.5 1-1.5	16.3		WV HGT (M) %	WV HGT (M) % WV HGT	5 46.1	0-0.5	14.
2~2.5	43.3		0-0.5 37.	6 0-0.5 43.5 0-0. 0 1-1.5 39.4 1-1.	5 42.3	1~1.5 2-2.5	43.0 28.0
3-3.5	8.5	•	> 1-1.5 41.			3-3.5	9.8
4-5.5	3.2	ila	$)^{12-2.5}$ 17.	1-00 00 11-3		4-5.5	3.9
≧6.0	0.4		$\sqrt{3-3.5}$ 3.7 4-5.5 0.5	3-3.5 2.0 3-4-5.5 0.5 4-5	5 0.81	≥6.0	0.3
N=	8682	ا مسهر	4-3.3 0.3	>6	0 0.	N=	9083
		1	N≈ 1237	506 N	= 1448	/ L	
- INV HO	÷ 60.				1.		
NV HGT	(m) 3			<del></del>		V HGT (M	
11-15	33.8 (0-05	(M) 2 WV HGT (M) 2		WY (46) Z W	/ HGT (M) 3	05 31.51	
12-25	47.6 1-15	19.9 0-0.5 23	WV HGT (M) %	WV HGT (M)	-0.5 27.0	1.15 47.71	
/3-3.5	$\frac{15.3}{2-25}$	19.9 0-C.5 23. 47.9 1-1.5 50	5/0-0.5 19.	910-0.5 23.11	1-1.5 50.6	1-1.5 47.71 1-1.5 15.91 2-2.5 3.91	
4-5.5	2.4 /3-35	19.9 0-C.5 23. 47.9 1-1.5 50.6 25.0 2-2.5 18.2 6.2 3-3.5 6.1 1.0 4-5.5	01 1-15 50.	5 2 25 20 4 2			,
		, / J.J h 1	12-2.5 24.	712-35 3/1-	3~3.7		. <b>₹</b> 3
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	· 1 \ ≥6.0	^ 1 3.3 1.4	14-5.5 0.	1 4-5.5 1.1	4-5.5 0.5	4-5.5 0.2	•
229	)5 N=	~· U 1 26 0			≥6.0 0.0	1 24	
1 2-	<u></u>	987   N = 625		2.00	N = 3217	1	
•			13/			1	
	WV HGT (M) 2			4	-	WV HGT (M) 3 71	
	10-05 3	WV HGT (M)		400	WY HGT (M) %	20-0.5 13.71 .9 1-1.5 43.11 .9 2-2.5 28.5	
	1-15 21.	6 0-0.5 23.4 1 1-1.5 45.3	WV HGT (M) %	WV HGT (M) Z	0-0.5 20	.2\ 0-0.5 43.1\ .9\ 1-1.5 28.5\ .9\ 2-2.5 28.5	1
f	2-25 21	1 1-1.5 45.3	0-0.5 18.	7 0-0.5 18.8	1-1.5 42	9 1-1.5 43.5	ì
1.	3-35 < 1.8	2-25	1-1.5 40.	6 1-1.5 45.2		914 = 10.4	
14	1_5 ~ ' • 0	3-3.5 6 0	2-2.5 24.		1 25 /	·/ = = 4 ·	١.
I I	<b>≥6.0</b> 2.4	4-5.5	3-3.5 7.4 4-5.5 2.4		4-5.5		11
la	N= 0.5 N= 4145	≥6.0 0.3	4-5.5 2.4 ≥6.0 0.3	' 1	≥6.0	)· 4 1 N= 020	1
-	T145	N= 5243	N= 4359		1 6	133 N-	
/			11- 430		1	+	
/	I			<b>4</b>	4	\ ! !	
/	- 1	}		1	1	1	
1	i i	1			(	1	

21 Wave Height Thresholds

1	Area A		<del>-</del>				
WAV	HEIGHT (M)	Marine Area B		Maria			
1	-O.F	WAVE HEIGHT (M)	_	Marine Area C		Marion	
1	_15 33.9	0-0.5	3	WAVE HEIGHT (M)	_	Marine Area D	
	-7e 42.4	1-1.5	16.4	0-0.5	30.5	WAVE HEIGHT (M)	•
	35	2-2.5	48.3	1-1.5	20.5	0-0.5	ž 10 -
,	55	3-3.5	23.8	2-2.5	50.9	1-1.5	18.2 43.7
≥	6.0	4-5.5	7.0	3-3.5	21.9 4.9	2-2.5	24.8
1	0.1 N= 2895	<b>≧6.0</b>	2.9	4-5.5	1.4	3-3.5	8.8
		N=	2708	≧6.0	0.3	4-5.5	3.8
Marine Area	((	J [	2700	N=	5072	≥6.0	0.7
MAYE MEIGH	(84)	7) 65	180		_	N=	6807
0-0.5	13.6		7	170			
1-1.5 2-2.5	39.2		WV HGT (M) %			Merine Area F	
3-3.5	30.1 11.5	7	0-05 33	V HGT (M) % WV HGT (N	0 %	WAVE HEIGHT (M)	*
4-5.5	4.9	, }	1-1.5 40 8	-0.5 40.2 0-0.5	37.0	0-0.5	11.6
≥6.0 N=	0.8	ر الر)		-1.5 36.6, 1-1.5 -2.5 17.6 2-2.5	45.1	1-1.5 2-2.5	39.5
	10019	arry 1			3.11	3-3.5	30.4 12.5
7		' / /	Se a 1.4 14-		1.41	4-5.5	5.3
1/2019	O.5 3				0.21		0.7
			1530	= 579 N=	1075 🤝 🧳	7	9003
1/ 12-3	1.5 44 · 0 0 - 0 5	3 / WY					
3-3	5 19 5 1-15 21	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	HGT (M)				
4-5.5	$4.9 \int_{0.2}^{2-2.5} \frac{49}{21}$	9 1-15 13.9 0-	0.5 14	IGT (M) % WV HGT (	M) 3   WV HGT (	73.6	
₹6.0	2. 1 3-3.5 5	9/2-2.5 30.3 1-	1.5 48 2 1	0.5 16.2 0-0.5	18.310-0.5	49.1	
55. N=	74.0 \$6.0 1.7	3-3.5 34.212-2	2.5 27.8 2-2	5 73 6 12 75	21.6 2-2.5	21.5	• •
1	N= 0.0	14-5.5	6.8 3-3	.5 7 5 3-3.5	5.8 3-3.5	3.7	
1	411	N= 0.0 ≥6.0	5 2.7 4-5	5 3.1 4-5.5	1.4 4-5.5	1.5 1 36	
/		231 N=	0.1 ≤6.1	2.2	0.4 ≥6.0	0.6	
	0-0.5 Z		867 N=	1573 N≃	3049 N=	221	
	1-0.5	V HGT (M) 3 WV HGT					
	0-0.5 15.7 0- 1-1.5 40.7 1- 2-2.5 27.7 1-	0.5 19.0 0-0.5	(M) >			T (11) 7	
1	3-2- 0 / '</td <td>1.5 41 5 0-0.5</td> <td>14 6 0 0</td> <td>T (M) % WV HGT</td> <td>(M) % WV HG</td> <td></td> <td></td>	1.5 41 5 0-0.5	14 6 0 0	T (M) % WV HGT	(M) % WV HG		
<i>1</i>		2.5 41.5 1-1.5 2.5 25.3 2-25	41.0 1-16	T (M) 2 WV HGT 5 16.3 0-0.5 5 40.4 1-1.5	14.8 0-0 41.7 1-1		
,	500 3.1 1. S	9.4 3 3	28.7 2-25	70.47 17 1.0	28.6 2-2	.5 30.0	
The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	$V= \begin{array}{ccc} 0.4 & 4-5 \\ 3351 & \ge 6.0 \end{array}$	4.3 14 55	10.6 3-3.5	10.9 3-3.5	9.9 3-3	1.5 12.1	
	N=	0.51	4. 1 4-5.5	4.6 4-5.5	4.5 4-5		
/	-	- 10.1 T ki	0.9 ≥6.0 1654 N=	0.8 ≩6.0	0.6 ≥6	~ ~ ^ ^ ()	
/			N= N=	5503 N=	6669 N	= 6306	
/	/		+			The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	
Waye	/	1			1		
Wave Height	Thresholds	<u> </u>				•	
					1	0	
, <b>*</b>							

1	A	Marine Area B		Marine Area C			
WAVE HEIGHT	(M) %	WAVE HEIGHT		Marine Area C		Marine Area D	
0-0.5		WAVE HEIGHT (M)	3	WAVE HEIGHT (M)	3	1	
1-1.5	30.7	∬ 0−0.5	13.4	0-0.5		WAVE HEIGHT (M)	3
2-2.5	.2.0	1-1.5	43,3	11	16.4	0-0.5	13.7
ſ	· · · · · · · ·	2-2.5	24.1	1-1.5	43.5	1-1.5	
3~3.5	5.8	3-3.5		2-2.5	26.3	2-2.5	35.6
4-5.5	2.9	4-5.5	10.3	3-3.5	8.7		26.7
≥6.0	0.6	1	6.1	4-5.5	4.2	3-3.5	13.6
N=	2130	≧6.0	2.8	≧6.0	1.1	4-5.5	8.2
	2130	N=	2240	N=	0.9	≧6.0	2.1
Marine Area E				14-	5573	N=	648;
1	173	**	180				0,0,
MAVE HEIGHT (M)	3	1,2	7	170		Marine Area F	
0-0.5	10.2		~ i = -	J		} !	
1-1.5	35.5 ∬		WV HGT (M) Z	WY HGT (M) Z WY HG	T (M) 3	MAVE HEIGHT (M.	*
2-2.5 3-3.5	28.9	į	0-0.5 23.	0-0.5 27.6.0-0.	5 31.1	0-0.5	10.6
4-5.5	14.4			1-1.5 43.9, 1-1.		1-1.5	34.9
<del>4</del> -3.5 ≧6.0	8.5	إسهام	12-2.5 24.0	2-2.5 19.9 2-2.	5 16.2	2~2.5	29.8
=0.0 N=	2.4	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	13-3.5 9.9	3-3.5 5.5 3-3.	5 4.6	3-3.5 4-5.5	14.9
	7585	197	14-5.5 3.8	4~5.5 1.8 4-5	5 2.8 <b>1</b>	#~5.5 ≩6.0	8.:
7		,	<b>!</b> ≥6.0 1 1	i>60 17.≥6	n 0.11	H N-	1.8
- 1 WV L.	60:_	1	N= 620	1 No 100 . No	- 958 🐎	E	85 10
10-0	T(M) 7.	3 MV HGT (M) 3 0.110-0.5 9.0 1.31 1-1.5 35.1 712-2.5 26.612	1	1	Ì.	1	
1 1 1 0.5	19 WV HGT (M)	2 WV HGT (M) 2 110-0.5 9.0 31 1-1.5 35.1 712-2.5 26.612 113-3.5 14.913	h	·	+	1	
12-7.5	41 010-0.5 1-	WV HGT (M) Z	· 1		_ WY HG	TEN TI	
13-3-5	25 7 1-1.5 36	.110-0.5	WV HGT (M) %	WV HGT (M) % WV	HGT (M)	5 24.51	
4-5.5	9 5 2-2.5 30	.31 1-1.5 35	0-0.5 9.4	0-0.5 14.0,0-	0.5 13.8	5 45.21	
, ≥6.0	3.7.3-3.5	7 2-2.5 26 61	<sup>1-1.5</sup> 37.31	1-1.5 44.91 1-	-1.5 42./1	5 20.31	
N- C	4-5.5	113-3.5	-2.5 26.8	2-2.5 24.012-	2.5 28.312-4	5 6.61	
11:	$76$ $\stackrel{?}{ }$ $\geq 6.0$ 0.3	2   WV HGT (M) 2 110-0.5 9.0 3   1-1.5 35.1 712-2.5 26.6 2 113-3.5 14.9 13 14-5.5 10.6 14 ≥6.0 3.7   3 N= 188	-3.5 15.61	3-3.5 9.613-	3.5 9.113	5.5 2.61	1
	N= 30.3	≥6.0	-5.5 9.3 <b>i</b>	4-5.5 4.914-	.5.5 4.8 4	0.8	1
	-1 Jao	, A	260 1 ¬ •	4-5.5 4.9 4- ≥6.0 2.6 ≥	- A 1 3 1 5	1	ſ
	1	,	N= 604 !	N= 1361	6.0 1.5 N= 4054 1	<b>'</b> -	ì
	I WV HGT	WV HGT (M) 7 WV 1-U.5 15.610-	į	ŧ			1
	0-05 % I	WV HGT (M) 7 WV 1-0.5 15.6 0- 1-1.5 35.8 1- -2.5 28 31 1-				· ·	
	1-15 11.710	HGT (M) WV	HGT (W)	WV HGT (M) Z W	WCT (M) % I W	V HGT (M)	1
	2-25 34.3/	15.610=	0.5 10 -	WV HGT (M) %	05 12 210	-0.5	1
	30 31	1.0 35 01	0.5 10.8	0-0.5 11.80	-0.5 12.2	1-1.5 35.31	-
$J_3$	J. )	-2.5 no a '-	35.2	1-1.5 33.8 1			- 1
$\int_{4}^{3}$	-55 14.715	~~ <0.31)_^	15 20 - 1			- 15.1	
, ,	<sup>29.5</sup> 7 2 3-	-3.5	2.5 28.5	2-2.5 27.912			[
١٤	6.0 7.7 4-	3.5 11.8 3-3 5.5 7.0	14.5	3-3.5 14.4 3	-3.5  13.7	4-5.5 8.1	
١٤	7.7 4 6.0 7.7 4 1= 2750 ≥6	3.5 11.8 3-3 5.5 7.0 4-5	5.5 14.5	3-3.5	-3.5 13.7 -5.5 7.4	4-5.5 8.1	
١٤	7.7 4 6.0 7.7 4 1= 2750 ≥6	3.5 11.8 3-3 5.5 7.0 4-5	0 2.1	3-3.5 14.4\3 1-5.5 9.4\4 ≧6.0 2.8	-3.5 13.7 -5.5 7.4	4-5.5 8.1	
١٤	7.7 4 6.0 7.7 4 1= 2750 ≥6	3.5 11.8 3-3 5.5 7.0 4-5	0 2.1	3-3.5	-3.5 $13.7$ $-5.5$ $7.4$	4-5.5 8.1	
١٤	7.7 4 6.0 7.7 4 1= 2750 ≥6	3.5 11.8 3-3 5.5 7.0 4-5	0 2.1	3-3.5 14.4\3 1-5.5 9.4\4 ≧6.0 2.8	-3.5 13.7 -5.5 7.4	4-5.5 8.1	
١٤	7.7 4 6.0 7.7 4 1= 2750 ≥6	3.5 11.8 3-3 5.5 7.0 4-5	0 2.1	3-3.5 14.4\3 1-5.5 9.4\4 ≧6.0 2.8	-3.5 13.7 -5.5 7.4	4-5.5 8.1	
١٤	7.7 4 6.0 7.7 4 1= 2750 ≥6	3.5 11.8 3-3 5.5 7.0 4-5	0 2.1	3-3.5 14.4\3 1-5.5 9.4\4 ≧6.0 2.8	-3.5 13.7 -5.5 7.4	4-5.5 8.1	
١٤	7.7 4 6.0 7.7 4 1= 2750 ≥6	3.5 11.8 3-3 5.5 7.0 4-5	0 2.1	3-3.5 14.4\3 1-5.5 9.4\4 ≧6.0 2.8	-3.5 13.7 -5.5 7.4	4-5.5 8.1	

21 Wave Height Thresholds

Marine Area A		Marine Area B		Marine Area C		Marine Area D	
WAVE HEIGHT (M)	<u>z</u>	WAVE HEIGHT (M)	<u>7.</u>	WAVE HEIGHT (M)	3	WAVE HEIGHT (M)	<u>3</u>
0-0.5	15.8	0-0.5	6.9	0-0.5	8.8	0-0.5	7.2
1-1.5	39.5	1-1.5	30.4	1-1.5	35.8	1-1.5	30.2
2-2.5	26.8	2-2.5	31.2	2-2.5	29.9	2-2.5	29.5
3-3.5	10.8	3-3.5	16.9	3-3.5	14.8	3-3.5	17.4
4-5.5	6.1	4-5.5	10.6	4-5.5	8.6	4-5.5	11.9
≥6.0	1.1	≧6.0	3.9	≥6.0	2.2	≧6.0	3.8
N=	1231	N=	1675	N=	3593	N=	6111
		L					
Marine Area E	173	) 65 	1896	170	27	160 Marine Area F	
WAVE HEIGHT (M)	3			7		WAVE HEIGHT (M	5
0-0.5	6.9	<i>₽</i> \	WV HGT (M) %	WV HGT (M) % WV HGT	(M) 2 1	0-0.5	8.1
1-1.5	27.8	اً ا	0-0.5 11.	90-0.5 15.3 0-0.5	- 13 9	1-1.5	26.6
2-2.5	31.3					2-2.5 3-3.5	28.3 18.6
3-3.5 4-5.5	18.3	Sh	) 2-2.5 30.	5, 1-1.5 46.3 1 2-2.5 26.6 2-2.	5 A 9 1	4-5.5	13.9
≥6.0	3.5		/ ↓3-3.5 13.			≥6.0	4.5
N=	6686		4-5.5 7.6	5 4-5.5 3.4 4-3		N=	7832
		~	1	1 ≥6.0 1.0 ≥6.	244		J
J. S. J. WV WO	60.		N= 840	) N= 203			
10-05	(M) 3 WY HGT		·			V HGT (M) 3 1	
1 1-15	15.9	(M) 7 WV HGT (M) 7 11.6 0-0.5 7.6 27.8 1-1.5 25.9 26.4 2-2.5 34.2	i		HGT (M) % 1 4	N HGT 15.01	-
12-25	33.4 1-15	11.610-05	WV HGT (M) %	1 ~		- Λ(). O'	
/3-35	28.2/2-25	27.81 1-15 25	0-0.5 8.	910-0.5 5.210	-1.5 33.8	75 22.0	
14-5-	'<.515	(0.417 25		01 1 13 34 1	-2.5 31.81	2-2.5	
≥6.0	$8.5 \left  \frac{3.5}{4-5.5} \right ^{2}$	11.6 0-0.5 7.6 27.8 1-1.5 25.9 26.4 2-2.5 34.2 21.8 3-3.5 17.1	2-2.5 30.	0 2-2.5 32.112	-3.5 15.3	3-3.5 6.5	jë K
55 N= 10	$1.6 \neq \frac{3.3}{6.0}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3-3.5 16.	013-3.5 17.713			` [
55.	U4   N= 1	.8 ≥60 2 =	3.5 10.	2 7 3.3	≥6.0 1.9	≥6.0 3.0 N= 899	
1	_	84 N= 3.8		2001	N = 2887	N= 899	
, "	7		N= 61	7 N= 899	_	-l	1
	WYHO			<u> </u>		ST (M) 73	ł
<b>j</b> .	WV HGT (M) 7	WV HGT (M) %		1	₩V HGT (M) %	WV HGT (M) 7.31	
ŀ	/ U.) ~	/	WV HGT (M) %	WV HGT (M) %	2 05 7.	910-0.5 7.3	
	2-2.5 25 8	7 0-0.5 9.4 3 1-1.5 25.5 2-2.5 26.8	0-0.5 6.	0 0-0.5 5.8	0-0.5 7.	.3 1-1.5 25.7	
1	2. A = -V.D	1117		2 1-1.5 27.4	2-25 30	.3 2-2.5 29.7 .7 2-2.5 18.9	١,
I	4-5 ~ ~	T 3-7 E	50.	4 2-2.5 30.7	12 25 10		3,
I	≥60 15.7	4-55	3-3.5 18.		1-55 10	10:7 . 4.	1
50:	A: 4. J	≥6.0 4.2	4-5.5 13.		>60	3.0 1 NI- 332	D #
	N= 2787	N= 3387	≥6.0 3.4		N= 56	506	
		3307	N= 344	5 N = 3747			
	Γ				+	* * * * * * * * * * * * * * * * * * *	
/	/					1	
/						\	
L							

21 Wave Height Thresholds

Marine Area A

WAVE HEIGHT (M)

**November** 

Marine Area B

3

WAVE HEIGHT (M)

WAVE HEIGHT (M)	3	WAVE HEIGHT (M)	2	WAVE HEIGHT (M)	2	WAVE HEIGHT (M)	2
0-0.5	8.9	0-0.5	7.6	0-0.5	7.3	0-0.5	5.9
1-1.5	31.7	1-1.5	30.4	1-1.5	29.3	1-1.5	22.6
2-2.5	30.5	2-2.5	27.9	2-2.5	29.3	2-2.5	28.1
3-3.5	15.3	3-3.5	18.8	3-3.5	17.9	3-3.5	20.6
4-5.5	10.1	4-5.5	11.8	4-5.5	12.7	4-5.5	17.4
≧6.0	3.6	≥6.0	3.6	≧6.0	3.5	≥6.0	5.5
N=	1094	N=	2246	N=	2793	N=	5810
						J	
Marino Area E	173	65	189	170°	- T	160 Marine Area F	
	-	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	- 7		T	WAVE HEIGHT (M)	
MAVE HEIGHT (M)	4.9		WY HOT ON A	WV HGT (M) % WV HG	T (M) 2	0-0.5	5 6.5
0-0.5	20.9		WV HGT (M) &	7 3 0 - 0	.5 13.8	1-1.5	22.8
2-2.5	29.8					2-2.5	27.9
3-3.5	20.6	1	≥ 1-1.5 23.	8 1-1.5 32.9 3 2-2.5 40.6 2-2	5 27.7	3-3.5	19.7
4-5.5	16.6	Sh	$)^{2-2.5}$ 21.	3 2-2.5 40.6 2° 3 5 3-3.5 13.2 3-	35 16.91	4-5.5	17.7
≥6.0	7.3		√ 3-3.5 12.	5 3-3.5 13.2 3	55 4.61	≥6.0	5.3
N=	5030		4-5.5 9.4	1 ~	5.0 9.21	N=	7079
L		~	≧6.0 3.0	) =0.0 0.5	1= 65 F		
7			N= 1073	N= 234	- K		<u></u>
WV MGT	(M) Z WY HC-		•	1_			1 / J
		8.8 0-0.5 8.21.8 1-1.5 21.835.442-25 20.0	<del></del>	+		IV HGT (M) 7.	ر ا
1-1.5	36.6 0-05	WV HGT (M) %	WV HGT (M) 2	WV HGT (M) %	V H01 1 -	1-0.5 34.9	1 18
2-2.5	31.3/ 1-15	8.8 0-0.5 8	3.0-05	0 05 6 6 0	-0.5 14.4	1-1.5 22.4	J 14 5
3-3.5	29.4 2-25	21.8 1-1.5 21	1 1 16 33	0 1 15 24 6	1-1.3 4	2 2 2 1 1 T	) \
4-5.5	3.8 3-35	8.8 0-0.5 8.3 21.8 1-1.5 21. 35.4 2-2.5 29.8 5.6 3-3.5	2 2 2 5 2 7	9 1-1.5 27.0	2-2.5 27.2	$\frac{2-2.5}{3-3.5}$ $\frac{12.2}{12.2}$	الم الم
<b>1</b> ≥6.0	$\frac{5.7}{2}$ $4-5.5$ 1		2 25 17	2 2 25 21 5	3-3.5 16.6	3-3.5 12.2	
1 / N= -	·< 1 >6 ^	1.314-55 47 -	1 5 5 10	- 1	1-5.5 11.31	4-5.5 8.8 ≥6.0 2.2	\
55,	95   N- 7	1 30.0 5 5		5 4-3.3	≥6.0 3.3	N= 882 W	
1 To	$\int_{-\infty}^{\infty}$	47 N= 218	1	0.00	N= 2584		
	1	1 210	N= 119	1 N= 862		and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th	
1/	340.	-				uct (M) 2	
1/	O-OF	Water			WV HGT (M) 3	WV HO	
V	19 0.5	WV HGT (M) %	WV HGT (M) %	WV HGT (M) %	111	210-0.5 -2 11	
	4 (-) 10	$\frac{10-0.5}{2}$ 3.5	0-0.5 3.	T -	10-0.0	1-1.5	<b>\</b>
$\mathbf{I}$	2-2.5 23.9 3-3.5 23.9	1-1.5 16.3	1-1.5 18.		1-1.0 2		•
1	3-3.5	12-25 25 11	2-2.5 28.	2 25 29 8	12-2.5 43	1 3-3.5	, <b>1</b>
1	4 ~ - '0./		3-35 20.		1 - 2 - 19	1 1 1 - 5.5	51
1	≥6.0 12.4	1 3.3 22.71	4-55 19	1 1 5 18	4-3.3	5.4 4 ≥6.0 5.4 4.5 ≥6.0 466	6
500	$N = \frac{12.0}{2567}$	1 1 1 3 1	≥6.0 9.	1 ≥6.0 6.9	,	VI-	
	230/	N= 2963	N= 281	, ,		681	
			·v- 201	)   14- 33.7			\
/	1			<del></del>	-		\
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Marine Area C

WAVE HEIGHT (M)

Marine Area D

<u>z</u>

WAVE HEIGHT (M)

21 Wave Height Thresholds

<u>%</u>

Marine Area A		Marine Area B		Marine Area C		Marine Area D	
WAVE HEIGHT (M)	3	WAVE HEIGHT (M)	2	WAVE HEIGHT (M)	<u>z</u>	WAVE HEIGHT (M)	<u>*</u>
0-0.5	19.2	0-0.5	8.8	0-0.5	13.2	0-0.5	5.2
1-1.5	32.3	1-1.5	32.3	1-1.5	29.9	1-1.5	23.8
2-2.5	22.6	2-2.5	27.3	2-2.5	26.8	2-2.5	27.1
3-3.5	11.8	3-3.5	16.1	3-3.5	18.7	3-3.5	21.1
4-5.5	9.8	4-5.5	11.4	4-5.5	9.4	4-5.5	16.3
≧6.0	4.3	≥6.0	4.1	≧6.0	2.1	≧6.0	6.5
N=	1865	N=	3030	N=	3161	N=	5237
Marine Area E	176	65	189	170°	27	160 Merine Area F	
MAVE HEIGHT (M)	<u>s</u>				- Kar	WAVE HEIGHT (M)	5
0-0.5	4.5		WV HGT (M) %	WV HGT (M) 3 WV HG	T (M) 3	0-0.5	5.9
1-1.5	22.6		0-0.5 18.	0 0-0.5 23.0 0-0	.5 28.9	1-1.5	22.6 28.0
2-2.5 3-3.5	28.9					3-3.5	19.0
4-5.5	16.7	She				4-5.5	18.1
≧6.0	7.6		′  3-3.5 13.1	513-35 4.313"		<b>1</b> ≥6.0	6.3
N=	4229		4-5.5 11.	7 4-5.5 3.0 4	5.0 2.6 1	N=	5955
	~~~ <del> </del>		≥6.0 5.3 N= 1465	€0.0 0.5	1= 38		
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	60:-		N= 1465	N- 309		<sup>lll</sup> - ¬	, ~ <u>`</u>
NV HGT	(M) Z WY HGT		<del></del>	<del></del>		V HGT (M) 7 1	′ {
0-0.5	13.4 WY HGT (	M) Z WV HGT (III)	į .		W HGT (M) Z	VHGI (1 32.3)	1.6
12-25	37.7	7.0 0-05	WV HGT (M) %	WV HGT (M) Z	05 11.80	1-1.5 29.6	2 1
3-35	$23.5 \int_{2}^{1-1.5}$	7.000-0.5 7.7 20.9 1-1.5 22 F	0-0.5 8.	0 0 - 0.5 9.4	1-1.5 27.3	1-1.5 19.9	) \ 1
4-55	$13.4 \frac{2-2.5}{3-35}$	7.0 0-0.5 7.7 20.9 1-1.5 22.5 31.3 2-2.5 28.7 6.5 3-3.5	1-1.5 31.	5 1-1.5 33.1	7-2.5 27.8	2-2.5 19.9	ا الم
≥6.0	0.4 4-55	7.0 0-0.5 7.7 20.9 1-1.5 22.5 31.3 2-2.5 28.7 6.5 3-3.5 17.2	2-2.5 23.	8 2-2.5 30.7	3-3.5 20.0	2-2.5 3-3.5 12.4 4-5.5 1.3	۱
			3-3.5 16.	6 4-5.5 9.5		26.0 1.3	'
55.			4-5.5 13. ≥6.0 6.4		≥6.0 2.4	12/	
0	-	15   N = 209	N= 1485		N= 2339		
<b>'</b>			.,= ;+0.			-	
[/	O-OF			+		WY HGT (M) 2 0	
<b>/</b>	0-0.5 4.4	WV HGT (M) %	W/UCTAA **	WV HGT (M) %	WV HGT (M) Z		
	1-1.5 17.8 2-2.5 26	* 10-0.5 E . I	WV HGT (M) %	0.05 1.6	0-0.5 5.	1-15 22 6	(
<i>i</i>	2-2.5 26.1 3-3.5 26.1	1-1.5 18.6 2-2.5 25 2	1-15 20	0 1-1.5 21.9	, ,,,,	212-25 20 1	<b>\</b>
<i>f</i>	3-3.5	2-2.5 25 0	2-2.5 26.	5 2-2.5 27.6	1 2 2 -	6 1 3 - 3.7	$\Lambda$
<i>f</i> •	9,5 )1	13-3.5 21 1	3-3.5 21.		13-3.5	1 4-5.5	5 \
500	8.8	7-5.5 20.7	4-5.5 19.	~ i ·	4-5.5	2 \$0.0 394	2
1	N = 2312	9.2	<b>≥6.0</b> 9.5	5 ≥6.0 7.4	1 20.0	005 N= 35.	
		N= 2742	N= 2519		N= 40		Ì
/	T			<del></del>	4		
/	1			}			\
/	/						\
L							
21 Wave Heigl	ht Threshold:	5					December

22 Legend Legend 22

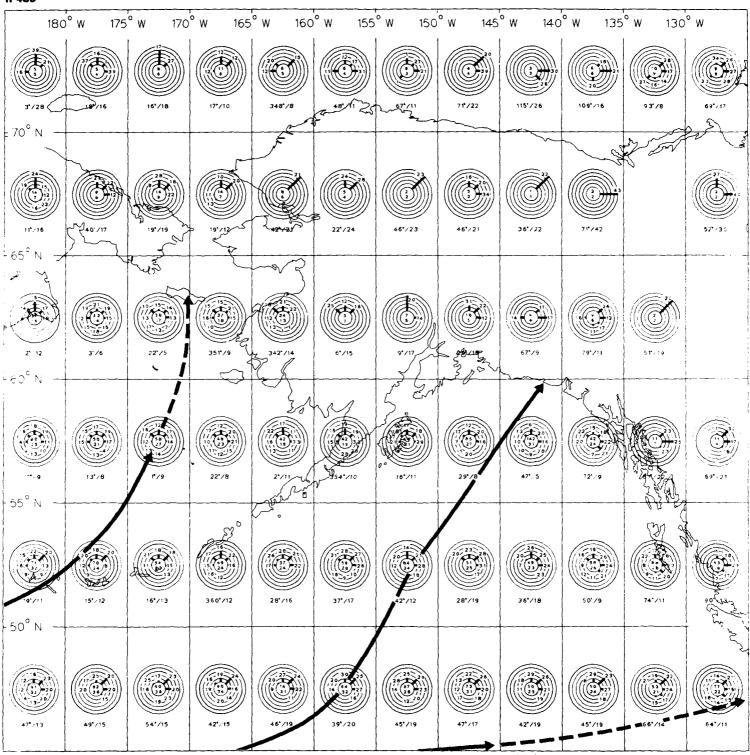
# Map 22. Low pressure center movement

ROSE - Percent frequency of low pressure center movement.

BLACK ARROWS — Preferred storm tracks (solid for primary tracks, dashed for secondary tracks). Exact Cylindrical Equidistant Projection

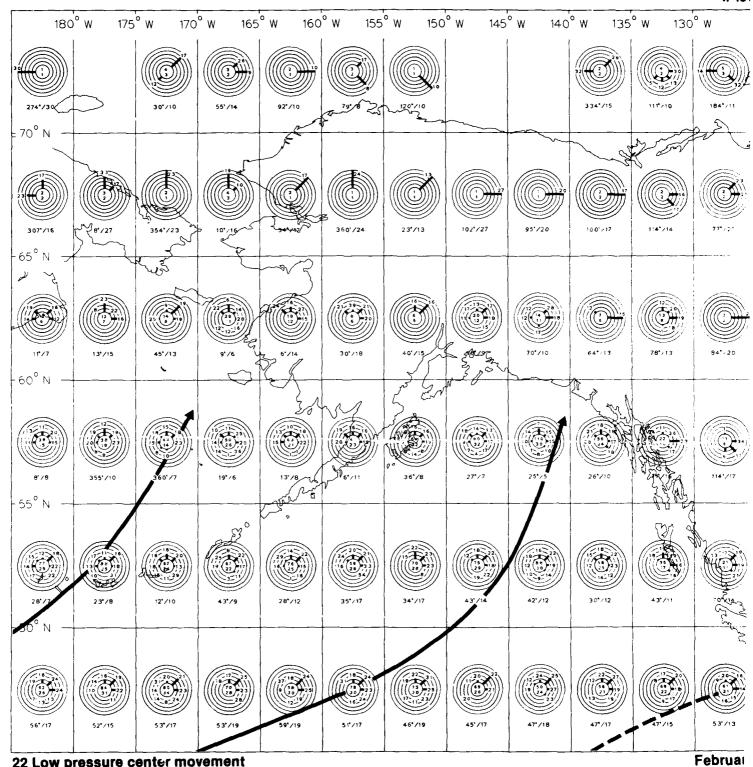
Six hour movements of low pressure centers considering only closed circulations. Mean speed: Printed figures at the end of each bar represent the mean speed of movement (in knots) toward the indicated direction. (Low pressure centers moving toward the N had a mean speed of 12 knots.) 12 Direction frequency: Bars represent percent frequency of six hour movements toward each direction. Each circle represents 20%. 9 (18% of all six hour movements were toward the NE.) (Statistics for this rose are based on 13 six hour movements.) (8 low pressure centers were observed in the 5° X 5° area during the 20 year period of record 1/66-12/85.) (Mean vector movement of all centers was toward 78° (ENE) at 13 knots.) 78°/13•

Refer to the introductory text for Section II for more information on low pressure center movement and preferred storm tracks.

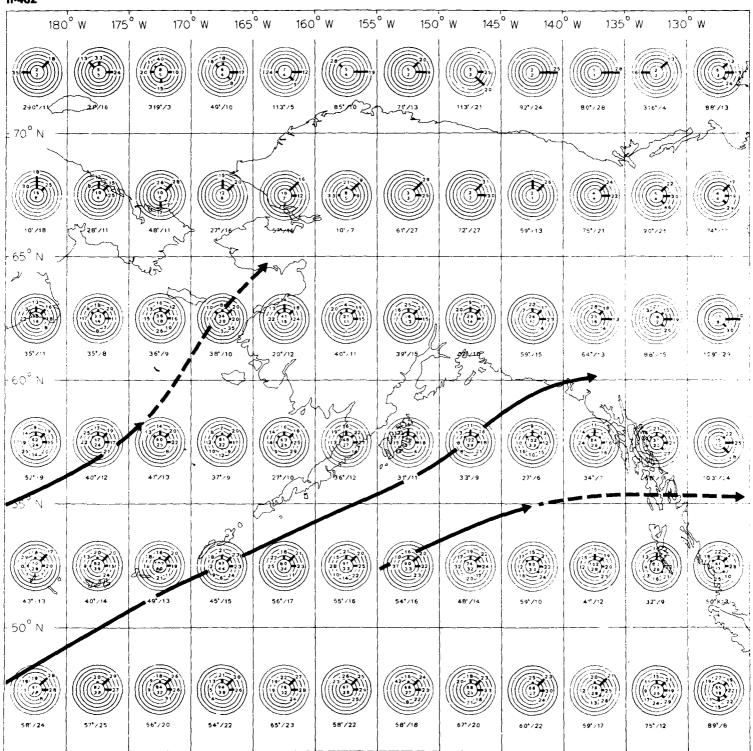


January

22 Low pressure center movement

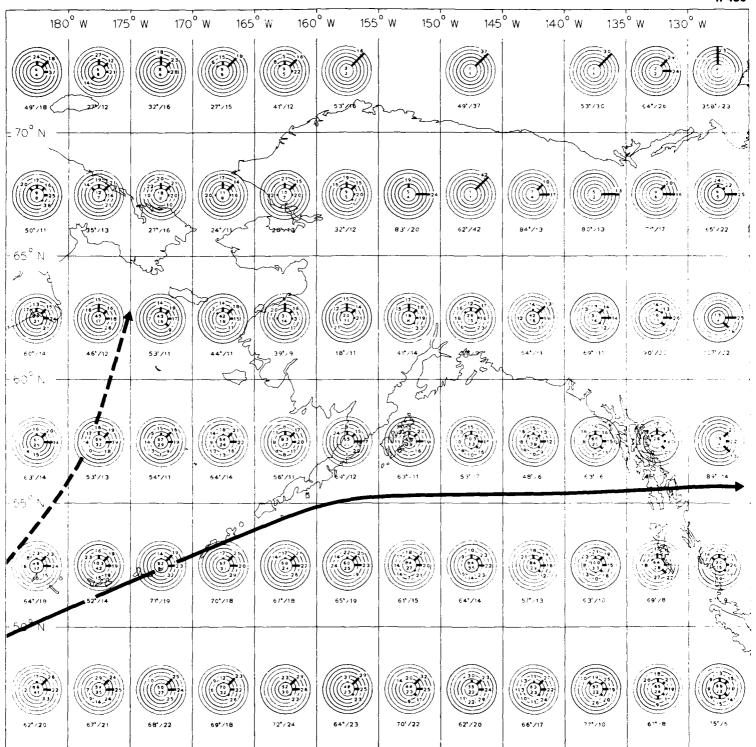


22 Low pressure center movement



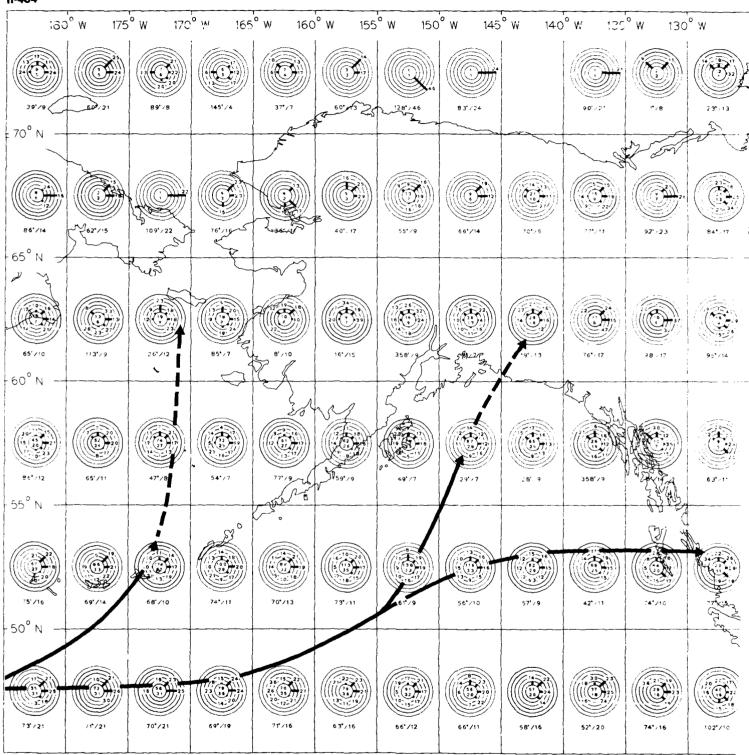
March

22 Low pressure center movement



22 Low pressure center movement

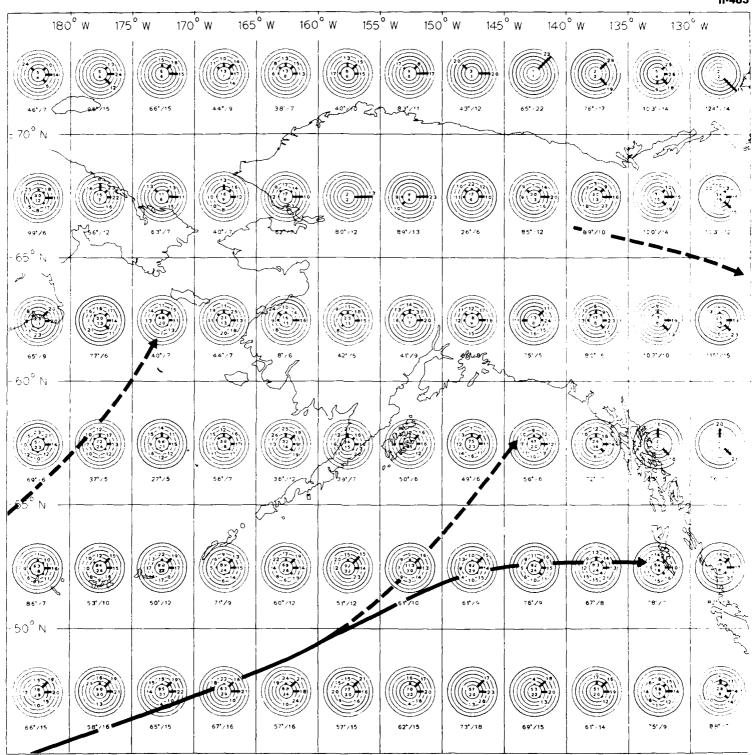
April



May

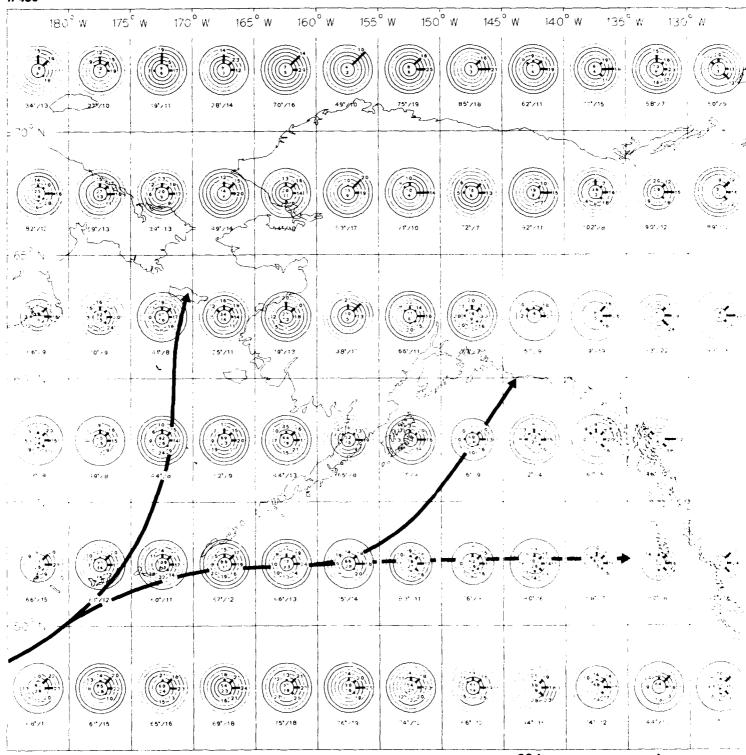
22 Low pressure center movemen

11-485



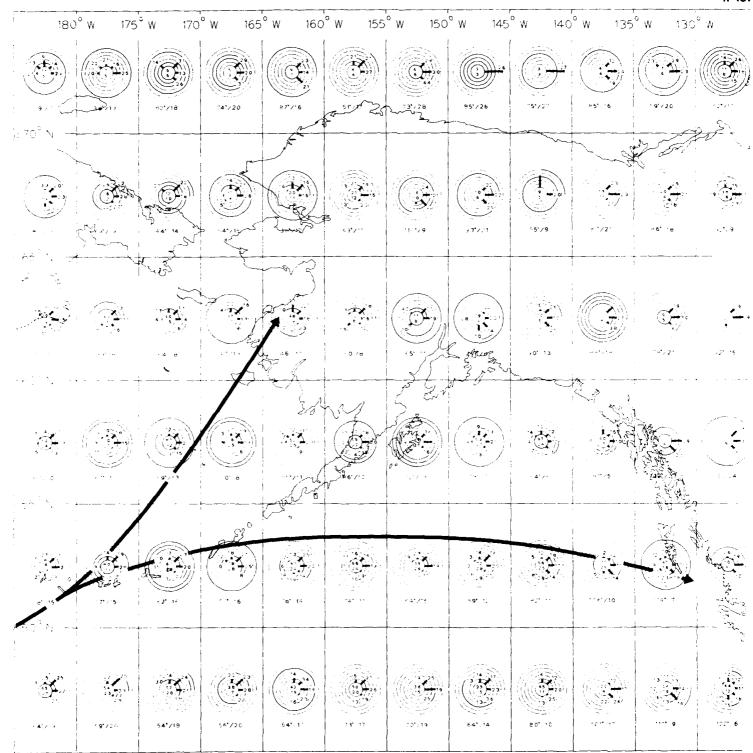
22 Low pressure center movement

June



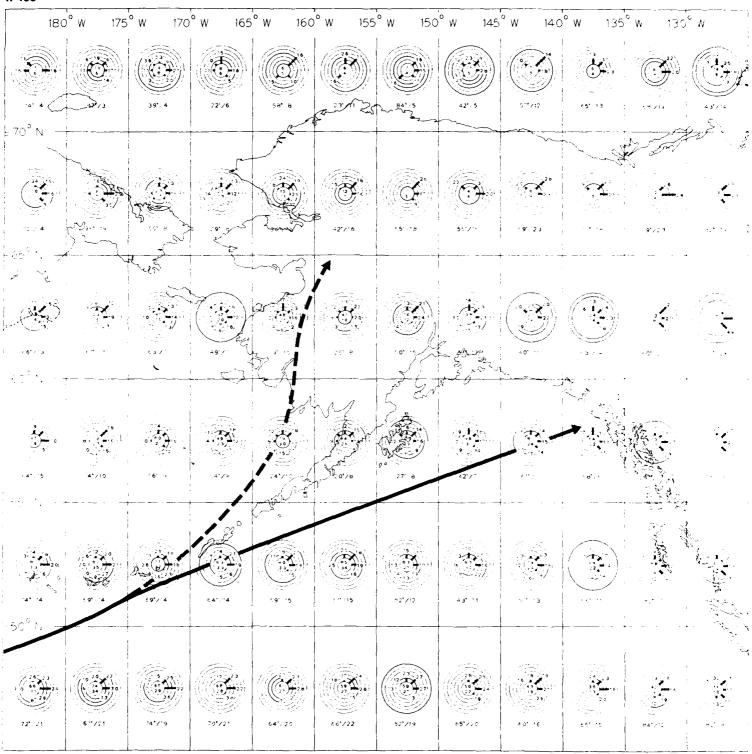
July

22 Low pressure center movemen



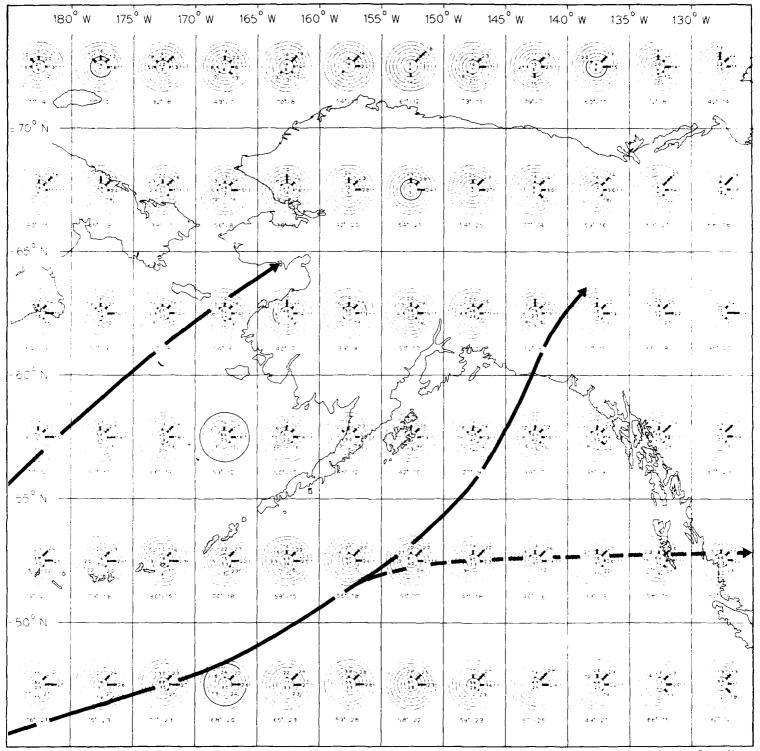
22 Low pressure center movement

Augu



September

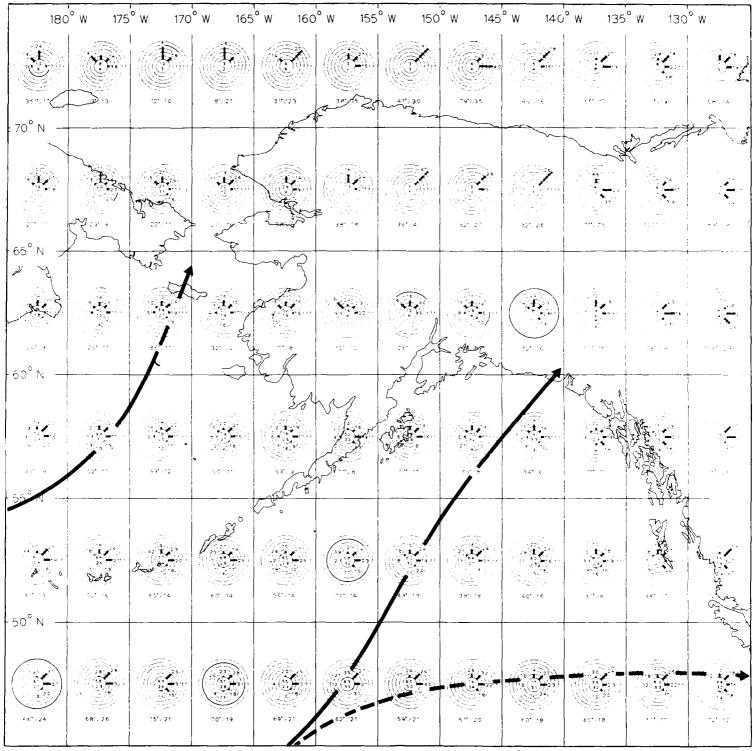
22 Low pressure center movement



22 Low pressure center movement

October

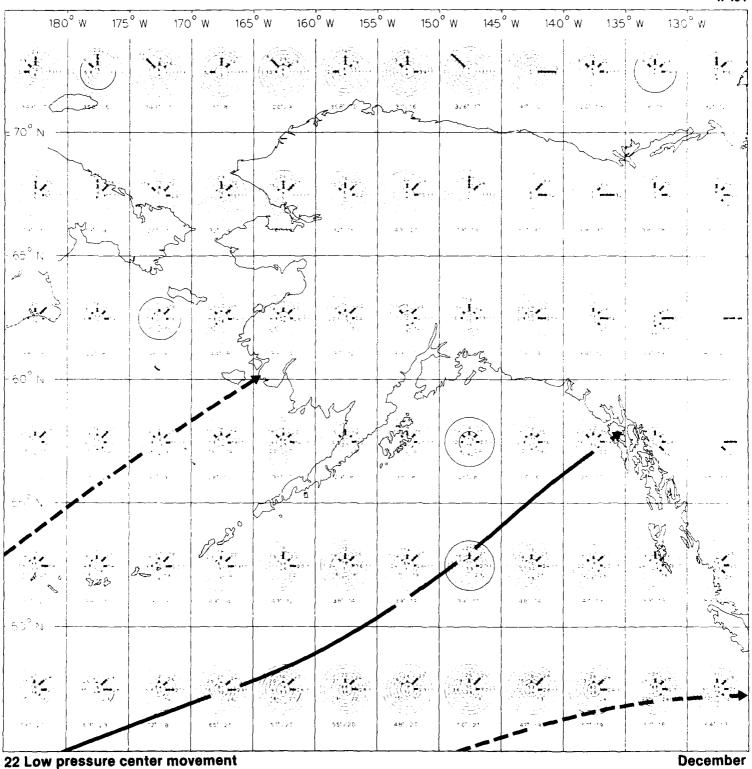
11-490



November

22 Low pressure center movement

II-491



# Set 23. Persistence of wind speed and wave height, seasonal

#### WIND SPEED DURATIONS - SEASONAL

						SI	QU	EN	CE	NU	МB	ER						LA	TITUDE	AND LON	GITUDE
w ≥ 64	2	1		1									Г				24-1	4	8	8	4332
: ≩48	24	10	4	1	+	1		_			$\Gamma$	$\Box$	Γ		Г		(36-1)	40	66	66	4332
N ≥41	59	31	16	7	4	1		3			Γ		Г				48 - 3	121	247	247	4332
≥ 34	85	52	50	22	22	9	3	2	4		2	1	$\overline{}$		1		90-1	252	701	709	4336
S ≥ 28	68	57	57	34	27	19	12	13	6	9	4	6		3	2	5	144-1	322	1353	1365	4362
F ≥ 22	79	63	33	35	30	21	26	15	4	15	10	8	9	9	3	22	252-1	382	2176	2201	4408
Ë ≥ 17	55	50	27	30	23	24	11	12	14	9	18	11	10	6	3	52	288 - 1	355	2884	2981	4432
D ≥ 11	30	17	18	21	21	12	11	В	2	6	5	5	7	5	3	89	558-1	260	3747	4015	4674
k ≥ 7	6	(6)	4	6	8	1.	9	5	3	4	4	1	2	3	2	<b>(</b> 5)	804-1	152	4079	4471	4753
n <u>≥</u> 4	4	11	3	1		5		3	1			1	1	1	1	54	(EA-)	(75)	(4483)	(5174)	(5269)
	4.	17	18	24	30	36	42	48	54	60	66	72	78	<b>a</b> 4	90	96+	MAX	TE	75	T.	TH T

HOURS DURATION OF EVENTS -6 Events with wind speeds ≥7 kn. persisted 12 hours; 85 events persisted ≥96 hours.

The longest event with wind speeds ≥4 kn. persisted for 3 months or more and it occurred 1 time. \_ \_ \_ \_ \_ The longest event with wind speeds ≥48 kn. persisted

36 hours and it occurred 1 time. -----75 Events had wind speeds ≥4 kn. which comprised a

total of 4,483 hindcasts.-----5,269 Hindcasts were examined, and 5,174 had wind speeds ≥4 kn.--

#### WAVE HEIGHT DURATIONS - SEASONAL

							SE	QU	EN	CE	ΝU	M B	ER						LA	TITUDE A	ND LON	GITUDE
	54																					4331
Ç.	48	Ξ							Ι.												1	4331
Ē.	34	7	6	9	1	1	1											(30 - 1)	24	55	65	4331
_ 3	28	1 1	13	12	10	6	5	2	1	2				Π.				54-2	62	213	225	4331
E	20	14	15	9	13	15	20	13	5	6		6	7	4	1	2	2	114-11	134	804	824	4336
1 2	16	21	11	:4	10	17	13	13	19	12	3	10	9	3	3	3	18	312-11	179	1397	1432	4339
H =	12	18	9	19	11	9	13	8	12	10	8	7	9	6	8	3	48	396 ~ 1	198	2275	2345	4367
Τş	9	19	9	5	9	10	6	13	6	10	9	4	3	2	6	1	68	426 - 1	180	2989	3140	4423
, 3	6	6	(e)	4	3	6	3	3	2	2		7	3	3	5	2	(65)	1140-1	122	3506	3977	4515
1 3	3	3	7	1			1		Γ.					1			22	SEA-	(28)	(3828)	(5137)	(5196)
		3	12	18	24	30	36	42	48	54	60	66	72	78	64	9 ¢	96+	MAXT	TE	7	1.	THY
	<u></u> :	<u>'</u>			-40	101	<u>s</u> (	101	(A ]	2 4	-01	= ;	LN	12			_'	, ,	\			- '-'

-8 Events with wave heights ≥6 ft. (1.8m) persisted 12 hours; 65 events persisted ≥96 hours.

The longest event with wave heights ≥3 ft. (0.9m) persisted 3 months or more and it occurred 1 time. --The longest event with wave heights ≥34 ft. (10.4m) persisted for 30 hours and it occurred 1 time --28 Events had wave heights ≥3 ft. (0.9m) which comprised a total of 3,828 hindcasts --5,196 Hindcasts were examined, and 5,137 had wave

Durations for a particular season extend from the time the event begins (or the first day of the season if already in progress), and terminate when the event ends. Events become undefined if missing data is encountered. Durations lasting a season or more are categorized together. Durations may persist into the next season.

#### **ABBREVIATIONS**

MAX: Maximum duration or interval, followed by the number of

TE or Tt. Total number of events or intervals Total number of hindcasts included in TE or TI.

T• Total number of hindcasts that met the stated criteria.
TH: Total number of hindcasts examined.

heights ≥3 ft. (0.9m).-----

#### WIND SPEED INTERVALS - SEASONAL

						SE	Qu	EN	CE	NU	M B	ΕR						LA	TITUDE A	ND LON	GITUDE
w ≩ 64	1	Π	1	Г												9	SEA-7	) 11	2761	4565	4573
1 ≥ 48	1	1		3	3			1					Г	2		33	SEA-6	44	4810	5951	6017
N ≥ 41	7	5	3	В	3	4	3	2	6	2	4	5	5	5	2	61	SEA-1	125	4325	4887	5134
	31	26	18	26	11	12	10	10	9	7	7	6	3	8	6	66	966-1	256	3613	3819	4524
S ≩ 28	50	34	34	33	17	16	15	15	11	8	11	7	10	6	4	51	654-1	322	2916	3035	4370
E ≥ 22	87	59	52	37	19	21	10	9	20	11	10	8	7	3	4	23	348 - 1	380	2157	2211	4336
Ē <u>≥</u> 17		(63)	48	30	23	20	13	12	10	9	2	3	Г		2	(ii)	216-1	352	1440	1452	4333
D ≥ 11	103	60	35	29	9	6	2	2	2	2	1	1				21	132-1	254	655	659	4332
	90	31	10	5	5	2	2	1	1			1				1	(72-1)	148	282	282	4332
n ≥ 4	52	12	2	2	1		_	Г	$\Gamma$			Π			Γ		30~1	(69)	(95)	(95)	(4332)
		12	ALR	24	30	36	4.7	48	54	60	66	72	7 A	H4	90	96+	1 MAX	Ti			<del></del>

HOURS INTERVAL BETWEEN EVENTS 1-There were 63 12-hour intervals between events of wind i speeds ≥17 kn.; 11 intervals persisted 96 hours or more. The longest interval between events of wind speeds ≧7 kn. was 72 hours and it occurred 1 time: ~ The longest interval between events of wind speeds

≥64 kn. was 3 months or more and it occurred 7 times.--There were 69 intervals between events of wind speeds ≥4 kn. which comprised a total of 95 hindcasts----

4,332 Hindcasts were examined, and 95 had wind speeds

### WAVE HEIGHT INTERVALS - SEASONAL

						SE	Qu	EN	CE	NU	мВ	ER						LA	TITUDE A	ND LON	GITUDE
₩≥64				1												8	(SEA-8)	9	2948	4393	4394
A ∨ ≥ 48	11		2			Г							Г	_		11	SEA-8	14	3796	5241	5256
Ė ≧ 34	Г	2		2	_	1	_			1	$\Gamma$			1		40	SEA-5	47	4394	5633	5758
<sub>н</sub> ≧ 28	5	3	3	2	5	1	3	4	2	3		1	1	2	1	57	SEA-1	93	4121	4950	53.4
20 ≤ ع	14	16	8	15	9	6	3	7	2	2	7	4	4	4	1	77	582-1	1179	3166	3298	4474
	25	21	16	14	11	8	15	7	10	7	В	8	3	5	8	47	498 - 1	213	Z502	2562	4433
G H ≥ 12	26	24	33	20	12	16	7	11	11	4	5	8	3	3	3	22	414-1	208	1642	1689	4370
T≥ 9	35	(25)	14	10	9	12	11	В	2	4	3	4	1	2	Γ	$(\cap)$	270-1	151	903	934	4334
, ≩ 6	24	23	10	9	11	3	2	2	2	5	5					41	(144-1)	97	406	412	4333
t ≥ 3	6	2	2	2	2	1		_	_	_					Γ,		36 – 1	1(15)	(40)	(40)	(4333)
	~;	12	18	24	30	36	42	48	54	60	56	72	76	44	90	96+	MAX	7.5		7.7	THI

HOURS INTERVAL BETWEEN EVENTS -There were 25 12-hour intervals between events of wave heights ≥9 ft. (2.7m).; 11 intervals persisted 96 hours or

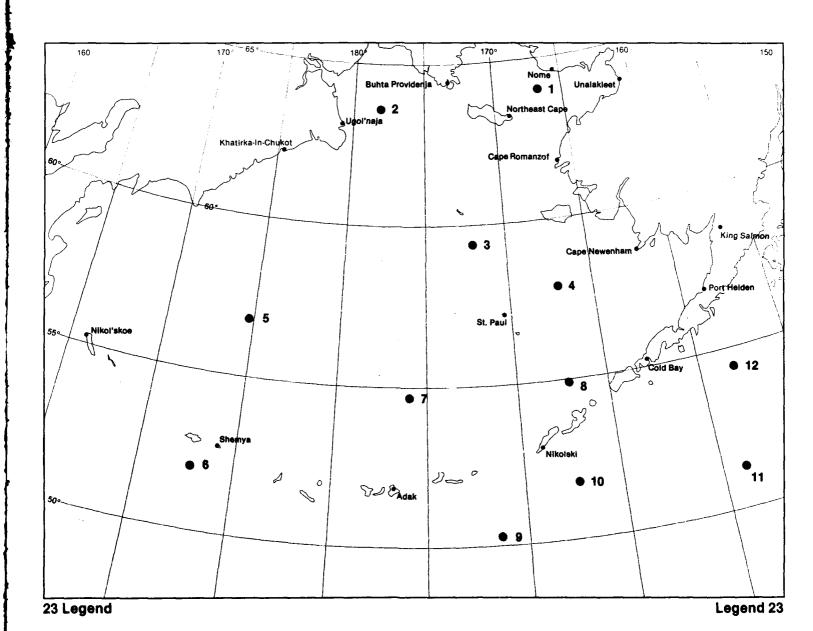
The longest interval between events of wave heights ≥6 ft. (1.8m) was 144 hours and it occurred 1 time.- ~ -The longest interval between events of wave heights ≥64 ft. (19.5m) was 3 months or more and it occurred 8

There were 15 intervals between events of wave heights ≥3 ft. (0.9m) which comprised a total of 40 hindcasts--4,333 Hindcasts were examined, and 40 had wave heights <3 ft. (0.9m).-----

Intervals for a particular season extend from the time the event ends (or the first day of the season if the event is not in progress), and terminate when the event begins intervals become undefined if missing data is encountered. Intervals lasting a season or more are categorized together. Intervals may persist into the next season.

feet	0	3	6	9	12	16	20	28	34	48	64
feet meters	0.0	0.9	1.8	2.7	3.7	4.6	6.1	8.5	10.4	14.6	19.5

The SEA code in the MAX column of the tables refers to season, i.e., the longest event or interval persisted for three months or more. Since the extreme wave statistics are based on the assumption of winds blowing over open water without fetch restrictions, the wave height extremes are likely to be unrealistically high during the winter season for those few grid points located within an area having a probability of ice restricting the development of waves. Refer to the ice statistics in sets 17-19. Refer to the introductory text in Section II for additional information on persistence of wind and waves.



1	ı.	. 4	a	A

N	\$ 6N 178 1 W 2
\$\frac{8}{4}\$   \$\frac{8}{5}\$   \$\frac{3}{3}\$   \$\frac{1}{1}\$    4333 400 4333 932 4333 1614 4344 2418 4368 3052 4372 3860 4497 4275 4629 	
N 441 19 9 10 7 2 2	450 4333 932 4333 1614 4334 2418 4368 3052 4372 3860 4497 4275 4629 70 70 3 4333 49 4333 59 4333 464 4335
\$\frac{2}{5} \frac{3}{2} \frac{10}{13} \frac{14}{6} \frac{13}{13} \frac{7}{6} \frac{15}{13} \frac{16}{6} \frac{13}{13} \frac{7}{6} \frac{15}{13} \frac{12}{6} \frac{15}{2} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{16}{15} \frac{15}{13} \frac{15}{13} \frac{15}{12} \frac{15}{13} \frac{15}{13} \frac{15}{12} \frac{15}{13} \frac{15}{13} \frac{15}{12} \frac{15}{13} \frac{15}{13} \frac{15}{13} \frac{15}{12} \frac{15}{13} \frac{15}{13} \frac{15}{12} \frac{15}{13}	1614 4.334 2418 4368 3052 4372 3860 4497 4275 4629 7 7 3 0N 167.0W 3 4333 49 4333 59 4333 464 4335
S 28 8 44 8 27 19 10 10 10 10 15 7 8 12 4 2 1 2 4 13 180-1 192 1047 1055 4334   S 2 20 20 20 10 13 10 10 13 12 21 10 10 10 4 7 2 5 3 3 13 12-1 238 1870 1897 4336   S 2 20 20 20 10 13 10 10 13 12 10 10 10 10 10 10 10 10 10 10 10 10 10	24 18
F = 22 33 28 23 21 15 13 12 21 10 10 10 10 10 15 15 13 10 8 11 11 13 7 5 2 5 2 3 38 1 312-1 238 1870 1897 4336  E \( \) 17 29 15 10 18 18 15 13 10 21 10 10 10 4 7 2 5 3 3 13 132-1 238 1870 1897 4336  E \( \) 2 1 15 17 16 13 12 7 10 7 10 7 4 7 5 6 5 5 3 4 4 7 4 888-1 194 3425 3588 4466  T \( \) 1 1 1 1 1 1 1 3 7 5 2 5 2 348-1 237 2650 2722 4349  E \( \) 1 2 1 1 17 18 18 18 18 18 18 18 18 18 18 18 18 18	3052 4372 3860 4497 4275 4629 77 77 3 ON 167 OW 3 4333 49 4333 59 4333 464 4336
C   17   16   13   12   15   10   18   18   15   13   10   18   11   11   13   7   5   2   22   348-1   237   2650   2722   4349	386C 4497 4275 4629 7 16 3 0N 167.0 W 3 4333 49 4333 59 4333 464 4335
7 5 7 6 6 4 9 1 3 6 7 1 3 6 7 1 3 6 7 1 3 6 7 1 3 6 7 1 3 6 7 1 3 6 7 1 3 6 7 1 7 1 3 6 7 1 7 1 4 7 1 6 1 6 3 1 9 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4275 4629 1915 7- 3 0N 167 0W 3 4333 49 4333 159 4333 464 4336
1	7- TH 3 ON 167 OW 3 4333 49 4333 59 4333 464 4335
## 6 12 16 24 30 36 42 46 54 60 66 22 78 ms 95046 MAX TC T TS TH HOURS DURATION OF EVENTS    See	T- Th 3 ON 167 OW 3 4333 49 4333 159 4333 464 4335
## HOURS DURATION OF EVENTS    Set   1   2	3 4333 49 4333 59 4333 464 4335
\$\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	3 4333 49 4333 59 4333 464 4335
348 11,5 3 4	49 4333 59 4333 464 4335
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	59 4333 464 4335
\$\frac{2}{2}\frac{3}{3}\frac{7}{2}\frac{1}{5}\frac{1}{3}\frac{7}{2}\frac{1}{5}\frac{1}{3}\frac{7}{2}\frac{1}{5}\frac{1}{3}\frac{7}{2}\frac{1}{5}\frac{1}{3}\frac{7}{2}\frac{1}{5}\frac{1}{3}\frac{7}{2}\frac{1}{5}\frac{1}{3}\frac{1}{3}\frac{7}{2}\frac{1}{3}\frac{1}{3}\frac{7}{2}\frac{1}{3}\frac{1}{3}\frac{7}{2}\frac{1}{3}\frac{1}{3}\frac{1}{2}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{2}\frac{1}{3}\frac{1}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac{1}{3}\frac	464 4335
S ≥ 28 31 37 29 19 18 15 13 8 7 3 7 6 5 7 210 -1 205 1061 1072 4334  S ≥ 28 31 37 29 19 18 15 13 8 7 3 7 6 5 7 210 -1 205 1061 1072 4334  S ≥ 28 33 31 29 19 17 16 12 16 6 10 7 3 7 2 24 246 -1 259 1834 1868 4342  E ≥ 22 43 46 38 30 19 21 16 14 15 11 7 4 7 7 4 6 16 246 -1 297 175 1  E ≥ 17 34 26 22 23 20 23 10 12 14 9 9 4 5 6 6 9 41 420 -1 273 2504 2601 4350  E ≥ 17 34 26 22 21 10 14 8 12 9 13 15 9 8 5 4 3 9 11 462 -1 224 2889 3568 4393  E ≥ 11 17 20 16 14 13 16 15 15 9 14 10 7 8 8 7 15 16 7 2 4 2 86 804 - 1 65 3887  E ≥ 11 17 20 16 14 13 16 15 15 9 14 10 7 8 8 7 18 14 18 18 18 18 18 18 18 18 18 18 18 18 18	— · - • ·
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
E ≥ 17 34 / 20 22 23 32 0 23 10 12 14 9 9 4 5 6 9 41 420 - 1 273 2504 2601 4350       E ≥ 17 49 32 39 28 18 20 21 12 8 9 15 7 7 4 6 43 372 - 1 318 25:5         ≥ 11 22 2 10 14 8 12 9 13 15 9 8 5 4 3 9 71 462 - 1 224 3289 3568 4393       D ≥ 11 17 20 16 14 13 16 15 15 9 14 10 7 5 8 3 7 154 - 1 253 34:3         ≥ 2 1 11 17 20 16 14 13 16 15 15 9 14 10 7 5 8 3 7 15 34 - 1 253 34:3	1769 4338
2 1 1 22 2 10 14 8 12 9 13 15 9 8 5 4 3 9 71 462 1 224 3289 3568 4393 ≥ 7 1 1 1 6 6 5 1 8 7 12 7 5 3 3 3 3 2 7 954 1 169 3733 4102 4478 ≥ 8 7 1 1 1 6 6 5 1 8 7 12 7 5 3 3 3 3 2 7 954 1 169 3733 4102 4478 ≥ 8 7 1 1 1 7 20 16 14 13 16 15 15 9 14 10 7 5 8 3 7 1 534 1 253 3413 × ≥ 7 6 6 7 4 4 1 10 8 7 5 6 7 2 4 2 86 804 1 165 3887	2546 435
x ≥ 7 1 1 1 6 6 5 1 8 7 12 7 5 3 3 3 2 79 954-1 169 3733 4102 4478 k ≥ 7 6 6 7 4 4 1 10 8 7 5 6 7 2 4 2 86 804-1 65 3887	3521 4382
	4 34 45 14
7 ≥ 4 3 2 1 2 1 5 1 3 4 3 3 1 62 134 - 1 91 3897 4501 4633	456" 4"02
6 .2 16 24 30 36 42 48 54 60 66 72 78 44 90 96 MAX TC T TO TH 6 .2 16 24 30 36 42 48 54 60 66 72 78 74 90 96 MAX TC T HOURS DURATION OF EVENTS HOURS DURATION OF EVENTS	Te Tr
5 56.8N 174.8E 6 5.	2.0N 172.9E
w≥64 4 3 2 18-2 9 16 16 4333 w≥64 7 3 12-3 io 13	:34333_
≥46 22 '3 '2 7 5 4 1 1 1 1 1 72-1 66 198 200 4333   ≥48 18 12 12 6 2 1 36-1 5 'E	118 43.13
N =41 21 26 5 22 11 6 6 3 2 1 3 1 2 102-2 120 469 479 4333 N =41 30 19 19 10 7 7 7 3 1 1 1 60- 197 28:	<u>285 43.34</u>
234 46 23 18 7 19 4 10 14 6 14 2 4 1 6 180 - 2 184 914 928 4337 ≥ 34 52 45 14 23 18 9 9 7 4 1 1 1 1 1 1 1 1 1 1 90 - 1 187 650 55 2 2 1 2 2 3 1 2 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	656 4336 1 1233 4337
9 = 25 40 35 24 10 10 20 13 13 13 13 13 13 13 13 13 13 13 13 13	2184 4343
	284 7 4364
1 ≥ 1 32 15 29 14 17 18 9 8 13 6 6 6 6 1 7 6 63 462-1 250 2875 2938 4362       2875 2938 4362       1 ≥ 1 35 29 28 18 27 21 19 17 11 13 8 5 9 8 5 53 282-1 306 278 5 534 1 5 12 8 15 6 8 6 3 16 90 450-1 246 1 3534 1 5 12 8 15 6 8 6 3 16 90 450-1 246 1 3534 1 5 12 8 15 6 8 6 3 16 90 450-1 246 1 3534 1 5 12 8 15 6 8 6 3 16 90 450-1 246 1 3534 1 5 12 8 12 8 12 8 12 8 12 8 12 8 12 8	3658 4396
3 - 6 - 6 - 7 - 13 - 6 - 2 - 7 - 8 - 4 - 2 - 1 - 1 - 10 - 3 - 7 - 4 - 10 - 147 - 4610 4124 4459   k ≥ 7 9 10 8 5 - 3 - 3 - 4 - 6 - 1 - 14 - 1 - 3 - 1 - 5 - 85 :086 - 1 - 149 - 3979	4145 445
≥ 4 3 3 2 3 3 3 3 2 5 1 1 1 2 1 611362-1 90 4345 4655 4781  n≥ 4 11 2 2 2 1 1 1 1 1 2 1 1 661410-1 91 4635	4953 5068
6 2 18 24 30 36 42 48 56 00 66 72 78 44 9096+ MAX TE T TO TH 6 12 18 24 30 36 42 48 54 60 66 72 78 44 9096+ MAX TE T	fe TH
HOURS DURATION OF EVENTS HOURS DURATION OF EVENTS 5.75 175.9W	4.9N 167 2W
M266 2 18-1 3 5 5 4333 W≥64 1 6-: 1 1	433
≥46 24 3 : 4 3 : 1 48-1 52 114 114 4333   ≥48 10 6 3 : 16-3 : 9 3:	34 4332
2 4 39 30 17 9 7 5 4 1	122 4333
≥ 34 49 4 1 23 14 14 7 7 7 5 2 3 1 1 1 2 2 4 150 -1 175 660 670 4336 ≥ 34 45 29 25 14 14 6 3 2 1 1 1 172 -1 '40 396 ≥ 36 6 5 44 76 16 16 8 6 16 5 7 3 2 2 3 7 180 -1 263 1142 1155 4338	405 4333 856 4334
2 ± 28 € 15 : 44   26 : 16 : 16   8 : 16 : 16   8 : 16 : 16   8 : 16 : 16   8 : 16 : 16   8 : 16 : 16   8 : 16 : 16 : 16 : 18 : 18 : 18 : 18 :	7659 4330
5 a. 3 a. 3 j. 4 a. 5 a. 7 a. 5 j. 1 a. 5 j. 2 a. 5 j.	2498 4368
2 · 29 21 16 22 17714 11 12 10 9 7 7 8 5 6 75 426 - 1 268 3467 3565 4368	3587 4462
L≥ 786 1010 7 6 11 8 6 2 6 3 3 5 1 88 636 1 180 3882 4118 4472 K≥ 7 11 8 6 7 9 9 4 7 5 8 9 2 4 5 7 91 732 1 192 4011	4158 4524
2 4 7 : 1 3 3 3 3 : 2 : 3 2 2 64 : 128 - 93 4 187 4598 4720	4646 4765
6 .2 18 24 30 16 42 45 54 60 66 72 78 44 90 46 MAY TE T TO TO 10 18 24 50 60 60 72 78 44 90 46 MAY TE T HOURS DURATION OF EVENTS HOURS DURATION OF EVENTS	та тн
9 50.3N 171.3W 10 5	1.8N 167.3W
n≥04	1 4332
24c 1 1 3 2 1 36-1 28 56 59 4332 ≥48 9 5 3 2 24-2 19 36	$\frac{36}{62} + \frac{4332}{4333}$
N ≤41 29 310 2 6 2 2	425 4333 425 4333
\$34 32 47 1317 (0 7 7 5 12 11 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1	908 4334
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1693 4356
F ≥ 17   64 46 136 42   33   32   92   31   7   20   14   8   10   5   4   7   27   252   1   385   2467   2540   4359   5 ≥ 17   64   46   36   42   33   32   23   18   18   20   15   7   7   8   3   4   37   222   1   377   2487	2545 4366
Dec : 38 (25) 15   25   18   19   12   17   13   18   13   9   11   3   7   7   444-1   314   3464   36   15   4474   Dec : 38   22   17   29   26   17   20   13   12   9   11   41   48   5   11   69   354-3   297   3449	3604 4452
. ≥ 7 16 9 9 5 5 14 7 5 7 4 6 4 10 5 1 92 624 1 199 3970 4250 4598 k ≥ 7 12 11 8 10 13 6 9 4 6 2 8 9 5 6 4 81 684 -1 197 3993	4199 4553
n ≥ 4 1 1 2 1 1 1 4 2 2 1 4 3 4 64 1452 - 1 96 4009 4584 4693 n ≥ 4 3 2 1 5 2 1 2 2 1 1 1 3 2 4 63 1398 - 1 93 4133	4510 4628
C -2 18 24 30 76 42 48 54 60 66 72 78 44 90 96+ MAX TE T TO TH 6 12 18 24 30 36 42 48 54 60 66 72 78 44 90 96+ MAX TE T	Te Th
11 51.3N 158.8W 12	4.4N 158.1V
w≥64 : 1 : 18-1 3 6 6 4333 w≥64 3 1 1 24-1 5 9	9 4333
≥48 18 1 6 3 2 1 1 42-1 34 77 77 4335 N≥48 14 7 5 3 1 2 1 42-1 33 79	79 4333
N 241 37 22 15 9 7 2 2 42-2 94 223 223 4337 N 241 37 22 13 11 5 1 3 1 1 78-1 94 238	240 4333 570 4342
234 65 45 34 20 12 10 5 3 2 1 1 1 1 1 90-1 200 582 586 4342 23 9 15 9 2 3 1 1 1 1 1 90-1 168 566 52 28 75 45 13 13 24 13 13 12 1 1 5 162-1 270 1083	1088 4346
2 2 2 7 3 4 3 3 7 3 0 1 2 2 1 7 1 6 1 4 0 1 3 1 7 1 4 1 2 1 3 1 2 1 4 1 3 0 1 2 2 3 1 1 1 0 1 1 1 2 3 1 2 1 4 1 3 0 1 2 2 3 1 1 1 0 1 1 1 2 3 1 2 1 4 1 3 0 1 2 2 3 1 1 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1909 4349
E € 22 64 55 39 36 20 22 8 28 13 14 7 2 5 6 1 22 216 -1 342 1963 2002 4368 E € 22 67 51 49 29 35 18 28 13 17 9 12 4 4 8 3 14 192 -1 357 1895 E ≥ 17 59 47 37 31 28 20 19 11 12 14 11 8 11 11 4 41 252 -1 364 2660 2730 4377 E ≥ 17 55 41 34 42 29 11 21 13 9 14 14 7 12 11 5 44 234 -1 362 2645	2669 4351
D = 11   32   20   35   20   22   12   12   4   11   9   12   8   8   10   5   82   492 − 1   302   3651   3733   4511   D ≥ 11   32   10   20   24   10   24   17   9   13   7   10   7   6   10   3   83   402 − 2   285   3649	3691 4465
	4197 4523
$k \ge 7 \cdot 10 \cdot 8 \cdot 10 \cdot 11 \cdot 7 \cdot 10 \cdot 7 \cdot 4 \cdot 6 \cdot 10 \cdot 5 \cdot 4 \cdot 8 \cdot 2 \cdot 3 \cdot 86 \cdot 948 - 2 \cdot 191 \cdot 4138 \cdot 4265 \cdot 4588 $ $k \ge 7 \cdot 12 \cdot 7 \cdot 9 \cdot 12 \cdot 4 \cdot 7 \cdot 6 \cdot 5 \cdot 4 \cdot 6 \cdot 8 \cdot 4 \cdot 4 \cdot 5 \cdot 3 \cdot 85 \cdot 900 - 1 \cdot 181 \cdot 4064$	4652 4754
1 2 4 4 2 4 1 2 2 2 1 1 1 3 1 1 2 3 67 1416 - 1 95 4549 4918 5034 1 2 3 2 2 1 1 1 1 1 3 1 65 1518 - 1 89 4316	h
1 2 4 4 2 4 1 2 2 2 1 1 3 1 2 3 67 1416-1 95 4549 4918 5034  6 12 18 14 30 36 42 48 54 60 66 72 78 114 90 95 MAX TE T TO TH  6 12 18 24 30 36 42 48 54 60 66 72 78 114 90 95 MAX TE T	Ts TH
	Te TH

	11-700
1 64.1N 166.7W	2 63 6N 178 1W
W ≥ 64 9 SEA - B 9 3080 4525 4527	W ≥ 64 11 SEA-8 i1 3386 4833 4836
13 55.2 7 19 55.2 5057 5052	N 248 5 3 3 2 1 1 1 1 4 33 SEA-€ 54 5334 6263 6393
	0 ≥41 16 2 1 2 3 3 4 5 3 3 1 3 1 1 56 5EA-1 104 4226 4644 5044 ≥34 14 6 17 5 4 8 7 7 9 4 6 4 5 3 4 65 984-1 168 36:5 3753 4685
	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
P = 26 23 0 10 7 3 7 9 11 12 12 3 9 3 3 0 00 760 - 1 198 3492 3608 4602	P
· · · · · · · · · · · · · · · · · · ·	E ≥ 22 35 22 19 18 16 25 17 11 5 6 6 6 6 10 2 6 34 408 - 1 238 2006 2045 4428
	C ≥ 17 3/ 23 24 24 21 10 9 8 6 6 3 4 3 i 3 21 222-1 203 :308 :344 4357
2 ≥ 11 36 36 39 15 13 15 8 5 2 4 3 2 2 2 2 5 114~1 189 819 830 4345 2 ≥ 7 47 28 20 10 9 4 3 4 1 1 1 1 1 78~1 128 358 361 4333	≥ 11 40 37 29 7 8 13 10 6 7 1 1 1 1 3 210 - 1 163 639 646 4342
1	k ≥ 7 53 25 12 9 9 4 4 1 1 3 1 1 264 - 1 121 353 354 4333
₹ 4 43 16 7 5 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	$0 \ge 4 \frac{6 11 8 6 3 1  2 2 }{12 12 13 13 13 13 13 13 13 13 13 13 13 13 13 $
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
3 59.4N 172.0W	4 58 ON 167 OW
W≥04 10 SEA-7 10 3:34 4672 4677	W ≥ 64 10 SEA-8 10 3375 4920 4823
≥48 2 1 1 2 1 1 2 20 SEA-6 30 389 5666 5727	1 ≥ 48 1 1 1 2 1 1 1 2 21 SEA-7 29 4134 5586 5636
D ≥ 41 3   3   1 2   1   5   1   1   2   3     1   48   SEA - 5   71   5282   5864   6066	N ≥41 2 1 2 3 1 5 2 1 1 1 4 1 1 46 SEA-4 7C 480° 552€ 56d5
≥ 34 9 3 5 4 2 7 8 3 4 5 9 3 6 3 4 68 SEA-2 :43 4419 4716 5263	≥34 13 7 6 8 3 8 6 5 3 4 2 6 5 1 2 76 SEA-1 155 4114 4365 4827
$\frac{5}{6} \ge 28 \cdot .6 \cdot 13 \cdot 9 \cdot 11 \cdot 14 \cdot 12 \cdot 14 \cdot 17 \cdot 4 \cdot 10 \cdot 9 \cdot 6 \cdot 3 \cdot 3 \cdot 3 \cdot 6 \cdot 62 \cdot 8 \cdot 6 - 1 \cdot 209 \cdot 3268 \cdot 3422 \cdot 4491$	S≥28 34 12 9 12 14 15 13 10 9 9 8 11 9 5 2 68 534-1 240 3254 3462 4455
E = 22,29,22,26,16,3,20,10,15,12,11,6,4,2,5,5,46,450-1,260,2453,25;3,4370	E ≥ 22 45 17 31 32 26 16 20 11 15 15 9 8 7 16 1 41 336-1 300 2485 26 15 43/9
L ≥ 17 44 34 34 34 23 21 15 6 14 5 3 7 2 6 4 22 420-1 274 1746 1772 4354	E ≥ 17   54   45   42   36   24   33   9     12   9   10   8   8   4   3   4   18   3   2 - 1   3   9     1507   183   435 3
3 ≥ 11 55 45 29 25 21 12 13 5 4 3 2 2 1 2 126~1 219 821 831 4337	≥ 11 69 58 44 22 13 11 5 11 5 4 2 1 1 1 3 26-1 249 851 862 4334
x ≥ 7 68 44 20 10 9 7 2 1 1 1 60 - 1 162 375 378 4333	k ≥ 7 64 47 19 9 5 6 4 1 1 1 96-1 57 376 350 4333
$^{0} \ge 4 \underbrace{61 \underbrace{15}}_{-12} 4 \underbrace{4}_{-1} \underbrace{1}_{-1} \underbrace{1}_{-1} \underbrace{1}_{-1} \underbrace{42-1}_{-1} \underbrace{86}_{-131} \underbrace{132}_{-131} \underbrace{4331}_{-132}$	n ≥ 4 65 25 2 3 2 3 2 4-3 95 133 135 433
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
5 56.8N 174.8E	6 52 ON 172.9E
₩≥64 1 15 SEA-8 17 35/0 49/8 4994	w≥64 2 14 SEA-7 16 36:1 533 5344
≥48 4 1 2 3 3 2 2 1 1 5 1 1 46 SEA-4 72 4676 5100 5300	N N 1 1 1 1 1 2 1 1 1 1 1 1 1 1 44 SEA-2 57 3945 499€ 5114
3 ± 41 · 15   7   6 · 3 · 3 · 3 · 4 · 4 · 1 · 5 · 3 · 5 · 4 · 2 · 6 · 1 SEA - 2 · 126 · 420 7 · 4463 · 4942 ≥ 34 · 6 · 12 · 9 · 13 · 9 · 6 · 7 · 15 · 6 · 7 · 18 · 5 · 6 · 4 · 4 · 70 · 648 - 1 · 182 / 3465 1 · 3616 · 4540	D ≥41 5 5 1 4 2 3 4 4 2 2 4 1 5 3 58 SEA-1 103 4224 4530 46 4
23. 0.2 2 3 0	\$34 17 20 13 12 6 7 10 6 6 6 6 7 6 5 13 4 62 044 - 1 192 3662 3620 447 f
· · · · · · · · · · · · · · · · · · ·	S ≥ 26 (56) 29 (25) 20 (13) 12 (18) 15 (9) 11 (5) 5 (6) 3 (5) 20 (354 - 1) 296 (354 - 3 59) 43mm
	E ≥ 22   54   44   31   30   23   16   16   14   7   12   7   7   7   7   4   35   246   1   315   216   2773   4347
	E ≥ 17 64 55 41 31 20 18 7 6 8 8 3 1 2 2 7 14 138 -1 303 477 1526 4342
\$\frac{2}{5}\$ \frac{1}{5}\$ \frac{6}{6}\$ \frac{1}{2}\$ \frac{24}{6}\$ \frac{1}{6}\$ \fr	
7 ≥ 4 60 16 5 2 1 1 36 - 1 85 126 126 4333	
( -2 'e 24 30 76 42 4e 54 60 66 /2 7e e4 +0.96+ MAX TI T Te TH	" 2 4 64 13 3 4 1 1 24 -4 64 115 115 4333 6 12 18 24 36 36 42 48 54 60 06 72 78 74 40 904 MAX TI T TO THE
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
7 54.7N 175.9W	8 54 9N 167 2W W≥64 8 SEA-7 8 271 45 4 45 5
348 8 2 2 1 111.1 2 37 SEA-5 58 4890 5454 5568	≥48   1   1   12   1   21   SEA-7   25   4286   514   5147
244 C C 6 2 3 3 3 2 5 2 3 3 2 2 2 62 SEA-1 120 1 4388 4633 4953	N 41 2 1 2 1 3 4 2 1 1 1 1 1 44 SEA = 2 63 425 533 545
≥34 5 1 C 111 € 7 9 4 3 12 5 4 4 3 70 864-1 181 3637 3814 448.	≥34 17.8 7 14 15 5 14 5 2 14 3 12 1 12 76.7eC=1 146 : 3944 421 4660
\$ 328 38 4 17 22 16 .4 17 11 9 7 15 6 6 6 6 6 6 6 6 6 6 1 264 3140 3229 4379	S ≥ 28   26   14   13   10   13   8   15   7   9   4   3   10   3     8     17   1552=1   271     33€ 1   3593   444€
= £22 56 36 38,29 25 21 19 13 12 13 10 3 5 5 13 137 390 - 1 327   2411   2445   4357	F ≤ 22 54 33 328 39 27 26 19 16 7 10 6 6 11 2 7 41 318 -: 332 26 8 7 2701 4355
3 ≥ 17 €3 64 54 38 19 16 19 10 11 5   6   2   5   9   3   14   246 - 1   338   1682   1709   4348	[ ≥ 17 68 63 52 37 25 25 16 12 11 9 7 9 2 1 2 20 240 - 1 359 84! 'e'5 4336
3 · 3 69 43 23 15 · 13 2 4 2 4 2 72-2 265 788 606 4336	D ≥ 11 98 77 41 22 19 15 5 5 2 3 2 2 2 126-1 293 654 861 4116
x ≥ 25 44 23 2 7 4 2 1 1 54-1 174 355 365 4334	k ≥ 7 10139 25 11 3 4 1 1 1 66-1 185 356 36 36 43 W
^ ≥ 4 63 <sup>-1</sup> 5 · · · · · · · · · · · · · · · · · ·	n ≥ 4 76 6   3
6 2 18 24 30 16 42 48 54 60 66 72 78 84 40 96 MAX TI T TH TH	6 (2 18 24 30 36 42 46 54 66 66 (2 78 64 90 96+ MAX)   T
HOURS INTERVAL BETWEEN EVENTS 9 50.3N 171.3W	HOURS INTERVAL BETWEEN EVENTS 10 51 8N :67 3W
% ≥ 04 9 SEA - 7 9 3007 4676 4679	w≥64 8 SE4-7 8 271. 45.5 45 €
≥46 2 3 2 1 1 1 26 SEA-5 36 4329 5351 5410	1 ≥48 1
24' 5 3 1 3 2 311 2 2 1 52 SEA-1 76 4561 4958 5122	N 341 5 2 2 3 2 2 1 2 2 1 2 2 1 2 53 SEA-2 79 4628 5266 5447
≥ 34 15 7 6 7 7 1 4 5 6 5 1 4 5 2 3 76 858 - 1 156 3869 4056 4496	≥34 17 8 5 7 7 2 5 4 3 3 6 3 75 936-1 145 3995 4249 4611
5 3 28 40 21 15 18 16 11 10 13 7 B 10 4 7 2 7 78 546 - 1 267 3425 3567 4487	\$ ≥ 28 36 22 13 10 20 13 5 10 8 5 8 8 7 15 1 81 480 - 1 252 3377 3510 4416
422 59 41 4 20 23 20 13 11 20 15 10 12 13 13 8 31 354 - 1 350 2674 2714 4402	£ \$22 60 44 35 23 22 22 14 15 11 11 13 7 7 7 5 46 3 2-1 342 2628 2691 4360
5 ≥ 17 89 63 47 37 28 23 23 17 13 9 12 8 2 1 1 2 11 198 - 1 385 1806 1837 4350	<u>F≥ 17 78 64 46 48 37 19 18 13 10 9 7 8 2 2 14 240-1 375 1782 1840 435</u>
2 10 78 36 36 8 8 5 4 3 4 2 1 1 12C - 1 309 849 859 4332	<sup>0</sup> ≥11 0479 37 22 72 7 6 6 6 2 1 1 1 2 1 2 1 2 96-2 295 854 855 4342
k ≥ 7 10456 20 4 3 4 1 1 1 54-1 193 348 348 4332	$k \ge 7 1442 18 10 4 1 2 2 1 54-1 194 357 357 4335$
<sup>9</sup> ≥ 4   7d   6   5   1	n ≥ 4 66 15 5 2 2 24-2 88 19 19 19 4333
6 2 18 24 30 36 42 48 54 60 66 72 78 84 40 96+ MAX TI T TE TH HOURS INTERVAL BUTWEEN EVENTS	6 .2 18 24 30 16 42 48 54 60 66 /2 78 64 40 46+ MAX TO THE HOURS INTERVAL BETWEEN EVENTS
1151.3N 158.8W	12 54.4N 158 1W
W ≥ 64 1 10 SEA-8 11 3411 4856 4862	W≧64 12 SEA-7 12 3623 5185 5.34
248 2 1 1 1 1 30 SEA-4 37 4069 5411 5486	1 ≥ 48 3 i 1 1 1 1 32 SEA-2 39 4336 5525 5604
0 41 7 4 5 2 2 2 3 4 4 1 1 3 1 60 1350 - 1 99 4152 4561 4780	N ≥ 41 7 3 1 1 2 5 1 4 2 2 2 1 71 1170-1 102 4083 4488 4728
≥ 34 28 :3; iC 10; 13 :3 7 6 5 2 3 8 i 2 1 83 690 -1 205 3719 3987 4564	≥ 34 (13 6 9 10 18 10 6 3 4 4 3 2 2 2 6 77 762-1 175 3763 3955 45:6
5 ≥ 26 40 29 22 20 21 9 13 9 15 9 6 12 2 7 4 67 438 -1 285 3i27 3260 4418	S≥28 27 25 26 23 23 12 12 5 11 11 7 7 3 4 5 74 444-1 275 3234 3380 4455.
£ ≥ 27 59 35 46 39 26 14 11 21 14 12 9 6 7 6 8 30 306 - 1 343 2366 2441 4408	E ≥ 22 69 50 47 32 23 20 19 16 12 4 5 8 5 7 6 35 378 1 358 24 15 2463 4356
E ≥ 17 90 70 53 28 30 17 20 6 6 5 7 7 5 1 16 198 -2 361 1618 1662 4348	E ≥ 17 71 71 58 39 22 25 17 12 6 4 4 7 4 4 3 13 186-1 360 1657 1694 4345
2 ≥ 11 116/79 37 23 12 5 5 6 1 3 3 i 2 84~2 293 762 782 4337	D ≥ 11 05 72 34 22 11 13 4 3 5 3 2 1 1 1 1 90-1 277 761 777 4336
x ≥ 7 1337 16 7 3 5 1 54-1 182 317 323 4333	k ≥ 7 97 38 21 7 5 3 1 1 1 66-1 173 325 326 4333
n ≥ 4 69 17 3 1 24-1 90 116 116 4333	n ≥ 4 65 12 4 1 101 102 4333
6 -2 16 24 30 36 42 46 54 60 66 72 78 84 90 96+ MAX TI T TO TH HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 H4 90 96+ WAX TI T TO TH HOURS INTERVAL BETWEEN EVENTS
23 Persistence of wind speed-interval	Winter

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ч		u	к

· <b>496</b>	64 1N 155 7W	2 63 6N 178 1W
· · · · · · · · · · · · · · · · · · ·	64.1N 166.7W	W ≥ 64 1 1 1 1 4241
w ≥ 64 1 ≥ 48 1 6-1 1	1 1 4241	≥48 1 1 2 5 5 4241
N = 41 1 30-1 1 AR = 1 11	5 5 4241	L = 41 8 2 4 2 1 36 -: 17 38 36 424:
D ≥ 34 5 2 1 ! ! ! ! !	31 31 4241	234 223 6 2 1 3
S ≥ 28 13 i5 8 6 3 2 3 i 60-1 51	152 153 4241	P 20 24 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
F = 22 18 19 18 21 12 6 2 9 2 3 1 3 1 1 1 108-1 117	517 523 4241	E ≥ 22 28 15 11 14 9 18 9 8 5 4 7 2 1 1 1 4 198 1 136 738 758 4.2 1 1 2 17 33 11 16 12 12 16 8 8 11 11 7 4 5 1 2 16 252 1 173 1256 1309 4241
$E \ge 17 \ 36 \ 15 \ 21 \ 15 \ 21 \ 20 \ 11 \ 8 \ 7 \ 9 \ 4 \ 4 \ 2 \ 3 \ 4 \ 9 \ 162-1 \ 189$	2241 233B 4243	D ≥ 11 34 30 15 19 11 9 10 12 10 8 14 6 8 6 4 42 354 - 1 238 2230 2409 4250
21	3056 3254 426/	27 16 7 16 17 16 17 16 10 4 7 5 68 402-1 211 3061 3321 4305
K = 727 10 17 10 12 10 10 10 10 10 10 10 10 10 10 10 10 10	<del></del>	n ≥ 4 21 20 8 6 5 16 3 4 5 2 2 € 4 5 3 71 846-1 181 3481 31-1 4.341
2 4 22 6 6 9 0 0 2 15 5 7 8 8 90 96 WAX TE	T T+ TH	6 12 18 24 3C 36 42 48 54 6C 6C 72 78 44 90 46 WAY TE T TO THE HOURS DURATION OF EVENTS
HOURS DURATION OF EVENTS	59.4N 172.0W	58.0N 167.0W
w≥64	4241	W = 04
, ≥48 1 1 2	7 7 4241	N 24 24 424 1 5 2 4 424 1
N = 41 5 2 1 30 - 1 8	80 80 4241	N ≥ 41 B   5   2     18 - 2   24   24   42   24   24   24   24
≥ 34 15 15 2 3 2 1 42-1 38 S > 76 (25 2) 116 10 9 1 1 3 2 1 54-1 88	80 80 4241 252 256 4241	S ≥ 28 28 23 20 14 € 6 1 1 2 1 60-1 102 299 309 4241
P = 20 23 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	<del></del>	P ≥ 22 43 25 27 19 15 16 7 4 4 1 1 4 3 126-1 169 665 684 424
E = 22 29 14 22 20 18 13 13 13 15 16 15 13 16 13 10 1 324	- <del> </del>	E ≥ 17 44 30 43 26 25 19 10 20 8 4 10 4 2 3 3 7 186-1 258 · 327 · 352 434
D ≥ 17 44 26:20 22:18 21 16 13 12 7 5 6 5 3 6 210 1 224 D ≥ 11 35 13 14 13 15 21 19 13 21 10 11 8 7 9 6 45 306~2 260		0 ≥ 11 26 20 27 24 23 21 16 11 17 11 11 11 11 18 9 43 300 - 1 2°0 2594 26°C 4249
N ≥ 7 26111 6 5 7 5 6 11 9 9 10 10 11 9 6 76 558 -1 217		k ≥ / (2010 10 18 17 10 14 15 15 15 15 15 15 15 15 15 15 15 15 15
$n \ge 4   15   6   7   2   3   3   5   2   2   2   5   1   1   5   5   76   936 - 1   140$		$0 \ge 4 \begin{array}{ c c c c c c c c c c c c c c c c c c c$
C 12 18 24 30 16 42 48 54 60 66 /2 78 44 40 46+ MAX TE	T TA TH	HOURS DURATION OF EVENTS 52.0N 172 9E
5	56.8N 174.8E	w≥64 424'
W≥64 24-1 8	i3 i3 4241	1 ≥ 48 5 3 4 1 16-4 12 23 23
N 44 8 7 5 2 2 30 -2 24	55 55 4241	$\frac{N}{D} \ge 41 \cdot 12 \cdot 7 \cdot 9 \cdot 3 \cdot 1$ $30-1 \cdot 32 \cdot 70 \cdot 10 \cdot 424^{\circ}$
234 13 12 13 7 2 3 3 1 48 -1 54	161 161 4241	≥ 34 26 14 17 5 7 2 3 424 42-3 74 193 93 424
S ≥ 2¢ 19 16 13 16 14 17 3 4 3 1 2 66-2 9E		S≥28 29 34 17 22 9 5 5 4 2 2 1 2 78 -2 132 453 459 424 1
F = 22 29 12 23 17 14 17 13 9 5 11 3 1 2 3 1 126-1 160		E = 22 46 29 33 30 17 10 17 12 13 13 13 13 13 13 13 13 13 13 13 13 13
5 ≥ 17 50 24 23 22 22 14 13 14 9 9 7 13 5 2 4 11 252-1 242		L & 17  47   30   23   33   20   22   10   13   17   13   14   15   15   15   15   15   15   15
<sup>3</sup> ≥ 11 37 23 23 15 16 120 24 14 11 9 12 12 7 9 4 52 288 -1 286	-+	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
7 27 9 10 7 13 9 7 7 7 15 8 2 3 5 8 89 546-1 22t		n ≥ 4 6 4 2 4 3 7 3 5 i 3 4 1 3 2 80 i30e - 1 128 36/0 42' ± 44"
T ≥ 4   C   7   C   4   7   4   1   4   3   2   2   2   4   80   826-1   140		6 .7 18 24 30 16 42 48 54 60 C6 /2 78 d6 90 96+ MAX TE
HOURS DURATION OF EVENTS	\$4.7N 175.9W	HOURS DURATION OF EVENTS 54 9N 167 2V
y ≥64 12-1 1	2 2 4241	w≥64 424
¥=04 ≥48 5 3 18-1 9	14 14 4241	7 ≥ 48 6 6 6 6 6 6 424 ·
30-2 31		D = 4   C   3   14   16   27
≥ 34 :5 20   14 2 6 4 1   48 - 1   62		≥ 34 17 11;10 6 3 1
S ≥ 28 3   34 23   20 4 8 4 4 3   1 1   78 - 1   13:		E ± 22   51   38   30   19   14   11   10   8   6   2   4   1   1   3   2   156 - 1   200   794   803   424
22 52 48 29 21 15 13 13 7 7 3 1 6 1 2 1 2 114-1 22 5 217 38 33 35 30 27 23 16 14 12 9 6 6 7 5 2 11 150 - 1 274		E ≥ 17   54   30   41   38   27   22   19   9   11   8   8   8   2   3   4   10   186 - 1   294   1545   1556   424   1
217 38 33 35 36 27 23 10 11 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	<del></del>	D = 11 41 26 20 20 33 27 11 26 7 17 7 8 12 8 3 51 336-1 317 2 45 2801 4254
21: 41 19:24 31 22:18:21 20:14:16:9 9 7 9 7 53 222-1 32 22: 15: 4 15: 9 12: 11 9 8 9 9 3 8 6 8 87 762-1 24:		$k \ge 7 \   14 \   13 \   8 \   10 \   9 \   13 \   8 \   7 \   13 \   2 \   7 \   3 \   7 \   11 \   7 \   85 \   504 - 1 \   217 \   35 \   6 \   3646 \   4295$
r ≥ 4   15   3   4   2   3   7   6   7   2   4   2   3   2   84   B22-1   144	4 3859 4137 4393	0 2 4 4 3 3 4 7 3 1 3 1 1 5 1 4 1 2 78 882-1 12' 3910 4'34 4363
6 .2 18 44 30 30 42 48 54 60 66 /2 78 84 40 96+ MAX TO	T Te TH	HOURS DURATION OF EVENTS
HOURS DURATION OF EVENTS	50.3N 171.3W	10 51.8N 167.3
W≥64 1 6-1 1		₩ 264 1 24° 3 4 1 24-1 8 15 17 424
≥4¢ 5 2 2 1 1 1 36-1 11		N = 41 10 6 3 2 1 1 1 42-1 23 5 55 4241
D 54 1 (6 3 3 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		≥34 31 20 13 3 5 1 1 1 1 60-1 75 173 17€ 424°
\$34 36 22 17 5 4 1 3 2 66-2 9C 5 \$228 137 28 19 18 11 7 6 3 3 6 1 1 1 102-1 14		S≥28 39 26 19 22 5 11 4 4 2 3 1 1 1 84-1 138 472 484 424
5 22 50 46 28 21 16 16 18 7 8 6 6 1 3 1 2 6 138 -1 23	5 1073 1096 4246	E ±22 50 44 34 19 20 16 8 12 10 6 6 2 2 1 1 4 132-1 235 1032 1053 424
F ≥ 17 55 47 28 51 16 15 16 15 15 7 6 7 4 4 3 19 252-1 30	8 1797 1864 4250	E ≥ 17 37 38 41 31 27 11 14 16 22 4 15 5 3 2 4 18 228 - 2 288 1773 1802 4256  D > 11 19 23 23 25 16 14 15 27 11 10 13 10 9 5 6 53 384 - 1 286 2862 29 4 4296
0 > 11.34.74.25 18 32 18 8 15 10 21 7 10 9 10 2 52 402 - 1 29		211 28 23 23 23 19 14 13 22 11 16 13 10 9 3
- $        -$	2 3565 3775 4355	k ≥ 7 18 10 21 15 11 6 8 12 10 6 8 5 3 7 3 89 612-1 232 3494 3713 432 n ≥ 4 11 4 5 8 4 8 4 8 4 4 4 1 5 3 2 2 4 74 738-1 143 3829 4160 438
1 2 4 6 2 4 3 7 1 2 4 4 1 1 2 6 8 918-1 12 6 .2 18 24 30 16 42 48 54 60 66 72 78 84 90 90 MAX TI		A 7 10 M 30 16 62 48 54 60 66 72 78 H4 90 96 MAX TO T THE TH
HOURS DURATION OF EVENTS		HOURS DURATION OF EVENTS 12 54.4N 158.1
11	51.3N 158.8W	w≥64 424
w≥64 >>48 3 4 1 36-1 8		1 ≥ 48 10 1 1 1 54-1 12 23 23 424
N ±41 19 11 6 2 2 1 42-1 4		$\stackrel{N}{\underset{D}{=}} 41 \ 21 \ 9 \ 4 \ 2 \ 1$ 1 1 66-1 38 75 75 424
D ≥ 34 29 23 12 11 4 1 3   i   1 1   78 - 1   81	6 237 239 4241	≥34 32 21 9 10 4 2 4 1 1 1 78-1 83 214 210 Tell
S = 28 50 39 24 20 19 10 5 4 3 1 1 2 90 -2 17		2 2 2 4 1 32 22 23 10 10 3 3 2
5 4 22 57 32 43 38 22 18 14 7 5 7 2 3 2 7 3 6 150 - T 26		E = 22 47 40 20 31 22 9 10 0 9 0 5 1 0 2 2 2 2
$E \ge 17 \cdot 44 \cdot 40 \cdot 34 \cdot 32 \cdot 24 \cdot 26 \cdot 25 \cdot 6 \cdot 10 \cdot 8 \cdot 9 \cdot 7 \cdot 5 \cdot 3 \cdot 5 \cdot 29 \cdot 240 - 1 \cdot 30 \cdot 6 \cdot 10 \cdot 10 \cdot 10 \cdot 10 \cdot 10 \cdot 10 \cdot 10$		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
D ≥ 11 25 15 15 18 25 16 16 13 16 11 14 5 6 3 7 64 564~1 26		k ₹ 7 19 5 9 12 7 5 10 9 9 5 7 5 10 1 4 90 600-1 207 3612 3774 433
* 2 / 13 10 12 8 0 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15		n ≥ 4 12 4 3
A 3 18 24 30 36 42 48 54 60 66 72 78 64 90 96+ MAX 1	E T TO TH	6 12 18 24 30 36 42 48 54 60 66 72 78 n4 90 96+ MAX TE T TO THE HOURS DURATION OF EVENTS
HOURS DURATION OF EVENTS		
Sorina		23 Persistence of wind speed-durati

Spring

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1	64.1N 166.7W 6 2208 4265 4265	2 63 6N 17/ w≥64 1 1 6 SEA-6 7 2220 4264 4
6 SEA-6 7 SEA-6	7 2257 4264 4265	w≥64 1 6 SEA-6 7 2220 4264 4 1≥48 2 6 SEA-6 8 2230 4260 4
7 SEA-6	7 2255 4260 4265	N > 41 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1 1 1 1 13 SEA-7	17 3077 4488 4519	D=1 2 2 1 1 2 2 2 1 1 24 SEA-8 36 4013 4951 5
3 1 4 1 2 1 2 2 1 3 1 3 31 SEA-5	55 3451 4990 5143	S≥28 14 1 2 2 2 1 3 2 1 2 1 3 3 43 SEA-2 80 3657 5003 5
<del> </del>	120 3889 4591 5114	P ≥ 22 14 3 11 8 6 11 4 7 5 1 6 7 1 4 51 SEA-1 139 3904 433? 5
<del>                                     </del>	194 3285 3519 4650	E = 22 17 3 13 12 14 7 5 9 8 1 3 6 2 6 6 51 1572-1 177 3119 3345 4
	234 1997 2046 4382	
46 43 15 73 14 17 10 5 4 5 3 3 5 11 210 - 1		
<del></del>	174   471   474   4246   TI T Ta TH	$0 \ge \frac{1}{6} \frac{142}{20} \frac{15}{12} \frac{10}{10} \frac{3}{3} \frac{3}{3} \frac{1}{10} \frac{1}{10} \frac{3}{126} \frac{126-1}{174} \frac{174}{537} \frac{537}{540} \frac{540}{4} \frac{4}{126} \frac{4}{126} \frac{1}{126}
6 12 18 14 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX HOURS INTERVAL BETWEEN EVENTS		HOURS INTERVAL BETWEEN EVENTS
3	59.4N 172.0W	4 58.0N 16
6 SEA-6	6 2208 4265 4265	w≥64 6 SEA~6 6 2208 4265 4
1 7 SEA-6	8 2265 4258 4265	1 ≥48 6   SEA~6 6   2208   4264 4
1 1 10 SEA-6	12 2524 4250 4266	C = 41 1 1 1 1 14 SEA-7 18 2976 4470 4
4 1 1 2 2 1 1 1 3 1 23 SEA-5	39 3718 4920 5000	≥34 2 1 1 4 1 1 2 2 2 2 3 28 SEA-2 49 3450 5349 5
4 2 2 2 7 3 5 3 3 3 5 1 4 2 44 SEA-1	90 3739 5213 5469	$S \ge 28 \ 6 \ 8 \ 5 \ 2 \ 3 \ 5 \ 4 \ 2 \ 4 \ 3 \ 7 \ 3 \ 3 \ 4 \ 2 \ 48 \ 2184 - 1 \ 109 \ 4538 \ 4962 \ 5$
12 9 6 9 9 5 6 7 6 3 8 3 3 3 4 58 2058 - 1	151 3829 4410 5070	F ≥ 22 11 11 13 13 4 10 11 10 4 8 3 5 8 4 3 57 1956-1 175 3853 4146 4
25 20 16 19 13 14 11 9 11 8 7 9 2 2 2 60 852-1	228 3150 3281 4538	$L \ge 17$ 40 30 22 22 16 16 10 4 7 4 11 6 7 3 1 61 954-1 260 3159 3329 4
55 35 30 27 19 12 7 12 8 2 5 8 1 3 1 34 372-1	259 1829 1880 4363	D ≥ 11 58 60 29 23 19 19 10 5 15 10 3 3 4 3 2 22 312-1 289 1647 1680 4
65 47 25 22 8 12 5 4 5 5 3 6 1 2 1 3 108 - 1	214 808 824 4260	k ≥ 7 75 56 19 25 20 9 7 7 2 1 2 1 2 1 1 1 126-1 228 726 742 4
69 28 : 3 9 3 3 3 5 2 1 72-1	136 324 325 4243	$n \ge 4   65   33   12   6   4   3   1                                $
6 12 18 24 30 36 42 48 54 60 66 72 78 H4 90 46+ MAX	TI T TO TH	6 12 18 24 30 36 42 48 54 60 66 12 78 n4 90 96+ MAX TI T Te
HOURS INTERVAL BETWEEN EVENTS	56.8N 174.8E	HOURS INTERVAL BETWEEN EVENTS 6 52.0N 17
6 SEA-6	6 2208 4265 4265	W≥64 6 SEA-6 6 2208 4265 4
1 1 1 1 1 SEA-6	14 2802 4711 4724	W = 04
1 1 1 1 1 1 1 21 SEA-7	28 3636 5071 5126	N = 41 1 1 7 1 2 1 1 1 25 SEA 5 34 3854 5155 5
3 1 1 1 1 3 1 2 1 1 1 1 37 SEA-1	55 4033 5529 5690	D ≥ 34 6 4 1 3 4 4 3 1 1 1 3 3 42 SEA-4 76 4270 5047 5
`- <del></del>	101 3861 4673 5053	_ \_+
0 3 3 3 4 4 3 1 3 2 3 3 3 3 3 7 2 3		
	<del></del>	
38 20 16 25 11 14 13 8 6 3 12 9 4 7 8 52 600-1	246 2703 2834 4305	E ± 17 34 38 32 26 12 16 12 8 9 7 6 7 5 2 7 55 426~1 276 2588 2633 4
64 46 33 30 19 16 16 10 7 6 7 4 4 4 2 18 216-1	286   1567   1639   4258	£ 11 91 49 40 22 17 12 19 8 , 8 17 12 18 13 13 12 113 1300~ 1 304 1410 1422 2
	220 744 783 4250	$k \ge 7 \ 83 \ 35 \ 38 \ 17 \ 11 \ 7 \ 8 $
71 27 18 4 2 4 10 1 1 1 1 2 1 1 90-1	133 300 303 4241	$n \ge 4 \begin{bmatrix} 62 \\ 23 \end{bmatrix} 24 \begin{bmatrix} 4 \\ 3 \end{bmatrix} \begin{bmatrix} 2 \\ 1 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} \begin{bmatrix} 1 \\ 84-1 \end{bmatrix} \begin{bmatrix} 257 \\ 259 \end{bmatrix} 4$
6 12 14 24 30 36 42 48 54 60 66 72 78 H4 90 96+ MAX HOURS INTERVAL BETWEEN EVENTS		HOURS INTERVAL BETWEEN EVENTS
7	54.7N 175.9W	8 54.9N 16
1 6 SEA-6	7 2218 4263 4265	w≥64 6 SEA-6 6 2208 4265 4
i 1 1 12 SEA-7	14 3078 4715 4729	1 ≥ 48 9 SEA-4 9 2284 4617 4
1 2 1 1 1 1 26 SEA-6	33 3562 5240 5305	D 241 1 1 1 15 SEA-4 18 25 5 4695 4
3 4 2 2 2 1 1 2 1 1 2 2 1 39 SEA-2	63 3875 4927 5094	≥34 3 i 1 1 1 1 2 1 1 1 2 34 SEA-2 50 3618 5223 5
9 4 8 7 9 7 8 3 6 2 1 4 4 2 2 58 2016-1	134 3865 4579 5008	S≥28 9 5 9 8 4 4 2 6 1 5 4 6 3 2 3 49 SEA-1 120 4655 5073 5
<u> </u>	231 3354 3509 4435	$\varepsilon \ge 22 \   18 \   16 \   18 \   17 \   12 \   11 \   10 \   5 \   6 \   3 \   7 \   5 \   5 \   5 \   3 \   62 \   1728 - 1 \   203 \   3849 \   4123 \   4$
<del> </del>	281 2596 2714 4312	E ≥ 17 51 25 36 29 19 10 11 7 11 6 B 6 4 2 6 60 804~1 291 2810 2961 4
87 60 36 28 24 25 9 7 11 3 3 5 3 2 3 17 168 -2	323 1513 1550 4290	D ≥ 11 83 63 40 23 17 19 11 11 15 5 5 3 3 1 2 17 198-1 318 1509 1522 4
10045 30 18 15 4 4 7 4 4 3 2 2 1 102-1	239 719 720 4250	k ≥ 7 83 48 28 13 15 10 3 3 2 3 2 1 2 3 2 132-1 218 685 689 4
74 42 11 6 3 1 2 54-2	139 255 256 4241	n ≥ 4 64 28 11 4 2 2 5 2 1 60-1 119 252 253 4
5 .2 :8 24 30 36 42 48 54 50 66 72 78 84 90 96+ MAX	TI T TO TH	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TI T
HOURS INTERVAL BETWEEN EVENTS 9	50.3N 171.3W	HOURS INTERVAL BETWEEN EVENTS 10 51.8N 16
1 1 6 SEA-6	7 2215 4264 4265	W≥64 6 SEA-6 6 2208 4265 4
1 1 1 1 1 1 SEA-5	17 2571 4554 4582	"≥48 1 1 11 SEA-4 12 2304 4606 4
2 1 1 3 1 2 1 24 SEA-4	35 3430 5120 5202	N = 41   1   1   1   2   1   1   18   SEA - 5   26   3155   4968   5
7 2 5 4 7 3 4 1 4 1 4 1 3 47 SEA-1	93 4481 5504 5734	D≥34 10 5 3 4 1 3 3 3 2 3 40 SEA-1 77 3794 5074 5
16 5 13 11 7 6 4 1 2 7 7 2 3 1 64 SEA-1	149 4313 4510 5039	S≥28 15 7 7 9 7 5 8 5 5 3 5 3 1 2 2 60 2112-1 144 4459 4803 5
\_ <del>\_\_\_\_\_\_\_\_\_\_\_\</del>	241 3153 3310 4401	P ≥ 22 34 29 25 13 10 12 7 6 6 8 3 6 9 4 66 816-1 238 3296 3537 4
<del></del>	314 2444 2468 4323	E ≥ 17 49 39 35 27 19 15 8 8 7 9 6 6 5 3 1 54 582-1 291 2476 2563 4
201-20-15 10 10 10 10 10 10 10 10 10 10 10 10 10	294 1305 1314 4267	D ≥ 11 74 42 42 26 21 17 10 12 11 5 4 6 1 3 2 13 162-1 289 1386 1388
80 58 38 25 19 15 9 4 7 10 6 2 5 4 2 10 102-1		
80 58 38 25 19 15 9 4 7 10 6 2 5 4 2 10 192-1		k ≥ 7   86   57   37   16   10   11   5   2   4   1   2   1
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96 44 29 15 8 7 8 3 3 1 2 1 1 1 90-1 67 31 11 4 2 1 1 1 72-1	119 224 226 4247	
96   44   29   15   8   7   8   3   3   1   2   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   72-1   61   21   16   24   30   36   42   48   54   60   66   72   78   64   90   96   MAX   HOURS INTERVAL BETWEEN EVENTS	119 224 226 4247 TI T T TH	6 12 18 24 30 36 42 48 54 60 66 72 78 H4 90 96+ MAX TI T TO HOURS INTERVAL BETWEEN EVENTS
96 [44 29   15   8 7   8   3   3   1   2   1   1   1   90-1   67 31 11   4   2   1   1   1   1   1   72-1   6 12 16 14 30 36 42 48 54 60 66 72 78 nd 90 96+ MAX HOURS INTERVAL BETWEEN EVENTS	119 224 226 4247 TI T T TH 51.3N 158.8W	6 12 18 24 30 36 42 48 54 50 66 72 78 74 90 96+ MAX TI T TO HOURS INTERVAL BETWEEN EVENTS 12 54.4N 15
96   44   29   15   8   7   8   3   3   1   2   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   72-1   67   31   12   4   30   36   42   48   54   80   66   72   78   74   90   96 + MAX   HOURS INTERVAL BETWEEN EVENTS  1   6   SEA-6	119 224 226 4247 TI T T TH 51.3N 158.8W 6 2208 4265 4265	6 12 18 24 10 36 42 48 54 60 66 72 78 74 90 96+ MAX TI T T+ HOURS INTERVAL BETWEEN EVENTS 12 54.4N 15  W ≥ 64
96   44   29   15   8   7   8   3   3   1   2   1   1   1   90-1     67   31   11   4   2   1   1   1   1   1   72-1     8   12   18   24   30   36   24   48   54   50   66   72   78   74   90   96 + MAX     HOURS INTERVAL BETWEEN EVENTS   11   6   SEA-6     13   SEA-8	119 224 226 4247 TI T T TH 51.3N 158.8W 6 2208 4265 4265 13 3399 4631 4648	6 12 18 24 10 36 42 48 54 60 66 72 78 46 90 96 MAX TI T T HOURS INTERVAL BETWEEN EVENTS  12 54,4N 15  W ≥ 64
96 44 29 15 8 7 8 3 3 1 2 1 1 1 1 90-1 67 31 11 4 2 1 1 1 1 72-1  1 12 16 24 30 36 24 48 54 80 66 72 78 44 90 96 MAX HOURS INTERVAL BETWEEN EVENTS 11  6 SEA-6 13 SEA-8 4 1 1 2 1 3 1 3 1 30 SEA-7	119 224 226 4247 T1 T T T T T T T T T T T T T T T T T T	6 12 16 24 10 36 42 48 54 60 66 72 78 46 90 96 MAX TI T T T T T T T T T T T T T T T T T T
96   44   29   15   8   7   8   3   3   1   2   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   90-1   67   31   12   4   30   36   42   48   54   80   66   72   78   64   90   96   MAX HOURS INTERVAL BETWEEN EVENTS  1	119 224 226 4247 T1 T T T T T T T T T T T T T T T T T T	6 12 16 24 10 36 42 48 54 60 66 72 78 46 90 96 MAX TI T T T T T T T T T T T T T T T T T T
96   44   29   15   8   7   8   3   3   1   2   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   1   1   67   31   12   30   36   32   48   54   80   66   72   78   74   90   96   MAX HOURS INTERVAL BETWEEN EVENTS  1	119 224 226 4247 TI T T TH 51.3N 158.8W 6 2208 4265 4265 13 3399 4631 4648 42 4084 5217 5301 88 4794 5543 5782 179 4510 4757 5344	6 12 16 24 10 36 42 48 54 60 66 72 78 74 60 90 90 MAX TI TE TO THOURS INTERVAL BETWEEN EVENTS 12 54.4N 15  W ≥ 64
96   44   29   15   8   7   8   3   3   1   2   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   72-1   67   31   11   4   2   1   1   1   1   1   72-1   67   31   12   30   36   22   48   54   80   66   72   78   74   90   96 + MAX    HOURS INTERVAL BETWEEN EVENTS  1	119 224 226 4247 T1 T T T T T T T T T T T T T T T T T T	6 12 16 24 10 36 42 48 54 60 66 72 78 46 90 90 MAX TI TENDOURS INTERVAL BETWEEN EVENTS
96 144 29 15 8 7 8 3 3 1 2 1 1 1 1 90-1 67 31 11 4 2 1 1 6 12 16 14 10 36 12 48 54 86 66 72 78 44 90 96 4 MAX HOURS INTERVAL BETWEEN EVENTS 11 6 8 SEA-6 4 3 7 1 2 3 5 2 2 4 1 1 3 6 SEA-7 4 3 7 1 2 3 5 2 2 4 1 1 4 5 45 58-5 17 16 17 16 17 14 9 6 6 6 4 7 6 4 2 5 4 3 65 1806-1 44 32 26 11 12 15 11 9 5 15 8 5 6 6 6 6 6 1722-1 50 50 30 28 22 22 14 16 15 11 3 1 6 7 2 34 570-1	119 224 226 4247 T1 T T T T T T T T T T T T T T T T T T	6 12 16 24 10 36 42 48 54 60 66 72 78 46 90 96 MAX TI TENDURS INTERVAL BETWEEN EVENTS $ \begin{array}{c c c c c c c c c c c c c c c c c c c $
96   44   29   15   8   7   8   3   3   1   2   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   90-1   67   31   12   4   30   36 + 2   48   54   80   66   72   78   rd   90   96 + MAX   68   40   10   10   10   10   10   10   10	119 224 226 4247 T1 T T T T T T T T T T T T T T T T T T	6 12 16 24 10 36 42 48 54 60 66 72 78 46 90 96 MAX TI TO TO TO THOURS INTERVAL BETWEEN EVENTS $ \begin{array}{c c c c c c c c c c c c c c c c c c c $
96   44   29   15   8   7   8   3   3   1   2   1   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   1   1   67   31   11   4   2   1   1   1   1   1   1   1   68   12   18   14   30   36   42   48   54   80   66   72   78   74   90   96   MAX  HOURS INTERVAL BETWEEN EVENTS  1	119 224 226 4247 T1 T T T T T T T T T T T T T T T T T T	6 12 16 24 10 36 42 48 54 60 66 72 78 46 90 99 MAX TI TE HOURS INTERVAL BETWEEN EVENTS $ \begin{array}{c c c c c c c c c c c c c c c c c c c $
96   44   29   15   8   7   8   3   3   1   2   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   90-1   67   31   11   4   2   1   1   1   1   1   1   90-1   67   31   12   4   30   36 + 2   48   54   80   66   72   78   rd   90   96 + MAX   68   40   10   10   10   10   10   10   10	119 224 226 4247 T1 T T T T T T T T T T T T T T T T T T	6 12 16 24 10 36 42 48 54 60 66 72 78 46 90 96 MAX TI TO TO TO THOURS INTERVAL BETWEEN EVENTS $ \begin{array}{c c c c c c c c c c c c c c c c c c c $

-498																			
W ≥ 0-	4	-	_	_	7	-	Ţ-	T	1		$\top$	7	ТТ			Γ	4.1N	166.7W	2 63.6N 178.1V ₩≩64 41CO
1 ≥48	ຄິ	++	+		+	+	+	+ 1	-+	+-	+	+	1-1		<del>                                     </del>	t		4100	¥=48 41co
N ≥4	ī	11		7	1	1	†	$\Box$	T	$\top$	+	<del>+</del>	11	12-1	1	2	2	4100	N ≥ 41 3 1 1 3 30-1 5 1C 10 41CC
ĭ≩3₄	4	1	2	1	7	+	1		_†	$\top$	+	1	$\sqcap$	30 - 1	4	16	16	4100	≥ 34 2 5 1 1 1 72-1 1C 32 32 41C0
\$ ≥ 28	8	6 4 2		1	1	1 3					T	T	П	48 - 3	18	62	62	4101	S ≥ 28 12 5 7 5 3 1 1 1 1 96-1 36 11B 23 4:00
E ≥ 23	2	5 15 7	5	2	1 4	1 3	1		2	1 1	I	I		78 - i	58	220	220	4104	$\xi \stackrel{?}{=} 22 \begin{array}{ c c c c c c c c c c c c c c c c c c c$
[ ≥ 17	7 [	14 13 18	14	13	9 6	4	4	4	2	3 2	1	1	9	180-1	137	744	748	4151	L ≥ 17 21 33   16   12   12   8   4   7   3   2   9   1   4   5   4   8   138 - 2   149   874   894   4 5
U ≥ 1.		7 27 17									12		+	234-1	240	1826	1893	4181	D ≥ 11 43 33 17 17 17 20 17 4 9 8 11 7 5 3 4 37 324-2 252 2024 2109 4192
k ≧ 7		9 14 16													2 4	68	3010	4223	$k \ge 7 4 : 17 24 19 14 11 9 8 7 12 3 8 9 4 7 67 522 - 1 260 2970 3:65 4294$
n ≥ 4	٠.		16			5					7			558-1	210	3286	3685	4308	$n \ge 4 29 15 11 13 9 6 10 5 4 6 5 7 2 2 5 79 918 - 1 208 3550 3836 4396$
		6 12 18						60 1 O F				90	96+	MAX	TC	т	T=	TH	6 12 18 24 30 16 42 48 54 60 66 72 78 44 90 96+ WAX TE T THE THE HOURS DURATION OF EVENTS
	_		,				-		3		<del></del>	-				r <u>-</u> 5	9.4N	172.0W	4 \$8.0N 167.0
w ≥ 64	-	44			<u>.</u>	4_	1	$\vdash$	+	+	+-	↓_	₩					4100	₩≩64 4100
. ≥48 N	٠,	2 -	4-4	$\dashv$	+	+	+-	₩	+	-	+-	+	+-+	12-2	2	4	4	4100	1≥48 2 1 12-1 3 4 4 41cc
D ≥ 4	٠,	; 2	+	-+	4	+-	+-	<del> </del> →	+	+	+	+-	+	36 - 1 42 - 1	11	34	34	4100	N ≥ 41 1 1 1 1 36-1 3 9 9 41cc
S ≥ 26			3	5	2 :	-+-	2	+	-	-+-	+-	+-		54-2	40	144	144	4102	≥34 5 9 1 1 3 1 42-1 20 56 56 4:c: S≥28 19 11 19 9 3 2 1 1 1 1 60-1 66 90 190 4:c2
p≃40 p≥20		9 8 6	$\overline{}$		6 9	-	+	2	<del>,</del> +	+2	1	+	+-+	90 - 1	101	435	438	+106	P
E ≥ 17	- +	3 20 18	+	14	_		12	+-+	<del>-</del> +	3 3			<del></del>	138 - 1	172	970	986	4135	E ≥ 22   24   16   14   16   13   16   5   3   3   3   1   1   1   102 - 1   117   492   493   4   107   102 - 1   17   492   493   4   107   1
ر ≤ ۵		1 30 24					-	+		9 8	<del>-</del> -		+ +	270-1	265	2212	2249	418)	D ≥ 11 39 26 19 23 22 19 17 22 17 6 10 9 10 6 1 41 264-1 287 2321 2372 415
, ≩ :	, 5	4 9 ,12	-	$\rightarrow$			+		<del>-</del>		8	-	+-+	360-1	227	3054	3317	4262	$k \ge 7$ 20 8 9 12 8 9 11 10 11 9 7 8 3 11 5 72 954-1 213 3295 3477 4327
n ≥ 4	1	4 4 10	4	3	1 2	2 4	+-	4		3 1	9	2	73	792-1	140	3608	4249	4624	n ≥ 4 20 9 8 5 4 5 4 2 4 4 3 2 5 3 2 65 1626-1 145 3838 4256 4585
		6 -2 16						60				90	96+	MAX	7.5	T	Th	тн	6 .2 18 24 30 36 42 46 54 60 66 72 78 d4 9096+ MAX TE T Te Tu
			нС	UR:	יסי	RAT	101	105	5 EVE	NTS						5	6.8N	174.8 E	HOURS DURATION OF EVENTS 52.0N 172 9
w ≩ 64	٦,	7	T	T	$\top$	T	T			_	T	T	$\Box$					4100	W≥64 4100
	_	Li		I	1	1	L				I	1-	$\Box$					4100	≥48 1 1 1 4100
N 2 341	ũ	,								$\Box$	I		П	6-5	5	5	5	4100	N ≥41 4 4 1 1 24-1 9 1€ 1€ 4100
_≥ 34	-	7 3 2	2	3		L	i				L	L		54-1	18	51	51	4108	≥34 10 4 8 3 2 1 1 48-1 26 72 72 4102
בי ק	,	7 11 8			5   2		-		4	2	1	1_	+-+	78 - 2	58	197	197	4118	S ≥ 28 26 19 12 6 6 4 1 1 2 1 84-1 78 225 225 4106
: ₹22	-		12	-		<del></del>	+		<u>4</u> j		Ļ	丄		114-2	112	534	538	4130	E ≥ 22   41   20   24   18   13   9   8   5   5   2   3   1   1   1   1   126 - 1   152   599   607   41   42
.≥17		6 27 23								5   5			+-+	132-1		1191	1214	4138	E ≥ 17 48 46 34 21 21 20 18 7 14 6 2 14 3 13 13 16 1 144 - 1 256 1232 12.4 4 2.0
` <u>≥</u> : :	_	9 27 22	<u> </u>		_		-				-			378 - 1	274	2543	2598	4224	0 ≥ 11 58 36 26 22 13 13 17 16 13 10 8 16 8 4 5 50 222-1 315 2481 2561 4154
· = /		116 7				2								492-1	218 i30	3143	3557 4066	4315 4345	k ≥ 7 23 5 16 11 10 13 14 11 12 9 B 17 7 8 5 72 582 - 23 3 3 0 3 605 432 ↑≥ 4 12 5 1 3 4 3 3 6 6 4 4 2 1 1 76 996 1 13 3490 422 44-
= "		5 2 18						60					741	MAX	75	23//	T.	Ti:	0 ≥ 4 12 5
			но	ÚRS	DU	RAT	IÓN	0F	EVE	NTS		,,,	,						HOURS DURATION OF EVENTS
v ≥ 6.4	-	+		<del>-</del>		_	7	7	<del>-</del> r	7	7	1	7			·	4.7N	175 9W	8 54.9N 167.2 ₩≥64 4.00
γ ≎ ∪ − - ≥48			++		-	+-	+	+	+	-+-	+	+	++	6-4	4	4	4	4100	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
1 241	_	4 2	Ţ	-	+	+-	1	1	+	+-	+	<del>-</del>	++	18 - 2	:3	21	21	4100	N ≥ 41 3 2 2 1 1 18 - 2 7 13 3 4 100
ິ <u>≩</u> 34	-	9 8	4 :	4	1	1:	<del></del>	-	+	Ť	$^{+}$	+		48 - 1	55	120	121	4105	2 34 13 6 6 1 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1
\$ ≥ 28	. 52	3 21 16	а	5	5   5	1	2	1	2	1	Ti	1		84-1	90	307	313	4111	S ≥ 28 (25 14 13 4 4 4 4 1 2 1 1 60-1 68 1et. 18: 4·c.)
₹22	[3	9 38 23	24	·7]:	C <sub>1</sub> 6	3	6	4	3 .	3 2	5	1	3	i20-1	184	779	787	4141	E ≥ 22 41 22 25 15 22 9 9 5 2 4 1 1 1 2 1 9 160 62e 633 4 1/5
≥ -	5	3 39 23	24	21/1	0 [19	9 1 3	ic	3	7] :	6	10	3	12 2	216-1	254	1423	1440	4152	E ≥ 17 49 30 26 30 24 21 12 13 5 13 7 4 3 1 3 10 21 25 1356 13 1 4 6€
′ ≩ 1 '	-	5 23 25		9 2	_	$\rightarrow$ $-$	18		_+	2 12	5	_	44 4	486 – 1	303	2754	2830	4250	D ≥ 11 [29 [16 [17 [15 [23 [21 [16 [18 [8 ]   2 [8 ]   3 [ 1 [ 13 [ 5 ] 43 [ 4 ] 4 - 1 ] 268 ] 263 ] 2 1 16 [ 4223
. ≥ ¬	1			7   8		0110				7 4	+	+	+ +	518-1	209	3357	3664	429	$k \ge 7 \ 18 \ 12 \ 9 \ 6 \ 8 \ 14 \ 8 \ 2 \ 9 \ 10 \ 7 \ 9 \ 5 \ 4 \ 14 \ 74 \ 636 - 1 \ 209 \ 3305 \ 36^{\circ} \ 434^{\circ}$
1 ≥ 4	Ľ		2		3 2					3 3			69 1		121	3590	4172	4405	$0 \ge 4 \cdot 10 \cdot 3 \cdot 6 \cdot 3 \cdot 7 \cdot 3 \cdot 1 \cdot 1 \cdot 1 \cdot 3 \cdot 2 \cdot 2 \cdot 77 \cdot 1746 - 1 \cdot 119 \cdot 3808 \cdot 4377 \cdot 4636$
		2 16						00				90	96+	M. A. X	TC	*	7.	ТН	6 12 18 24 30 36 42 48 54 60 66 72 78 H4 90 VET MAX TO TO TO THE THE
	_				_				9							5	0.3N	171.3W	10 51.8N 167 31
y≥64	-		-	-	+	<del>-</del>	· 	4			<del>-</del>	⊢	<u> </u>					4100	W≥64
: ≧4ë	-			-	+-	+-	-	-	+	<del></del>	+-	÷	+ +	18 - 1 24 - 1	4	6	6	4100	N ≥ 48 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
) ≥41 ≥34	- <del>(</del>		2	2   2	,+-	+-	╙		+		+-	+-		36-2	39	18 87	19 91	4100	M ≤ 41 1 2 1 1 1 2 4 -1 5 2 13 4 13 2 3 4 13 8 6 6 12 1 3 6 -2 29 1 59 62 4 11
2 3 2 8	_		12		4	2	+	1	+	+-	+-	<del>!</del>		72-1	97	301	309	4111	
€ 22			18		1		3	5 1		3 2	+-	2		96-3	174	798	817	4126	≥ ≥ 28 31 12 18 9 8 3 3 1 1 1
		9 32 30		-			<u> </u>		Ö S	-	1	5	+	162-1	274	1582	1606	4164	£ ≥ 17 43 39 28 27 29 18 9 13 6 12 14 5 7 2 1 15 162-1 268 1533 556 4 42
≥ 11	-	9 18 16		-+-				16 1		<del></del>	+			138 - 1	275	2768	2854	4190	0 ± 11   35   14   23   5   14   13   14   11   17   13   4   12   12   9   8   56   366 - 1   270   2775   2855   42 5
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	1	4 2										2	69 1	680 - 1	115	3769	455 i	4796	n ≥ 4 9 6 5 3 4 5 2 3 4 2 3 2 3 4 68 i152-1 123 3536 4300 4548
	-	- 2 1€	24	3 C 3	6 4	2 48	54	60 €	6 7	2 76	84			MAX	TE	T	Ť.	TH	6 .2 18 24 30 36 42 48 54 60 68 72 78 64 90 98 MAX 11 T To Th
			но	כאט	טע	KAI	IUN	OF	1	NI3						5	1.3N	158.8W	HOURS DURATION OF EVENTS
2€4					T	T			Ţ		Ţ							4100	w≥64
≥48	-			- !					I	T				6-2	2	2	2	4100	1 ≥ 48 2 1 18-1 3 5 5 4102
441	-		2		Ī	I		I	T		1	_		24-2	11	20	21	4101	N ≥41 7 3 3 1 1 30-1 15 31 31 41C2
≥ 34			5			$\perp$	L	1	4	4	L			36 – 2	38	87	90	4102	≥ 34 10 5 / 5 2 1 1 1 1 48-1 32 92 92 4104
, ≥ 28		25 17						$\perp$	$\perp$	+	+-	$\perp$	+	54-2	101	280	295	4105	S ≥ 28 29 12 12 6 3 9 1 2 1 60-1 75 215 226 4107
±22		24 28									+-	لبإ		102-2	185	779	821	4111	E ≥ 22 35 37 29 15 13 9 5 6 6 4 1 1 1 1 1 102-1 164 622 646 4:15
2 17	4	1 39 32										-		204 – 1	264	1571	1641	4138	E ≥ 17   56   46   35   28   17   14   14   15   11   7   4   5   3   2   4   9   162 - 1   270     1331     1386   4   25
2 11 ≤	3	20 19					_			2 6		-		524 – 1	252	2920	3051	4296	D ≥ 11 35 20 25 17 18 16 11 15 11 10 9 7 9 6 7 59 648-1 275 2730 2862 4227
ر <u>≥</u> 7 1 <u>≥</u> 4	-	13 8							$\overline{}$		_	+		768 - 1	192	3431	3855	4407	$k \ge 7$ 24 10 11 13 10 13 8 4 6 9 4 3 2 5 7 78 798 -1 207 3518 3636 4424
≤ 4	E	2 2	4				1 54	3 60 6		2 78				032-1	90 TE	3579 T	4353	4526 7H	0 3 4 12 2 5 3 2 5 1 6 5 3 3 1 1 65 1152-1 114 3613 4193 4424
			но	URS	טס	RAT	IÓN	OF	EVÉ	NTS	., -	. •				•			6 -2 18 24 30 36 42 48 54 60 66 72 78 n4 90 96+ MAX TE T TN TH HOURS DURATION OF EVENTS
	_																		
ımı	П	<del>U</del> I																	23 Persistence of wind speed-duration

### 11-499

	11-439
1 64.1N 166.7W	2 63 6N 178 1W
W≥64 6 SEA-6 6 2208 4224 4224	W ≥ 64 6 SEA-6 6 2208 4224 4224
6 SEA-6 6 2208 4224 4224	\$48
N = 41 7 SEA-5 7 2402 4418 4420 9 SEA-2 9 2300 4402 4418	N 441 1 8 SEA-3 9 2127 4267 4277 ≥34 2 1 1 1 10 SEA-1 14 2306 4227 4259
	S ≥ 28 1 1 2 2 1 1 1 34 1842 - 1 42 28 4 4 124 4247
P	p = 22 7 3 4 1 1 3 3 1 2 1 1 2 148 1416 - 1 77 288 1 3805 1 4174 1
$\frac{2}{6} \ge 22 \begin{vmatrix} 4 & 6 & 3 & 2 & 2 & 1 & 1 & 1 & 1 & 1 & 3 & 36 & 1710 - 1 & 60 & 2940 & 3966 & 4182 \\ 1 \ge 17 & 16 & 10 & 5 & 3 & 1 & 7 & 4 & 6 & 6 & 5 & 7 & 4 & 3 & 3 & 55 & 690 - 1 & 135 & 2904 & 3432 & 4129 \\ 1 \ge 17 & 16 & 10 & 5 & 3 & 1 & 7 & 4 & 6 & 6 & 5 & 7 & 4 & 3 & 3 & 55 & 690 - 1 & 135 & 2904 & 3432 & 4129 \\ 1 \ge 17 & 16 & 10 & 5 & 3 & 1 & 7 & 4 & 6 & 6 & 5 & 7 & 4 & 3 & 3 & 55 & 690 - 1 & 135 & 2904 & 3432 & 4129 \\ 1 \ge 17 & 16 & 10 & 5 & 3 & 1 & 7 & 4 & 6 & 6 & 5 & 7 & 4 & 3 & 3 & 55 & 690 - 1 & 135 & 2904 & 3432 & 4129 \\ 1 \ge 17 & 16 & 10 & 5 & 3 & 1 & 7 & 4 & 6 & 6 & 5 & 7 & 4 & 3 & 3 & 55 & 690 - 1 & 135 & 2904 & 3432 & 4129 \\ 1 \ge 17 & 16 & 10 & 5 & 3 & 1 & 7 & 4 & 6 & 6 & 5 & 7 & 4 & 3 & 3 & 55 & 690 - 1 & 135 & 2904 & 3432 & 4129 \\ 1 \ge 17 & 17 & 17 & 17 & 17 & 17 & 17 & $	E ≥ 17 14 13 10 5 5 7 6 5 3 6 2 3 4 3 4 58 188 - 1 148 3025 1 3305 414€
D≥11 36 22 20 20 24 16 5 7 7 7 7 3 9 6 5 13 35 474-1 236 2215 2292 4104	D ≥ 11 44 25 23 17 26 16 13 9 6 17 12 6 5 4 6 32 396 - 1 251 2004 2087 4:04
k ≥ 7 56 41 37 26 23 17 8 5 6 6 6 6 3 4 10 198-1 248 1208 1216 4103	k ≥ 7 58 46 39 31 13 17 15 15 2 7 3 3 4 3 4 144-1 260 1124 1131 4102
2 (6) 13 25 11 6 2 5 6 2 2 2 2 1 1 84-1 2** 6*9 624 4101	n ≥ 4 73 56 23 12 11 11 7 3
6 12 16 24 30 16 47 48 54 60 56 72 78 44 90 98+ MAX TI T TO TH	6 12 16 24 30 36 42 46 54 60 66 12 78 H4 9096+ MAR TI T TO TH HOURS INTERVAL BETWEEN EVENTS
HOURS INTERVAL BETWEEN EVENTS 59.4N 172.0W	4 58 ON 167.0W
w≥64 6 SEA-6 6 2208 4224 4224	w≥64 6 SEA-6 6 2208 4224 4224
≥48 7 SEA-5 7 2226 4264 4268	1 ≥ 48 1 7 SEA - 5 8 2226 4264 4268
N ≥41 9 SEA-3 9 2277 4315 4326	D = 41 B   SEA - 4 B   2165   4202   42
≥ 34   15   SEA - 2   15   2616   4274   4307	≥34 1 1 2 1 1 16 2100 - 1 21 2 500 4235 4290 S≥28 5 1 1 4 1 1 1 2 1 1 1 3 1 46 500 - 1 66 3 30 4086 4274
S ≥ 28 ! 2	S≥28 5 1 4 1 1 2 1 1 3 1 1 46 5500-1 66 3:30 40E6 4274 F ± 22 114 4 8 6 3 2 3 4 1 2 2 1 2 2 63 (602-1 117 3:69 3:679 4:65
E \(\frac{2}{1}\) 2 \(\frac{4}{1}\) 4 \(\frac{1}{4}\) 4 \(\frac{4}{4}\) 4 \(\frac{4}{4}\) 4 \(\frac{3}{4}\) 3 \(\frac{3}{4}\) 5 \(\frac{1}{1}186\) -1 \(\frac{1}{1}03\) 3159 \(\frac{3}{1}70\) 4202 \(\frac{2}{1}\) \(\frac{2}{1}7\) 19 \(\frac{1}5\) 10 \(\frac{1}3\) 10 \(\frac{8}{5}\) 5 \(\frac{4}{8}\) 4 \(\frac{4}{2}\) 3 \(\frac{3}{4}\) 6 \(\frac{1}{9}78\) -1 \(\frac{1}{1}3\) 2848 \(\frac{3}{2}03\) 4154	E ≥ 17 16 11 15 12 14 6 13 8 8 9 1
D≥ 11 34 37 30 25 17 19 12 11 12 8 5 7 6 2 6 29 252-1 260 1858 1934 4102	D ≥ 11 58 43 39 31 19 17 14 11 10 6 5 5 3 4 4 21 264-1 290 1709 1783 4 4 24
$k \ge 7.62414423128844532155126180-12279219454100$	k ≥ 7 56 52 29 16 12 8 14 7 2 3 1 1 2 1 7 186 - 1 21 1 836 850 412
$0 \ge 4   65   32   20   9   6   1   2   2   1   4   126 - 1   142   374   375   4100   375   41$	$n \ge 4$ 72 26 18 11 8 3 3 2 1 66-1 144 328 329 415:
6 .2 18 24 30 76 42 48 54 60 66 /2 78 44 90 96+ MAX TI T T+ TH	6 12 18 24 30 76 42 48 54 60 66 72 78 H4 90 96 WAY TI T TO TH
HOURS INTERVAL BETWEEN EVENTS 5 56.8N 174.8E	HOURS INTERVAL BETWEEN EVENTS 6 52.0N 172.9 E
W≥64 6 SEA-6 6 2208 4224 4224	w≥64 6 SEA-6 6 2208 4224 4224
≥46 6 SEA-6 6 2208 4224 4224	1 ≥ 48 7 SEA-6 7 239C 4392 4393
10 SEA-5 11 2441 4350 4355	D 241 14 2655 4372 4365
≥34 2 1 1 1 1 1 19 SEA-1 24 2746 4129 4172	251 2 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
S ≥ 2e   5   2   1   1   4   1   1   44   1602 - 2   6C   3295   4066   4245   6   6   22   6   6   2   5   3   3   5   7   2   2   8   3   1   2   2   56   1056 - 1   113   3265   3663   4171	Plantata ta ta ta ta ta ta ta ta ta ta ta ta
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
D ≥ 11 52 32 40 22 25 18 17 6 9 8 6 8 4 4 4 4 17 186 - 1 272 1587 1637 4111	D ≥ 11 72   50   37   27   25   29   16   9   9   6   6   9   3   2   4   15   174 - 1   3   6     1552 + 1554   + 111
k ≥ 7 62 45 3 ; 25 20 9 6 ; 5 4 3 ; 1 1 1 1 1 2 138 - 1 217 752 764 4106	R ≥ 7 93 51 31 18 14 13 6 5 4 11 1 2 3C-2 229 671 68 4105
n ≥ 4 64 28 20 9 5 3 1 1 72-1 130 277 279 4100	n ≥ 4 63 39 13 9 3 1 1 42-1 129 244 250 4100
( .2 18 24 30 36 42 48 54 50 66 72 78 34 90 96+ MAX TI T T+ TH HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 16 42 48 54 60 66 72 78 74 90 96+ VAX 7 7 7+ 7+ HOURS INTERVAL BETWEEN EVENTS
7 54.7N 175.9W	8 54 9N 167 2W
w ≥ 64 6 SEA-6 6 2208 4224 4224	w≥64 6 SEA-6 6 2206 4224 4224 +≥48 9 3EA-5 9 2292 4162 4166
3 48 9 SEA-4 9 2386 4369 4373 3 13 SEA-2 18 2462 4235 4256	N >41
234 10 3	D ≥ 34   2   1   1   1   1   3   1   2   1   21   5EA = 1   32   2665   4.9 1   4261
$3 \ge 22 - 10 = 6 - 3 - 5 = 2 + 2 - 5 = 1 + 1 + 1 + 2 + 2 + 2 + 2 + 2 + 1 + 1 +$	S ≥ 28 5 1 3 5 2 3 2 2 3 1 43 15 36 - 1 3202 4056 4242
E = 22 22 1017 9 8 6 6 7 5 4 1 7 4 6 4 67 774-1 183 3020 3401 4147	E = 22 16 11 7 8 8 7 4 5 7 2 3 2 6 5 4 66 1374-1 16 3 98 3544 415
£ ≥ 1 , 25 24 23 27 16 12 12 7 11: 13 8 7 3 11 4 50 552-1 252 2566 2734 4122	E ≥ 17 40 27 25 14 11 8 10 12 8 11 8 3 2 6 7 59 642- 25 2689 282 4 36
$^{2} \ge 11 64 50 57 30 25 1111 11 7 2 7 5 3 3 3 3 13 168 - 1 206 1399 1439 4119$	D ≥ 11 43 44 35 32 22 12 16 21 9 9 3 4 5 3 1 13 210 -1 212 1474 1614 4158
x ≥ 7 74 42 36 21 13 6 1 5 3 4 1 2 1 96-1 209 620 633 4106	$k \ge 7 67 48 28 19 14 8 10 7 2 3 1 2 1 2 1 108 - 1 2 4 724 736 4 0 2$
$0 \ge 4 \frac{63}{32} \frac{32}{14} \frac{14}{3} \frac{3}{2} \frac{2}{1} \frac{1}{2} \frac{1}{1} \frac{1}{1} \frac{60-1}{60-1} \frac{118}{118} \frac{224}{223} \frac{233}{4100}$	0 ≥ 4 58 32 10 6 6 3 3 1 48-1 19 253 256 4101
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL DETA EEN EVENTS
9 50.3N 171.3W w ≥ 64 6 SEA-6 6 2208 4224 4224	10 51.8N 167 3W W≥64 6 SEA-6 6 2206 4224 4224
w≥64 6 SEA-6 6 2208 4224 4224 ≥48 10 SEA-5 10 2299 4160 4166	(≥48) 10 SEA-5:10 2302 4'62 4'66
N 241 1 13 SFA-2 16 2352 4260 4279	N ≥41 1 10.SFA-5 11 2295 4153 4166
≥ 34 5   2   1   1   2   1   2   28   1734 − 1   43   2986   4199   4289	≥34 2 1 1 2 1 1 1 23 20 70 - 1 32 2954 4235 4297
5 ≥ 28 8 7 4 3 2 3 3 2 6 4 4 2 4 2 45 1524-1 99 3178 3875 4173	S ≥ 28 6 2 4 3 1 2 3 3 2 3 3 2 3 5 1468 1 9C 3225 3983 4228
E = 22   22   B   B   5   6   12   6   2   4   4   4   6   7   4   8   68   1356 - 1   174   3   3107   3349   4140	$\varepsilon \le 22 \ 26 \ 18 \ 14 \ 12 \ 10 \ 6 \ 6 \ 5 \ 7 \ 3 \ 5 \ 4 \ 7 \ 5 \ 4 \ 58 \ 1344 - 1 \ 190 \ 3 \ 13.3 \ 34.2 \ 4.4^{\circ}$
E ≥ 17 39 25 25 26 18 12 11 12 9 9 8 10 6 5 4 52 336-1 271 2447 2586 4128	E ≥ 17 42 33 21 22 18 11 6 9 12 8 9 5 5 4 60 606-1 265 2488 2€ 1 4 25
≥ 11 47 56 42 26 23 15 14 10 6 4 16 5 2 3 5 9 174-1 273 13 12 1343 4107	\$11 B9 B0 B B B B B B B B B B B B B B B B B
k ≥ 7 72 42 28 i9 i0 7 7 4 1 5 i 1 1 1 126-1 199 606 616 4102	$k \ge 7   72   45   33   15   10   8   5   3   3   4   3   1   108 - 1   202   596   6 \cdot 6 \cdot 4 \cdot 6 \cdot 7   \geq 4   65   33   14   6   1   4   1   1   1   60 - 1   125   245   246   4 \cdot 6 \cdot 7   25   246   4 \cdot 6 \cdot 7   25   246   4 \cdot 6 \cdot 7   25   246   4 \cdot 6 \cdot 7   25   246   4 \cdot 6 \cdot 7   25   246   4 \cdot 6 \cdot 7   25   246   4 \cdot 6 \cdot 7   25   245   246   4 \cdot 6 \cdot 7   25   25   25   25   25   25   25   $
7 ≥ 4 60 31 14 5 3 2 1 2 60 66 12 78 m4 90 96+ MAX T1 T T+ TH	6 12 18 24 30 16 42 48 54 60 66 12 78 #4 90 46 MAX 7' T
HOURS INTERVAL BETWEEN EVENTS 11 51.3N 158.8W	HOURS INTERVAL BETWEEN EVENTS 12 54.4N 158 1W
W≥64 6 SEA-6 6 2208 4224 4224	w≥64 6 SEA-6 6 2208 4224 4224
≥48 6 SEA-5 6 2191 4266 4268	7 SEA-5 2385 4255 4258
N = 41 i 1 1 11 SEA-2 14 2472 4217 4237	N = 41 2 14, SEA - 3 '6 2728 4230 4259
≥ 34 5 i 1	≥34 1 1 1 2 1 1 262100-1 33 3001 4190 4278
S ≥ 28 13 2 6 6 2 2 1 2 5 1 4 3 2 2 3 51 1506-1 105 3380 3939 4229	S≥28 2 4 3 3 i 1 1 2 3 2 2 1 3 1 50 i506-1 79 3210 3969 4138
E = 22   23   18   13   7   10   6   8   7   5   6   6   5   3   2   7   62   1098 - 1   188   3   3   29   3305   4115	E ≥ 22 24 9 6 4 5 6 5 7 7 6 5 5 4 4 3 66 720-1 166 3255 3506 413
C \(\frac{1}{2}\) 17 \(\frac{53}{20}\) 20 \(\frac{25}{24}\) 9 \(\frac{12}{16}\) 10 \(\frac{11}{11}\) 1 \(\frac{9}{1}\) 7 \(\frac{9}{2}\) 2 \(\frac{5}{45}\) 552-1 \(\frac{268}{268}\) \(\frac{2378}{2378}\) \(\frac{2505}{2408}\) 4 \(\frac{102}{4102}\) \(\frac{2}{2}\) 1 \(\frac{3}{2}\) 2 \(\frac{9}{144-1}\) 249 \(\frac{1192}{1192}\) 1247 \(\frac{4102}{4102}\)	$E \ge 17 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
	≥ 11 61 52 48 19 22 16 8 13 9 2 3 5 2 3 4 12 227-1 279 340 13 1 4 106 k ≥ 7 76 56 25 16 10 10 3 3 2 1 1 1 3 132-1 206 581 592 4104
k ≥ 7     78     37     28     20     6     7     4     1     3     1     2     120-1     191     544     553     4101       n ≥ : 5i     23     8     7     1     1     1     72-1     91     169     173     4100	$n \ge 4$ [59] [29] 11 [3   4   2   1   1   1   1   90-1   111   227   231   4100
6 .2 18 24 30 16 42 48 54 60 66 /2 78 d4 90 96+ MAX T/ T Th TH	6 .2 18 24 30 35 42 48 54 60 66 72 76 H4 90 46 4 MAY T T TO TH
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
23 Persistence of wind speed-interval	Summe

23 Persistence of wind speed-interval

Summe

1-500	
64.1N 166.7W	2 63 6N 178 1W
w≥64 1 1 2 2 4545 18 1 7 11 11 4545	w ≥ 64 3 1 1 12-1 4 5 5 4545 1 ≥ 46 24 7 6 10 1 3 1 1 1 72-1 54 49 155 4545
\$40,4121112112112112112112112112112112112112	N = 41 30 14 16 11 6 9 8 1 1 2 4 132-1 102 402 432 4546
D = 4 1913113 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	≥ 34 39 22 31 16 8 9 7 3 7 4 5 1 4 2 2 4 162-1 164 765 879 4552
$\frac{33}{5} \frac{33}{28} \frac{21}{42} \frac{20}{31} \frac{14}{12} \frac{7}{17} \frac{7}{3} \frac{3}{3} \frac{1}{12} \frac{2}{17} \frac{1}{17} \frac{114}{114} \frac{114}{114} \frac{368}{140} \frac{407}{140} \frac{4303}{140}$	S ≥ 28 35 31 17 23 22 10 12 7 12 7 6 3 4 5 17 210-3 211 1352 1500 458C
E = 22 42 33 30 32 2 17 3 14 7 4 7 7 1 3 21 222-1 264 1673 1819 4590	E = 22 32 15 34 25 19 15 9 13 10 12 6 9 4 5 4 34 366-1 246 2043 23 4 45 73
E ≥ 17 29 28 19 24 24 18 11 11 18 8 11 8 [7 12 2 39 384-1 269 2420 2652 4606	$E \ge 17 \frac{36}{20} 21 \frac{19}{120} 19 \frac{12}{19} 9 \frac{14}{4} \frac{4}{8} \frac{8}{12} 9 \frac{4}{7} \frac{7}{5} \frac{52}{52} \frac{654-1}{654-1} \frac{252}{252} \frac{2648}{2648} \frac{3025}{3025} \frac{4664}{4630}$
D ≥ 11 18 14 14 14 13 16 10 11 11 11 10 6 8 8 13 68 906-1 245 3484 3853 4823	211 19 11 9 13 0 11 10 11 1 1 1 1 1 1 1 1 1 1 1 1 1
K ≥ 7 21 3 5 7 13 6 10 8 2 3 10 6 1 4 3 78 1848 - 1 180 3683 4458 4908	$k \ge 7$ 10 4 5 4 5 4 5 4 5 4 2 7 6 2 4 2 4 73 1026 - 1 141 3484 4463 475 $n \ge 4$ 8 3 1 2 3 3 1 3 3 3 2 2 1 54 1734 - 1 89 335: 4664 4828
n ≥ 4 11 3 1 4 4 4 6 2 4 2 2 4 2 3 1 58 SEA-1 111 3252 4755 4933	6 12 18 24 30 36 42 48 54 60 66 /2 78 /4 90 96 MAX TE T TO TH
HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS 58.0N 167.0W
	w≥64 1 12-1 1 2 2 4545
w ≥64 11 (≥48 7 5 7 18-7 19 38 39 4545	1 ≥ 48 8 5 2 1 24-1 16 28 29 4545
N = 41 7 21 10 8 5 2 36 - 2 63 158 160 4545	N ≥ 41 28 18 6 6 2 1 1 48 -1 61 124 126 4545
≥ 34 49 33 26 10 14 9 3 3 3 3 1 1 1 1 72-1 15 1 44 1 444 4546	≥34 41 34 28 19 11 4 4 2 1 1 1 66-1 145 412 415 4545 5>28 53 60 37 22 28 15 8 3 5 3 1 2 1 3 120-1 241 86 6.2 4545
S ≥ 28 53 31 37 25 25 26 8 5 2 6 3 2 2 1 5 132-1 231 980 996 4547	D = 20   5   5   5   5   5   5   5   5   5
E \(\frac{22}{48}\)\frac{31}{31}\]\frac{30}{30}\]\frac{23}{21}\]\frac{15}{12}\]\frac{14}{14}\]\frac{11}{13}\]\frac{7}{5}\]\frac{4}{3}\]\frac{4}{4}\]\frac{19}{246}\]\frac{1}{293}\]\frac{1815}{1812}\]\frac{1842}{4582}\]\frac{4582}{5232}\]\frac{12}{5202}\]\frac{259}{12}\]\frac{12}{5202}\]\frac{12}	$\frac{1}{6} \ge 22   59   47   55   37   35   26   20   11   13   10   4   7   4   2   3   8   156 - 1   341   165   1763   4574   6 \ge 17   53   33   44   42   23   33   19   23   18   13   15   11   8   5   6   31   204 - 1   377   253   2618   4583   2648   4583   2648   264$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	D ≥ 11 29 21 23 12 18 22 13 9 16 9 10 5 7 9 9 83 492-1 295 3659 3622 4709
$k \ge 7   12   6   7   6   9   2   8   4   5   5   5   6   2   5   7   83   1014 - 1   172   3858   4439   4780$	k ≥ 7 20 11 3 11 6 4 4 9 5 5 9 3 8 5 7 81 876-1 191 4148 4425 4792
n ≥ 4   8   2   1   2   2   1   1   2   4   1     1	n ≥ 4 7 1 3 2 1 3 3 1 1 3 2 1 2 58 1788 - 1 88 4085 4964 5085
6 .2 18 24 30 76 42 48 54 60 66 /2 78 44 90 96+ MAX TC T T+ TH	6 .7 18 24 30 36 47 48 54 60 66 77 78 44 90 96 MAX TE T THE HOURS DURATION OF EVENTS
HOURS DURATION OF EVENTS 56.8N 174.8 E	6 52.00 172 92
w ≥ 64 2 1 12-1 3 4 4 4545	W = C+ O
248 i8 i4 7 3 i	N ≥ 41 50 35 112 7 4 1 3 1 1 1 66-1 114 2: 256 4545
D = 1 505 621 4565	D ≥ 34 54 58 48 25 11 4 3 8 4 1 1 78 -1 2 € 627 639 454
$\geq 34 \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$S \ge 28 62 57 54 44 33 15 8 11 5 7 2 1 1 4 120 - 1 304 1151 1175 4549$
F = 22 45 30 38 32 36 27 24 18 16 14 9 2 3 3 1 24 198 -2 322 2021 2096 4580	E ≥ 22 67 47 50 40 43 39 20 16 11 8 12 7 3 3 2 14 174-2 382 1975 205 4564
C ≥ 17 30 29 26 25 29 25 24 22 15 i9 8 i1 8 7 3 47 474-1 328 2875 2985 4667	$E \ge 17 \frac{45}{36} \frac{36}{45} \frac{45}{32} \frac{32}{33} \frac{28}{32} \frac{32}{19} \frac{15}{13} \frac{11}{11} \frac{10}{10} \frac{6}{11} \frac{16}{6} \frac{36}{36} \frac{210-1}{210-1} \frac{380}{380} = \frac{2723}{2836} \frac{2836}{467} = \frac{467}{20}$
D ≥ 11 29 16 18 6 16 12 17 16 11 8 11 10 5 6 4 64 486-2 269 3660 3973 4741	2 1 32 1 24 20 24 20 1 22 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
x ≥ 7 14.6 4 5 6 7 3 5 9 8 2 7 4 2 3 80 654-1 165 3/41 4487 4800 0 ≥ 4 m 5 2 2 3 2 2 2 3 2 2 2 2 3 4 1 53 2022-1 82 3997 5034 5143	$k \ge 7$   12   6   8   7   9   12   5   12   7   5   7   5   3   7   4   87   666 - 1   196   38.24   44.09   4   61   62   63   63   64   65   65   65   65   65   65   65
1 = 4 +   3   2   2   3   2   2   3   1   4   1   53   2022 - 1   82   3997   5034   5143   6   -2   16   -4   30   16   42   48   14   60   60   72   78   74   90   96   64   87   71   7   78   78   78   78   78	6 12 18 24 30 36 42 48 54 60 66 /2 78 44 90 46 + MA3 TE
HOURS DURATION OF EVENTS 7 54.7N 175.9W	HOURS DURATION OF EVENTS 54.9% 167 2W
w≥64 3 2 12-2 5 7 7 4545	w≥64 1 6-1 1 1 4546
≥48 27 19.6 4 24-4 56 99 99 4545	N → 148 8 9 2 2 2 24-2 21 40 4 4545
N = 41 42 22 22 9 6 2 1 1 1 54-1 105 246 248 4545	D 241 (21)16 (10)3   2
234 67 54 3 26 12 10 3 5 4 1 1 1 96 - 1 214 615 622 4550	≥34 47 28 23 12 6 3 3 3 3 1 1 1 2 12C-1 129 368 5 228 69 39 50 29 18 10 6 7 4 3 4 1 3 3 132-2 243 644 663 454
2 2 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	F ≥ 22 84 47 54 33 32 25 17 12 11 12 17 5 7 6 1 6 198 -1 359 1677 1735 45€€
E 22 /3 5 147 30 32 20 28 37 17 11 18 8 7 3 1 14 192 1 367 1933 2000 4367 E 2 17 64 43 48 38 35 26 19 19 20 19 15 4 10 12 5 31 294 1 408 2744 2869 4606	E ≥ 17 63 29 40 32 29 33 28 19 17 14 7 10 10 10 12 11 24 264-1 378 2588 2709 4586
D 2: 21.13 7715 27.17 17 12 9 14 14 18 14 6 5 70 366-1 295 3601 3911 4726	D ≥ 11 29 15 22 22 24 13 17 12 14 21 11 7 10 9 8 75 378 -2 309 3509 3719 4€.3
7 13 1 15 3 5 9 9 8 5 8 3 3 7 6 2 82 924-1 185 4049 4527 4884	$k \ge 7$ 16 7 7 8 5 14 6 6 5 15 2 6 4 5 6 83 744-1 195 389: 43:5 463.
7 ≥ 4 5 (2 6 2 2 3 1 2 3 1 1 2 2 2 61)1362-1 95 3911 5081 5212	n≥ 4 3 2 3 4 2 1 2 5 1 3 64 1452-1 90 4:74 4939 50€
HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS 51.8N _ 167.3W
9 50.3N 171.3W	w≥64 4545
$w \ge 64 \ 2$ $\ge 46 \ (9 \ 7 \ 5 \ 2 \ 1)$ $0 - 2 \ 2 \ 2 \ 4545$ $0 - 1 \ 34 \ 61 \ 61 \ 4545$	¥ ≥ 48   12   7   5   2     24 - 2   26   49   49   454 <sup>6</sup>
N 441 46:26:916 1 3 2 14 48-4 97 218 220 4545	N ≥ 41 25 17 4 5 3 2 2 1 54-1 59 '41 '43 454'
≥ 34 73 44 34 17 11 12 2 2 1 1 3 i : 120 -1 201 558 563 4549	≥34   54   50   19   13   5   8   4   2   2   4
5 ≥ 28 73 69 40 35 24 21 18 6 8 4 4 3 1 2 3 132-1 5,1 1180 1189 4549	2 2 2 80 35 37 34 20 17 9 8 2 4 4 3
F ≥ 22 (57) 59 (60) 33 (31) 29 (17) 22 (16) 9 (14) 5 (7) 4 (1) (16) 288 - 1 (380) 2075 2104 4568 F ≥ 17 (52) 39 (46) 33 (26) 27 (25) (6) 21 (13) 14 (10) 8 (4) 4 (42) 366 - 1 (380) 2847 2959 4594	$E  ext{ }  $
E ≥ 17 52 39 46 33 26 27 25 16 21 13 14 10 8 4 4 42 366-1 380 2847 2959 4594 C ≥ 11 30 15 17 24 16 8 13 8 20 7 9 8 5 9 3 85 498-1 277 3715 3944 4666	D ≥ 11 23 20 20 18 19 14 10 13 12 11 6 6 9 4 5 89 396-1 279 3696 3903 4652
x ≥ 7 6 5 8 12 4 5 8 6 7 4 5 3 4 3 2 90 798-1 172 3952 4358 4669	k ≥ 7 10 10 6 B 9 6 B 6 B 6 B 6 5 2 5 2 B7 864-1 178 4018 4392 4 34
0 ≥ 4 8 2 2 2 2 3 1 1 2 1 1 2 62 1536-1 87 3554 4769 4881	n ≥ 4 2 3 2 4 3 3 3 1 3 2 57 1458 - 1 83 3655 4979 5395
6 .2 18 .4 30 16 42 48 54 60 66 72 78 H4 90 96+ MAX TC T TE TH	6 12 18 24 30 36 42 48 34 0 66 02 78 00 9
HOURS DURATION OF EVENTS 11 51.3N 158.8W	12 54.4N (38 )
W≥64 3 1 12-1 4 5 5 4545	w ≥ 64 1 1 1 12-1 2 3 3 4545 1 ≥ 48 13 5 3 2 3 130-3 26 55 55 4545
2 46 12 6 3 3 3 30 30 3 24 48 48 4545 N 44 138 6 10 7 3 1 1 1 1 54 1 77 167 168 4545	N = 41 38 25 5 6 3 2 2 42-2 81 168 168 4548
N ≥ 41 38 6 10 7 3 1 1 1 1 54-1 77 167 168 4545 ≥ 34 65 48 19 16 13 7 4 1 2 1 1 96-1 177 469 476 4545	D ≥ 34 55 35 34 20 10 6 3 1 3 2 60-2 169 4€3 477 4545
5 28 96 62 47 34 18 24 14 12 6 2 1 1 1 1 2 2 108 2 322 1102 1116 4545	S ≥ 28 75 51 55 128 125 19 8 10 3 7 3 1 2 96 - 2 287 1004 'C28 454
F ± 22 67 57 54 50 35 32 23 2 18 14 6 7 7 3 4 11 210-1 409 2102 2156 4603	E ≥ 22 81 60 52 37 37 32 20 12 15 11 8 2 8 2 14 162-1 391 189C 193' 456-
F ≥ 17 39 57 30 37 29 24 18 23 i7 17 10 9 9 7 8 47 282~1 38i 2951 3060 4630	E ≥ 17 57 48 46 35 28 25 36 18 21 10 5 14 12 4 5 37 240 - 1 401 2757 2840 4591
D ≥ 11 27 23 16 15 18 7 14 6 15 5 12 6 4 6 6 86 564-1 266 3757 4002 4680	£ 11 2918 23 26 23 10 10 10 7 7 9 9 13 13 1 1 1 1 1 2 2 3 1 1 1 1 1 1 1 1 1
x ≥ 7 13 5 10 6 7 8 4 4 2 2 4 5 5 8 85 828 -1 168 3874 4434 4738	$k \ge 7 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$
1 2 4 4 1 2 3 6 3 2 2 1 2 2 2 1 51 1218-1 82 3348 4674 4774	6 12 16 24 30 36 42 48 54 60 66 72 78 H4 90 96+ MAX TE T TO TH
HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS
Fall	23 Persistence of wind speed-durat
1 Will	

			II-t
w≥64 1 6 SEA-5 6	2202 4928 4930	V W≥64 8 SEA~5 6	63 6N 178 1 247: 5306 5311
1 ≥48 10 SEA-4 11	2464 5189 5200	W ± 64	3169 4951 5106
	3363 4994 5107	N ≥ 41 8 5 R 2 2 2 2 4 2 2 4 62 84C-1 105	3423 4295 472t
≥34 11 4 3 i 4 3 4 2 1 5 2 2 2 73 1440~1 117	3593 4356 4739		3272 38:1 4683
P	3330 3702 4638 2630 2843 4617	5 ≥ 28 22 13 10 12 11 12 8 12 5 7 11 10 5 4 6 70 708 - 1 218 p ≥ 22 32 17 24 19 23 15 14 15 14 9 3 8 7 8 7 8 4 38 312 - 1 250	2979 3:60 4625
	1946 2001 4592	E ≥ 22   32   17   24   19   23   15   14   15   14   9   3   8   7   8   4   38   312-1   250   E ≥ 17   45   35   27   30   18   18   10   13   9   8   7   4   10   1   1   21   246-1   257	2206 2312 4596 1587 1621 456
D ≥ 11 65 51 37 25 20 18 4 3 5 3 1 2 3 2 7 162-1 246	951 973 4548	D ≥ 11 60 47 32 21 15 14 8 7 3 1 3 1 2 2 228-1 216	776 779 4560
x ≥ 7 /8 45 22 19 6 2 2 2 2 1 1 1 126-1 180	436 451 4546	k ≥ 7 62 41 16 11 8 1 1 2 1 1 60-1 143	315 319 4545
$n \ge 4$ $77$ $21$ $7$ $6$ $1$ $1$ $36-1$ $113$ $36-1$ $113$	175 179 4546 T Te TH	n ≥ 4 51 23 5 6 3 1 1 54-1 89 6 12 18 24 30 16 42 48 54 60 66 /2 78 r4 70 76 max 71	160 164 4545
HOURS INTERVAL BETWEEN EVENTS	59.4N 172.0W	HOURS INTERVAL BETWEEN EVENTS	
"	2201 4927 4929	W ≥64 6 SEA-5 €	58.0N 167 0 2201 4927 4929
1 ≥ 48 1 1 21 SEA-1 23	2836 5053 5092	≥48   2   16 SEA-! 18	2813 4934 4963
	3392 4529 4689	N ±41 1 2 1 2 5 1 2 2 2 43 1098 - 01	2984 4571 4697
	3293 4224 4667 3172 3723 4717	≥ 34 12 5 3 8 9 4 4 6 3 3 5 4 4 2 72 966-1 144 5 2 ≥ 28 24 11 12 15 15 15 8 12 6 8 12 8 11 3 5 74 444-1 239	3345 4255 4670 3191 3768 4640
E ≤ 22 42 32 20 30 26 19 6 18 15 9 3 5 6 5 10 48 318 -1 294	2512 2812 4617	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3191 3768 4640 2661 2924 4598
E ≥ 17 51 38 57 41 33 23 17 19 7 6 6 5 5 5 1 19 252-1 333	1841 1916 4591	E ≥ 17 85 57 59 40 19 16 18 15 12 8 4 9 10 5 3 16 204-1 376	1888 1985 4565
2 ≥ 11 64 81 38 22 13 12 4 4 4 4 5 2 3 3 126-1 255	827 846 4545	D ≥ 11 96 75 52 15 17 13 7 5 3 4 3 1 1 1 114-1 293	868 894 455.
K ≥ 7 95 41 15 10 3 3 2 1 1 1 72-1 171 N ≥ 4 57 17 5 1 18-5 79	335 341 4545 106 107 4545	k ≥ 7 10048 18 B 6 3 1 1 60-1 185 n ≥ 4 66 14 2 2 1 36-1 B5	351 367 4545 116 121 4545
6 .2 18 24 30 16 42 48 54 60 66 /2 78 H4 90 46+ MAX TI	T T* TH	6 12 18 24 30 36 42 48 54 60 66 72 78 44 90 96+ MAX Y:	116 121 4545 T T+ ++
HOURS INTERVAL BETWEEN EVENTS	56.8N 174.8E	HOURS INTERVAL BETWEEN EVENTS 6	52.0N 172.9
	2052 1774 4778	W≥64 1 1 10 SEA-5 12	2563 5276 5292
· · · · · · · · · · · · · · · · · · ·	3167 4918 5013 3248 4450 4702	≥48   1   1   1   2   1   1   1   35   SEA   1   44	3368 4722 48 c
≥ 34 15 8 6 4 6 6 9 5 6 5 6 9 7 3 3 74 894-1 172	3248 4450 4702 3508 4004 4615	0 ±41 8 6 3 12 3 1 3 4 2 1 4 2 3 2 1 72 SEA-1117 ≥34 19 19 11 13 8 9 5 10 5 11 2 9 3 6 5 81 618-1 216	3675   457   48.1 3625   4055   4692
3 ≥ 28 28 16 17 19 16 12 14 15 9 15 10 12 7 4 8 67;438 - 1 269	3117 3414 4602	S ≥ 28 35 21 38 26 19 16 11 16 11 9 5 7 4 7 7 7 70 396 - 1 362	3136 3473 4642
	2366 2514 4575	E ±22 63 52 5: 36 23 25 17 19 12 16 11 6 9 8 3 34 3/2-1 385	2448 2601 46 3
E ≥ '7 .58 58 46 34 27 28 9 12 15 11 5 7 3 3 7 9 144-1 332 ≥ 1 85 70 44 24 20 12 6 3 3 1 1 1 78-1 270	1661 1709 4572 754 769 4546	E ≥ 17 76 77 59 34 25 24 12 18 14 9 9 8 3 5 1 10 132-1 384	1761 1789 4569
$k \ge 7 \cdot 8^7 \cdot 46 \cdot 20 \cdot 10 \cdot 4 \cdot 1 \cdot 1 \cdot 1 \cdot 1 \cdot 1 \cdot 1 \cdot 1 \cdot 1 \cdot 1$	754 769 4546 313 313 4545	2 11 128/73 37 34 20 6 17 2 4 3 1 2 102-1 3;7 k ≥ 7 10745 25 12 5 2 1 1 78-1 197	833   545   4559 370   373   4546
^ ≥ 4 66   11 4 1   1   30 - 1   83	109 109 4545	R ± 7 (07/45/25/12/5/25	370   373   4546 126   127   4546
F 12 18 24 30 16 42 48 54 60 66 72 78 84 9096+ MAX TI HOURS INTERVAL BETWEEN EVENTS	Т Т* ТН	6 12 18 24 30 36 42 48 54 60 66 12 18 44 90 96 4 VAT TE	
7	54.7N 175.9W	8	54.9N 167 21
· · · · · · · · · · · · · · · · · · ·	2437 4909 4916 3138 4731 4850	W ≥ 64 5 SEA - 4 5	1833 4510 4511 3376 5468 5509
241 5 4 5 1 4 2 3 2 3 4 2 2 3 2 62 1134-1 104	3458 4530 4778	N ≥ 41 3 1 1 2 1 1 48 1464-1 57	3376 5468 5509 3382 4804 4937
≥34 (9,17 8 (2 7 9 8 6 9 6 9 3 9 7 4 81 894-1 214 )	3474 4086 4703	≥34 11 6 8 7 2 2 5 3 2 5 3 3 2 2 69 i242-1 13C	3550 4317 466 <del>~</del>
· · · · · · · · · · · · · · · · · · ·	3089 3458 4649 2496 2609 4593	$S \ge 28$ 25 23 14 17 6 15 11 6 13 11 11110 3 6 5 67 438 -2 243 .	3226 3.79 4632
	2496 2609 4593 1729 1761 4569	E ≥ 22 67 35 33 30 31 20 20 10 18 :2 5 :0 7 9 6 43 282 -1 356 E ≥ 17 71 82 58 41 22 19 16 :0 6 :16 7 7 5 .2 2 :14 276 -1 :378	2641 2981 4595 1815 1901 4569
D ≥ 1 10784 43 22 12 7 4 2 5 3 3 2 1 1 1 114-1 296	804 817 4547	D ≥ 11 11477 40 31 14 9 8 5 5 2 3	866 909 4550
x ≥ 7 10646 75 8 3 2 3 2 1 60-1 186	351 357 4545	k ≧ 7 0648 22 5 4 4 1 1 1 1 60-1 192	359 318 4545
7 ≥ 4 7 14 7 2 3 30-2 94 6 2 18 14 7 15 16 42 48 54 60 65 /2 78 84 90 96+ MAX TI	130 131 4545 T T4 TH	n ≥ 4 66 17 2 1 1 2 36-2 89 1	128 4544
HOURS INTERVAL BETWEEN EVENTS	T T4 TH 50.3N 171.3W	HOURS INTERVAL BETWEEN EVENTS	-
· · · · · · · · · · · · · · · · · · ·	2201 4926 4928	W≥64 5 SEA-5 5	51.8N 167.31 1840 4566 4566
≥48 4 27 SEA-1 33 2	2982 5260 5321	≥48 3 1 1 1 1 2C SEA-2 26	2989 5176 5225
	3670 4726 4946 3537 4378 4887	N ≥41 5 1 2 2 2 2 1 1 1 1 1 43.SEA-1 6:	3437: 4894 5031
	3537 4328 4887 2942 3447 4632	e     <del>                               </del>	3417 4260 4701 3202 3622 4616
F 422 50 55 52 33 32 27 18 24 10 12 8 4 12 5 5 27 366-1 374	2314 2484 4565	P F	3202 3622 46 6 2451 2626 4536
E ≥ 17 84 65 62 46 32 26 14 12 5 5 8 5 3 4 2 6 120-2 319	1573 1652 4562	E ≥ 17 86 72 53 43 34 23 15 16 7 6 5 6 5 1 2 9 270-1 383	1649 1752 4556
	701 725 4548	D ≥ 11   24 € 2   36   28   9   4   7   1   2   3   1   1   1   1   1   1   1   1   28 ;	713 751 4547
- 10000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	308 311 4545 111 112 4545	k ≥ 7 97 51 17 6 3 1 2 1 54-1 178 n ≥ 4 69 9 2 2 2 2 3 30-2 84	320 342 4545
6 12 18 24 30 16 42 48 54 60 66 72 78 H4 90 96+ MAX TI	111   112   4545   T	6 12 18 4 30 16 42 48 54 60 66 72 78 H4 90 96+ MAX T	111 t11 4545 T Te Te
HOURS INTERVAL BETWEEN EVENTS	51.3N 158.8W	HOURS INTERVAL BETWEEN EVENTS	54.4N 158.11
	2380 4920 4925	w ≥64 7 SEA-5 7	2546 5272 5275
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2407 4777 4825 3359 4716 4884	N	2980 5121 5176 3617 4714 4882
≥ 34 16 5 7 B 16 10 3 5 6 5 6 2 4 5 B1 840-1 179 3	3359 4716 4884 3631 4334 4810		3617 4714 4882 3619 4257 4734
S ≥ 28 35 31 38 30 26 21 19 17 11 9 5 5 7 4 2 63 426 - 1 323	3204 3561 4677	S ≥ 28 34 27 16 22 24 17 16 6 15 7 6 11 5 2 4 77 480-1 289	3332 3676 4704
· r· + +-+-+-+-+	2376 2498 4596	e ≥ 22 69 57 46 46 29 24 19 11 12 14 7 7 3 9 6 36 240-1 395	2505 2654 4567
_^;	1527 1587 4562 667 683 4550		1727 1768 4555
k ≥ 7 0436 14 B 4 2 2 1 48-1 171	667         683         4550           304         304         4545	k ≥ 7 1935 20 12 5 2 1 1 84-1 194	765 773 4545 348 349 4545
n ≥ 4 65 13 3 18-3 81	100 100 4545	n ≥ 4 75 15 5 1 24-1 96	124 124 4545
5 2 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TI HOURS INTERVAL BETWEEN EVENTS	T Te TH	5 12 18 24 30 36 42 48 54 60 56 72 78 84 90 96+ MAX TI HOURS INTERVAL BETWEEN EVENTS	T To TH
3 Persistence of wind speed-interval		ETENIO	F٤
: mile opour interfel			F >

i 64.3N 166.7W	2 63 6N 178 1W
w ≥ 64 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	w ≥ 64 5 3 1 1.72 9
248 110 5 4 1 1 1-1 20 37 37 17219	≥ 48 41 21 11 18 12 2 3-1 '05 264 290 '172'9
N 241 38123121 10 9 2-5 101 237 239 17219	N ≥ 41 60 37 37 24 51 9 3 2
2	P
§ ≥ 28 10268 59 51 104 36 14 9 7 8-1 450 2161 2204 17219	S ≥ 28 04 66 56 60 12 154 31 15 22 1 15-1 539 3292 3505 17214
£ 22 2 3 3 9 2 7 6 7 7 6 3 7 6 28 1 3 3 4 1 1 1 3 - 1 6 6 5 4 2 2 8 4 4 0 7 1 7 2 1 9	£ 822   11 64   70   60   181 84   46   16   42   9   1   1   1   18   1   168   1   5395   579€   172   9
E ≥ 17 12768 66 70 210 2257 28 56 11 16-1 815 6783 7125 17219	E ≥ 17 10469 71 55 172 1365 30 56 24 2 2 27-1 763 7532 813 772 9
D ≥ 11 10766 62 64 1841 2486 47 10431 4 1 38 - 1 880 10492 11238 17219	D ≥ 11 10485 49 56 1641 2560 54 92 39 9 3 41-1 840 10720 11914 11214
x ≥ 7 8: 35 36 38 42 03 75 50 116 57 10 3 : 77 - 1 747 12560 14 182 172 19	k ≥ 7 87 40 50 37 97 82 64 43 2958 10 4 51- 701 12302 14429 17214
$n \ge 4.62  30  24  28   61   59   43   38   05   62   18   11                              $	n ≥ 4 57 41 20 21 67 51 30 31 0865 17 11 1 72-1 520 12962 15181 17214
25 5 75 1 2 3 4 5 10 20 30 60 90 180360 00 MAX TE T T+ TH	25 5 75 7 2 3 4 5 10 20 30 60 90 80360 00 MAY TE T THE THE
DAYS DURATION OF EVENTS 3 59.4N 172.0W	DAYS DURATION OF EVENTS
	58.0N 167.0W
" ····································	w≥64 1 2 1-2 3 5 5 1224
≥48 18 12 11 5 1 1 17217	1 ≥ 48  21  13   4   6
24 39 34 29 17 18 1 5~ 138 383 389 17217	N ≥ 41 60 39 16 16 11 2-2 142 316 318 177.9
≥ 34 *0175,44 33,63 16 1 1 1 8-1 334 1092 1:03 17217	≥34 107,95 56 35 60 7 1 3=1 361 1028 1036 17219
5 = 28 1 696 87 58 44 39 8 6 6 9-1 560 2430 2461 17217	c
**	P P P P P P P P P P P P P P P P P P P
22 13296 90 89 226 94 33 15 20 2 10-2 791 4680 4754 17217	g = 22   168  3   1   33  100  240   85   34   17   7   9 - 1   9 - 5   45   6   6   6   72   9
5 ≥ 17 16 197 188 87 268 33 63 30 47 8     18 - 1 982   7170   7465   17217	E ≥ 17   75   20   43   18  30   43  62   35   38   1           16 - 1   136   7364   7574   172   4
2 . 94 68 62 62 220 73 99 66 92 33 2 23-1 971 11062 11856 17217	≥ 11 0682 83 71 peg 6 7 05 70 1426 2 22-1 1095 11694 12 13 12 4
. 2 7 7: 34 29 24 198 1676 61 3570 10 2 42-1 747 :3380 14750 17217	$k \ge 7.63  31   28   32   20   12   62   62   54   70   9   5     40-1   755   13974   14995   172   9   $
	$^{0} \ge 4 \frac{38}{38} \frac{13}{13} \frac{10}{10} \frac{46}{40} \frac{40}{27} \frac{27}{30} \frac{30}{82} \frac{26}{31} \frac{31}{14} \frac{4}{3} \frac{3}{75} - \frac{423}{423} \frac{14377}{16357} \frac{6357}{77} \frac{7}{9}$
25 5 75 2 3 4 5 10 20 30 60 90 180360 00 MAX TE T TO THE DAYS DURATION OF EVENTS	25 5 75 1 2 3 3 4 40 22 35 60 90 HA360 00 MAX TE TO THE THE DAYS DURATION OF EVENTS
5 56.8N 174.8E	6 52.0N 172 9E
1.864 2 4 2 1 1 1 1 2 12 20 20 17219	w≥64 13 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
≥48 46 26 23 11 12 3   3-1 118 303 308 17219	1 ≥ 48 43 24 25 8 6 2-2 10€ 236 23€ 170 3
24' 6' 54 36 32 40 B 1 2 4-2 240 778 791 17219	D ≥ 4 1 195 165 40   21   27   3   3 + 25   6 1   6 2   72   9
\$ 14 108 1 62 48 102 19 19 5 8 - 2 424 1709 1739 17219	≥ 34 34 21 1986 56 84 11 4 4 4-1 502 1535 1553 1714
\$28 13293 90 74 h 7547 18 7 16 9-1 642 3208 3268 172 19	\$ ≥ 28 19015 7 2010 116 146 13 6 3 1
= = 22 133/6 98/75 b5/197/31/30/34/2   13-1/833 5539 5672 17219	P P
~ · · · · · · · · · · · · · · · · · · ·	
E e 17 15693,99 73 preji 4759 40 60 16	E≥17 17 11 4 11 321 0 1922 15 285 37 48 6 12-1 197 8257 8532 172 4
3 1 1 6 3 66 43 p2 4 4 8 9 7 6 2 1 3 7 5 2 2 4 - 1 9 9 2 1 1 9 3 8 1 2 4 8 8 1 7 2 1 9	M≥ 11   50 87  80   75   669146  08 68   34 30   19-1147   1246   17519
	k ≥ 7,60 28 42 30 3 3 1 90 75 58 15 7 3 1 5 1 3 45 - 1 75 2 1 3880 15 2 5 4 1 1 2 3
s = 2 5 20 1 37 32 25 22 87 80 27 14 1 84 - 1 398 13866 16402 17219	0 ≥ 4 31 13 5 11 41 29127 25 100 70 24 16 2 66 -1 394 19930 16468 1.1-
25 5 5 2 3 4 5 10 20 30 60 90 181360 00 MAX TO T THE TH	25 5 75 5 2 3 4 5 10 20 30 60 VOTE 360 00 WAY 35 THE TH
DAYS DURATION OF EVENTS	DAYS DURATION OF EVENTS
	8 54 9N 167 2 W
264 5 3 t t_= 19 14 14 17219	w≥64 2
245 no 31 18 8 14 2 2 1 121 231 231 231 17219	≥48 25 16 5 2
. V	N + +- + + + + + + + +-
8.34 58/23/6.46 8, 216 2 1 6-1 502 1549 1567 17219	≥34 12273 64:33 47 4 : 1 5 - 345 943 956 °.
### 19292 #### 11 6 4	28 ≥ 28 183 1 10 1 1 1 7 1 1 2 4 29 . 5   1   2
9-1 1085 5434 5568 7219	F ≤ 22 242/50/60/97 25: 90 35: 9: 6 8- 040 4686 4719 17: 1
2 221509 387 250 93 5 386 33 45 2 12-1 125?   8145   8433   17219	E ≥ 17 2273 258 409 3283 36 (B1 33 33 1 1 1 1 1 - 1 7 26 2 7 8 7 3 8 2 2 7 1 2 1
20-1 17379 80 94 2778 818 10 68 10 5 35 1 20-1 1153 12049 12680 17219	↑ <del>                                     </del>
· ≥   64 39,36 33136 89 73 6015770 12 3   39-1   772   13936   15170   17219	k ≥ 7 58 37/30 31 12 110 796 64 15 169 10 2 31~1 176 14031 15066 TJ
- 4 37 2 7 10 41 36 30 25 93 76 23 88 1 80 - 1 409 13825 16477 17219	n ≥ 4 23 7 114 11 32 25 25 27 99 74 31 12 n 1 72 - 383 1434 16463 172 1
25 5 75 2 3 4 5 10 20 30 60 90 90360 00 MAX TE TO THE	25 5 75 1 2 3 4 5 0 20 30 60 90 60360 00 MAY TE TO THE
DAYS DURATION OF EVENTS 9 50.3N 171.3W	DAYS DURATION OF EVENTS
	10 51.8N 167.3A
<del> </del>	w≥64 !
≥46 38 20 11 5 3 1 1 2-2 77 148 154 17216	≥48 28 16 8 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
24 97 54 24 1 23 1 3-1 210 47° 485 17218	N ≥ 41 (61 )0 (20 12 14 ) 2 - 1 50 3.2 12 ±
£ 34 (68 574 40 59 11 1 1 5 - 1 477   1291 1319 17218	≥ 34 126 1568 37 44 9 2 4 4 1 403 CB 125
3 2 3 2 1 1 7 4 1 1 2 9 8 1 5 6 4 2 7 3 3 3 6 6 7 1 8 0 6 2 8 8 8 2 9 3 2 1 1 7 2 1 8 1	S ≥ 28 218 43 05 85 62 28 6 2 1 5-1 750 2577 2-29 77. H
+ 27 go4b11148h0obee 108 35   15   13   1	E ≥ 22 p49191143113p82102/27 15 10 1 1 12-1133 5273 5419 711e
F = 17 21815 38 3715 39 818 64 37 46 6 15 15 -1 1323 8531 8820 17218	E ≥ 17 (92) 65\ 54\ 34\ \partial \part
114180172 81 b39 83 00 72 126 34 1 1 1 1 2 1 2 1 - 1 1129 12389 13013 17218	≥ 11 05 72 94 83 p34 66 0774 32 35
. 2 1 5 4 36 35 35 1692 69 68 5275 1 2 35 1 750 14107 15365 7218	k ≥ 7 66 41 43 39 12084 66 64 7161 15 2 36 72 14 369 15 298 12 =
- 4 25 1 0 7 31 29 31 20 92 88 22 12 2 70 - 378 3586 16532 172 18	
25 5 15 2 3 4 5 10 20 30 60 90 180360 00 WAX TE T TO TH	
DAYS DURATION OF EVENTS	25 5 75 1 2 3 4 5 10 20 30 60 90 180360 00 MAR TO TO TO TO
11 51.3N 158.8W	12 54 4N 158.1W
h 8:4 4 2 1 1-1 7 11 11 17219	≥64 4 2   1
2-1 67 142 142 17219	1 ≥ 48 39 11 9 6 7 1
	N ≥41 0358 25 20 18 2 1 3.1 227 513 5.2 12.4
≥ 34 1 77 2 367 51 67 10 3 4-1 498 1364 1380 17219	≥ 34 14394 74 56 69 10 3 4-1 449 328 340 14
28 555 70 24 90 86 32 13 3 2 7-1 877 3106 3151 17219	\$ ≥ 28 207  42  33  81  72  32  7   4
1 4 2 2 23 6 66 6 3 3 5 9 0 0 1 1 4 6 18 1 3 9 - 1 1 1 8 8 5 9 6 7 6 1 1 9 1 7 2 1 9	F ≥ 22 229 BS 556 12229 1336 15 12 8-1 113 5434 5530 17. 9
2 · 7   7 9   3   1   2 9   6 4 9 9   38   63 2     12 - 1   12 9 3   9 0 4 6   9 3 5 3   1 7 2 1 9	E ≥ 17 210164/135/144325/145/99 39 46 10-1 11307 8430 8641 11307
26 - 1 1050 12846 13491 17219	n F
2 7 50 34 38 26 97 75 72 46 56 79 13 4 40-2 690 14337 15607 17219	$k \ge 7 63 30 38 43 11 86 75 51 55 74 12 5 39 1 743 14202 15392 72 9$
2 4 21 7 8 10 29 25 27 18 69 61 33 24 59 1 332 13866 16677 17219	n ≥ 4   28   8   9   11   33   31   26   26   92   82   21   19   1
25 5 75 1 2 3 4 5 10 20 30 50 90 180360 ∞ MAX TE T T+ TH	25 5 75 1 2 3 4 5 10 20 30 60 90 180360 00 MAX TE THE
DAYS DURATION OF EVENTS	DAYS DURATION OF EVENTS
innual	23 Persistence of wind speed-duration
	7.5 PRINISIMORN DI WIND SONNIOU(ATION

**Annual** 

23 Persistence of wind speed-duration

	166.7W 2 63.6N 178.1W 172.19 w≥64 2 43-1 2 316 172.08 172.9
<b>"</b>	17219 W≥64 2 2 43-1 2 316 17208 17219 17219 (≥48 8 3 7 3 4 5 3 5 1313 13 7 2 88-1 86 4440 16929 17219
\'\'\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	17219 N 41 25 8 8 4 19 14 13 14 35 27 21 9 2 179 1 199 8256 16340 172 9
	17219 ≥ 34   34   15   21   9   48   45   32   27   65   33   8   5   4
	17219 S ≥ 28 67 26 25 24 88 68 48 26 93 35 11 5 2 1 131-1 519 10500 13714 17219
0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
	17219 E 2 17 11483 73 70 161 77 46 42 62 23 8 3 1 66-1 763 8482 9088 17219
	17219 D = 11 1888 3 10 1265 19664 39 21 34 € 17-1 856 5154 5305 17219
	17219 k ≥ 7 21605091 71 4330 16 5 5 1 11-1 728 2764 2786 172.9
	17219 n ≥ 4 233 3162 39 69 11 1 2 1 1 5-1 549 1426 1438 172 3
25 5 75 1 2 3 4 5 10 20 30 60 90 180360 00 MAX TI T	Th .25 5 75 1 2 3 4 5 10 20 70 60 90 100 760 00 MAK T1 T4 TH
DAYS INTERVAL RETWEEN EVENTS	DAYS INTERVAL BETWEEN EVENTS 172.0W 4 58.0N 167.0W
"	17217   ≥48   1   1   4   1   1   5   3   7   2   2   1.79 - 1   27   3652   17:35   72:9
	17217 N ≥41 2 2 1 4 7 14 8 2 22/34 7 12 1 1 1 1 188 - 1 1 8 7 165 16901 17219
	17217 ≥34 2712 7 12 46 34 24 24 64 53 16 7 3 2 174-1331 11374 6184 17219
	17217 S≥28 68 30 26 29 1185 57 44 88 53 11 6 4 1 1 91-1 613 12727 148571 72 9
	17217 F ≥ 22 1765 89 82 81 1266 47 84 38 9 6 : 82-1 897 11390 1261: 12:9
	17217 $E \ge 17  92 40 36 08 226 21 70 40 64 22 4 1                                $
	17217 D≥ 11 27623516290 9 774 28 21 20 2 :3-1 1105 4960 5106 17219
k ≥ 7 2891 721 0262 87 33 13 4 4 8-1 766 2410 2467	17217 K ≥ 7 294 202 84 58 10 14 7 4 4 8 8 -1 777 2275 2324 72 9
	17217
25 5 75 - 2 3 4 5 -0 20 30 60 90 180360 00 MAX TI T	TH 25 5 75 1 7 3 4 5 10 20 30 60 90 80 360 00 MAX T. T.
DAYS INTERVAL BETWEEN EVENTS 5 56.8N	DAYS INTERVAL BETWEEN EVENTS 174.8ε  DAYS INTERVAL BETWEEN EVENTS 52.0N 172.9E
% ≥ 64 1 1 1 1 1 1 1 127-1 6 785 17199	17219 w≥64 1 1 1 3 2 66 8 38 790 72'9
	17219 248 2 1 2 1 3 6 5 2 18 9 14 8 3 1 9 - 1 65 5696 6983 2 9
23 10 2 5 16 20 16 10 49 41 12 7 1 1 1 233 -1 214 86 12 16428	17219 0 841 13 11 6 5 24 18 21 14 40 48 10 11 2 4 176 - 1227 10624 16593 12.9
≥ 34 33 21 14 17 54 53 33 31 65 53 11 6 6 2 93 - 1 399 11448 15480	17219 ≥ 34 44 41 25 26 67 55 39 31 72 49 14 6 2 4 1 166-1 475 12333; 15666 12.9
5 T T 1	17219 S≥28 0860 68 57 3973 49 44 1 1041 17 7 1 1 1 197-1 775 12632 14 43 172 9
£ ≥ 22 92 70.8 53 19 1 1 1 59 36 76 32 13 5 44-1 819 10496 11547	17219 E ≥ 22 1601 251 0887 2161 1367 47 88 29 11 1 43 - 1 '1052 10.742 1.1518 1.7219
	17219 E ≥ 17 208 93 49 07 234 25 64 40 59 19 8 - 1 1198 8438 8687 72 9
" 2 ' 24719014539 19317 30 12 22 9-1 1009 4580 4731	17219  ≥11 b72b22 53 04 95 75 26 12 8 1
. ≥ 7 2831 78 0458 87 22 4 5 3 7-1 744 2135 2180	17219 k ≥ 7 348 63 06 59 81 12 8 1 1 6-1 779 992 20 5 12 4
^ ≥ 4 26 82 47 16 19 5 1 4-1 431 812 817 125 5 5 5 2 3 4 5 0 20 30 60 90 (60360 00 WAK 7/ 7 7)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
DAYS INTERVAL BETWEEN EVENTS	DAYS INTERVAL BETWEEN EVENTS
	175.9₩ 8 54.9N 167.2₩ 17219 W≥64 7215
39-1 3 1203 348 9 3 3 1 2 5 10 2 17 18 9 10 4 1 129-1 94 5900 16988	17219   ¥48 1   2   2   1   1   5   1   10   2   4   1   230 - 30   5€38 - 7.3.
	17219 N 241 4 2 1 7 6 7 6 17 27 14 16 2 1 1 230 - 11 8619 1 6929 121
	17219 D 34 29 17 15 10 30 30 19 17 61 55 20 6 5 2 1 56-1 3 6 11 29 626 2
2 4 78 199 54 49 42 555 89 62 45 95 48 7 8 2 84-1 755 12190 14147	17219 S ≥ 28 60 41 36 39 97 85 45 35 98 57 6 10 2 1 121-16 2 12 29 498 1 22 1
E < 22 1501 21309 1 2241 2 167 55 83 37 5 1 1 66-1 1077 10937 11651	17219 F 22 5393 83 9 1 225 05 80 45 97 40 3 4 11 2-1 520 1477 2436 2
C 2 17 2385 891 771 19238 1467 37 65 11 1 3 23-1 1258 8440 8786	17219 E ≥ 17 2278 958 688 1823 1 2952 48 7 1 1 3 1 34 - 1255 8797 92.5 12
2 - 335262 70028267 20 15 13 7-3 1169 4439 4539	17219 D ≥ 11 B36257 52 08207 69 18 77 12 9-1 1176 4609 4738 72
v ≥ 7 364 770 159 7 i 23 7 1 4-1 803 2029 2049	17219 k ≥ 7 854 83 034 7 85 17 9 2 1 6-1 80 2082 2 29 12 1
" \(\alpha\) 4 27 \(\begin{array}{c c c c c c c c c c c c c c c c c c c	17219 n ≥ 4 262 83 24 13 28 1 3 -1 411 736 754 121
- 5 '5 Z 3 A 5 10 20 30 60 90 160 360 00 MAX TI T THE DAYS INTERVAL BETWEEN EVENTS	TH 25 5 75 1 2 3 4 5 10 20 30 60 90 180360 00 MAX T T TO THE DAYS INTERVAL BETWEEN EVENTS
9 50.3N	171.3W 10 51.8N 167.3W
,, ≥64 17212	17218 w≥64 "21"
₹48 6 3 5 1 3 3 6 11 3 9 5 1 98-1 56 4492 17064	17218 ≥48 4 1 3 1 3 1 3 7 9 4 1 228 -1 37 41 228 -1 37 4 1 1 228 -1 37 4 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
4 34 47 16 23 23 54 54 36 28 85 54 13 13 3 2 162-1 451 12849 15899	17218 ≥ 34 41 20 15 16 42 32 30 24 62 64 18 B 4 1 1 144 - 1 377 12:34 16:13 172:4
3 ≥ 28 10756 43 51 447 0858 47 94 56 4 7 2 1 121-1 781 12703 14286	17218 S≥28 89 53 40 35 3888 54 51 04 56 7 8 3 88 -1 +726 . 12908 :4589 :1218
£ 22 1631 291 1972 223 3 1 97 50 87 33 5 1 57 - 1 1110 10951 11567	17218 E ≥ 22 866 30 20 88 22 1 24 74 43 98 37 3 3
5 2 17 26-198(8 t) 26b72(25)62 38 (48 9 ) 1	17218  $E \ge 17$   $b \ge 2005   5.3   38   665   1642   52   58   9   2                                $
2 1 33/2731501 1017161 23 12 17 8-1 1144 4130 4205	17218   $\stackrel{>}{\sim}$   11   56 $\stackrel{>}{\sim}$   3   65 $\stackrel{>}{\sim}$   3   9   14
. ÷ 7 3/71 7697 43 69 14 4 1 5-1 781 1834 1853 - ± 4 2/5/24 33 11 9 5 3-1 412 683 686	17218 0 ≥ 4 28988 30 14 10 3 3 3 -1 434 698 703 3 9
$\stackrel{?}{=} 4 \stackrel{?}{?} \stackrel{?}{?} \stackrel{?}{?} \stackrel{?}{3} \stackrel{?}{3} \stackrel{?}{1} \stackrel{?}{9} \stackrel{?}{.} \stackrel{?}{.} \stackrel{?}{1} $	TH 25 5 75 1 2 3 4 5 10 20 30 60 90 180360 00 WAX 7 7 1 1 1
DAYS INTERVAL BETWEEN EVENTS	DAYS INTERVAL BETWEEN EVENTS
	158.8W 12 54.4N 158.1W 17219 w≥64 17219 17219
44e   1   3   2   1   2   9   9   5   10   2   3     178 - 1   48   5391   17077	17219 (≥48 4 1   3 1 1   8 7 7 15 3 2 1   208 -1 53   70°0   17059   12°9
244 15 3 4 5 13 15 12 6 133 47 18 12 3 146 1 192 9470 16728	17219 N 241 16 5 5 1 11 17 6 7 4442 21 11 2 15 178 - 1 198 11269 16702 17219
±34 52 21 21 17 82 44 34 29 88 59 11 6 2 5 167~1 471 13073 15839	17219 ≥ 34 33 12 17 20 69 42 31 20 78 73 16 3 4 3 145 - 1 421 12930 15879. 1219
22810476,73 678620255 4280948 8 8 2 75-1 856 12780 14068	17219 S≥28 70 68 49 46 13494 57 55 1026: 10 5 3 75-1 754 12861 14403, 11219
E 22 202142132 10236128173 43 79 31 1 2 1 72-1 1180 10539 11100	
( 21 28922216 11 11265 145 1 29 46 10 1 24-1 1299 7571 7866 )	17219 € ≥ 17 23522917512726611667 30 53 7 3 1 31-1 1309 8272, 85 18 17219
35822215093 6548 17 5 8 6-1 1066 3633 3728	17219 5≥1: 36724616688 88652 25 9 5 1 13-1 1139 4048 413 172 9
2 / D75 4485 53 47 12 2 2 5-1 720 1596 16:2	17219 . ≥ 7 0/2 67 0 2 49 63 10 5 2 1 6-1 771 1808 1827 1 17212
2 4 255 78 17 10 4 1 3-1 365 537 542	17219 °≥ 4 p77 84 31 7 12 3 1 4-1 415 677 687 17219
75 5 75 7 2 7 4 5 10 20 30 60 90 180360 00 MAR TI T TO DAYS INTERVAL BETWEEN EVENTS	TH 25 5 15 1 2 3 4 5 10 20 31 60 90 180360 00 MAX TI T TO THE DAYS INTERVAL BETWEEN EVENTS
	_
23 Persistence of wind speed-interval	Annua

<b>3U4</b>	9
1 64.1N 166.7W W≥64 4333	2 63 6N 178.1W W≥64 4333
A ≥ 48 1 6-1 1 1 4333	A ≥ 48 1 1 1 24-1 2 5 5 4333
E ≥ 34	E ± 34 3 3 3 3 1 1 48-1 13 38 38 4333
28 1 1 1 1 1 1 1 42-1 5 17 17 4333	⊔≥28 6 8 6 3 5
£ <u>20 13 7 6 5 3 1 1 1 1 1 108-1 37 116 116 4333</u>	E ≥ 20 36 10 10 13 5 8 6 4 2 4 2 1 1 1 1 84-1 103 404 404 4334
1 ≥ 16 21 8 10 4 4 8 5 1 2 1 1 1	1 ≥ 16 25 11 16 5 15 11 9 9 6 4 11 3 1 2 1 7 132-1 136 832 839 4335
G ≥ 12 98 23 24 14 9 8 10 4 1 2 5 3 1 2 8 144-1 212 784 787 4335	$H \ge 12   51   12   17   6   11   9   8   9   16   3   6   4   7   7   3   24   252 - 1   193   1462   1526   4335  $
T≥ 9 60 16 30 6 22 11 14 10 8 8 7 7 11 7 6 26 216-1 249 1823 1832 4338	$T \ge 9   55   19   19   5   8   5   10   11   9   8   5   5   5   6   5   51   294 - 1   226   2248   2334   4337$
+ ≥ 6 36 8 10 14 4 10 11 6 5 9 5 3 2 6 7 60 870 - 1 196 3025 3149 4387	<sub>1</sub> ≥ 6   28   11   9   5   5   7   4   1   5   9   2   5   8   5   7   66   678 - 1   177   3118   3314   4382
$t \ge 3 \begin{bmatrix} 3 & 1 & 2 & 3 & 1 & 1 & 4 & 4 & 2 & 1 & 2 & 2 & 2 & 1 & 1 & 48 & 1980 - 1 & 78 & 4131 & 4371 & 4720 \end{bmatrix}$	$\frac{1}{2} \ge 3 \ \frac{10}{2} \ \frac{2}{3} \ \frac{4}{4} \ \frac{2}{2} \ \frac{1}{2} \ \frac{2}{4} \ \frac{4}{1} \ \frac{3}{3} \ \frac{1}{1} \ \frac{1}{1} \ \frac{1}{57} \ \frac{1038-1}{1038-1} \ \frac{92}{92} \ \frac{3795}{3795} \ \frac{4210}{4210} \ \frac{4566}{4566}$
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T TE TH HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS
3 59.4N 172.0W	4 58.0N 167.0M
₩ ≥ 64 A ≥ 48	₩≥64 4333
V = 10	$\begin{picture}(20,0) \put(0,0){\line(1,0){16}} \put(0,0$
E ≥ 34   6   3   5   4   1   1   1   1   1   1   1   2   1   1	≥ 28 9 8 11 14 6 4 1 3 1 1 1 1 78-1 59 232 232 4333
H = 20 20 13 19 13 17 11 9 7 4 5 4 2 3 3 1 4 198-1 135 763 775 4332	H = 20 11 19 19 9 17 13 12 11 4 3 5 7 1 3 1 4 144-1 139 834 834 4340
1 £ 16 24 16 11 9 13 11 24 8 11 6 10 7 4 2 3 15 216-1 174 1322 1341 4333	1 ≥ 16 18 17 9 9 16 12 9 12 12 10 7 3 9 3 3 18 318-1 167 1382 1383 4341
$G_{H} \ge 12$ 20 9 11 15 14 13 6 11 13 8 7 9 2 7 6 41 426-1 192 2072 2116 4347	G ≥ 12 22 10 12 12 10 15 11 7 12 6 6 7 6 5 5 45 378-1 191 2144 2177 4350
T≥ 9 6 9 9 8 5 12 5 9 11 6 7 3 4 6 4 65 546-1 169 2740 28\$7 4383	T≥ 9 15 9 7 8 11 10 16 4 9 8 9 2 1 5 3 66 840 - 1 183 2949 3021 4409
<u>3 6 13 3 5 5 5 4 8 5 4 6 4 4 1 1 1 68 912-1 137 3260 3642 4445</u>	1 ≥ 6 14 4 3 6 2 4 2 5 4 2 2 4 3 3 67 1440-1 125 3606 3869 4470
t ≥ 3 2 3 3 1 1 1 1 2 2 45 1584-1 60 3783 4731 4923	t ≥ 3 5 1 3 4 1 1 1 1 31 SEA-1 47 3973 4888 4984
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T T+ TH HOURS DURATION OF EVENTS	6 12 18 24 30 36 42 48 54 50 66 72 78 84 90 96+ MAX TE T TA TH HOURS DURATION OF EVENTS
5 56.8N 174.8E	6 52.0N 172.9E
W≥64 4333	₩ ≥ 64 4333
A≥48 1 1 1 1 1 24-1 4 10 10 4333	V≥48 2 1 2 18-2 5 10 10 4333
E ≥ 34 15 7 6 12 6 1 7 2 2 1 1 108-1 60 242 242 4333	E ≥ 34 9 16 11 5 8 5 1 2 1 54-1 58 196 201 4333
L ≥ 28 14 11 17 9 13 10 4 2 1 2 4 1 1 1 1 7 168 - 1 97 547 553 4333 E ≥ 20 19 13 13 13 10 18 70 20 11 5 5 6 4 4 5 15 234 - 1 171 1364 1389 4334	H ≥ 28   15   16   10   10   14   10   6   3   4   1   1   2   4   108 - 2   96   464   480   4333 F ≥ 20   27   26   19   12   11   11   15   13   11   5   7   2   1   4   6   14   216 - 1   184   1236   1272   4339
£ £20 19 13 13 13 10 10 6 10 20 77 5 3 6 4 4 5 13 234-7 17 1 1364 1389 4334 1 ≥ 16 14 12 12 10 10 6 15 15 11 15 4 4 6 5 5 40 318-2 184 2051 2115 4349	$E \ge 20$   27   26   19   12   11   11   15   13   11   5   7   2   1   4   6   14   216 - 1   184     1236     1272     4339     $\ge$ 16   21   12   15   20   4   14   16   13   11   11   8   11   4   7   1   36   240 - 1   204     1904     1971     4339
G ≥ 12 10 6 8 13 2 4 5 5 5 8 8 7 3 3 4 66 546-1 157 2817 2952 4380	$G = 12 \ 23 \ 16 \ 8 \ 10 \ 9 \ 5 \ 8 \ 9 \ 5 \ 6 \ 5 \ 6 \ 8 \ 7 \ 6 \ 66 \ 390 - 1 \ 197 \ 2792 \ 2889 \ 439C$
T≥ 9 15 8 6 6 3 5 2 4 2 1 3 3 5 3 1 65 714-1 132 3358 3567 4404	T≥ 9 10 8 5 5 8 4 4 4 7 4 4 4 6 3 2 77 816-1 155 3551, 3670 4431
<u>  ≥ 6 8 2 2 2 5 2 4 2 2 1 52 1914-1 82 3613 4112 4455</u>	, ≥ 6 8 3 2 1 2 2 3 1 1 2 53 1602-1 78 3921 4322 4605
1 ≥ 3 2 1 1 1 20 SEA-2 25 3475 4807 4859	t ≥ 3 1 1 18 SEA-4 19 3496 4719 4750
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T 74 TH HOURS DURATION OF EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T T+ TH HOURS DURATION OF EVENTS
7 54.7N 175.9W	8 54.9N 167.2W
₩≥64	W≥64 433:
○≥48 1 4 4 4333	V≥48 1 433
E ≥ 34   8   5   3   5   4   2   2     72-2   31   117   121   4333   ≥ 28   24   14   11   8   6   6   4   3   1   2   1   2   1   90-1   83   318   322   4333	E ≥ 34 7 6 9 1 1 30-1 24 55 65 433° ≥ 28 11 13 12 10 6 5 2 1 2 54-2 62 213 225 433°
_ ≥ 28 24 14 11 8 6 6 6 4 3 1 2 1 2 1 90-1 83 318 322 4333 = ≥ 20 22 12 15 17 13 19 9 8 6 6 8 2 5 6 1 7 156-1 159 1024 1029 4341	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
= 16 18 17 12 9 10 12 10 17 13 9 7 5 8 2 7 25 228 - 1 181 1569 1623 4344	1 ≥ 16 21 11 14 10 17 13 13 19 12 3 10 9 3 3 3 18 312-1 179 1397 1432 4339
2 + 12   8   17   10   13   11   7   7   4   9   11   13   4   6   7   2   56   432 - 1   185   2400   2495   4371	$\frac{G}{H} \ge 12$ 18 9 19 11 9 13 8 12 10 8 7 9 6 8 3 48 396 - 1 198 2275 2345 436
7 2 9 19 5 4 8 5 8 4 6 8 7 5 7 4 4 7 67 546-1 168 3093 3270 4406	$T \ge 9   19   9   5   9   10   6   13   6   10   9   4   3   2   6   1   68   426 - 1   180   2989   3140   4423$
≥ 6 11 1 7 6 1 4 1 3 1 2 4 1 2 61 1170 - 1 104 3747 4085 4535	<u>2 6 6 8 4 3 6 3 3 2 2 7 3 3 5 2 65 1140-1 122 3506 3977 4515</u>
t ≥ 3 1 3 1 23 SEA-3 28 3871 4909 4954	t ≥ 3 3 1 1 1 22 SEA-1 28 3828 5137 5196
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ WAX TE T TH TH HOURS DURATION OF EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T TO THE HOURS DURATION OF EVENTS
9 \$0.3N 171.3W	10 51.8N 167.3W
N ≥ 64 4332	W≥64 4332
7≥48 1 1 1 1 1 18-1 3 6 8 4332	ó48 111 18-1 2 5 8 4332
F ≥ 34 7 5 4 4 3 4 2 48-2 29 100 109 4332	E ≥ 34 10 4 7 1 1 2 2 42-2 27 74 85 4332
28 13 12 5 10 7 1 6 2 1 2 1 1 1 1 108 1 62 266 278 4332	≥ 28   16   12   15   8   7   2   4   2   3   1   1
E = 20 23 18 22 15 15 11 15 8 4 6 5 2 2 3 4 8 174-2 161 973 1002 4352	E ≥ 20 17 15 15 17 16 17 18 8 6 6 6 3 4 3 3 1 7 156~1 156 960 985 4352° 1≥ 16 18 18 12 9 14 17 17 17 9 9 6 4 9 4 3 30 186-1 196 1677 1719 436€
$G = 12 \ 21 \ 13 \ 11 \ 10 \ 12 \ 6 \ 4 \ 17 \ 9 \ 11 \ 11 \ 7 \ 9 \ 8 \ 3 \ 59 \ 318 - 1 \ 211 \ 2563 \ 2724 \ 4380$	$\frac{1}{2} = 10   18   18   12   9   14   17   17   7   9   9   6   4   9   4   3   30   186 - 1   196   1   187   17   19   436   6   \frac{1}{2} = 12   15   10   6   8   4   14   7   6   10   7   4   9   12   6   7   64   426 - 1   189   2620   27   19   4407   1   1   1   1   1   1   1   1   1   $
T ≥ 9 15 10 9 6 5 2 9 2 2 6 3 4 4 2 3 78 900 - 1 160 3360 3644 4486	T≥ 9 13 13 7 8 3 3 3 5 3 7 6 2 6 7 2 78 762-1 166 3294 3499 4455
≥ 6 4 2 1 3 4 1 1 2 1 2 59 1356 - 1 80 3608 4478 4721	<u>2</u> 6 2 3 1 2 3 3 2 1 2 2 2 1 67 1686 - 1 89 3752 4435 4 25
≥ 3 1 1 16 SEA-4 17 3545 5114 5141	t ≥ 3 2 1 1 1 15 SEA-4 19 3176 4898 4928
5 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T Te TH	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T TO TH
HOURS DURATION OF EVENTS  11 51.3N 158.8W	HOURS DURATION OF EVENTS 12 54.4N 158.1W
W≥64 1 6-1 1 1 4333	₩≥64 4333
A ≥ 48 1 3 1 1 30-1 6 15 15 4333	A≥48 2 2 1 1 3 30~1 6 15 15 4333
E ≥ 34   11   9   8   5   4   3     1	E ≥ 34 8 10 5 B 4 1 1 1 1 78-1 38 123 123 4333
<u>228   11   11   14   21   12   6   4   1   5   1     1   96   1   87   362   364   4333   </u>	H ≥ 28 15 10 8 14 11 12 5 3 2 1 1 84~1 82 349 349 4333
E ≥ 2C 23 17 16 10 7 17 17 8 14 8 9 5 1 6 3 12 138-1 173 1202 1209 4366	E ≥ 20 25 16 10 17 B 16 9 14 5 2 7 7 6 1 3 11 13B-1 157 1035 1043 4341
2 16 20 20 17 21 10 10 8 13 8 3 16 10 9 7 5 31 342-1 208 1887 1914 4376	1 ≥ 16 23 24 16 6 10 10 11 15 9 11 4 6 8 3 3 3 32 216-1 191 1649 1667 4372
H 2 12 17 20 6 15 10 13 7 8 7 10 9 6 6 4 10 62 414-1 210 2701 2762 4414- T 2 9 10 7 6 7 5 8 7 6 7 2 2 2 5 6 76 834-1 156 3359 3551 4484	
T ≥ 9 10 7 6 7 5 8 7 6 7 2 2 2 5 6 76 834-1 156 3359 3551 4484 ≥ 6 6 4 5 6 7 3 2 2 1 2 1 2 2 1 158 1530-1 102 3944 4370 4782	$T \ge 9 \ 21 \ 10 \ 13 \ 13 \ 9 \ 6 \ 7 \ 5 \ 3 \ 5 \ 2 \ 3 \ 4 \ 3 \ 6 \ 80 \ 492 - 1 \ 190 \ 3269 \ 3364 \ 4456$ $\searrow 6 \ 12 \ 6 \ 2 \ 3 \ 4 \ 7 \ 4 \ 3 \ 3 \ 4 \ 2 \ 2 \ 3 \ 1 \ 61 \ 1566 - 1 \ 117 \ 3907 \ 4157 \ 4626$
2 5 6 4 5 6 7 5 2 2 1 2 1 2 2 1 361530 102 3944 4370 4782 2 3 1 1 1 1 1 18 SEA-6 21 3738 5010 5050	(± 3 1 3 1 1 1 25 SEA-3 31 4036 5094 5145
6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TE T T+ TH	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T TH TH
HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS
/inter	23 Persistence of wave height-duration

e			
1 64.1N 166.7W W ≥ 64 8 SEA-8 8 2944 4389 4389	2 63.6N 178.1W ₩≥64 8 5EA-8 8 2944 4389 4389		
0 SEA-8 9 3081 4526 4527	\$\frac{1}{\sqrt{248}}\$		
E ≥ 34 1 9 SEA-8 10 3076 4521 4530	E ≥ 34 2 1 1 1 1 1 13 SEA-8 19 3650 4888 4926		
1 2 9 SEA-8 12 3086 4531 4548	H ≥ 28 1 1 1 1 1 2 1 1 1 1 2 2 3 6028		
E ≥ 20 4 1 3 1 2 2 2 1 1 2 25 SEA-2 39 3684 5027 5143	C ≥ 20 10 6 4 4 6 3 2 1 2 3 3 4 1 1 53 SEA-1 103 4053 4621 5024		
1 ≥ 16 5 5 1 4 1 1 3 1 3 2 1 1 1 40 SEA-1 69 4073 4867 5146	G≥ 16 13 4 10 4 4 5 2 7 2 2 3 4 3 3 71 1032-1 137 3652 3916 4753		
H 2 2 37 20 20 7 4 6 9 6 3 10 8 2 1 1 1 8 73 13 14 - 1 2 15 3 3 3 5 3 5 1 4 6 9 6	H≥ 12 29 7 21 6 10 7 10 8 8 8 8 5 3 8 3 6 59 618-1 198 2984 3060 4584 T≥ 9 55 19 14 14 10 12 12 8 8 12 8 5 4 3 4 40 498-1 228 2080 2117 4447		
T≥ 9 65 13 17 11 8 16 13 11 6 8 12 8 5 4 4 4 49 378 - 1 250 2497 2596 4423 ≥ 6 4123 19 11 14 8 10 11 14 6 4 4 6 3 4 15 252 - 1 193 1246 1270 4365	$T \ge 9   55   19   14   14   10   12   12   8   8   12   8   5   4   3   4   40   498 - 1   228   2080   2117   4447   4447   444   22   19   10   13   9   12   7   6   4   2   3   4   1   2   16   324 - 1   174   1084   1108   4373  $		
$\begin{array}{c} \geq 6 & 41 & 23 & 19 & 11 & 14 & 8 & 10 & 11 & 14 & 6 & 4 & 4 & 6 & 3 & 4 & 15 & 252-1 & 193 & 1246 & 1270 & 4365 \\ t \geq 3 & 15 & 10 & 15 & 5 & 6 & 2 & 6 & 1 & 3 & 4 & 1 & 1 & 1 & 1 & 1 & 1234-1 & 72 & 350 & 360 & 4344 \end{array}$	t ≥ 3 25 12 11 8 5 7 1 5 4 2 1 1 2 138 - 1 84 352 362 4339		
6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T T# TH	6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T T+ TH		
HOURS INTERVAL BETWEEN EVENTS 3 59.4N 172.0W	HOURS INTERVAL BETWEEN EVENTS 4 58.0N 167.0W		
W≥64 7 SEA-7 7 2576 4379 4379	W≥64		
A ≥ 48 9 SEA-7 9 3008 4675 4678	A≥48 1 1 11 SEA-8 12 3528 4973 4982		
E ≥ 34	E ≥ 34 1 2 1 1 2 2 24 SEA-7 31 4643 5928 6009		
H ≥ 28 2 1 2 2 2 2 2 1 1 1 1 1 38 SEA-5 55 4838 5776 5986	H ≥ 28 2 3 2 4 1 3 1 2 1 1 2 42 SEA-4 64 4303 5625 5857		
E ±20 6 9 7 4 6 8 12 2 5 4 2 3 7 1 1 62 SEA-1 139 3943 4233 5007	E ≥ 20   13   6   5   5   5   10   5   3   6   4   2   4		
	I ≥ 16     13     9     7     8     12     14     8     4     4     4     6     6     5     564-1     170     2913     3082     4457       H≥ 12     21     16     15     13     16     12     12     7     8     9     9     2     5     1     5     42     438-1     193     2139     2244     4404		
$H \ge 12$ 23 16 19 13 14 19 7 6 5 3 4 8 5 3 2 47 510-1 194 2275 2333 4433 $H \ge 9$ 21 21 18 11 12 11 11 7 8 7 4 3 5 5 2 25 486-1 171 1535 1558 4363	T≥ 9 25 16 24 15 15 17 7 8 7 9 10 4 2 2 3 18 366-1 182 1379 1417 4362		
≥ 6 25 21 18 10 15 6 5 5 4 4 4 4 1 4 2 7 330-1 135 803 817 4345	2 6 27 20 13 18 12 5 9 5 3 1 1 1 5 318-1 120 602 611 4343		
<u>1</u> ≥ 3 17 10 6 6 2 3 2 1 3 2 1 102-1 53 193 194 4333	t ≥ 3 20 7 5 1 4 1 2 48-2 40 96 97 4334		
6 12 18 24 30 36 42 46 54 60 66 72 78 84 90 96+ MAX TI T T4 TH HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 36 42 48 54 50 56 72 78 84 90 96+ MAX TI T TA TH HOURS INTERVAL BETWEEN EVENTS		
5 56.8N 174.8E	6 52.0N 172.9E		
W≥64 8 SEA-8 8 2944 4389 4389	₩≥64 8 SEA-8 8 2944 4389 4389		
V≥48 1 1 11 SEA-8 12 3502 4947 4957	\$\frac{1}{2} \geq 48		
E ≥ 34   3   1   2   1   1   2   1   1   2   3   46   SEA - 5   63   4971   6078   6320   ≥ 28   4   4   3   2   1   4   9   1   3   3   6   2   2   3   54   SEA - 3   101   4439   4834   5387	E ≥ 34 1 3 2 2 3 1 1 4 4 1 2 1 2 1 2 2 42 SEA-2 67 4563 5047 5248 ≥ 28 6 4 4 4 1 5 4 4 2 4 3 7 3 1 53 SEA-1 105 4068 4378 4858		
M ***   <u>-+</u>	H ≥ 28 6 4 4 4 4 1 5 4 4 2 4 3 7 3 1 53 SEA-1 105 4068 4378 4858 E ≥ 20 18 12 8 9 8 11 10 16 6 2 5 6 3 3 6 66 504-1 189 3036 3183 4449		
E \(\frac{2}{2}\) \( \begin{array}{c c c c c c c c c c c c c c c c c c c	l ≥ 16 25 24 13 15 12 9 10 9 10 5 8 5 3 8 2 51 462~1 209 2366 2455 4420		
G ≥ 12 15 20 17 10 12 7 7 10 7 7 7 4 6 3 1 23 354-1 156 1398 1475 4380	G ≥ 12 26 25 23 17 9 12 9 16 5 8 3 3 8 2 4 27 228 1 197 1505 1554 4386		
T≥ 9 23 17 9 16 10 8 9 7 4 3 3 4 2 14 222-1 129 849 879 4375	T≥ 9 38 22 14 13 10 7 10 8 5 5 2 5 2 2 2 2 5 126~2 150 755 772 4344		
<u>1 ≥ 6 22 8 9 9 6 2 5 4 4 4 2 1 1 1 108-1 78 351 351 4341</u>	$f \ge 6 \ 16 \ 19 \ 6 \ 5 \ 8 \ 6 \ 2 \ 3 \ 3 \ 1 \ 1 \ 3$		
$\frac{1}{2}$ 3 $\frac{7}{4}$ $\frac{4}{3}$ $\frac{1}{1}$ $\frac{1}{2}$ $\frac{2}{2}$ $\frac{1}{2}$ $\frac{48-2}{19}$ $\frac{19}{57}$ $\frac{57}{57}$ $\frac{4338}{4338}$	$t \ge 3 \boxed{4} \boxed{2} \boxed{4} \boxed{1} \boxed{1} \boxed{1} \boxed{1} \boxed{48-1} \boxed{12} \boxed{32} \boxed{32} \boxed{4334}$		
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS		
7 54.7N 175.9W ₩≥64	8 54.9N 167.2W W≥64 7 SEA-7 7 2576 4379 4379		
V≥48 9 SEA-8 9 3077 4522 4526	A≥48 8 SEA-8 8 2944 4394 4395		
E # 34 2 1 2 1 1 1 2 1 1 1 28 SEA-8 40 4812 5518 5639	E ≥ 34 1 1 1 1 1 1 1 26 SEA-7 32 4894 6056 6121		
H ≥ 28 6 5 2 2 2 2 1 2 3 2 1 4 2 3 52 SEA-5 89 5101 5380 5702	H ≥ 28 1 1 3 2 2 3 1 5 1 2 1 45 SEA-3 67 4412 5772 5997		
E ≥ 20 12 9 11 6 11 9 4 5 8 5 6 3 3 3 2 64 846-1 161 3288 3464 4485	£ ≥20 4 13 5 3 5 7 6 3 5 3 6 3 3 3 69 762-1 138 3527 3766 4585		
G = 16 18 11 11 10 15 8 11 13 5 12 3 4 2 2 3 58 822-1 186 2719 2796 4408 G = 18 11 12 13 15 12 3 4 2 2 3 58 822-1 186 2719 2796 4408			
$\frac{1}{1} \ge 12 \   23 \   20 \   9 \   21 \   17 \   17 \   5 \   8 \   4 \   6 \   9 \   5 \   3 \   3 \   34 \   594-1 \   187 \   1876 \   1905 \   4362 \  $ $1 \ge 9 \   33 \   18 \   25 \   15 \   5 \   9 \   15 \   4 \   7 \   4 \   3 \   4 \   2 \   4 \   5 \   15 \   378-1 \   168 \   1151 \   1151 \   1151 \   4348 \  $	H≥ 12   22   19   21   14   18   6   8   12   10   9   7   7   6   5   3   32   456-1   199   1984   2084   4393   1 ≥ 9   29   29   19   23   10   10   11   7   8   7   7   1   3   2   1   17   324-1   180   1250   1290   4338		
$T \ge 9 \   33 \   18 \   25 \   15 \   5 \   9 \   15 \   4 \   7 \   4 \   3 \   4 \   2 \   4 \   5 \   15 \   378 - 1 \   168 \   1151 \   1151 \   1151 \   4348 \  $ $\ge 6 \   24 \   15 \   12 \   8 \   12 \   7 \   1 \   4 \   6 \   2 \   2 \   2 \   1 \   3 \   132 - 1 \   99 \   454 \   454 \   4337 \  $	≥ 6 24 25 18 14 11 5 7 3 1 2 2 1 1 1 4 216-1 119 520 541 4334		
3 11 4 4 1 1 1 66-1 21 46 46 4334	(≥ 3 11 6 1 1 2 48 -2 21 49 59 4331		
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TI T TA TH	6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T THE TH		
HOURS INTERVAL BETWEEN EVENTS 9 50.3N171.3W	HOURS INTERVAL BETWEEN EVENTS 10 51.8N 167.3W		
W≥64 7 SEA-7 7 2576 4380 4380	₩≥64 7 SEA-7 7 2576 4380 4380		
A≥48 1 1 11 SEA-8 12 3521 4966 4974	V≥48 1 1 10 SEA-8 11 3222 4667 4675		
E = 34	E ≥ 34 2 1 1 1 1 2 1 1 1 2 24 SEA-6 34 4578 5971 6056 ≥ 28 4 1 4 5 1 2 1 3 1 1 1 2 2 50 SEA-2 77 4554 5284 5554		
H ≥ 28 3 1 3 3 3 1 2 1 1 1 1 1 2 45 SEA-1 69 4104 4662 4940 E ≠ 20 10 12 7 5 6 9 4 4 8 7 5 6 5 5 72 828-1 165 3373 3538 4520	H ≥ 28   4   1   4   5   1   2   1   3   1   1   2   2   50   SEA - 2   77   4554   5284   5554   6 ≥ 20   15   7   10   6   5   5   6   4   3   6   6   4   6   4   2   71   702 - 1   160   3351   3574   4539		
1 ≥ 16 30 17 17 12 13 8 9 7 9 12 8 6 8 2 55 504-1 213 2628 2711 4444	l ≥ 16 24 7 11 14 11 10 9 9 9 6 12 5 6 6 5 54 492-1 198 2599 2754 4439		
G ≥ 12 34 27 20 18 14 9 17 4 6 6 12 5 2 1 7 30 252-1 212 1645 1686 4362	$ G \\ H \ge 12 \\ 19 \\ 23 \\ 20 \\ 11 \\ 11 \\ 19 \\ 12 \\ 7 \\ 13 \\ 10 \\ 8 \\ 3 \\ 1 \\ 3 \\ 4 \\ 26 \\ 420 \\ -1 \\ 190 \\ 1706 \\ 1729 \\ 4373 \\ 1706 \\ 1729 \\ 1706 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1729 \\ 1706 \\ 1706 \\ 1729 \\ 1706 \\ $		
$T \ge 9  36 21 12 19 12 12 8 7 8 5 3 3   3 2 6 204-1 157 841 843 4333 $	T≥ 9 35 17 17 17 16 17 8 6 7 1 2 5 3 1 1 11 240-1 164 946 958 4334		
<u>1 6 25 14 9 9 7 2 3 3 1 1 1 1 96 1 75 243 243 4332</u>	r ≥ 6 28 13 14 9 3 3 4 1 2 1 1 1 1 1 108-1 82 289 290 4332		
$t \ge 3   5   2   1   1                            $	$\frac{1}{2} \ge 3 \begin{bmatrix} 7 & 1 & 1 & 2 & 1 & 1 & 1 & 60-1 & 12 & 30 & 30 & 4332 \\ 6 & 12 & 18 & 24 & 30 & 36 & 42 & 48 & 54 & 50 & 66 & 72 & 78 & 74 & 90.95 & MAX & T1 & T & T9 & TH & T1 & T1 & T9 & T1 & T1 & T1 & T1 & T1$		
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS		
11 51.3N 158.8W ₩≥64 1 8 SEA-8 9 2948 4393 4394	12 54.4N 158.1W W≥64 8 SEA-8 8 2944 4389 4389		
W≥64 1 8 SEA-8 9 2948 4393 4394 A≥48 1 2 11 SEA-8 14 3796 5241 5256	A≥48 1 1 12 SEA-7 13 3610 5171 5186		
E ± 34 2 2 1 1 1 1 40 SEA-5 47 4394 5633 5758	E ≥ 34		
≥28 5 3 3 2 5 1 3 4 2 3 1 1 2 1 57 SEA-1 93 4121 4950 5314	H ≥ 28 3 2 5 4 1 1 3 1 1 1 2 4 1 2 2 55 1512-1 88 4066 4725 5074		
E ≥ 20 14 16 8 15 9 6 3 7 2 2 7 4 4 4 1 77 582-1 179 3166 3298 4474	E ≥ 20 12 14 7 7 8 8 4 7 7 3 1 3 3 3 3 71 738-1 161 3322 3475 4510		
1 2 16 25 21 16 14 11 8 15 7 10 7 8 8 3 5 8 47 498-1 213 2502 2562 4433	$  \ge   16   25   16   11   8   12   10   8   6   7   6   9   5   4   4   60   450 - 1   195   2742   2801   4429   60   60   60   60   60   60   60   6$		
H = 12 26 24 33 20 12 16 7 11 11 4 5 8 3 3 3 22 4 4 4 ~ 1 206 1642 1669 4370	H = 12 [29   22   31   16   15   9   11   9   10   10   5   4   6   1   4   30   396 - 1   212   1826   1863   4333		
T = 9 35 25 14 10 9 12 11 8 2 4 3 4 1 2 11 270~1 151 903 934 4334 = 6 24 23 10 9 11 3 2 2 2 5 2 4 144~1 97 406 412 4333	T ≥ 9 38 30 25 15 12 13 14 4 4 6 3 1 4 2 1 12 276-1 184 1068 1093 4334 ≥ 6 23 24 15 13 8 7 5 3 3 2 2 2 3 1 180-1 109 456 470 4334		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	\$\frac{1}{2} \frac{1}{3} \frac{1}{11} \frac{7}{2} \frac{1}{1} \frac{2}{2} \frac{1}{3} \fra		
6 12 18 24 30 36 42 48 54 80 66 72 78 84 90 96+ MAX TI T TA TH	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TI T TH		
HOURS INTERVAL BETWEEN EVENTS HOURS INTERVAL BETWEEN EVENTS  Winter  3 Parsistance of wave height-interval  Winter			
23 Persistence of wave height-interval	Winter		

	FOR	
- 21	I-SUO	

, 64.1N 166.7W	2 63.6N 178 IW
4241	₩≥64
"=04	A ≥ 48 4241
V <sup>≤40</sup>	E ≥ 34
C ± 34	≥28 1 1 1 1 1 1 1 1 42-1 5 19 19 424:
H \$28	F≥20 7 2 4 3 1 1 1 1 1 72-1 20 67 67 4241
E = 20   2   2   63   63   4241	1 ≥ 16 8 4 1 7 2 4 1 3 1 1 1 B4-1 33 147 147 424 1
6 10 / 3 3 3 / 1 / 1 + + + + + + + + + + + + + + + +	G ≥ 12 19 6 3 9 5 5 4 4 2 2 2 1 4 2 138-1 68 355 359 4241
H = 12 10 0 3 10 2 2 1 1 1 1 578 579 4741	T≥ 9 22 8 11 7 7 7 8 7 3 6 2 4 3 3 8 186-1 106 708 728 4241
1 £ 9 [36 [4] 11 [12] / [B ] / [3 [0] 3 [2 [2 [3 ]]	≥ 6 31 9 12 9 7 8 7 1 8 10 7 4 10 5 1 24 306-1 153 1370 1431 4244
£ 6 49 16 6 13 11 10 10 10 10 10 10 10 10 10 10 10 10	1 ≥ 3 20 16 7 8 5 8 13 9 4 5 7 4 9 7 5 56 672-1 183 2515 2735 4265
(= 3[34]77[0]13[9]3]10[0]0]0]0]0]	6 17 18 24 30 36 42 48 54 60 66 72 78 d4 90 46+ MAX TE T Te TH
HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS 58.0N 167.0W
3 23.44 17.04	W≥64 4241
W≥64 4241	V≥48 424'
A≥48 4241	V = 40 E ≥ 34 1 1 1 12-1 2 3 3 4241
E ≥ 34 2 1 18-1 3 7 7 4241	_ 5 \$ J* ( '   '   1   1   1   1   1   1   1   1
≥ 28 2 2 1 2 30-2 7 10 19 4241	228 4 2 3 2 1 3 36-1 12 31 31 4241 E 20 11 6 6 4 5 4 5 2 2 1 1 66-1 47 196 20: 424
E € 20 B   1 6 3 3 3 3 1 2	1 \ge 16 10 13 10 8 7 6 13 4 4 1 2 1 2 96-2 81 407 417 424
\$16 3 9 10 10 3 4 7 3 3 3 1 1	GH ≥ 12 7 7 11 10 B 10 14 12 7 11 7 2 1 5 5 126-1 117 B37 B63 424
H E I Z   0 / 0 / 12 9 7 10 9 3 2 0 3 1 10 2 10 2 10 2 10 2 10 2 10 2	T≥ 9 16 11 9 12 5 11 10 8 6 10 10 10 6 8 3 18 312-1 153 1389 1450 424.
9 16 8 16 12 10 0 0 0 9 0 11 3 3 4 4 13 330	≥ 6 19 9 10 8 9 8 7 7 10 6 10 5 6 6 4 55 348-1 179 2235 2334 4250
§ 6120 9 1 7 19 10 10 13 11 10 10 10 1 7 1 1 10 10 10 1 1 1 10 10 10 10 10 10 10	{ ≥ 3 17 9 3 3 5 4 1 2 8 4 5 2 2 8 2 59 1200-1 :34 3374 3641 4335
t ≥ 3 12 6 3 4 7 3 4 5 2 4 3 2 5 5 9 63 1056 - 1 137 3091 3338 4334	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAY TC T TH
HOUSE DURATION OF EVENTS	HOURS DURATION OF EVENTS 52.0N 172.9E
5 36.dN 1/4.0L	W≥64 424:
W≥64 4241	" <b>6</b> 04 )
A ≥ 48 4241	V <sup>240</sup>
E ≥ 34 2 1 24-1 3 8 8 4241	C ± 34 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
≥ 28 4 3 1 2 2 31 31 4241	H = 28   10   3   7   7   7   7   7   7   7   7   7
E ≥ 20 5 2 9 9 6 5 5 2 4 1 60-1 48 229 229 4241	=======================================
≥ 16 11 8 8 2 10 14 7 2 3 4 5 1 1 84-1 76 406 407 4241	G = 12 16 14 11 10 15 14 111 4 1 7 3 6 4 2 1 2 1 90-1 105 537 539 42-1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
$\frac{6}{12} \ge 12 \ 11 \ 9 \ 12 \ 11 \ 6 \ 10 \ 7 \ 12 \ 10 \ 7 \ 6 \ 3 \ 3 \ 5 \ 5 \ 162 - 1 \ 117 \ 815 \ 824 \ 4241$	T≥ 9 19 13 8 9 9 13 15 5 9 7 4 8 6 4 7 33 240-1 169 1049 1711 421
T≥ 9 8 7 9 6 9 12 6 7 10 4 8 5 10 7 2 24 318-1 144 1370 1405 4241	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
<u>, ≥ 6 11 16 9 7 10 6 9 7 6 4 7 4 4 5 1 54 624-1 160 2132 2293 4256</u>	≥ 6 22 12 14 9 3 8 9 6 5 3 8 3 4 4 6 59 6 2 1 1 5 8 12 18 - 1 16 3436 3917 4494 ≥ 3 13 4 3 3 4 3 4 2 5 2 3 2 8 1 1 58 12 18 - 1 116 3436 3917 4494
1 ≥ 3 19 7 7 3 2 3 7 3 1 3 5 1 5 3 1 54 1584-1 124 3055 3569 4361	6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TE T TA TH
HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS 54.9N 167.2W
7 54./N 1/3.9W	₩≥64 424'
W≥64 4241	
A≥48 4241	$     \begin{array}{c cccccccccccccccccccccccccccccccc$
E = 34 1 1 3 18-3 5 12 12 4241	30 424
3 4 2 3 1 1 54-1 14 47 47 4241 3 1 1 54-1 14 47 47 4241	
E = 20 8 11 8 11 7 3 3 4 2 1 60-1 58 232 232 4241	1 ≥ 16 18 11 18 9 7 10 11 3 3 3 4 1 1 114-1 98 446 459 424
2 16 15 12 19 11 7 7 9 6 3 4 6 1 1 102-1 91 460 462 4241	G 2 12 18 10 11 12 14 7 12 9 13 11 6 4 1 5 2 7 132-1 142 968 992 424
212 (18/10) 18/19/8 / 6 6 13 / 2 9 6 1 2 6 180-1 130 900 923	$T \ge 9 \ 21 \ 13 \ 7 \ 8 \ 18 \ 10 \ 7 \ 12 \ 11 \ 8 \ 11 \ 8 \ 8 \ 4 \ 7 \ 25 \ 252 - 1 \ 178 \ 1585 \ 1620 \ 424$
$7 \ge 9$ 27 14 7 7 14 19 9 6 7 4 7 9 3 9 3 25 282-1 170 1495 1566 4247	≥ 6 16 4 12 7 15 11 5 5 7 4 8 3 10 3 1 68 474-1 179 2530 2626 4260
2 6 33 6 13 6 11 9 9 6 8 5 4 8 4 7 2 55 444-1 186 2311 2490 4288	2 3 13 10 3 5 5 1 1 1 2 6 1 1 4 2 2 62 1194 - 1 119 3347 3765 433
( E 3 10 14 14 1 13 1 1 1 2 1 3 1 2 1 2 1 2 1 2 1 2 1	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T
HOUSE DISATION OF FVENTS	HOURS DURATION OF EVENTS
9 50.34 171.34	10 51.8N 16/ 3W W≥64 4.4
W≥64 4241	7 = 04
$\stackrel{\wedge}{\downarrow} \ge 48$ $\stackrel{1}{\downarrow}$	V≥48 E ≥34 2 1 1 1 42-1 4 13 14 42-1
$\xi \ge 34$ 2 1 1 2 42-2 6 22 23 4241	E 5 3 4 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
≥28 9 8 2 1 4 1 1 1 60-1 26 73 75 4241	\(\frac{28}{6} \) 6 6 6 4 2 2 1 1 1 1 60-1 22 63 6 42 8 424 8 8 4-1 65 274 28 424
E 20 116 12 9 14 67 67 67 67 67 67 67 67 67 67 67 67 67	E € 20 17 17 7 8 9 4 0 3 3 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
\$ 16 13 20 6 6 7	G≥12 14 11 14 6 6 12 10 3 8 11 9 11 4 4 6 15 246-1 144 1233 1265 424
H = (2)14 17 (2) 9 7 (13) 8 4 11 9 1 7 (8) 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	T≥ 9 21 9 10 11 14 8 8 8 13 10 10 9 8 1 3 37 324-1 180 1854 1954 4.
2313 14 252	≥ 6 14 10 7 5 7 5 5 6 3 7 4 8 4 7 10 58 528-1 '60 2"56 29' 4
1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1 ≥ 3 7 1 4 4 5 2 2 1 2 1 2 52 1476-1 83 3349 3969 44.
2 3 6 5 1 2 4 4 1 2 2 3 1 2 2 48 1476-1 83 3065 3915 4356	5 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 95 + MAX TE
HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS 12 54.4N 158 1 W
11 51.3N 158.8W	W≥64
W ≥ 64 4241	V ≥ 48
A≥48 4241	V ≤ 40 E ≥ 34 1 2 1 3 24-3 7 20 20 424
E ≥ 34 1 2 2 1 1 1 1 36-1 8 26 26 4241	≥ 28 2 4 6 4 1 1 3 1 48-1 22 84 84 424 1
≥ 28 3 3 6 2 5 2 1 54-1 22 85 85 4241	H ≥ 28 2 4 6 4 1 1 3 1
20 17 11 20 8 8 7 6 8 4 1 2 1 96-1 93 409 414 4241	I ≥ 16 22 10 15 11 11 10 9 8 6 5 7 4 2 1 3 126 - 1 124 697 715 424 1
≥ 16 14 15 17 12 17 5 17 4 11 6 7 1 1 2 5 126~1 134 792 806 4241	H ≥ 12 16 9 15 11 12 16 7 9 8 10 8 5 2 1 2 26 192-2 157 1339 136 424
S ≥ 12 16 4 21 14 9 14 10 8 13 8 10 5 6 2 1 21 330-1 162 1456 1498 4241	T≥ 9 17 15 12 5 4 8 10 8 8 8 5 6 11 6 5 39 348-1 167 1901 2001 4244
$7 \ge 3 \frac{15}{12} \frac{13}{13} \frac{9}{13} \frac{13}{8} \frac{8}{7} \frac{7}{11} \frac{17}{7} \frac{7}{7} \frac{8}{8} \frac{8}{8} \frac{5}{5} \frac{5}{43} \frac{432}{432} \frac{178}{178} \frac{2116}{12} \frac{2211}{12} \frac{4243}{12}$	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
2 6 10 5 6 4 5 9 8 9 9 6 6 7 3 5 4 60 714-1 156 2906 3180 4282	$\stackrel{\geq}{}$ 6 21 12 11 9 4 8 15 6 6 5 2 5 4 5 6 62 576 1 187 2 26 2534 4 2 5 $\stackrel{\geq}{}$ 2 3 7 2 3 4 1 3 1 2 2 1 1 4 1 2 50 1314 1 84 3233 3959 4342
+≥ 3 1 1 2 2 2 1 2 1 2 1 1 1 1 3 (43)(524-1) 62   3377   4130   <del>442</del> 3	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T To TH
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T TO THE HOURS DURATION OF EVENTS	HOURS DURATION OF EVENTS
	23 Persistence of wave height-duration
WASTIELD I	—— — · · · · · · · · ·
Spring	

t 64.1N 166.7W	2 63 6N 178.1W
W≥64 6 SEA-6 6 2208 4265 4265	W≥64 6 SEA-6 6 2208 4265 4265
Ç≥46 6 SEA-6 6 2208 4265 4265	A≥48 6 SEA-6 6 2208 4265 4265
E ≥ 34 7 SEA-6 7 2256 4262 4265	E ≥ 34
≥28 7 SEA-6 7 2256 4261 4265	H ≥ 28 27 11 2878 4365 4364
€ ≥ 20     1     12 SEA-5 13 2716 4464 4485       1 ≥ 16 1     1     2     120 SEA-5 24 3252 4975 5038	$\xi \ge 20 \ 1$
G ≥ 12 8 2 1 2 3 1 3 1 1 31 SEA-3 53 3796 4871 5096	1 ≥ 16     3     1     1     1     1     3     3     25     SEA-5     37     3931     4732     4879       H≥ 12     4     1     4     1     1     1     1     1     1     1     1     4     1     1     1     2     1     43     SEA-3     71     4119     4736     5095
T≥ 9 15 3 7 4 3 3 1 7 2 5 2 6 2 1 6 55 SEA-1 122 4248 4616 5195	T≥ 9 13 2 6 7 2 2 7 3 6 1 4 2 3 4 47 SEA-1 109 3589 4020 4748
≥ 6 42 9 11 12 10 8 8 9 7 6 6 4 3 3 4 48 972-1 190 3026 3232 4623	≥ 6 16 12 12 5 5 11 5 8 3 1 3 7 8 3 1 55 906 - 1 155 2832 2980 4408
t ≥ 3 37 27 20 5 12 14 9 10 7 7 6 5 2 2 30 372-1 193 1600 1637 4349	( ≥ 3 31 22 16 15 14 16 7 7 8 4 2 5 2 5 1 29 288-1 184 1544 1580 4291
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 46+ MAX TI T TO THE HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAS TI T TO TH HOURS INTERVAL BETWEEN EVENTS
3 59.4N 172.0W	4 58.0N 167.0 W
6 SEA-6 6 2208 4265 4265	W ≥ 64 6 SEA-6 6 2208 4265 4265
6 SEA-6 6 2208 4265 4265	Å≥48 6 SFA-6 6 2208 4265 4265
1 B SEA-6 9 2431 4423 4430	E ≥ 34 8   SEA - 6 8   2582   4427   4430
28 1 1 1 9 SEA-6 12 2452 4412 4431 2420 1 1 2 3 1 2 1 22 SEA-6 33 2860 4813 4943	
₹¹6 1 1 2 4 2 1 2 2 4 2 2 2 1 37 SEA~3 63 3912 5214 5530	≥ 16 4 5 2 1 2 5 3 1 2 1 3 3 1 B 1 43 SEA-3 85 4492 5065 5482
G≥:2 5 5 6 4 7 5 1 5 1 4 2 5 3 3 1 502130-1 108 4045 4389 5059	G≥12 7 6 9 9 4 4 4 7 2 3 5 4 1 1 2 54 1950-1 122 3860 4118 498
7 ≥ 9 6 13 7 4 12 5 5 7 7 3 2 4 5 1 58 1362-1 139 3295 3544 4731	T≥ 9 12 8 14 16 6 4 8 10 5 4 6 2 3 2 1 54 1716-1 155 3136 3363 48 3
, ≥ 6 18 15 17 10 12 € 6 5 6 5 4 3 6 4 2 47 558 - 1 168 2251 2379 4377	<u>2 6 30 20 20 15 7 10 6 4 10 4 4 2 3 2 42 810 - 1 179 2026 2155 4480</u>
t ≥ 3 18 16 16 18 9 9 7 2 6 4 2 4 2 1 2 19 258-1 135 1017 1044 4289	$t \ge 3 \ 40 \ 17 \ 12 \ 13 \ 10 \ 6 \ 4 \ 4 \ 4 \ 6 \ 1 \ 2 \ 1 \ 2 \ 11 \ 204 - 1 \ 133 \ 728 \ 745 \ 4292$
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TI T T= TH HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 74 44 90 96+ MAX TI TO THE HOURS INTERVAL BETWEEN EVENTS
5 56.8N 174.8E	6 52.0N 172.9E
W≥64 6 SEA-6 6 2208 4265 4265	₩≥64 A - 6   SEA - 6   2208   4265   4265
\$\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	A≥48 6 5EA-6 2208 4265 4265 E≥34 2 1 1 13 SEA-5 16 2539 4412 4431
≥28 1 1 1 1 1 1 13 SEA-7 18 3139 4925 4956	E ≥ 34 2 1 1 1 13 SEA - 5 16 25 39 44 12 44 3 1 H ≥ 28 1 1 1 1 1 1 1 1 1 1 20 SEA - 6 28 33 13 50 16 50 85
F ≥ 20 3   1 3 2 2   1 2 3   32 SEA-4 49 3646 5251 5480	H ≥ 20 5 2 3 1 4 1 3 1 1 2 47 SEA - 4 70 4264 4956 5294
≥ 16 4 2 4 4 3 4 1 3 2 2 1 2 3 43 SEA-3 78 3970 5267 5674	1 ≥ 16 9 2 7 10 4 3 1 4 2 5   2 2 3 2 50 SEA-3 106 4141 4601 5'60
$\frac{6}{5} \ge 12$ 7 6 7 5 5 3 2 5 3 6 3 2 4 4 6 51 1740 - 1 119 3580 4232 5056	G H ≥ 12 16 13 13 4 4 2 12 2 5 5 4 3 7 4 2 50 1398 - 1 146 3283 3558 4623
T≥ 9 17 9 7 10 12 6 9 4 2 8 4 6 5 4 1 43 942-1 147 2846 3134 4539	$T \ge 9 20 20 14 13 11 10 4 4 5 3 3 3 2 3 5 5 744 - 1 171 2719 2805 45 6$
. ≥ 6 23 14 19 11 10 10 6 3 4 4 3 5 5 2 43 546 - 1 162 1893 1991 4269	$f \ge 6   25   25   11   13   9   10   5   5   7   3   2   6   4   2   3   42   306 - 1   172   1678   1714   4255$
$t \ge 3 \begin{bmatrix} 24 & 15 & 14 & 7 & 9 & 6 & 11 & 6 & 4 & 5 & 4 & 1 & 1 & 4 & 2 & 9 & 222-2 & 121 & 772 & 804 & 4253 \\ 8 & 12 & 18 & 24 & 30 & 36 & 42 & 46 & 54 & 60 & 66 & 72 & 78 & 44 & 90 & 96 & MAX & T1 & T & T6 & TH \end{bmatrix}$	$t \ge 3 \ 31 \ 16 \ 14 \ 11 \ 7 \ 4 \ 3 \ 6 \ 4 \ 3 \ 3 \ 2 \ 2 \ 1 \ 2 \ 4 \ 282 - 1 \ 113 \ 573 \ 584 \ 4248$
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
7 54.7N 175.9W ₩≥64 6 SEA-6 6 2208 4265 4265	8 54.9N 167.2W ₩≥64 6 5EA-6 6 2208 4265 4265
A ≥ 46	Q≥48 6 SEA-6 6 2208 4265 4265
F & 34   1   1   9   SEA-6   11   2431   4416   4428	E ≥34 1 8   SEA - 6 9 2371 4426 4432
_≥28 1 1 1 14 SEA-6 18 2625 4603 4650	H ≥ 28 1 1 1 1 13 SEA-4 '6 2483 4586 4€27
c ≤ 20 5 3 2 1 3 1 1 3 1 1 4 2 30 SEA-2 57 3529 5379 5611	E ≥ 20 3 2 1 1 2 1 1 2 3 1 1 35 SEA-2 54 3488 5064 529
≥ 16 5 6 10 3 4 3 4 2 3 2 2 4 3 1 1 38 SEA-1 91 3546 4746 5208	(≥16 9 4 3 1 2 7 4 4 3 3 5 4 4 1 1 1 46 SEA-1 101 4232 4948 5427
2 12 13 15 7 8 10 6 4 6 4 5 2 4 2 3 54 1998 - 1 143 3505 3830 4763	H ≥ 12   15   10   10   5   B   B   5   B   3   1   2   4   1   1   4   2   59   1686 - 1   145   3848   4   29   5   2
7 ≥ 9   24   21   1   15   10   6   11   4   6   4   6   5   2   6   2   42   978 - 1   175   2628   2811   4371   ≥ 6   31   22   19   16   12   7   9   11   7   4   4   3   3   3   2   34   354 - 1   187   1765   1838   4281	$T \ge 9   22   17   15   13   9   4   5   5   8   5   6   4   4   4   4   2   680 - 1   177   3002   3205   4624$ $\ge 6   26   23   15   14   15   11   7   8   6   3   4   4   4   1   2   34   450 - 1   177   16   3   1740   4347$
≥ 6   31   22   19   16   12   7   9   11   7   4   4   3   3   3   2   34   354 - 1   187   1765   1838   4281         ≥ 3   24   11   10   12   9   3   7   4   7   5   1   1   3   3   11   150 - 2   111   722   742   4268	$\frac{2}{3} = \frac{6}{26} \frac{23}{25} \frac{15}{15} \frac{14}{15} \frac{11}{11} \frac{7}{8} \frac{8}{6} \frac{6}{3} \frac{3}{4} \frac{4}{4} \frac{4}{4} \frac{1}{1} \frac{2}{2} \frac{34}{15} \frac{450-1}{177} \frac{16^{\circ}3}{162-1} \frac{740}{118} \frac{4347}{606} \frac{4347}{615}$
6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T T+ TH	6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAY TI T
HOURS INTERVAL BETWEEN EVENTS 9 50.3N 171.3W	HOURS INTERVAL BETWEEN EVENTS 10 51.8N 167.3W
"≥64 6 SEA-6 6 2208 4265 4265	W≥64   6 SEA-6 6 2208 42c5 42c5
6 SEA-6 7 2215 4264 4265	A ≥ 48 6 SEA-6 6 2208 4265 4265
5 ÷ 34 1 1 11 SEA-6 13 2470 4467 4490	E ≧34 1 1 1 9 SEA-6 11 2421 4417 4431
→ 26 1 3 1 1 1 1 21 SEA-5 31 3292 4877 4952	H ≥ 28 1 1 1 2 1 1 1 18 SEA-5 25 3174 4995 5062
£ \$20     6     2     3     1     5     3     4     2     4     2     3     1     1     42     SEA-2     79     4347     5201     5561       \$16     12     6     8     16     6     2     4     2     5     3     1     2     48     SEA-2     118     4384     4626     5321	E≥20 3 1 1 1 1 2 3 2 1 2 3 2 1 4 1 39 SEA-2 66 3951 5182 5463 1≥16 7 6 5 10 6 6 9 1 4 2 2 4 4 2 3 50 SEA-1 121 4283 49 8 5556
\$ 16 112 6 6 8 6 6 2 4 2 5 5 3 1 2 48 SEA-2 118 4384 4626 5321 5 2 2 16 20 9 4 8 4 4 7 3 5 4 2 3 3 3 57 [8]8 1 152 3216 3399 4709	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
7 + 9 28 19 11 6 14 11 7 7 6 7 4 5 4 1 3 47 642-1 180 2285 2361 4375	T≥ 9 22 18 17 11 6 6 13 2 3 5 4 7 4 2 6 51 8:0~1 177 2405 2609 4554
e 6 27 21 12 12 9 5 4 8 4 5 2 1 2 4 33 330-1 149 1359 1395 4328	≥ 6 32 20 13 17 8 7 5 7 4 3 4 3 4 2 4 27 468 - 1 160 1403 1436 4326
. 2 3 11 11 13 8 12 6 5 1 1 2 4 1 1 1 6 144-2 83 472 472 4272	t ≥ 3 14 15 7 12 6 7 4 2 1 2 2 3 4 2 4 144-1 B5 479 479 428°
6 -2 18 44 30 16 42 48 54 60 65 72 78 84 90 96+ MAX TI T TA TH HOURS INTERVAL BETWEEN EVENTS	5 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T 7+ TH HOURS INTERVAL BETWEEN EVENTS
11 51.3N 158.8W	12 54.4N 158.1W
# ≥ 64 6 SEA-6 6 2208 4265 4265	W 264 6 SEA-6 6 2208 4265 4265
248 6 SEA-6 6 2208 4265 4265 5 € 34 1 1 12 SEA-7 14 3038 4558 4584	V≥48 6 SEA-6 6 2208 4265 4265 E≥34 1 1 12 SEA-7 13 3076 4595 4615
E € 34	E ≥ 34
E 220 4 7 4 2 8 3 2 2 3 5 3 2 2 3 43 SEA-5 93 4681 5655 6069	H ≥ 20 5 3 5 4 2 2 1 3 1 1 1 2 46 SEA-3 77 4606 5435 5808
≥ 16 9 5 11 12 6 4 9 6 4 2 4 4 4 3 54 SEA-1 137 4357 4674 5480	1 ≥ 16 5 7 5 11 5 4 5 2 2 3 5 3 5 2 63 SEA-1 127 4425 4706 5421
H≥ 12 12 18 8 13 6 8 10 4 4 3 5 3 2 6 5 56 1722-1 163 3453 3620 5118	G H = 12 14 17 8 8 7 6 7 5 6 6 3 2 3 3 5 59 1722-1 159 3465 3651 5012
7 £ 9 23 17 13 12 14 11 3 9 9 5 3 6 7 3 42 1218-1 177 2561 2629 4838	T≥ 9   13   12   13   12   17   11   2   11   11   6   2   6   1   1   4   44   864 - 1   166   2585   2734   4732
<u>≥ 6 25 23 19 10 13 10 9 7 2 2 7 3 1 1 2 22 402-1 156 1301 1320 4459</u>	≥ 6 37 28 18 12 7 14 7 7 6 4 5 5 2 2 5 23 684-1 182 1630 1656 4541
$1 \ge 3 \begin{bmatrix} 16 & 6 & 13 & 6 & 3 & 4 & 2 & 1 & 1 & 1 & 3 & 2 \\ 6 & 12 & 18 & 24 & 30 & 36 & 42 & 48 & 54 & 60 & 66 & 72 & 78 & 64 & 90 & 96 & MAX & 77 & 7 & T8 & TH \end{bmatrix}$	1 ≥ 3 19 14 14 10 5 4 4 1 1 2 3 5 5 258-1 81 377 394 4252 1 6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX 71 7 7 7 7 TH
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
23 Persistence of wave height-interval	Spring

1	64.1N 166.7W	2	63 6N 178.1W
₩≥64	4100	W ≥ 64	4100
Å V≥48	4100	<b>♦</b> ≥48	4100
€ ≥ 34	4100	E ≥ 34	4100
H ≥ 28 1 6-1 1	9 9 4100	H ≥ 28 E ≥ 20 4 2 1 36-1 7	18 18 4100
E ± 20 1 2 1 2 1 24-1 4 1 ± 16 1 2 1 1 1 1 60-1 7	32 32 4103	<u>1 ≥ 16 2 1 3 2 3 42-3 11</u>	
$G \stackrel{?}{=} 12 \mid B \mid 3 \mid 3 \mid 2 \mid 2 \mid 1 \mid 2 \mid 1 \mid 1 \mid 1 \mid 1 \mid 1 \mid 1$	<del></del>	G ≥ 12 10 4 1 6 3 2 2 2 3 1 84-1 34	<del></del>
T ≥ 9 24 4 4 7 4 3 1 1 1 2 1 2 2 1 4 150-1 61	<del></del>	T≥ 9 22 8 11 7 4 5 3 4 4 1 3 1 2 3 2 2 126-1 82	<del></del>
≥ 6 42 8 15 8 10 4 6 3 3 4 1 2 3 2 2 16 222-1 12	824 851 4125	, ≥ 6 27 11 17 6 5 7 5 4 3 3 5 4 7 4 24 228-1 13	2 1087 1124 4133
≥ 3 35 17 20 9 11 12 14 4 9 2 11 7 4 3 5 39 372-1 20		$t \ge 3 28 18 16 8 5 9 9 10 2 3 7 7 5 5 2 57 324 - 1 19$	
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TO HOURS DURATION OF EVENTS		6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX THE	
3	59.4N 172.0W	W≥64	58.0N 167.0W
W≥64 A≥48	4100	N ≤ 04	4100
V ≤ 40 E ≥ 34	4100	V=70 E≥34	4100
≥ 28	4100	≥28 3 1 1 24-1 5	
H ≥ 20 3 4 2 1 2 42-2 12	46 46 4100	E ≥ 20 4 5 5 1 3 1 2 2 48-2 23	3 84 84 4103
≥ 16 6 4 5 2 3 1 3 1 2 1 1 90-1 29	131 131 4106	≥ 16 4 7 4 7 4 4 3 2 5 1 60-1 4	1 194 194 4107
G ≥ 12 11 5 8 7 10 9 8 4 2 2 1 1 2 108-2 70	<del></del>	H ≥ 12 / 9 10 8 / 8 4 8 4 1 5 4 1 2 2 132-1 80	<del></del>
$T \ge 9 \   11 \   4 \   10 \   6 \   3 \   5 \   10 \   8 \   8 \   4 \   5 \   4 \   4 \   3 \   2 \   9 \   132-2 \   96$		T≥ 9 9 6 12 9 6 13 7 9 8 4 5 5 2 2 3 13 246-1 11	<del></del>
≥ 6 22 13 13 5 14 12 9 8 11 6 6 6 6 3 2 6 30 348-1 160		≥ 6 21 6 9 10 8 9 8 7 11 7 5 8 6 9 3 37 402-1 16 ≥ 3 17 14 8 6 5 8 9 1 5 1 4 4 4 3 3 66 2094-1 15	
t ≥ 3 21 16 9 13 10 6 7 1 2 3 4 4 2 7 4 58 888 1 16  6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX 78		6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX T	
HOURS DURATION OF EVENTS	56.8N 174.8E	HOURS DURATION OF EVENTS	52.0N 172.9E
₩≥64	1 4100	₩≥64	32.01 1/2:92
A ≥ 48	4100	A ∨ ≥ 48	4100
E ≥ 34	4100	E ≥ 34 1 6-1 1	
4 ≥ 28 1 6-1 1	1 1 4100	H ≥ 28 1 2 18-2 3	<del></del>
£ ≥20 6 1 2 1 1 1 1 1 60-1 13		$E \ge 20 \ 8 \ 1 \ 5 \ 2 \ 1 \ 1 \ 1 \ 1 \ 78 - 1 \ 20 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ $	<del></del>
3 16 9 8 3 4 4 2 2 1 2 2 84-2 37 S		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$\frac{1}{12} \ge 12$   12   7   8   5   8   6   5   7   3   5   4   1   1     4   126-1   76   78   9   18   8   11   6   11   5   9   9   4   2   4   5   5   2   1   14   240-1   11   11   12   13   14   15   15   15   15   15   15   15		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
≥ 6 22 17 7 10 11 10 10 9 4 1 8 3 12 4 5 40 378-1 17		≥ 6 20 7 9 9 13 14 3 14 3 5 12 8 7 4 1 47 300-1 17	<del></del>
(≥ 3 19 8 8 6 13 2 2 5 4 6 5 2 8 3 2 64 750-1 15		2 3 22 11 4 4 3 7 5 5 6 6 4 4 2 6 2 69 SEA-1 16	
6 12 18 24 3. 30 42 48 54 60 66 72 78 84 95 96+ MAX TE	тн	0 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX T	E T Te TH
HOURS DURATION OF EVENTS 7	54.7N 175.9W	HOURS DURATION OF EVENTS	54.9N 167.2W
₩ ≥ 64	4100	W ≥ 64	4100
Å ≥ 48	4100	<sup>2</sup> ó48	4100
E = 34	4 4 4 4100	E ≥ 34 ∴ ≥ 28 2 1 18 - 1 3	410C 3 7 7 4100
± 28 2 1 12-1 3 € ± 20 12 5 5 8 1 1 2 1 54-1 35		H ≥ 28	
16 9 7 7 5 6 7 3 3 1 3 1 2 2 84-2 56	<del></del>	1 ≥ 16 12 6 9 4 7 5 1 1 4 2 60-2 5	<del></del>
$G \ge 12 \ 19 \ 8 \ 8 \ 6 \ 8 \ 5 \ 3 \ 5 \ 7 \ 5 \ 4 \ 3 \ 3 \ 1 \ 3 \ 6 \ 162-1 \ 94$	<del></del>	$G_{H} \ge 12$ 17 4 9 10 12 10 5 6 6 2 2 3 2 1 5 114-1 9	4 552 568 4120
7 ≥ 9 18 11 17 14 8 13 9 7 5 4 10 5 7 6 4 15 234-1 15	3 1235 1246 4180	T≥ 9 16 5 18 7 8 10 10 7 10 7 7 8 5 3 2 14 258-1 13	1124 1167 4160
≥ 6 21 14 11 14 9 13 7 4 2 8 7 7 8 6 6 50 396-1 18		$f \ge 6 \ 17 \ 11 \ 13 \ 11 \ 8 \ 12 \ 5 \ 5 \ 7 \ 7 \ 5 \ 5 \ 10 \ 11 \ 9 \ 42 \ 414 \sim 1 \ 17$	_+
3 12 6 4 5 7 5 6 3 3 5 1 3 5 4 1 65 SEA-2 13		$t \ge 3 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE HOURS DURATION OF EVENTS		HOURS DURATION OF EVENTS	_
9	50.3N 171.3W	₩≥64	51.8N 167.3W
W≥64 A>49	4100	A ≥ 04 A ≥ 48	4100
V ≥ 48 E ≥ 34	4100	V = 40 E ≥ 34	4100
≥ 28 3 2 12-2 5	7 7 4100	H ≥ 28 1 1 1 12-1 2	_+
E ≤ 20 12 8 5 5 1 1 1 2 48-2 35	<del></del>	E ≥ 20 7 4 3 5 3 3 3 36-3 2	5 77 B1 4100
2 16 10 10 4 8 7 7 2 2 1 4 2 1 1 1 1 102-1 60		1 ≥ 16 11 6 6 6 7 2 6 4 2 2 102-2 5	
G ≥ 12 14 8 15 7 7 8 6 4 9 5 2 2 5 1 11 156-1 10	<del></del>	$H \ge 12$ 22 10 11 9 13 5 8 5 4 5 4 1 7 2 1 4 222-1 11	
T≥ 9 22 14 11 13 11 7 4 10 12 4 7 6 7 6 6 21 240-1 16	<del></del>	$T \ge 9 \ 24 \ 9 \ 6 \ 12 \ 5 \ 12 \ 5 \ 11 \ 4 \ 8 \ 7 \ 5 \ 7 \ 6 \ 6 \ 20 \ 282 - 1 \ 14 \ 14 \ 14 \ 14 \ 14 \ 14 \ 14 $	<del></del>
2 6 13 10 8 7 9 8 9 13 6 7 4 6 9 6 4 55 498-1 17		≥ 6 14 11 11 11 12 13 6 6 5 3 8 6 3 8 2 62 636-1 18	<del></del>
2 3 5 4 4 1 3 5 2 2 2 2 1 1 69 SEA-3 10		$t \ge 3 \begin{bmatrix} 8 & 1 & 4 & 2 & 4 & 3 & 2 & 2 & 4 & 4 & 1 & 2 & 3 & 2 & 3 & 59 \end{bmatrix} SEA - 1 10  6 12 18 20 30 36 42 48 54 60 66 72 78 64 90 96 MAX T$	E T T+ TH
HOURS DURATION OF EVENTS	51.3N 158.8W	HOURS DURATION OF EVENTS 12	54.4N 158.1W
₩≥64	31.3N 138.8W	₩≥64	4100
2 ≥ 48	4160	A ≥ 48	4100
₹ ≥ 34	4100	E ≥34 1 1 18 - 1 1	3 3 4100
≥ 28 2 2 1 1 1 36-1 6	17 19 4100	H ≥ 28 2 2 1 1 . 30 - 1 €	<del></del>
£ ≥ 20 4 4 5 4 1 1 3 2 54-2 24		E ≥ 20 5 6 3 4 2 4 3 1 60-1 2	<del>+</del>
16 12 10 7 4 7 6 4 4 4 1 1 1 1 84-1 61		G ≥ 16 12 7 6 5 3 5 6 3 3 4 2 72-2 5 G > 13 10 5 0 13 7 5 6 5 3 2 0 3 2 1 1 1 1 1 1 1 2 1 3 2 0	<del></del>
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		$_{\text{H}} \ge 12$ 10 5 9 13 7 6 5 6 3 3 9 2 3 1 1 8 132-2 9 $_{\text{T}} \ge 9$ 22 16 10 14 11 7 10 8 5 2 5 6 6 4 4 23 330-1 15	<del></del>
	<del></del>	\\_\\\\\\\\	74 2304 2636 4469
≥ 6 12 8 13 8 9 14 6 4 10 7 5 8 5 5 7 56 882-1 17 t≥ 3 9 3 4 2 2 2 1 2 1 1 1 2 61 SEA-2 90		1 ≥ 3 15 8 2 3 2 3 3 3 4 3 2 1 1 1 1 60 SEA-1 1	
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TI		6 12 18 24 30 36 42 48 54 60 55 72 78 84 90 95+ MAX T	E T To TH
HOURS DURATION OF EVENTS		HOURS DURATION OF EVENTS	
Summer		23 Persistence of wave	neight-duratio

1 64.1N 166.7W ₩≥64 65EA-6 6 2208 4224 4224	2 63 6N 178 1W W≥64
A ≥ 48 6 SEA-6 6 2208 4224 4224	₩264
E ≥ 34 6 SEA-6 6 2208 4224 4224	E ≥ 34 6 SEA-6 6 2208 4224 4224
H ≥ 28 7 SEA-6 7 2432 4448 4449	H ≥ 28 6 SEA-6 6 2208 4224 4224
E ≥ 20 1 1 8 SEA-4 10 2311 4210 4219	E ≥ 20 1 11 SEA-2 12 2218 4305 4323
9 SEA-4 11 2286 4143 4172	1 ≥ 16 1 1 17 2136 - 1 18 2780 4403 4449
$r_1 \ge 12 \   \ 1 \   \ 1 \   \ 1 \   \ 1 \   \ 1 \   \ 20 \ SEA - 1 \ 28 \ 2734 \ 4222 \ 4327$ $T \ge 9 \   14 \   3 \   2 \   \ 1 \   \ 1 \   \ 1 \   \ 1 \   \ 1 \   \ 36 \   \ 1866 - 1 \   \ 62 \ 2953 \ 3902 \ 4200$	$H \ge 12$ 2 1 1 1 1 1 3 31 1860 - 1 38 2836 4172 4338
. ≥ 6 27 6 2 5 4 5 2 2 2 4 4 4 1 2 3 53 1080 - 1 126 2883 3301 4127	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
£ ≥ 3 37 19 18 11 12 18 7 6 5 7 9 2 6 6 1 39 294-1 203 1868 1936 4122	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T T+ TH	5 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T TP TH
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS  58.0N 167.0W
W ≥ 64 6 SEA-6 6 2208 4724 4224	W≥64 6 SEA-6 6 2208 4224 4224
Å≥48 6 SEA-6 6 2208 4224 4224	A ∨≥48 6 SEA-6 6 2208 4224 4224
E ≥ 34 6 SEA-6 6 2208 4224 4224	E ≥ 34 6 SEA-6 6 2208 4224 4224
$14 \le 28$	H ≥ 28 10 SEA-4 10 2399 4229 4242
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E ≥ 20
$G \ge 12 \ 6 \ 2 \ 3 \ 1 \ 1 \ 4 \ 1 \ 2 \ 1 \ 2 \ 3 \ 45 \ 1470 - 1 \ 71 \ 3239 \ 3894 \ 4245$	≥ 16   2   1   2   1   1   2   1   34   2100 - 1   44   3055   4100   4287     ≥ 12   4   1   4   2   1   2   2   2   2   3   3   1   55   1500 - 1   82   3132   374:   4230
T ≥ 9 2 2 3 7 2 6 4 3 4 4 2 3 2 3 1 49 990-1 97 2902 3426 4158	T≥ 9 7 5 5 6 6 4 4 3 2 2 1 2 1 3 3 59 834-1 113 2877 3251 4156
<u>,</u> ≥ 6 20 16 15 10 4 9 5 6 3 7 6 3 2 6 2 54 462-1 168 2366 2606 4136	, ≥ 6 26 10 9 8 11 8 4 6 7 3 3 4 8 6 6 47 570-1 166 2203 2389 4'35
2 3 35 14 17 12 14 13 7 9 6 4 7 5 3 6 5 11 264-1 168 1120 1167 4104	t ≥ 3 29 15 23 13 20 11 4 7 9 5 1 4 1 8 12 228 - t 162 980 1026 4 104
6 12 18 24 30 36 42 48 54 60 66 72 78 64 90 96+ MAX TI T T+ TH HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 44 90 964 WAY TI TO THE HOURS INTERVAL BETWEEN EVENTS
5 56.8N 174.8E	6 52.0N 172.9 E
W≥64     6 SEA-6     6 2208     4224     4224       A≥48     6 SEA-6     5 SEA-6     2208     4224     4224	W≥64     6 SEA-6 6 2208 4224 4224       A≥48     6 SEA-6 6 2208 4224 4224
E ≥ 34	V≥48     6 SEA-6 6 2208 4224 4224       E ±34     7 SEA-6 7 2255 4223 4224
≥28 7 SEA-6 7 2324 4331 4332	L ≥ 28 7 SEA-5 7 2201 4250 4256
€ ≥ 20 1 1 16 SEA-1 18 2822 4326 4365	E ≥ 20 1 1 1 1 2 20 SEA-1 25 3:61 4188 4245
$\frac{2}{6} = 16 + 3 + 2 + 2 + 2 + 1 + 1 + 25 = 2124 - 1 + 39 + 3014 + 4122 + 4252$	1 ≥ 16 3 2 1 1 1 1 1 1 2 1 33 1818-1 47 3058 3988 41 <sup>-9</sup>
-, ≥ 12   4   5   3   3   1   4   1   2   1   2   2     48   1494 - 1   76   3092   3816   4238	H ≥ 12 6 6 1 3 6 3 5 1 2 1 2 1 1 57 1182-1 95 3190 3661 4.62
* \(\frac{2}{2}\) 9 \(\frac{10}{3}\) 3 \(\frac{1}{2}\) 10 \(\frac{3}{3}\) 4 \(\frac{6}{3}\) 3 \(\frac{3}{2}\) 5 \(\frac{2}{3}\) 1 \(\frac{10}{1050}\) -1 \(\frac{115}{15}\) 29 \(\frac{15}{2915}\) 3354 \(\frac{4168}{4168}\) \(\frac{2}{2}\) 6 \(\frac{12}{2}\) 11 \(\frac{16}{11}\) 11 \(\frac{16}{11}\) 9 \(\frac{9}{3}\) 5 \(\frac{8}{3}\) 3 \(\frac{5}{2}\) 6 \(\frac{2}{6}\) 49 \(\frac{672}{2}\) -1 \(\frac{173}{3}\) 2188 \(\frac{2386}{386}\) 4125	T ≥ 9 9 5 6 10 7 7 5 5 3 3 4 4 2 3 69 870-1 142 2860 3172 4166
t ≥ 3   27   17   16   8   12   14   8   3   2   5   1   4   3   4   12   156   153   165   2366   4123	$rac{1}{2} \ge 6 \   19 \   8 \   18 \   10 \   8 \   11 \   14 \   4 \   6 \   4 \   5 \   7 \   2 \   5 \   7 \   44 \   282-2 \   172 \   963 \   2209 \   4130 \   12 \   230 \   13 \   14 $
6 12 18 24 30 36 42 43 14 60 66 72 78 84 90 96 MAX T) T TO TH	6 12 18 24 30 35 42 46 54 60 66 72 78 84 90 96+ MAX TI TE TE
HOURS INTERVAL BETWEEN EVENTS 7 54.7N 175.9W	HOURS INTERVAL BETWEEN EVENTS 8 54.9N 167.2W
M 264 6 SEA-6 6 2208 4224 4224	W≥64 6 SEA-6 6 2208 4274 4224
6 SEA-6 6 2208 4224 4224 √ ≥48	Å≥48 6 SEA-6 6 2208 4224 4224
5 ± 34	E ≥ 34 6 SEA-6 6 2208 4224 4224
1 2 2 2 2 2 2 3 2 4 2 4 2 4 3 1 1 1 1 2 2 2 3 1 3 5 1 3 5 1 3 5 1 3 1 3 1 3 1 3 1 3	H ≥ 28 8 24 13 4373 4380 E ≥ 20 1 2 2 1 20 SEA-1 26 2815 4178 4251
≥ 16 7 2 2 3 2 1 4 1 1 1 37 1506-1 61 3009 3951 4224	E ₹20 1
$\frac{3}{5} \ge 12 \cdot 6 \cdot 7 \cdot 3 \cdot 1 \cdot 4 \cdot 1 \cdot 4 \cdot 3 \cdot 3 \cdot 3 \cdot 3 \cdot 1 \cdot 2 \cdot 5 \cdot 1398 - 1 \cdot 96 \cdot 3084 \cdot 3579 \cdot 4171$	$G \ge 12 \ 5 \ 2 \ 4 \ 6 \ 4 \ 3 \ 2 \ 3 \ 2 \ 1 \ 3 \ 1 \ 6 \ 1 \ 1 \ 53 \ 1398 - 1 \ 97 \   \ 3122 \ 3624 \ 4 \ 72$
T≥ 9 14 10 2 7 8 5 6 10 6 6 4 3 1 5 5 58 774-1 150 2642 2972 4138	T≥ 9 10 7 10 9 7 4 3 3 4 4 6 2 2 4 4 58 1392-1 137 2772 3034 4:41
, ≥ 6 25 16 15 11 11 17 3 7 7 7 6 10 6 5 1 36 714-1 183 1900 2089 4122	, ≥ 6 25 21 9 12 8 6 6 8 5 7 7 5 8 3 7 40 582-1 177 1960 2110 4:36
r ≥ 3 25 19 16 20 14 5 B 1 4 6 2 4 4 1 3 3 132 -1 134 674 705 4108	$t \ge 3 \ 20 \ 19 \ 19 \ 14 \ 9 \ 13 \ 7 \ 7 \ 3 \ 7 \ 2 \ 5 \ 1 \ 2 \ 1 \ 4 \ 186 - \ 133 \ 724 \ 777 \ 4 \ 03$
HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX T. T. TA TH HOURS INTERVAL BETWEEN EVENTS
9 50.3N 171.3W W 264 6 SEA-6 6 2208 4224 4224	10 51.8N 167 3W ₩≥64 6 5EA-6 6 2208 4224 4224
A≥48 6 SEA-6 6 2208 4224 4224	W ≥ 64     6 SEA-6 6 2208 4224 4224       A ≥ 48     6 SEA-6 6 2208 4224 4224
E = 34 6 SEA-6 6 2208 4224 4224	E ≥ 34 6 SEA-6 6 2208 4224 4224
H ≧ 28 9 SEA-3 9 2326 4318 4325	u ≥ 28
E = 20 2 1 2 2 1 2 1 2 1 29 1976 - 1 40 3:79 4213 4315	E € 20 2 1 1 3 1 1 21 SEA-1 29 2877 4:68 4249
\$\frac{2}{6}\frac{1}{2}\$     \$\frac{1}{6}\$     \$\frac{1}{6}\$     \$\frac{1}{6}\$     \$\frac{1}{6}\$     \$\frac{3}{6}\$     \$\frac{1}{6}\$     \$\frac{3}{6}\$     \$\frac{1}{6}\$     \$\frac{3}{6}\$     \$\frac{3}{6}\$     \$\frac{2}{6}\$     \$\frac{1}{6}\$     \$\frac{3}{6}\$     \$\frac{3}{6}\$     \$\frac{2}{6}\$     \$\frac{3}{6}\$     ≥ 16 2 2 1 1 1 1 3 1 3 4 1 39 1500 - 1 58 30 16 3985 4235	
H ≥ 12 5 4 7 4 5 7 4 2 2 5 3 4 3 4 46 1356-1 105 2867 3468 4176  T≥ 9 13 14 11 6 8 3 5 7 8 5 2 5 8 6 58 846-1 159 2556 2786 4131	$H \ge 12 \   12 \   4 \   5 \   6 \   5 \   5 \   1 \   3 \   6 \   3 \   2 \   1 \   2 \   3 \   5 \   5 \   1386 - 1 \   115 \   3042 \   3505 \   4180 \  $ $T \ge 9 \   11 \   11 \   12 \   6 \   6 \   12 \   3 \   5 \   4 \   5 \   6 \   1 \   5 \   4 \   54 \   1332 - 1 \   145 \   2634 \   2849 \   4141 \  $
2 6 17 17 15 17 13 10 8 6 7 6 11 6 5 3 8 27 288 - 1 176 1562 1660 4110	, ≥ 6   18   19   21   12   8   9   8   10   5   7   11   9   4   8   2   29   312-2   180   1640   1760   4115
t ≥ 3 13 23 11 10 7 8 6 12 1 3 1 2 1 2 126-1 100 480 509 4105	t ≥ 3 19 20 17 11 11 10 9 3 2 1 1 2 3 132-2 109 479 502 4101
6 12 18 24 30 36 42 48 54 50 66 22 78 64 90 96+ MAX TI T THE THE HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 H4 90 96+ MAX T) T TH TH
11 51.3N 158.8W	HOURS INTERVAL BETWEEN EVENTS 12 54.4N 158.1W
₩ ≥ 64 6 SEA - 6 6 2208 4224 4224	W≥64 6 SEA-6 6 2208 4224 4224
A ≥ 48 6 SEA-6 6 2208 4224 4224 E ≥ 34 6 SEA-6 6 2208 4224 4224	V≥48 6 SEA-6 6 2208 4224 4224
6 SEA-6 6 2208 4224 4224 3 28 1 9 SEA-3 10 2641 4509 4528	E ≥ 34 7 SEA-5 7 2389 4167 4170 H ≥ 28 10 SEA-4 10 2593 4376 4390
£ 20 1 1 1 1 22 21 18 - 1 27 2853 4154 4257	10  SEA-4 10 2593 4376 4390 $10  SEA-4$ 10 2593 4376 $10  SEA-4$ 10 2593 437
≥ 16 3 1 3 2 1 1 1 4 1 2 2 1 40 1758 - 1 62 3286 3948 4233	1 ≥ 16 2 1 2 1 1 3 1 2 2 1 1 2 38 1842 - 1 57 3007 3979 4244
GH≥12 10 11 4 2 3 3 6 5 3 5 3 3 2 3 60 1392-1 123 3055 3368 4153	G <sub>H</sub> ≥12 1 4 4 1 3 6 4 2 2 3 3 1 1 1 56 1122-1 92 3075 3502 4147
T≥ 9 15 8 10 9 8 8 8 7 5 4 5 2 2 8 4 45 1008-1 148 2519 2665 4109	T≥ 9 14 8 8 8 9 10 6 5 7 5 8 4 1 1 2 57 654-2 153 2637 2878 4115
+ ±     6     24     27     18     12     9     6     13     7     9     6     2     5     4     6     2     29     108     1     179     1568     1632     4105       + ±     3     17     17     17     5     8     4     2     2     6     1     1     2     3     5     222     1     90     478     520     4100	1 ≥ 6 23 10 18 17 14 8 11 7 8 5 7 5 5 2 7 31 552-1 178 1744 1845 4112
6 12 18 24 30 36 42 48 54 50 66 72 78 04 90 96+ MAX TI T TE TH	$t \ge 3 \ 28 \ 22 \ 13 \ 13 \ 11 \ 2 \ 6 \ 3 \ 3 \ 2 \ 3 \ 1 \ 1 \ 1 \ 1 \ 6 \ 168 - 1 \ 115 \ 546 \ 559 \ 4^{\circ}00$
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
B Persistence of wave height-interval	Summer

Summer

64 - 48				
_	1	64.1N	166.7 W	2 63.6N 17
48	╾ <del>┊┊┊┊┊┊</del> ┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼	<del></del>	4545 4545	W≥64 A>40
	1 1 1 1 24-1 3	7 7	4545	V≥48 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
·- (_	<del>\</del>			
-	<del></del>		4545	H = 24   15   16   16   16   16   17   17   17   17
-		214 224	<del></del>	E ≥ 20 23 B 7 5 10 9 3 5 6 3 4 3 1 1 108-1 88 440 459 4
~ L	17 12 5 9 6 6 8 3 2 1 1 2 1 1 4 162-1 78	413 427		≥ 16   26   12   19   10   4   11   10   7   3   2   5   6     2   1   10   162 - 1   128   784   811   4
-	56 20 13 8 12 1 2 3 9 5 2 3 3 2 12 240-1 153 59 23 23 12 17 9 14 6 6 15 9 7 7 4 3 21 282-1 238	807 848		G ≥ 12 44 16 13 11 9 16 11 10 8 6 8 2 6 4 2 23 246-1 189 14:5 147!
- +	55/25/25/12/17/5/14/5/5/14/5/25/25/25/25/25/25/25/25/25/25/25/25/2	1665 1752		$T \ge 9 \begin{tabular}{ c c c c c c c c c c c c c c c c c c c$
-	37 19 15 10 13 14 20 7 13 5 7 3 7 10 3 53 714-1 236	2745 2956		1 ≥ 6 26 11 7 B 7 9 7 5 4 11 12 6 3 4 5 65 750-1 190 2951 330:
3 į	8 10 3 4 8 6 4 3 2 4 2 3 4 2 62 SEA-1 125	3960 4685		$t \ge 3 \ 4 \ 4 \ 3 \ 6 \ 6 \ 5 \ 3 \ 2 \ 4 \ 2 \ 1 \ 3 \ 3 \ 4 \ 68 \ 242 - 1 \ 118 \ 3753 \ 4436 \ $
	6 12 18 24 30 36 42 48 54 80 66 72 78 84 90 96+ MAX TE HOURS DURATION OF EVENTS	7 т.	TH	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 46+ MAX TO TO TO
_	3	59.4N	172.0W	4 58.0N 16
4 ′_			4545	W≥64
6 <u>.</u>	1 12-1 1	2 3	4545	Ç≧48 1 6-1 1 1 2
-	5 5 3 1 1 3 30-1 15	33 36	4545	E ≥ 34 4 1 4 2 3 1 42~1 15 48 51
8 :1	10 11 10 9 6 3 3 42-3 52	167 171	4547	H ≥ 28 12 12 11 3 5 2 2 1 1 66-1 48 143 148
0 1	15 17 14 16 14 12 9 6 5 7 6 1 1 2 2 114~1 127	677 685	4557	E ≥ 20 30 20 24 19 6 10 8 5 5 2 4 1 7 186-1 141 660 668
6 🗓	16 24 10 23 15 9 14 16 10 3 4 7 6 6 13 192~1 176	1239 1258	4601	L ≥ 16   28   18   16   21   25   10   16   18   9   3   3   5   8   2   2   9   198 - 1   193   189   1226   3
2 2	21 14 13 10 12 16 15 17 12 11 9 7 7 5 4 34 276~1 207	1933 2016	4614	G <sub>H</sub> ≥12 27 18 19 13 11 8 18 15 13 13 19 10 10 3 2 30 270-1 229 1964 2053.
9 1	12 6 14 8 12 8 10 11 10 12 7 7 9 6 5 62 618-1 199	2733 2898	4707	T≥ 9 21 11 11 15 7 10 16 11 5 10 5 6 8 6 11 67 564-1 220 2028 2988 .
6 [1	11 7 9 11 5 8 6 6 7 6 3 6 5 2 6 77 996~1 175	3620 3878	4876	. ≥ 6 B 7 9 6 7 6 5 2 9 7 3 2 6 3 79 350-1 159 3976 4266
3 <u>.</u>	7 4 1 1 1 3 1 2 1 1 43 SEA- 1 65	4312 5358	5575	( ≥ 3 2 1 2 1 1 2 1 1 2 1 2 2 5EA-4 32 3409 5294
	6 .2 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE	T T=	тн	6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 90+ MAX TC "-
	HOURS DURATION OF EVENTS 5	56.8N	174.8E	HOURS DURATION OF EVENTS6
4		-	4545	W≥64 : 6~1
• _	18-1 2	4 4	4545	A ≥ 48 2 1 1 1 18-1 4 7 7
	3 5 3 2 3 2 3 1 48-1 22	86 88	4546	E ≥ 34 5 9 B 3 2 4 1 1 1 48-1 33 105 110
; [	10 14 8 7 7 4 5 2 2 1 2 1 1 78-1 64	275 279	4547	28 20 12 6 4 10 7 5 3 3 1 1 1 1 72-1 73 289 295
7	19 18 19 17 16 4 18 12 5 7 5 4 3 6 7 186-1 160	991 1016	4561	E ≥ 20 30 22 33 19 18 12 10 9 7 9 2 3 1 1 3 4 5 132-1 187 969 986
-	16 11 18 17 22 12 18 9 8 11 7 5 7 2 7 25 216-1 195	1642 1745	4596	1 ≥ 16 25 20 16 26 31 11 15 12 10 7 7 6 9 2 22 210 - 1 219 1570 1641
2 2	20 11 11 10 13 17 15 13 12 9 9 10 5 4 2 51 438 - 1 212	2442 2644	4629	G <sub>H</sub> ≥12 23 23 31 20 13 16 12 13 10 13 8 8 9 7 5 47 270-1 258 2395 . 2634
, <sup>-</sup>	9 6 9 3 8 8 7 6 5 8 10 3 4 1 7 77 852-1 171	3302 3709	4917	T≥ 9 11 16 8 6 14 13 10 12 11 10 11 9 6 7 2 70 558 -1 216 3157 3557
, –		4277 5028		≥ 6 7 4 5 1 6 4 3 5 2 4 5 3 4 3 6611746-11122 4340 498€
-	5   3   1   2   3   1   19   SEA-4   34	2863 4941		t ≥ 3 3   2 1   1   1   1   1   2   20   36A=5   32   3289   5290
_	6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TE	7 T.	TH	6 :2 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TE T T+
	HOURS DURATION OF EVENTS	54.7N	175.9W	HOURS DURATION OF EVENTS  8 54 9N 16
<u>.</u> –		- 34./N	4545	8 54 9N 16 ₩≥64
	12-1 2	3	4545	A
<u></u>	4 2 6 4 5 30 -5 41	07 100		V≥48 E≥34 2 4 3 3 2 1 36- 5 47 50
-	8 5 10 7 16 7 3 2 1	274   279	<del></del>	\$28 16 6 7 5 4 3 2 11 60-1 44 13: 135
~ <del>-</del>	35 19 16 18 18 10 . 7 16 17 . 7 19   2 1 1 1 5   29 1 1 7 1	904 920	<del></del> ;	H = 20   23   20   16   17   8   13   6   11   4   3   1   2   2   4   132 - 1   30   62   646
_	33 24 18 18 15 11 19 17 15 10 9 9 2 3 18 210~1 221	1327   1573		≥ 16 20 19 19 23 10 21 14 15 9 9 5 7 6 2 4 8 444-1 19 1235 2 2
- 3		2407 2533	+	
	3 3 3 3 3 7 12 2 10 7 10 3 10 7 10 331	3191 3457		"
, 5	20 20 20 20 21 21 6 22 6 20 2 7 2 2 6 6 6 78 696 1 222 1	3191 3437		P-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1
_	······································	4020 4677		*
, [	8 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124	4039 4622	+	
, [	B 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124 2 1 1 1 1 1 1 1 1 18 SEA-6 23	3097 5309	5363	t ≥ 3 2 2 3 2 2 3 24 SEA - 3 31 29-6 5227
, [	8 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124		+	t ≥ 3 2 2 3 1 2 4 50 6 72 78 64 60 96 72 78 64 60 90 96 WAX TE THOUSE DURATION OF EVENTS
	8 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124 4 1 1 1 1 1 8 SEA-6 23 6 2 8 24 30 36 42 48 54 60 56 72 78 r4 90 90 MAX TC	3097 5309	5363 TH 171.3W	6 .2 '8 '2" 30 16 42 48 54 60 66 12 78 64 40 96 MAX TE HOURS DURATION OF EVENTS 10 51.8N 16
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2 1 1 3 3 5 4 4 5 4 6 0 50 7 2 7 8 7 4 90 90 MAX TC  HOURS DURATION OF EVENTS	3097 5309 T F•	5363 TH 171.3W 4545	6 .2 78 24 30 36 42 48 54 60 66 72 78 64 90 96 MAX TE HOURS DURATION OF EVENTS  10 51.8N 16
Ē	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3097 5309 T T• 50.3N	171.3W 4545 4545	6 2 78 24 30 36 42 48 54 60 66 72 78 64 90 96 MAX TE HOURS DURATION OF EVENTS  10 51.8N 16  W \$64
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3097 5309 7 7• 50.3N 96 99	171.3W 4545 4545 4545	6 .2 '8 24 30 16 42 48 44 60 66 72 '8 64 40 96 6 MAX TE HOURS DURATION OF EVENTS  10 51.8N 16  W 264
	9 3 3 5 7 4 1 1 5 4 4 1 1 4 2 3 : 69 1146-1 124  2	3097 5309 7 7* 50.3N 96 99 277 282	171.3W 4545 4545 4545 4545	6 12 18 24 30 16 42 48 14 60 66 72 18 64 90 96 MAY 75 HOURS DURATION OF EVENTS  10 51.8N 16  W \$64
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 7 7• 50.3N 96 99	171.3W 4545 4545 4545 4545	6 12 18 24 30 16 42 48 14 60 66 72 18 64 40 90 96 MAY 75 HOURS DURATION OF EVENTS  10 51.8N 16    N
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 50.3N 96 99 277 282 991 1016 1686 1746	171.3W 4545 4545 4545 4545 4546 4567	6 .2 '8 .44 JO 16 42 48 54 60 66 12 78 64 90 96 MAX 76 HOURS DURATION OF EVENTS  10 51.8N 16  W 264  \[ \text{A} \text{A} \text{B} \text{A} \text{B} B
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3097 5309 7 7* 50.3N 96 99 277 282 991 1016	3 5363 TH 171.3 W 4545 4545 4545 4545 4567 4578	6 12 18 12 10 16 42 48 14 60 68 72 78 64 90 96 MAX TE HOURS DURATION OF EVENTS  10 51.8N 16  W \$64
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3097 5309 50.3N 96 99 277 282 991 1016 1686 1746	171.3W 4545 4545 4545 4545 4545 4567 4567 4578 4631	6 12 18 24 30 16 42 48 44 60 66 12 18 64 90 96 MAY 75 HOURS DURATION OF EVENTS 1
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  4 1 1 1 1 1 18 SEA-6 23  8 2 0 1 2 1 1 1 1 1 18 SEA-6 23  8 3 0 1 2 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3097 5309 7 50.3N 96 99 277 282 991 1016 1686 1746 2801 3515 3844 3970 4951	171.3 W 4545 4545 4545 4545 4545 4545 4545 4545 4545 4567 4578 4631 4810 5340	6 12 18 24 30 36 42 48 44 60 66 12 78 64 40 0 66 12 78 64 70 78 64 10 0 65 12 78 64 10 0 0 65 12 78 64 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
[8] 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 7 50.3N 96 99 277 282 991 1016 1686 1746 2674 2801 3515 3844 3970 4951 2830 5433	171.3 W 4545 4545 4545 4545 4545 4567 4567 4631 4810 5340 5478	6 12 18 24 30 16 42 48 54 60 68 72 78 64 90 96 MAX TE HOURS DURATION OF EVENTS  10 51.8N 16  X ≥ 64  X ≥ 48  X ≥ 48  X ≥ 80 13 5 6 8 9 6 4 1 1
[8] 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  4 1 1 1 1 1 18 SEA-0 23  HOURS DURATION OF EVENTS  9  7 5 9 2 6 1 1 1 1 1 1 1 102-1 71  15 16 10 7 5 4 7 4 4 1 1 1 1 1 102-1 71  10 19 24 19 20 9 7 11 8 7 8 3 3 3 3 7 144-1 178  10 19 24 19 20 9 7 11 8 7 8 3 3 3 3 7 144-1 178  10 19 24 19 20 9 7 11 8 7 8 3 3 3 3 7 144-1 178  10 19 24 19 20 9 7 11 8 7 8 3 3 3 3 7 144-1 178  10 19 24 19 10 10 10 11 3 15 10 9 3 6 5 8 8 8 8 100-1 291  10 10 11 11 11 11 11 11 11 11 11 11 11 1	3097 5309 7 50.3N 96 99 277 282 991 1016 1686 1746 2801 3515 3844 3970 4951	171.3 W 4545 4545 4545 4545 4545 4545 4545 4545 4545 4567 4578 4631 4810 5340	6 12 18 24 30 16 42 48 14 60 66 12 18 64 90 96 MAY 75 HOURS DURATION OF EVENTS 10 51.8N 16    W ≥ 64
[8] 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 7 50.3N 96 99 277 282 991 1016 1686 1746 2674 2801 3515 3844 3970 4951 2830 5433	171.3 W 4545 4545 4545 4545 4545 4567 4567 4631 4810 5340 5478	6 12 18 24 30 36 42 48 54 60 66 72 78 64 60 90 90 90 90 90 90 90 90 90 90 90 90 90
[8] 4 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 50 3N 50 3N 96 99 277 282 991 1016 1686 1746 2674 2801 3515 3844 3515 3844 3515 3845 1746	171.3W 4545 4545 4545 4545 45467 4567 4578 4631 4810 5340 7 5478	6 12 18 24 30 36 42 48 54 60 66 72 78 64 90 96 MAY 75 HOURS DURATION OF EVENTS 10 51.8N 16    W ≥ 64
[8] 4 6 1 1 1 1 2 1 4 1 5 1 5 1 6 1 9 1 1 6 1 1 1 1 1 1 1 1 1 1 1 1 1	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 50 3N 50 3N 96 99 277 282 991 1016 1686 1746 2674 2801 3515 3844 3515 3844 3515 3845 1746	171.3w 4545 4545 4545 4545 4546 4567 4567 4578 4631 4810 5340 55478 TH	6 12 18 24 30 36 42 48 54 60 66 72 78 64 90 96 MAY 75 HOURS DURATION OF EVENTS 10 51.8N 16    W ≥ 64
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  4 1 1 1 1 18 SEA-0 23  HOURS DURATION OF EVENTS  9 1 1 1 102-1 71  10 19 24 19 20 9 7 11 8 7 8 3 3 3 3 7 144-1 178  10 19 24 19 20 9 7 11 8 7 8 3 3 3 3 7 144-1 178  11 12 14 14 7 14 10 11 13 15 10 9 3 6 54 486-1 29  9 4 2 4 3 5 5 5 9 3 1 1 1 5 2 59 1446-1 104  1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3097 5309 7 7. 50 3N 96 99 277 282 991 1016 1686 1746 2674 2801 3515 3844 3970 4951 2830 5433 7 7. 51.3N	5363 71 171.3w 4545 4545 4545 4545 4567 4578 4631 4810 5340 5478 71 158.8w 4545	6 12 18 12 13 16 42 48 54 60 66 72 78 64 60 96 MAY TE HOURS DURATION OF EVENTS  10 51.8N 16   \$ 51.8N 16  \$ 28 13 5 6 8 9 6 4 1 1
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 7 7 7 7 8 2 7 7 2 8 2 7 7 2 8 2 7 7 2 8 2 7 7 2 8 2 7 7 2 8 2 7 7 7 7	5363 7H 171, 3W 4545 4545 4545 4545 4545 4567 4578 4631 4810 5340 1 5478 7H 158.8W 4545 4545 4545	6 12 18 12 13 16 42 48 34 60 66 72 78 64 90 96 MAY TE HOURS DURATION OF EVENTS  10 51.8N 16   \$ 51.8N 16  \$ 28 13 5 6 8 9 6 4 1 1
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3097 5309 7 7. 50 3 N 96 99 277 282 991 1016 2674 2801 3515 3844 3970 4951 7 7. 51.3 N 7 7 60 60 204 205	5363 74 171, 3 W 4545 4545 4545 4545 4545 4567 4631 4810 5340 1 5478 74 158.8 W 4545 4545 4545 4545	6 12 18 24 30 16 42 48 34 60 68 72 78 64 40 98 6 MAX TE HOURS DURATION OF EVENTS  10 51.8N 16   \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 7 7. 50 3 N 96 99 277 282 991 1016 2674 2801 3515 3844 3970 4951 2830 5433 7 7. 51.3 N 7 7 60 60 204 205 919 946	5363 74 171.3w 4545 4545 4545 4545 4567 4567 4581 4810 5340 5478 71 158.8w 4545 4545 4545 4545 4545	6 12 18 24 30 16 42 48 54 60 66 72 78 64 €0 96
63 4848062963 484806	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 7 7. 50. 3 N 96 99 277 2822 2991 10:16 1686 1746 2674 2801 3970 4951 2830 5433 7 7. 51. 3 N 7 7. 60 60 204 205 204 1755	5363 7H 171.3W 4545 4545 4545 4545 4545 4567 4578 4631 4810 5340 5478 7H 158.8W 4545	6 12 19 24 30 36 42 48 54 60 66 72 78 64 6 9 9 6
63 4848062963 4848062 611 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2	3097 5309 7 7 7 7 282 999 1 1016 1666 1746 2674 2801 3515 3844 3515 3844 3570 4951 7 7 7 60 60 204 205 919 946 1674 1755 2723 2865	5363 7H 171, 3W 4545 4545 4545 4545 4545 4567 4631 4810 5340 158.8W 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4545 4646 7H	6 12 18 24 30 36 42 48 54 60 66 72 78 64 6 0 68 72 78 64 6 0 68 72 78 64 6 0 68 72 78 64 6 0 68 72 78 64 78 78 72 20 69 69 4 20 1 2 21 1 1 2 2 2 2 2 24 2 20 69 69 4 22 1 22 20 69 69 4 22 1 22 20 69 69 4 22 1 22 1 24 22 20 69 69 4 22 1 22 1 24 22 20 69 69 4 22 1 24 16 37 25 18 14 19 13 11 19 5 7 3 18 28 12 11 6 68 7 4 12 2 2 2 3 3 1 1 3 5 138 1 44 832 846 4 12 24 25 38 18 14 19 14 19 14 19 15 6 6 6 19 4 2 1 1 3 1 4 56 4 7 5 2 20 69 69 4 4 6 6 37 2 51 8 19 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124  2 8 14 10 15 6 2 45 56 66 66 72 / 18 46 90 96 9	3097 5309 7 7 7 50 3 N 96 99 277 282 991 1016 1666 1746 2801 3515 3844 3893 1 7 7 7 60 60 204 205 919 946 1674 1755 3644 3893 3644 3893	5363 7H 171, 3W 4545 4545 4545 4545 4545 4546 4563 1 5478 4631 1 5478 1 5478 4545 4585	6 12 18 24 30 36 42 46 54 60 66 72 78 64 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	9 3 3 5 7 4 1 5 4 4 1 4 2 3 : 69 1146-1 124	3097 5309 7 7 7 7 282 999 1 1016 1666 1746 2674 2801 3515 3844 3515 3844 3570 4951 7 7 7 60 60 204 205 919 946 1674 1755 2723 2865	5363 7H 171, 3W 4545 4545 4545 4545 4546 4567 4578 4631 4810 5340 1 5478 7H 158.8W 4545 454	6 12 18 24 30 36 42 46 54 60 66 72 78 64 90 96 MAX TE    W ≥ 64

Fall

23 Persistence of wave height-duration

Section   Sect	1 64.1N 166.7W	2 63 6N 178 1W
## 1		W≥64
Section   Sect	A ≥ 48 5 SEA-5 5 1840 4566 4566	A≥48 7 SEA-5 7 2274 4804 4808
	E ≥ 34 8 SEA-5 8 2406 4937 4944	
Section   1	H = * * L + - + - + - + - + - + - + - + - + - +	M
1		
The control of the		
Part	H = 10	
Second Column   19   19   19   19   19   19   19   1		
Section   Sect	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
	6 12 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T Te TH	6 12 16 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T To Th
## 1		
Section   Sect		W≥64 5 SEA-5 5 1846 4566 4566
Column   C	A ≥ 48 7 SEA-5 7 2532 5062 5065	A≥48 7 SEA-5 7 , 2170 , 4706 4702
Company   Comp	E ≥ 34 3 1 1 15 SEA-2 19 2143 4645 4681	
Company   Comp	H = * L + <del>* + - + - + - + - + - + - + - + - + - + </del>	H ≥ 28 4 3 1 2 1 1 2 2 33 1482-1 49 2845 4553 475
Second Process   Seco		$E \ge 20 \   11 \   4 \   6 \   4 \   5 \   3 \   8 \   4 \   5 \   1 \   2 \   3 \   2 \   6 \   5 \   68 \   972 - 1 \   137 \   3137 \   4031 \   4664$
2   2   2   2   2   2   2   2   2   2		
8   20   20   20   20   20   20   20   2	M = -   -   -   -   -   -   -   -   -   -	
2   2   2   2   2   2   3   2   3   3		
State   Stat	· · · · · · · · · · · · · · · · · · ·	1
## MOUS INTERVAL BETWEEN VEHTS    1	6 .2 18 24 30 36 42 48 54 60 66 72 78 d4 90 96+ MAX TI T Te TH	6 12 18 24 30 36 42 48 54 60 66 72 78 84 9096 MAK T
Section   Sect	HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
\$\frac{\frac{2}{6}}{2} = \frac{1}{6} \frac{1}{6} = 1		W≥64 6 SEA-6 6 220€ 4930 493
2 3 2 1 2 1 2 1 2 1 3 1 4 1 2 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	A	A ≥ 48 1 1 1 6 SEA-5 8 1984 4568 45 5
2 2 3 2 1 2	V <sup>-</sup>	E ≧34 2 2 1 1 2 26 SEA-1 33 3.52 4882 4992
Section   Sect	≥ 28 3 2 1 2 2 1 4 1 2 1 45 1914-1 64 3067 4477 4754	N ≥ 28 5 3 2 2 4 1 1 2 1 1 52 SEA-1 74 3050 4413 4708
## 20 12   17   15   15   19   10   12   13   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   12   14   15   14   15   15   14   15   15	£ ≥20 € 8 7 8 9 10 3 8 9 3 6 7 8 3 6 59 894-1 160 3075 3613 4613	C ≥ 20 11 15 1 11 13 10 6 5 9 8 2 7 5 3 5 76 600-1 187 3295 3675 465
2 2 2 2 3 3 4 2 1 1 1 2 2 1 1 1 2 2 1 1 1 2 3 5 5 2 4 5 5 1 80 4 8 5 1	≥ 16 15.7 15 10 14 6 10 10 8 11 11 9 2 3 5 63 456-1 199 2693 2901 4595	
8   28   27   12   14   15   15   28   15   15   15   15   15   15   15   1	"	H ≥ 12 42 20 35 26 21 18 10 4 13 10 8 8 6 8 2 31 288 - 1 262 1938 203 4568
2   1   2   2   2   3   3   0   81   4545   1   1   1   1   1   1   1   1   1		}
HOURS INTERVAL BETWEEN EVENTS    Section   Sec		1
HOURS INTERVAL BETWEEN VENTS  54.7N  17.9N  824	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
See	HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
\$\frac{2}{636} \frac{1}{5} \frac{1}{6} \fr	· · · · · · · · · · · · · · · · · · ·	
22   2   1   1   2   1   1   2   29   58   A   4   2863   A   35   A   735   Feb.   A   73   A   735   A		
## 22 13 15 8 4 9 4 9 6 1 7 3 12 2 7 6 74 846 1 170 3236 9617 473   ## 6 2 13 15 13 15 13 15 13 15 13 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	E = 34 3 1 1 1 2 1 1 2 1291SEA - 1 41 2863 4635 4735	
\$\frac{6}{2}\frac{1}{13}\frac{1}{5}1	≥28 7 2 1 1 1 3 2 1 1 4 3 1 1 1 2 48 SEA-1 79 3490 4749 5026	H ≥ 28 2 3 1 3 1 1 1 2 1 31 1464-1 46 2848 4737 46 7
\$\frac{1}{2} \frac{1}{2} \frac	7 ≥ 20 :3 :5 8 4 9 4 9 8 1 5 3 2 2 7 6 74 846 - 1 170 3236 3817 4723	
2 3 1 29 7 7 23 1 9 9 10 13 1 0 9 5 8 11 7 7 5 33 444-1 235 1963 2188 4601   2 3 9 8 2 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	<u>4 16 2 13 15 19 15 10 1 7 11 6 4 7 5 3 10 63 468 1 220 2641 3086 4632</u>	
***   1		$\frac{1}{3} \ge 12 \frac{23}{26} \frac{26}{16} \frac{16}{19} \frac{19}{24} \frac{15}{12} \frac{12}{12} \frac{16}{6} \frac{5}{19} \frac{9}{2} \frac{2}{7} \frac{7}{7} \frac{3}{3} \frac{43}{420} \frac{420}{129} \frac{1}{226} \frac{226}{246} \frac{246}{46} \frac{46}{3} \frac{1}{2}$
*** *** *** *** *** *** *** *** *** **		<del></del>
*** HOURS INTERVAL BETWEEN EVENTS***  *** HOURS INTERVAL BETWEEN EVENTS****  *** HOURS INTERVAL BETWEEN EVENTS************************************	· · · · · · · · · · · · · · · · · · ·	
HOURS INTERVAL BETWEEN EVENTS    Name		6 12 18 24 30 36 42 48 54 60 66 72 78 c4 90 96+ MAX TI T T+
N 264	HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
\$\frac{8}{6} \frac{1}{6} \frac		
E 23 4 2	Δ · · · · · · · · · · · · · · · · · · ·	A≥48
E 4 22 20, 5 9 9 7 4 12 6 9 10 4 2 3 2 4 70 834-1 176 3018 3752 4745  2 16 20 24 22 15 14 14 7 10 11 3 11 4 8 4 10 54 396-1 231 2509 2950 4663  2 2 13 35 26 20 29 22 12 10 15 3 11 5 8 4 2 2 23 372-1 227 1645 1866 4581  2 9 40 30 21 21 14 8 3 5 4 7 4 2 3 2 5 7 168-1 176 887 978 4557  2 9 40 30 21 21 14 8 3 5 4 7 4 2 3 2 5 7 168-1 176 887 978 4557  2 9 40 30 21 21 14 8 3 5 4 6 5 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	E ≥ 34 2 1 1 1 2 1 1 2 24 SEA-1 33 2829 4753 4852	
\$ 16 27 24 12   5   14   14   7   10   1   3   1   4   8   4   10   54   396   1   231   2509   2950   4663   \$ 2   2   35   26   20   29   22   12   10   15   3   11   5   8   4   2   2   23   372   1645   1866   4581   \$ 2   9   40   30   21   21   14   8   3   5   4   7   4   2   3   2   5   7   1685   1066   4581   \$ 2   9   40   30   21   21   14   8   3   5   4   7   4   2   3   2   5   7   1685   1066   4581   \$ 2   9   40   30   21   21   14   8   3   5   4   7   4   2   2   2   3   372   12   \$ 2   14   15   15   14   14   16   16   16   16   16   16	≥ 28 5 5 1 3 1 1 1 1 1 1 1 1 51 1554-1 73 3671 4847 5129	_ ≥ 28 2 2 3 1 1 2 1 1 2 39 1434 -1 54 3311 4011 5005
## 21 35 76 20 29 22 12 10 15 3 11 5 8 4 2 2 23 372—1 227 1645 1866 4581    2 9 40 30 21 21 14 8 3 3 5 4 7 4 2 3 2 5 7 168—1 176 887 978 4557   2 6 35 19 13 9 5 4 6 5 2 1 1 1 1	c ≥ 20 20 5 9 9 7 4 12 6 9 10 4 2 3 2 4 70 834-1 176 3018 3752 4746	· · · · · · · · · · · · · · · · · · ·
The second secon		
\$\frac{2}{6}\$ \frac{35}{19}\$ \frac{13}{19}\$ \frac{9}{5}\$ \frac{1}{6}\$ \frac{1}{6}\$ \frac{1}{12}\$ \frac{1}{12}\$ \frac{1}{12}\$ \frac{1}{12}\$ \frac{3}{12}\$ \frac{1}{12}\$ \fr		
2   3   5   4   2   1   1   1   2   3   3   42   46   54   50   66   72   76   76   76   76   76   77   76   77		
8 2 18 24 30 36 42 48 54 60 66 72 78 84 90 96 8 MAX 71 7 7 7 8 17		
HOURS INTERVAL BETWEEN EVENTS 11 51.3N 158.8W    N	9 2 18 24 30 35 42 48 54 60 66 72 78 84 90 96+ MAX 71 7 7+ TH	5 12 18 24 30 36 42 48 54 50 66 72 78 H4 90 96+ MAX T T T ** **
## 864	HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS
\$\frac{\chi}{2} \chi \frac{\chi}{2} \chi \fra		
E ≥ 34    2     3   2   1   2   2     1   1   2   2   1   1		
F < 20   13   12   12   8   8   9   10   8   6   6   6   6   6   8   7   8   15   10   8   10   10		E≥34 1 1 1 20 SEA-1 23 2449 4721 4790
F < 20   13   12   12   8   8   9   10   8   6   6   6   6   6   8   7   8   15   10   8   10   10	H =	H ≥ 28 2 2 2 1 1 1 3 1 1 1 42 1860 - 1 57 3016 4637 4857
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		£ ≥ 20   7   8   5   5   6   8   7     6   4   7   3   2   4   2   69   816 - 1   143   3187   3852   4696
2 2 35 38 26 24 21 15 12 8 10 10 5 1 3 2 6 26 294 - 2 241 1691 1880 4603  ≥ 3 43 29 27 14 16 12 4 7 3 2 6 7 3 1 10 270 - 1 184 972 1009 4584  ≥ 6 35 18 7 10 6 1 3 2 2 2 1 2 1 1 1 102 - 1 92 323 330 4560  ≥ 3 5 2 4 2 2 1 2 1 1 1 1 84 - 1 17 62 62 4548  6 12 18 12 30 36 42 48 54 50 66 72 78 84 90 56 72 78 84 90 56 8 72 78 84 90		
2 6 35 18 7 10 6 1 3 2 2 2 1 2 1 1 1 1 102-1 92 323 330 4560 2 3 5 2 4 2 2 1 2 1 1 1 84-1 17 62 62 4548  6 12 18 24 30 36 42 48 54 80 86 72 78 84 90 86 MAX TI T TO TH  6 12 18 24 30 36 42 48 54 80 86 72 78 84 90 86 MAX TI T TO TH	2 ≥ 2   35   38   26   24   21   15   12   8   10   10   5     3   2   6   26   294-2   241     1691   1880   4603	$H \ge 12  32 33 26 25 18 13 5 11 10 10 8 1 3 6 2 40 318~1 243 1976 2156 46:3.$
$\frac{1}{6} \stackrel{?}{12} \stackrel{?}{13} $		
6 12 18 24 30 36 42 48 54 50 65 72 78 Ha 90 96 + MAX TI T To TH 6 12 18 24 30 36 42 48 54 50 65 72 78 84 90 96 + MAX TI T To TH		= 030/2/101/1/0 0 2 3 2 1 1 1 2 2 108~2 119 445 448 455:
		> 3 9 7 4 3  +  11 1  +  11 1  +  11 64=1 26+64  64+64  64+666
FOURS INTERVAL BETWEEN EVENTS	1 2 3 5 2 4 2 2 1 1 8 4-1 17 62 62 4548	t ≥ 3 9 7 4 3 1 1 1 1 54-1 25 64 64 4545 1 6 12 18 :4 30 36 42 48 54 60 66 72 78 84 90 96+ MAY 7: T T+ TH

1 64.1N 166.7W	2 63 6N 178.1W
W≥64 17219	W≥64 17219
ó48 1 1 1 1 17219	A ≥ 48 2 1 1 1 1 1 1 1 1 4 8 9 17219
Z = 34 1 1 2 1 1 2 1 1 2 -1 6 19 19 17219	E ≥ 3+ 8 6 6 6 4 1 3-1 3: 97 'CO . :72'9
≥28 5 2 5 2 2 2 2 2 2 2 2 16 45 50 17219	<u>228 20 13 16 6 16 3 1 4-1 75 256 264 172:9</u>
E ≥ 20 44 19 12 12 19 4 1 5-1 111 338 348 17219	E ≥ 20 68 20 21 22 52 27 3 1 5-1 214 915 934 7219
£ 16 44 25 18 16 45 13 3 3 1 7~1 168 758 772 17219	1 ≥ 16 61 27 38 22 90 41 8 10 6 7-1 303 1766 :800 72.9
2 12 180 5 1 44 23 72 36 10 11 8 10 1 1 435 1858 1902 17219	$\vec{q} \ge 12 \cdot [23 37 33 26 13 65 35 21 22 2                               $
T≥ 9 17856 66 37 3786 51 21 25 2 12-1 659 4252 4349 17219	$T \ge 9 \frac{15151}{52} \frac{52}{33} \frac{12279}{27} \frac{49}{49} \frac{27}{160} \frac{5}{5} \frac{1}{1} \frac{21-1}{530} \frac{630}{5340} \frac{5652}{5652} \frac{72}{72} \frac{3}{5}$
≥ 6 16051 48 44 3888 70 37 64 28 2 1 36-1 731 7708 8116 17219	<u>2 6 10841 42 27 84 96 77 38 83 28 5 1 31-1 630 8233 8959 17215</u>
≥ 3 80 42 30 28 95 66 44 33 83 35 16 8 3 1 1 121-1 564 11449 12834 17219	$t \ge 3 (60) 38 (28) 25 (83) 52 (50) 43 (05) 40 (17) 11 (52-1) 552 (11457) (3129) 172 (11457) (3129) (312$
25 5 75 , 2 3 4 5 10 20 30 60 90 180 360 00 MAX TE T TO THE DAYS DURATION OF EVENTS	25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 00 WAX TE T THE DAYS DURATION OF EVENTS
59.4N 172.0W	58.0N 167 0
V≥64 17217	W≥64 172.
ó48 2 1-2 2 4 6 17217	V≥48 2 1 2 1 -2 5 10 11 172.5
≥34 11 10 9 5 3 1 2-1 39 106 115 17217	E ≥ 34 12 7 5 10 7 1 3-1 42 132 135 17215
≥ 28 18 20 23 16 27 2 1 5-1 107 387 398 17217	H ≥ 28   25   26   20   24   3   1   3 - 1   124   4   9   4   24   172   1
≥ 20 42 34 42 36 98 35 12 2 2 8 8 -1 303 1601 1623 17217	E ≥ 20   55   48   54   33   05   34   8   5   2
≥ 16 48 51 36 43 3770 23 9 16 9-1 433 2939 2982 17217	1 ≥ 16   59   55   38   44   59   64   32   15   8   1
12 67 34 40 37 167 0344 29 34 6 18-1 561 4930 5068 17217	$H \ge 12   61   43   52   43   64   22   50   28   37   6   16 - 1   606   5347   5508   12   1   1   1   1   1   1   1   1   $
≥ 9 44 25 40 32 36 1369 37 74 12 4 26-1 586 7109 7460 17217	T≥ 9 57 37 38 42 53 08 70 46 76 21 2 1 35-1 65 78:7 8:60 72
£ 6 64 30 33 30 18 95 63 42 92 50 3 4 42-1 624 9798 10603 17217	≥ 6 59 23 30 29 88 90 72 50 0336 11 7 60 - 1 598 1086 116 14 172 1
23 4: 26: 216 49 30 42 76 67 47 20 13 4 1 95-1 394 12164 14649 17217	$t \ge 3 \frac{ 38 }{23} \frac{ 34 }{11} \frac{ 39 }{36} \frac{ 32 }{32} \frac{ 5 }{59} \frac{ 28 }{28} \frac{ 31 }{3} \frac{ 3 }{3} \frac{ 3 }{3} \frac{ 3 }{1} \frac{ 20 }{20 } \frac{ 336 }{13} \frac{ 1679 }{336} \frac{ 5 }{15} \frac{ 30 }{3} \frac{ 3 }{15} \frac{ 30 }{15}  3$
DAYS DURATION OF EVENTS	DAYS DURATION OF EVENTS
5 56.8N 174.8E	6 52.0N 172.9
17219	W≥64 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
≥48 2 1 2 1 1-1 6 14 14 17219 ≥34 17:14 9 15 25 3 1 5-1 84 335 337 17219	V540 4 2 3
≥ 26 29 27 26 18 49 4 4 3 3 7-1 173 852 862 17219 ≥ 20 47 32 43 39 1 285 3 26 5 13 10 -1 386 2606 2656 17219	H * * * * * * * * * * * * * * * * * * *
	~ ~ <del>  -   -   -   -   -   -   -   -   -   </del>
\$16     50     36     40     32     4780     37     20     35     4     13     -2     481     4162     4330     17219       \$12     52     32     37     38     32053     28     62     21     2     23     -1     546     6363     6711     17219	
	H ≥ 12 175   61   62   46   45   56   00   71   36   59   12   16 - 1   677   65   15   69   12   15   15   15   15   15   15   15
* 9 56 29 33 21 108 74 61 39 75 26 12 2   36 - 1 538   8341   9052   172 19   8 6 48 45 26 20 90 51 51 48 69 42 10 7 3   83 - 1 510   10336   11977   172 19	≥ 6 55 25 30 19 87 64 42 33 92 38 16 9 2 73 - 1 5 14 11242 25 79 17.1
	(≥ 3 36 16 7 8 32 29 27 15 57 41 5 8 2 6 173 1 284 10832 5635 12 1
25 5 75 . 2 7 4 5 .0 20 10 60 90 180360 00 VAX TE T THE TH	25 5 75 1 2 3 4 5 10 20 30 60 90 180 160 00 MAX TE T
DAYS DURATION OF EVENTS	DAYS DURATION OF EVENTS 8 54.9N 167.2
\$4.7N 175.9W	W ≥ 64 ( T T T T T T T T T T T T T T T T T T
2 4 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	A ≥ 48
<u>34 23 16 12 9 113 2</u> 3-2 77 226 233 17219	E ≤ 34   11   11   12   4   4   2   106   3   2
≥ 2= 47.33;23;15,5;,6 3; 4-1,178,641,650,17219	_ ≥ 28 29 24 25 17 24 3 3 3 - 1 122 369 406 721
\$22.76 47 43 54 11951 18 5 5    7-1 418  2240  2261  17219	E ≥ 20 48 50 39 40 1 10 34 12 2 1
\$ 16 73 60 45 43 156 95 32 14 22 10 10 -1 540 3787 3893 172 19	1 ≥ 16 71 46 59 46 6479 23 17 7 1 3 -1 5 3 324 7 33±9
2 3 48 49 45 26 34 6 1 4 1 50 8 1 22-1 636 6 34 6 395 72 19	2 ≥ 12 75 37 53 48 1 70 2665 28 43 6 9-1 651 5764 59 4 12
\$ 9 82 48 38 40 14 11 04 76 37 88 32 3	T≥ 9 73 34 40 38 149 2771 55 80 31 20 - 1 648 6455 PEE 1721
6 71 28 32 25 89 64 58 42 88 49 12 10 49 -1 568 11209 12441 17219	≥ 6 50 26 31 30 93 64 76 46 1 248 13 4 53 - 1 53 3 1 240 1235 → 1 21
23 23 11 8 5 36 26 18 15 59 34 9 7 1 5 1 254-1 258 10454 15708 17219	(≥ 3 31 23 7 13 25 18 23 23 54 31 10 11 5 3   169 - 1 277 16362 15 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
25 5 75 , 2 3 4 5 ,0 20 30 60 90 180360 00 MAX TE T T# TH	25 5 75 : 2 1 4 5 :0 20 30 60 V0180360 00 VAX TE T "" ""
DAYS DURATION OF EVENTS 9 50.3N 171.3W	DAYS DURATION OF EVENTS 51.8N 167 3
V≥64	₩≥64
248 2 1 1 1-1 4 7 9 17218	V≥48 1 1 1
≥34 16 11 13 / 19 2-3 66 218 231 17218	E ≥ 34   13   9   10   9   9   2-3   50   5   165   172
≥ 28 40 38,17 18 37,11 1 2 5-1 164 623 642 17218.	H ≥ 28 36 24 24 18 37 7 3-1 146 512 534 172
≥ 20 75 53 63 48 2651 16 5 8 T-2 445 2369 2438 17218	E ≥ 20 59 51 43 44 2741 (17 5 3 7-1 390 2054 2 07 12
£ 16 82 71 39 57 7095 42 23 22 2 1 13 1 603 4315 4444 17218	1 ≥ 16 82 57 50 51 8083 34 26 18 8-1 58 3955 4088 12
≥ 12 71 50 48 39 33 3365 51 64 13 1 20 -1 674 7062 7409 17218	H ≥ 12 68 46 45 39 55 26 32 39 65 8 20 - 1 6 73 68 56 745 75
2 9 63 47 42 33 1399 67 44 86 45 9 1 38 -1 649 9638 10428 17218	T≥ 9 66 42 34 41 09 16 80 51 98 38 1 1 32-1 677 9346 1056 12
£ 6 34 24 14 15 83 47 59 33 88 47 15 12 1 60-1 472 11427 13628 17218	1 ≥ 6 33 25 21 24 77 53 58 45 88 56 13 7 1 74-1 5C1 1159 13433 172
2 3 1 9 6 3 17 13 14 12 42 30 11 8 2 4 1 205 -1 183 9469 16201 17218	$t \ge 3 \frac{15}{2} \frac{2}{116} \frac{1}{6} \frac{1}{22} \frac{15}{15} \frac{9}{9} \frac{11}{11} \frac{144}{30} \frac{13}{13} \frac{10}{10} \frac{1}{11} \frac{1}{12} \frac{241-1}{191} \frac{191}{8317} \frac{8317}{1699} \frac{1699}{12}$
DAYS DURATION OF EVENTS	DAYS DURATION OF EVENTS
11 51.3N 158.8W	12 54.4N 158 3
1 1 1 17219	W≥64 A≥48 4 2 1 3 (1 1-1 1 28 28 2
248 2 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	V
234 17 12 13 10 14 1 4-1 67 211 211 17219 228 26 30 30 33 34 31 10 1 4-1 173 668 673 17219	
	H = 1
20 76 47 65 39 4056 21 12 4 6-1 460 2587 2639 17219	· Later and the second of the
2 16 78 64 67 55 70 00 045 23 26 1 16-1 629 4519 4660 17219 2 12 67 48 56 55 726 276 243 63 17 18-1 716 7393 7687 17219	
<sup>▘▀</sup> ▔▐▃▐ <del>▗▊▃▐▃▐▃▐▃▐▃▐▃▋▃</del> ▋▃▋▃▋▃▋▃▋▃▋▃▊▄▋▃▙▃▋▃▙▃▊▃▊▃▊▃▃▃▃▃ <u>▊</u> ▃▊▃▃▃▃ <u>▀</u> ▃	H≥ 12 82 54 44 43 74 1062 47 70 4 1
1	$\frac{2}{12} \stackrel{6}{12} = \frac{6}{12} = \frac{2}{12} = $
25 5 75 1 2 3 4 5 10 20 30 60 90 180360 00 MAX TE T THE TH	25 5 75 1 2 3 4 5 10 20 30 60 90 180360 CC MAX TE T TH TH
DAYS DURATION OF EVENTS	DAYS DURATION OF EVENTS

23 Persistence of wave height-duration

	II-513
1 64.1N 166.7W	2 63.6N 178.1W
₩ ≥ 64 17219 17219	W≥64 17219 17219
Å ≥ 46 17218 17219	A≥48 1 2 49-1 3 328 17210 17219
E ≥ 34 1 2 51-1 3 526 17200 17219	E ≥ 34 2 1 2 1 1 3 4 4 1 69-1 19 1670 17119 17219
H ≥ 28	H ≥ 28 1 1 3 4 5 6 2 7 10 8 9 2 63-1 58 3851 16955 17219
E ≥ 20   15   6   4   5   3   5   3   7   10   13   5   11   6	E ≥ 20   21   10   6   7   21   14   10   8   26   38   13   10   1   3
	E ≥ 16 31 9 14 8 34 22 21 21 45 48 13 6 4 2 133-1 278 9758 15419 17219 E ≥ 12 65 20 37 11 70 50 43 18 77 44 14 7 1 1 1 132-1 458 10500 13764 17219
$rac{1}{12} \ge 12 \   \ 58 \   \ 32 \   \ 31 \   \ 11 \   \ 51 \   \ 38 \   \ 27 \   \ 23 \   \ 73 \   \ 40 \   \ 10 \   \ 5 \   \ 4 \   \ 3 \   \   \ 159 - 1 \   \ 406 \   \ 11151 \   \ 15317 \   \ 17219 \  $ $rac{1}{2} \ge 9 \   \ 38 \   \ 35 \   \ 38 \   \ 24 \   \ 04 \   \ 79 \   \ 81 \   \ 45 \   \ 3 \   \ 10 \   \ 3 \   \ 1 \   \ 132 - 1 \   \ 637 \   \ 11113 \   \ 12870 \   \ 17219 \  $	$T \ge 9 \cdot 10640 \cdot 45 \cdot 39 \cdot 10576 \cdot 49 \cdot 23 \cdot 80 \cdot 36 \cdot 12 \cdot 7 \cdot 1 \cdot 1 \cdot 115 - 1 \cdot 620 \cdot 10295 \cdot 11567 \cdot 17219$
≥ 6 15659 51 42 14893 48 22 69 18 10 6 45 - 1 722 8342 9103 17219	€ 6 1161 53 37 1373 50 35 62 29 3 5 56-1 632 7725 8260 17219
3 2170 68 39 25 66 29 19 36 9 16-1 582 4247 4385 17219	£ 3 1369 57 44 4758 23 17 35 4 12-1 567 3924 4090 17219
25 5 75 1 2 3 4 5 10 20 30 60 90 180360 OD MAX TI T Te TH	.25 5 75 1 2 3 4 5 10 20 30 60 90 180360 00 MAX TI T To TH
DAYS INTERVAL BETWEEN EVENTS 3 59.4N 172.0W	DAYS INTERVAL BETWEEN EVENTS 4 58.0N 167.0W
W≥64 17217 17217	W≥64 17219 17219
A ≥ 48 1 1 83-1 1 330 17211 17217	A≥48 1 1 1 69-1 2 330 17208 17219
E ≥ 34 1 2 4 1 5 3 5 6 1 109-1 28 2212 17102 17217	E ≥ 34 6 2 3 6 3 8 1 114-1 29 2638 17084 17219
H ≥ 28 1 3 1 2 9 5 5 3 15 20 12 9 1 63-1 86 4759 16819 17217	$\geq 28 \mid 6 \mid 3 \mid 4 \mid 3 \mid 6 \mid 9 \mid 3 \mid 1 \mid 11 \mid 32 \mid 8 \mid 11 \mid 2 \mid 3 \mid 179-1 \mid 102 \mid 6863 \mid 16795 \mid 17219 \mid 1820 \mid 25 \mid 9 \mid 13 \mid 7 \mid 43 \mid 31 \mid 21 \mid 24 \mid 66 \mid 47 \mid 15 \mid 6 \mid 5 \mid 3 \mid 167-2 \mid 315 \mid 11672 \mid 15477 \mid 17219 \mid 1820$
$\frac{1}{6} \ge 20$   15   12   9   7   43   32   26   18   57   40   9   6   2   2     168 - 1   278   9101   15594   17217   $\frac{1}{6} \ge 16$   37   18   17   20   70   56   36   32   66   41   12   4   3   3     149 - 1   410   10950   14235   17217	$E \ge 20$   25   9   13   7   43   31   21   24   66   47   15   6   5   3     167 - 2   315   11672   15477   17219   1 ≥ 16   32   22   23   15   82   45   50   31   74   54   13   4   2   3     142 - 2   450   11830   14056   17219
	G 217 5170 40 78 278 140 78 58 42 0 6 12 1 181 1 501 10424 11711 17719
H≥ 12     52     32     45     37     0661     40     32     79     41     7     8     4     89     -1     544     10761     12149     17217       T≥ 9     49     54     49     29     36     74     51     24     68     25     10     7     57     1     26     8721     9757     17217	$T \ge 9 74 59 60 56 14073 47 28 62 31 8 2 1 72-1 641 8241, 9059 172 19$
≥ 6 89 76 70 56 12266 40 26 55 23 2 23-1 627 6154 6614 17217	, ≥ 6 1878 62 58 11 59 35 22 44 14 1 2 34-1 604 5240 5605 17219.
. ≥ 3 91 54 48 41 87 42 23 14 12 2 11-1 414 2491 2568 17217	2 3 97 47 43 30 77 30 19 10 6 10 10 10 10 10 10 10 10 10 10 10 10 10
.25 5 75 - 2 3 4 5 :0 20 30 50 90 180360 00 MAX TI T TO TH	.25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 00 WAX T T T+ TH DAYS INTERVAL BETWEEN EVENTS
DAYS INTERVAL BETWEEN EVENTS 5 56.8N 174.8E	6 52.0N 172.9E
W ≥ 64 17219 17219	W ≥ 64 172.8 .72.9
V≥48 1 1 1 1 63-1 3 406 17205 17219	V≥48 1 1 1 70-1 3 295 77202 17219
E ≥ 34   3   1   2   3   3   5   6   10   13   7   9   2   1	E ≥ 34 3 3 3 1 5 7 6 3 10 20 5 10 3 67-1 82 5309 6858 7219 ≥ 28 12 8 5 6 19 13 12 9 28 44 11 6 1 1 1 181-1 176 7632 16369 7219
≥ 28 6 5 4 4 4 7 17 12 7 28 31 11 8 1 1 1 216 -1 153 7272 16357 17219 ≥ 20 21 20 20 15 65 49 32 27 51 45 6 6 6 3 4 157 -1 364 10292 14563 17219	H ≥ 28   12   8   5   6   19   13   12   9   28   44   11   6   1   1   1   1   181   176   7632   16369   72   9   1   20   33   27   10   21   77   49   38   33   75   45   11   6   1   4   166   1   430   11591   4622   72   72   9
≥ 16 43/29 31 21/88/65 34 38 75 28 5 6 2 3 156 - 1 468 10081 12889 17219	1 <u>2 16 49 48 42 36 89 63 63 34 74 30 9 10 1 3 1 109 - 1 55 1 10993 12888 172 19</u>
$\frac{3}{2}$ 12 41 50 47 30 1373 56 25 59 27 11 5 3 73-1 540 9016 10508 17219	G <sub>H≥12</sub> 89 62 69 47 2480 56 29 67 30 16 4 58-1 673 9355 1026 7 7219
7 ≥ 9 75 50 33 43 2267 36 27 41 31 10 4 44-1 539 7298 8167 17219	T≥ 9 1676 60 53 3168 45 15 65 29 3 3 3 36-1 664 7158 7609 17219
≥ 6 90 52 60 40 10949 37 26 44 15 2 28-1 524 4921 5242 17219	<u>2 6 92 77 42 42 1554 35 19 48 7 13-1 531 4347 4643 172 19</u>
$\frac{1}{2}$ 3 $\frac{74}{4}$ $\frac{41}{4}$ $\frac{1}{4}$	$t \ge 3 \ 80 \ 4 \ + 3 \ 30 \ 56 \ 32 \ 16 \ 5 \ 2 \ 1$ $t > 17 - t \ 310 \ 1540 \ 159t \ 1219$
DAYS INTERVAL BETWEEN EVENTS	DAYS INTERVAL BETWEEN EVENTS  8 54 9N 167 2W
7 54.7N 175 9W N≥64 17219 17219	8 54 9N 167 2W
7 54.7N 175.9W	8 54.9N 167.2W ₩≥64
7 54.7N 175 9W N≥64 17219 17219	8 54.9N 67.2W  \$64  \$248  E≥34 1 1 4 1 1 3 5 1 10 2 1 102-1 30 3 4 108 72 72 72 72 72 72 72 72 72 72 72 72 72
7 54.7% 175 9W  A ≥ 48	8 54 9N 167 2W  2 48
7	W ≥ 64     S4     9N     167     2W       \$\frac{2}{2}\$ 248     \$\frac{1}{2}\$ 248     \$\frac
N ≥ 64         SA.7N         175 9 W           N ≥ 48         SA.7N         175 9 W           E ≥ 34         SA.7N         172 19 1	8 54 9N 167 2W
N ≥ 64         0         1         1         31-1         1         1221 9129 17219	W ≥ 64     B     54 9N     67 2W       Q ≥ 48     1 1 1 3 5 5 1 10 2 1     102-1 30 3 4 1098     12 102-1 30 3 4 1098       E ≥ 34 1 1 1 2 4 1 1 1 3 5 5 1 10 2 1 1 102-1 30 3 4 1098     12 102-1 30 3 4 1098     12 102-1 30 3 4 1098       E ≥ 20 11 25 10 4 4 1 38 15 18 63 58 15 5 4 1 189- 309 1230 5476     12 102-1 30 30 3 4 1098     12 102-1 30 3 4 1098       E ≥ 20 11 25 10 20 24 68 54 49 37 78 48 8 4 5 1 134- 492 1327 3888     12 102-1 30 30 3 4 1098     12 102-1 30 30 3 4 1098       G ≥ 12 20 24 68 54 49 40 68 56 32 73 43 8 6 1 1 102-1
7	W ≥ 64     S4     9N     167     2W       Q ≥ 48     1     1     3     5     1     10     2     1     102-1     30     3 **14     1098     2       E ≥ 34     1     1     4     1     1     3     5     1     10     2     1     102-1     30     3 **14     1098     2       E ≥ 20     11   125   10     4     1     18     15     16     55   8     15     5     15     5     4     1     189-309     1239     54*     2       E ≥ 10     65   52   20     24     88     54     9     37*     48     8     4     5     1     134-4     492     1327     1388     2       E ≥ 17     62   56   50     50     47   4068   56     32   73   43     8     6     1     10-6     61*     100-1     1243     1       T ≥ 9     10682   63     59   12484   48   38   57   28   3     2     1     70-1     695     7745     6356     1
7	W ≥ 64     S4     9N     167     2W       A ≥ 48     S4     S4     S4     S4     S5
N ≥ 64         7         54.7N         175.9 w           5 ≥ 48         1         1         1         31-1         1         1221 91219 17219           5 ≥ 34         4         1         2         1         2         5         6         1         7         14         7         5         2         1         98-1         58         3645         16986         17219           € 28         12         6         3         2         12         14         16         7         29         30         12         7         1         207-1         15         6272         16569         17219         17219         16569         17219	W ≥ 64     S4     91     67     2W       Q ≥ 48     1     1     3     5     1     10     2     1     102-1     30     3 * 4     1098     12       E ≥ 34     1     1     4     1     1     3     5     1     10     2     1     102-1     30     3 * 4     1098     12       E ≥ 20     11   125     10     4     138     15     166     35     15     5     4     1     189-309     1239     1239     126-5     12       E ≥ 12     120   246     14     138     15     166     35     15     5     4     1     189-309     1239     1239     126-5     12       E ≥ 12     102   246     10     46     10     10     134-4     49     1322     1888     127       G ≥ 12     10
N ≥ 64         S4.7N         175.9 w           N ≥ 66         S4.80         S4.7N         172.19 172.19 172.19           N ≥ 64         S4.80         S4.7N         S4.7N         172.19 172.19 172.19           N ≥ 64         S4.7N         <	W 2 6 4     6     6     7     8     54     9N     67     2 W       € 2 48     1     1     1     3     5     1     10     2     1     102-1     30     3 T4     1098     10       € 2 83     1     1     1     1     3     5     1     10     2     1     102-1     30     3 T4     1098     10       € 2 80     11 125     10     4     4     138     15     18 63     58     15     5     4     1     19-1     1327     6665     68     10       € 2 10     12 25     10     4     4     138     15     18 63     58     15     5     4     1     19-2     19-3     32.79     55     12     10     102-1     1327     6665     68     10       € 2 10     25 50     20     24     40     38     37     78     48     8     4     5     134-1     49     1327     3886     10       T 2 9     10682     35     59     12484     48     38     5     1     70-1     695     7745     6356     13       2 6     15     10     1
N ≥ 64         7         54.7N         175.9W           1 ≥ 48         1         1         1         31-1         1         12219         17219         17219           1 ≥ 34         4         1         2         1         2         5         6         1         7         14         7         5         2         1         98-1         58         3645         1698b         17219           2 ≥ 28         1 ≥ 6         3         2         12         14         16         7         29         30         12         7         1         207-1         15         6272         16569         17219           2 ≥ 2         13         29         20         10         60         33         7         7         4         1         207-1         15         6272         16569         17219           2 ≥ 2         13         36         34         98         63         37         7         4         1         104-1         522         10650         13266         17219           3 ≥ 2         19         38         37         8         4         2         83-1         630         9881         10924	# 264
N ≥ 64         N ≥ 64	8   54   9N   167 2W
N ≥ 64	# 264
N ≥ 64         N ≥ 64	# 264
N ≥ 64         N ≥ 64	# 264
N ≥ 64         SA.7N         175 9 W           2 ≥ 48         SA.7N         175 9 W           5 ≥ 34         SA.7N         172 19 1	# 264
N ≥ 64	\$2.64
N ≥ 64	# 264
N ≥ 64	\$\begin{align*}{c c c c c c c c c c c c c c c c c c c

## Set 24. Annual maximum wind and wave for selected return periods (Refer to introductory text of Section II for additional information.)

Annual Maximum Winds for Selected Return Periods

Values oif the annual maximum sustained wind speeds for selected return periods are presented in the table below for selected coastal stations. These tabular values may be used to construct a graphical analysis of the data similar to the one in Figure 1. The procedure is as follows:

- 1. Use Fisher-Tippett, Type 1 extreme value probability paper with a natural logarithmic ordinate scale and a probability scaled abscissa. A linear reduced variate scale is also useful in locating intermediate probabilities.
- 2. Select and plot the annual maximum wind speeds at their corresponding probability values from Table.
- 3. Draw a straight line connecting those points. This is the line of best fit from which wind speed estimates for intermediate probabilities can be obtained.
- 4. A one standard error confidence band may be drawn by computing the upper and lowert bound according to Gumbel (1958). The computational procedure is as follows:

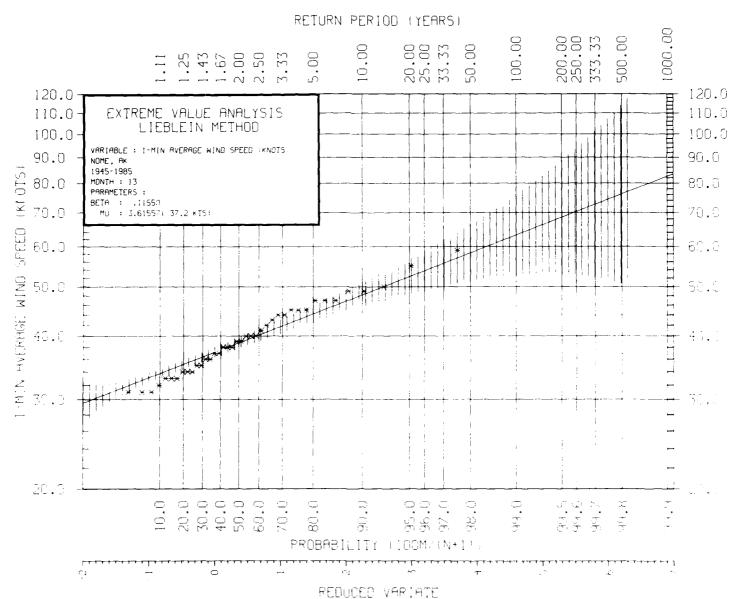
```
    a. S9 = \( \sqrt{11/P-11/1-\text{IP}} \) |
    b. TP = S9 * A1/ N , A1 = 1/B
    c. Upper Bound (P1 = Exp(Ln(x(P))) - TP
    d. Lower Bound (P1 = Exp(Ln(x(P))) - TP
```

where S9 = a probability term, TP = standard error at probability P, A1 = scale term  $1/\beta$ , x [P] is the wind speed at probability [P] in knots, and [N] = sample size. This will give an envelope of the 68-percent confidence band for the estimates.

Graphs similar to Figure 1 have been drawn for each station's annual and monthly values and are available on microfiche from the National Climatic Data Center, Federal Building, Asheville, NC, 28801. Any questions regarding the application of the extreme value model should be addressed to Larry Nicodemus, telephone number (704) 259-0366.

ANNUAL MAXIMUM	SUSTAINED	WINDS	⊬ \ <u>[</u> ]	75 FD	R JEL		#ETT:54	-04100	Ξ.
STATION NAME				100 y£				AMETERS	
NIKOL SKOE, RA KHATIRKA-IN-CHUKOT, RA UGOL NAJA RA BUHTA PROVIDENJA, RA NORTHEAST CAPE, AK	65.4 53.0 73.8 40.9 48.5	79.4 61.5 84.9 46.5 56.2	93.2 67.9 93.1	25 102.0 74.6 101.8 55.1 68.1	84.3 114.3 61.3	160 134.8 92.4 124.6 66.0 84.1	MIDE 61.4 50.5 77.5 74.3	BETA .1789 .1311 .1239 .1301	
NOME, AK UNALAKLEET, AK CAPE ROMANZOF, AK CAPE NEWENHAM, AK KING SALMON, AK	38.8 42.1 52.0 44.1 40.6	44.2 47.5 60.4 51.1 47.0	48,2 51.4 56.7 56.3	52.4 55.4 57.4 51.7 51.7	58.3 51.3 54.6 64.8	63 66 78	77.4 41.3 47.4 47.4 48.4 58.4	.::30 .::56 .:320 .:321	A STATE OF THE STA
COLD BAY, AK NIKOLSKI, AK ST. PAUL, AK ADAK, AK	50.6 46.1 49.1 49.2	56.1 54.0 55.6 58.0	60.1 60.6 60.3 64.7	64.1 66.3 65.3	19.8 75.3 72.4 82.4	74.4 83.3 78.1 91.3		.0911 .1395 .1098 .1459	(3) (2) (3) (4) (5) (4) (4) (4) (4)

NOTE: SOME OF THE HIGHER RETURN PERIOD VALUES MAY BE UNREALISTIC BECAUSE OF THE SMALL SAMPLE SIZE. THE CONFIDENCE BANDS AT THESE VALUES MAY BE UNUSUALLY WIDE, WHICH INDICATES A HIGH LEVEL OF UNCERTAINTY.



Fugure 1. Graphical analysis of annual extreme sustained wind speeds for Name, th

## 24 Return period winds and waves

Annual

ANNUAL MAXIMUM SUSTAINED WINDS (KNOTS) FOR SELECTED RETURN PERIODS

GRID PT.	LATITUDE	LONGITUDE		RETU	JRN PERI	OD TYE	ARSI		PARA	METERS	
			2	5	10	25	50	i 00	MODE	BETA	Ν
01 02 03 04 05	64.1 N 63.6 N 59.4 N 58.0 N 56.8 N	166.7 W 178.1 W 172.0 W 167.0 W 174.8 E	49.3 61.7 56.0 58.0 64.4	56.4 68.8 61.5 64.6 72.1	61.7 73.9 65.4 69.4 77.6	67.2 79.2 69.5 74.3 83.3	75.1 86.6 75.0 81.2 91.3	81.6 92.6 79.5 86.7 97.7	47.2 59.6 54.3 56.0 62.2	.1190 .0958 .0828 .0950 .0984	12 12 12 12 12
06 07 08 09 10	52.0 N 54.7 N 54.9 N 50.3 N 51.8 N	172.9 E 175.9 W 167.2 W 171.3 W 167.3 W	68.5 63.0 55.6 60.3 56.6	77.6 67.7 58.9 69.1 61.7	84.2 71.0 61.2 75.6 65.3	91.2 74.4 63.4 82.5 68.9	101.0 78.9 66.4 92.3 74.0	109.1 82.5 68.8 100.4 78.0	65.8 61.5 54.6 57.7 55.1	.1101 .0639 .0502 .1205 .0757	12 12 12 12
11	51.3 N 54.4 N	158.8 W 158.1 W	60.8 62.7	70.1 72.9	77.1 83.6	84.4 88.8	95.0 100.5	103.8 110.5	58.0 59.7	.1265 .1339	12 12

ANNUAL MAXIMUM WAVE HEIGHT (FEET) FOR SELECTED RETURN PERIODS

GRIC PT.	LATITUDE	LONGITUDE				ob lybA			PARAMETERS	
01 02 03 04 05	64.1 N 63.6 N 59.4 N 58.0 N 56.8 N	166.7 M 178.1 M 172.0 M 167.0 M 174.8 E	40.5 41.0 44.1	45.3 47.0 53.0	10 40.0 49.5 51.0 58.9 56.8	25 43.8 52.9 54.9 64.5 6:.1	50 48.7 57.4 59.9 71.8 66.8	100 52.4 60.7 63.6 77.3	MODE BETA 28.1 5.2793 38.7 4.7787 39.0 5.3380 41.3 7.8307 43.1 6.0778	1222233
06 07 08 09 10	52.0 N 54.7 N 54.9 N 50.3 N 51.8 N	172.9 E 175.9 w 187.2 w 171.7 k 187.3 w	41.8 4 41.7 4 44.0 9	48.4 49.2 51.6	57.3 52.8 54.0 55.7	51.0 58.3 60	51.1 62.4 65.1 65.1 60.1	63.9 66.5 53.7 70.3	49.2 5.3611 39.7 5.8353 39.7 6.6019 41.7 6.2109 39.0 5.4090	
: <u>:</u>	51.3 N 54.4 N	158.8 W 158.1 W			57.3 5:.4	62.5 56.7	68.5 73.6	73.0 78.7	43.4 6.4503 44.4 7.3438	: Z

NOTE: SOME OF THE HIGHER RETURN PERIOD VALUES MAY BE UNREQUISTIC BECAUSE OF THE MMALL SAMPLE NICE. THE CONFIDENCE BANDS AT THESE VALUES MAY BE UNUSUALLY WIDE, WHICH INDICATES A HIGH LEVEL OF NICERTHINTS.

Graphical analysis of wave data sumician to Figure 1 may be done using the same pricedures out, near in the first page of this set. Mowever, the fraxis should be linearly scaled instead of the logar time scale used for the wind data. Since the extreme wave statistics are based on the assumption of wirds blowing over open water without fetch restrictions, the wave height extremes are likely to be unrealistically high during the winter season for those few grid points located within an area having a probability or restricting the development of waves. Peren to the location in Sets 17.19. Refer to the map in Set 23 for the location of the 12 grid points and to the introductory text for additional information in this set.

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